

**CE 3372 Water Systems Design**  
**Fall 2016 <sup>1</sup>**

1. (1 pts.) The hydraulic radius in a conduit containing a flowing liquid is
  - (A) the mean radius from the center of flow to the wetted side of the conduit
  - (B) the ratio of the cross-sectional area of the conduit and the wetted perimeter
  - (C) the ratio of the wetted perimeter and the cross-sectional area of the conduit
  - (D) the ratio of the cross-sectional area of flow and the wetted perimeter
2. (1 pts.) The rational runoff coefficient for a 14.81 acre parcel property is 0.85. The rainfall intensity is 4.56 inches per hour. The peak discharge from this property is anticipated to be about
  - (A) 23.82 cfs
  - (B) 28.41 cfs
  - (C) 33.01 cfs
  - (D) 48.18 cfs
  - (E) 57.86 cfs
  - (F) 65.90 cfs
  - (G) 80.18 cfs
  - (H) 97.81 cfs
3. (8 pts.) A storm sewer (reinforced concrete pipe) is 400-feet long and 30-inches in diameter. The sewer flows from a junction box (invert elevation 101.00 feet) to a lift station sump (invert elevation 100.00 feet). Assuming Manning's roughness coefficient is 0.013 for all flow depths, the sewer maximum flow capacity without surcharge is about
  - (A) 17.8 cfs
  - (B) 19.2 cfs
  - (C) 20.6 cfs
  - (D) 22.1 cfs
  - (E) 28.9 cfs
  - (F) 31.2 cfs
  - (G) 33.4 cfs

---

<sup>1</sup>For partial credit show work

4. (8 pts.) The storm sewer in the question above is flowing at  $\frac{3}{4}$  full. What is the discharge in the sewer?
- (A)  $Q_{75\%} = 3.6$  cfs  
(B)  $Q_{75\%} = 8.1$  cfs  
(C)  $Q_{75\%} = 12.5$  cfs  
(D)  $Q_{75\%} = 18.1$  cfs  
(E)  $Q_{75\%} = 19.2$  cfs  
(F)  $Q_{75\%} = 20.6$  cfs  
(G)  $Q_{75\%} = 22.1$  cfs  
(H)  $Q_{75\%} = 28.9$  cfs
5. (11 pts.) A pipe with a diameter of 2.4 meters is depicted in Figure 1. The pipe is flowing partially full.

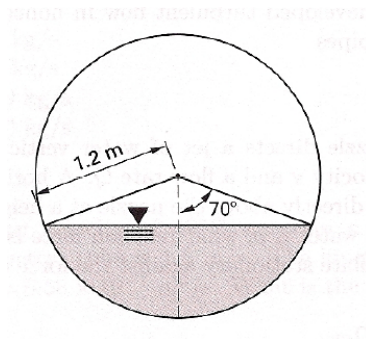


Figure 1: Circular channel flowing partially full.

What is the hydraulic radius of flow in the circular section?

- (A) 0.21 m  
(B) 0.44 m  
(C) 0.57 m  
(D) 0.88 m  
(E) 1.10 m  
(F) 1.88 m  
(G) 2.30 m  
(H) 2.80 m

6. (12 pts.) A smooth concrete channel ( $n=0.012$ ) is depicted in Figure 2. The channel's dimensionless slope in the direction of flow is 0.008. If the flow width at the surface is 2-meter, what is the flow rate in the channel using Manning's equation?

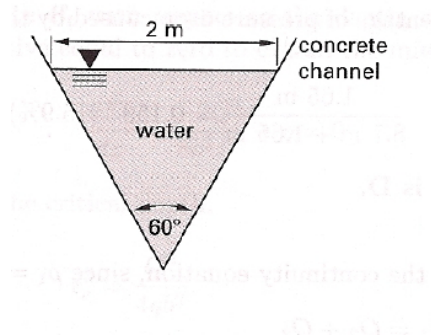


Figure 2: Triangular channel.

- (A) 0.25 cms (cubic meters per second)
- (B) 2.53 cms
- (C) 3.91 cms
- (D) 4.41 cms
- (E) 4.45 cms
- (F) 5.83 cms
- (G) 7.38 cms
- (H) 9.31 cms

7. (19 pts.) A 24-inch diameter sewer pipe, with Manning's  $n$  of 0.015 is laid on slope  $S_0 = 0.02$  as shown in Figure 3.

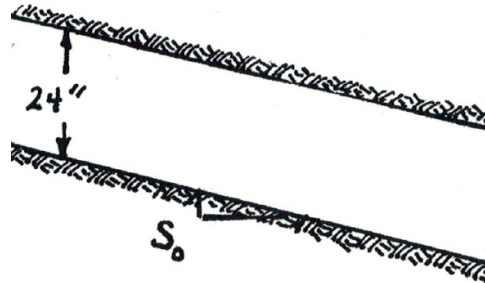


Figure 3: Sewer pipe sketch

Use Manning's equation and the depth-area, and the depth-perimeter equations on the equation sheet to complete Table 1.

Table 1: Depth-Area, Depth-Perimeter, Depth-Hyd. Radius, and Discharge for Circular Sewer

$y$ (ft)	$A$ (ft <sup>2</sup> )	$P_w$ (ft)	$R_h$ (ft)	$Q$ (ft <sup>3</sup> /sec)
1.00				
2.00				

8. (8 pts.) Figure 4 is a sketch of a 24 inch line with Manning's  $n$  of 0.015, laid on a slope of 0.02, connecting to a 48 inch line (also at 0.02) at a junction box. The flowlines (invert elevations) match at the junction box. The downstream boundary conditions cause the flow depth in the 48 line to be 12 inches deep.

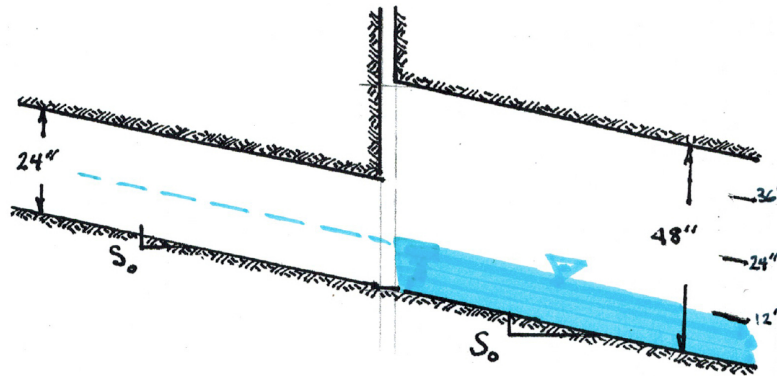


Figure 4: Sewer pipes connected at a junction box. Matching flow line elevations.

- (A) The likely flow depth in the 24 inch line is
- i) 12.0-inches
  - ii) 18.0-inches
  - iii) 24.0-inches
  - iv) 36.0-inches
  - v) 48.0-inches
- (B) The discharge in the 24 inch line, assuming normal flow at the flow depth in the pipe is
- i) 0.00 cfs
  - ii) 4.92 cfs
  - iii) 9.83 cfs
  - iv) 13.86 cfs
  - v) 19.66 cfs
  - vi) 27.72 cfs
  - vii) 39.32 cfs

(C) The full-pipe discharge in the 24 inch line, assuming normal flow, is

- i) 0.00 cfs
- ii) 4.92 cfs
- iii) 9.83 cfs
- iv) 13.86 cfs
- v) 19.66 cfs
- vi) 27.72 cfs
- vii) 39.32 cfs

(D) What is the unused flow capacity in the 24 inch line?

9. (8 pts.) Figure 5 is a sketch of a 24 inch line with Manning's  $n$  of 0.015, laid on a slope of 0.02, connecting to a 48 inch line (also at 0.02) at a junction box. The soffit(crown) elevations match at the junction box. The downstream boundary conditions cause the flow depth in the 48 line to be 36 inches deep.

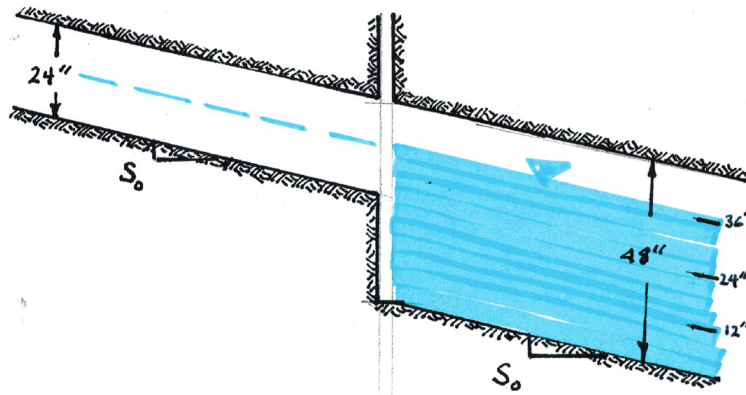


Figure 5: Sewer pipes connected at a junction box. Matching soffit elevations.

- (A) The likely flow depth in the 24 inch line is
- i) 12.0-inches
  - ii) 18.0-inches
  - iii) 24.0-inches
  - iv) 36.0-inches
  - v) 48.0-inches
- (B) The discharge in the 24 inch line, assuming normal flow at the flow depth in the pipe is
- i) 0.00 cfs
  - ii) 4.92 cfs
  - iii) 9.83 cfs
  - iv) 13.86 cfs
  - v) 19.66 cfs
  - vi) 27.72 cfs
  - vii) 39.32 cfs

(C) The full-pipe discharge in the 24 inch line, assuming normal flow, is

- i) 0.00 cfs
- ii) 4.92 cfs
- iii) 9.83 cfs
- iv) 13.86 cfs
- v) 19.66 cfs
- vi) 27.72 cfs
- vii) 39.32 cfs

(D) What is the unused flow capacity in the 24 inch line?



10. (8 pts.) Figure 6 is a sketch of a 24 inch line with Manning's  $n$  of 0.015, laid on a slope of 0.02, connecting to a 48 inch line (also at 0.02) at a junction box. The soffit(crown) elevations match at the junction box. The downstream boundary conditions cause the flow depth in the 48 line to be 36 inches deep.

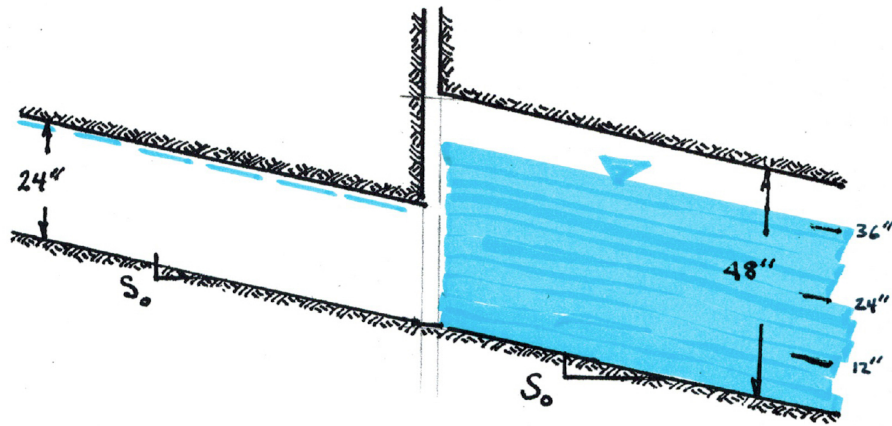


Figure 6: Sewer pipes connected at a junction box. Matching flow line elevations.

- (A) The likely flow depth in the 24 inch line is
- i) 12.0-inches
  - ii) 18.0-inches
  - iii) 24.0-inches
  - iv) 36.0-inches
  - v) 48.0-inches
- (B) The discharge in the 24 inch line, assuming normal flow at the flow depth in the pipe is
- i) 0.00 cfs
  - ii) 4.92 cfs
  - iii) 9.83 cfs
  - iv) 13.86 cfs
  - v) 19.66 cfs
  - vi) 27.72 cfs
  - vii) 39.32 cfs

(C) The full-pipe discharge in the 24 inch line, assuming normal flow, is

- i) 0.00 cfs
- ii) 4.92 cfs
- iii) 9.83 cfs
- iv) 13.86 cfs
- v) 19.66 cfs
- vi) 27.72 cfs
- vii) 39.32 cfs

(D) What is the unused flow capacity in the 24 inch line?

11. (46 pts.) An EPA-NET simulation model for a reservoir-pump-network was constructed and operated for four (4) different operational scenarios. Figure 7 is a depiction of the network. The numbers next to the nodes are Node\_ID values in the reports that follow, and the numbers next to the pipes are the Link\_ID values. The network is supplied from a reservoir through a booster pump, both are depicted on Figure 7.

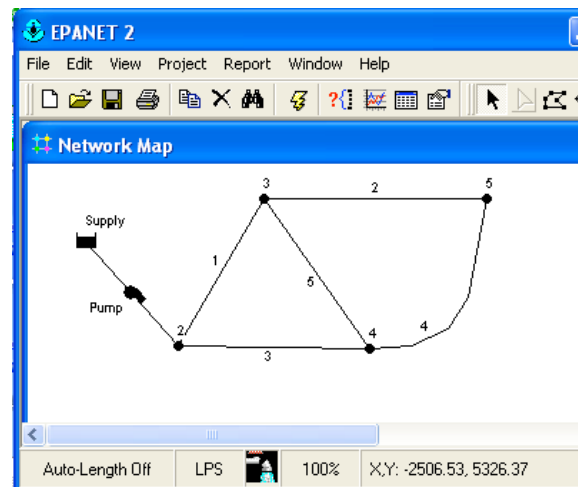


Figure 7: EPA-NET system topology.

Figure 8 is the a portion of the summary report for simulation 1. Figure 9 is the a portion of the summary report for simulation 2. Figure 10 is the a portion of the summary report for simulation 3. Figure 11 is the a portion of the summary report for simulation 4.

These four simulation represent different demand scenarios for the same system.

Interpret these reports, to answer the following questions:

- (a) Complete the table below.  $Q_{pump}$  is the discharge in liters-per-second through the pump station,  $H_{Supply}$  is the head at the supply reservoir,  $H_{Node2}$  is the head at Node 2, and  $\Delta H_{pump}$  is the added head supplied by the pump.

Table 2: Pump Discharge and Supplied Head				
Simulation #	$Q_{pump}$	$H_{Supply}$	$H_{Node2}$	$\Delta H_{pump}$
1				
2				
3				
4				

- (b) Complete the table below.  $Q_{pump}$  is the discharge in liters-per-second through the pump station,  $\Delta H_{Node2-to-5}$  is head loss in the system from Node 2 to Node 5.

Table 3: System Discharge and Head Loss

Simulation #	$Q_{pump}$	$H_{Node2}$	$H_{Node5}$	$\Delta H_{Node2-to-5}$
1				
2				
3				
4				

- (c) If the pump performance curve has the mathematical structure:  
 $H_{pump} = H_{shutoff} - K_{system} \times Q_{pump}^2$ , estimate the value of  $K_{system}$ .

- (d) If the frictional loss from Nodes 2 to Node 5 has the mathematical structure:  
 $\Delta H_{Node2-to-5} = K_{loss} \times Q_{pump}^2$ , estimate the value of  $K_{loss}$

- (e) What effect would removing the pipe joining nodes 3 and 4 have on the system performance? Explain your reasoning.
- (f) Estimate the flow distribution and head losses the the system if the the pipe joining nodes 3 and 4 are removed, and the pipe joining node 4 and 5 is removed if the nodal demands are the same as SIMULATION 2.

Page 1

10/4/2010 2:27:47 PM

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                 *
*                               Version 2.0                               *
*****

```

Input File: SIMULATION #1

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	2	3	1000	124
2	3	5	1000	124
3	2	4	1000	124
4	4	5	1000	124
5	3	4	1400	124
7	6	2	#N/A	#N/A Pump

Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality
2	0.00	20.00	20.00	0.00
3	0.00	20.00	20.00	0.00
4	0.00	20.00	20.00	0.00
5	0.00	20.00	20.00	0.00
6	0.00	0.00	0.00	0.00 Reservoir

Link Results:

Link ID	Flow LPS	Velocity m/s	Unit Headloss m/km	Status
1	0.00	0.00	0.00	Open
2	0.00	0.00	0.00	Open
3	0.00	0.00	0.00	Open
4	0.00	0.00	0.00	Open
5	0.00	0.00	0.00	Open
7	0.00	0.00	-20.00	Open Pump

Figure 8: EPA-NET Summary Report, Simulation #1

Page 1

10/4/2010 2:28:15 PM

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.0                                *
*****

```

Input File: SIMULATION 2

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	2	3	1000	124
2	3	5	1000	124
3	2	4	1000	124
4	4	5	1000	124
5	3	4	1400	124
7	6	2	#N/A	#N/A Pump

Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality
2	0.00	19.28	19.28	0.00
3	1.00	19.03	19.03	0.00
4	1.00	19.03	19.03	0.00
5	1.00	18.99	18.99	0.00
6	-3.00	0.00	0.00	0.00 Reservoir

Link Results:

Link ID	Flow LPS	Velocity m/s	Unit Headloss m/km	Status
1	1.50	0.12	0.25	Open
2	0.50	0.04	0.03	Open
3	1.50	0.12	0.25	Open
4	0.50	0.04	0.03	Open
5	0.00	0.00	0.00	Open
7	3.00	0.00	-19.28	Open Pump

Figure 9: EPA-NET Summary Report, Simulation #2

Page 1

10/4/2010 2:29:00 PM

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.0                                *
*****

```

Input File: SIMULATION 4

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	2	3	1000	124
2	3	5	1000	124
3	2	4	1000	124
4	4	5	1000	124
5	3	4	1400	124
7	6	2	#N/A	#N/A Pump

Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality
2	0.00	17.12	17.12	0.00
3	2.00	16.16	16.16	0.00
4	2.00	16.16	16.16	0.00
5	2.00	16.04	16.04	0.00
6	-6.00	0.00	0.00	0.00 Reservoir

Link Results:

Link ID	Flow LPS	Velocity m/s	Unit Headloss m/km	Status
1	3.00	0.25	0.96	Open
2	1.00	0.08	0.12	Open
3	3.00	0.25	0.96	Open
4	1.00	0.08	0.12	Open
5	0.00	0.00	0.00	Open
7	6.00	0.00	-17.12	Open Pump

Figure 10: EPA-NET Summary Report, Simulation #3



Page 1

10/4/2010 2:29:46 PM

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                 *
*                               Version 2.0                               *
*****

```

Input File: SIMULATION 3

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	2	3	1000	124
2	3	5	1000	124
3	2	4	1000	124
4	4	5	1000	124
5	3	4	1400	124
7	6	2	#N/A	#N/A Pump

Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality
2	0.00	13.52	13.52	0.00
3	3.00	11.40	11.40	0.00
4	3.00	11.40	11.40	0.00
5	3.00	11.15	11.15	0.00
6	-9.00	0.00	0.00	0.00 Reservoir

Link Results:

Link ID	Flow LPS	Velocity m/s	Unit Headloss m/km	Status
1	4.50	0.37	2.12	Open
2	1.50	0.12	0.25	Open
3	4.50	0.37	2.12	Open
4	1.50	0.12	0.25	Open
5	0.00	0.00	0.00	Open
7	9.00	0.00	-13.52	Open Pump

Figure 11: EPA-NET Summary Report, Simulation #4