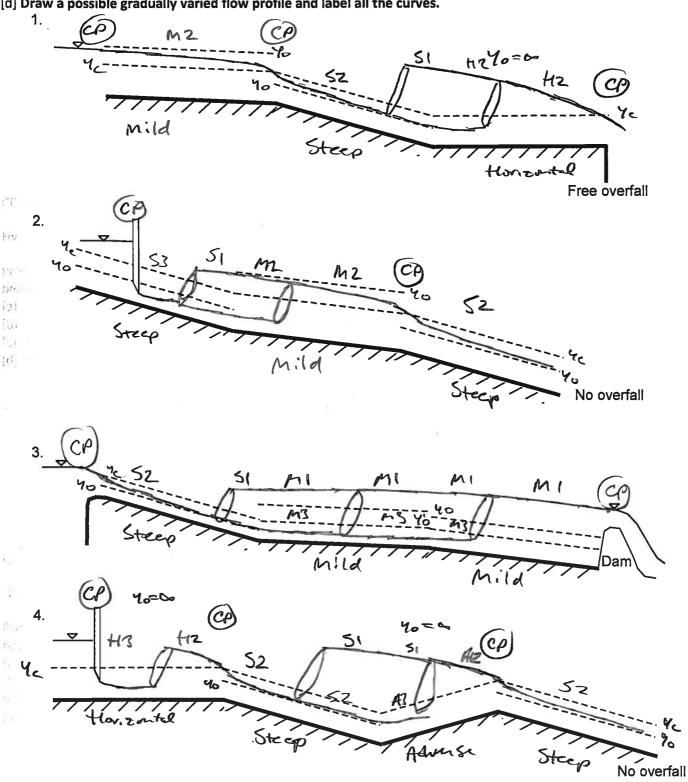
HW 7, Due October 27, 2014

Problems 1-4. Assume the following channel slopes occur in a prismatic open channel. Note where the water surface begins on the left.

- [a] Label y_c and y_o for each reach (state if y_o is infinite).
- [b] Label the bed slopes.
- [c] Label the control points.
- [d] Draw a possible gradually varied flow profile and label all the curves.



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	145
216 wen: 1	Reservoir discharges into long trapezoidal channel. 5 = 20 ft, m = 3, n = 0.025 So = 0.001. Reservoir water suitee 10th above inventof channel ditunce
	6 = 20 to m=3 n=0020 5=0001.
	Received when a first chart some took a contract
C.0. 5	TOPPOST SOUTHER TOTAL RESIDENCE OF THE PROPERTY OF THE PROPERT
Fid: Q	
1) Assume	step slope
:	72
	$\frac{Q^{2} B_{2}}{q^{3} A_{2}^{3}} = 1 - \frac{Q^{2}}{5} = \frac{A_{2}^{3}}{B_{2}} \qquad (a = 1)$
	- 43
	716 (02
	$A = 7c + \frac{Q^2}{24Ac^2} = 4c + \frac{Ac^3}{Bc} = \frac{1}{2Ac^2}$
	21A2 Te + TR. 2A2
4	1 = 4c + Ac = 4c + 4c(b+m7e)
	2R C + 20 2
X	2(5+2m/c)
	of = $y_c + \frac{y_c(20t + 3y_c)}{2(20t + 2(3)y_c)}$
(,	0ft = 4 + 1c (colf + 37E)
	2/20ft + 2(3)4)
1	75612 6-05-4: Fred
	7c = 7.5++to - using Goal Seck in Excel
	$A_{c} = 321 ft^{2} B_{c} = 65.2 ft P = 6+31c (1+m^{2})^{1/2} = 20 ft + 2(7.5 ft)$ $R_{c} = \frac{A_{c}}{P_{c}} = 4.75 ft$ $P = 67.7 ft$
(Ac= 32/16 BC 03.271 P= 0.0 12 0.1111 - 0010+ 1.115/10)
	2 4 P= 67.7fz
	h = = 475 te
	Q = [3 Ac3] /2 = [(32.24/12) (32/48)] /2 = 4040) c/s
	1 4 Ac3 (2 / (32.2 H/(2) (32(H)) /2 - 4040) ch
	Q= 105.2tt
	L De 7
1 -1	(Q. 7) (Java 1.1 225) 72
54=	9 n /2= 14040 cTs (0.00)
	Qn 72 = [4040 cts (0.025)]2 1.49 A=R273] [1.49 (321/42)(4.75/42)3]
	11797214
15, =	0.0056 >50=0.001, so slope is mild
	0.000
H. = 4	0 + (12) = 40 + (02) 2 25 [40 (6+m40)]2
11.0	25to 10 2c/4-(b+myo)
	.13
	Yo + - (22) (12) (2) (4 + 3 4)]]
1014-	40 + 2(32,24t/3) [40(20te+340)] [1]
	200,000
Λ -	149 7/2 1/2 1/2 V
Q =	1.49 Ao Rosso = 149 Ao 8/3 Sole
	h Po 3
	20 4 /204, 20 15k - 1/4
Q = 1	199 Yolzofe+340) 5/8 (0.001) /2 [2]
. 0	1.025 /204+24 (4-32) /3 73
	[20,6, 2,30,0]
Using	Goal Seek nExcel 14 = 9.43 ft () = 2750cts
3	Goal Seek nexcel Ty = 9.43 ft Q = 2750cts

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W. C.
C. T.C.

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5.5	Given:	Reetongul	er channel	5=6,1m	N=0,014	5=201	
		П			Q=	7 m3/sec	
) Ye	-0-				
		0.514					
	Fin	di Water	suture p	rofiler d	hydrenlie je	ing location	
	5						
		6	16.1m	C2 R7/2	= 0.925m		
	4	= (3	3 = 6.7	P. W/2	= 0.925m		
			245 (1/2	1 1./.	37 73 6 16		
	Q) = \(\frac{1}{2}\)	1 - 16	1 19 753	12y 3/3 501/2		
		I milber =	0.014	m +2 5 72/3	(0.001) 1/2		
		u = 1;	31m - 60	alseek in	Excel		
		and the state of t					
10	west 5	tep heth					
	A;=	by = 6	(h) yi				
	12 =	Aip:	(6. (n) + 2 g	ė –			
	V.=	J = 1	In 1/sec		See Spre	edeb oot	
	Ei	7:+ 2	= 4+ 2/48	(1/2)	255 36.0		
	5.	= [n Vi	2 _ [0.01+	V. 2			
	Ei	Rills.	2 = [0.01+ 12273				
	Sel	= E2-E	1+5e2				
	Λī	= F2-E	. 2				
	ΔX	$=$ ΔE $S_0 - S$					
		5, - 5	ebul				
For	r hydra	wite Jum	p - need 1	homentum fu	neha		
	M=	Ah + "	12 - by2	W2_	(6.12)2 L	(17,3/5)2 (9,8/1/62)(6,1/2)4	
			好艺	Sby	2 (9.81~152)(6.1m)4	
12	Intex				n -> 4n=		
					> 1/3 -	1.24 m	
	Fr,=	Vi	= (4.16-15	(0.672)/2=	1,62		
		(2N1)-	16.0(-150)	Coultry			

33kg/

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ASCE STUDENT CHAPTER	



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Check !	$\frac{42}{5} = \frac{1}{2} \left[-1 + \frac{1}{2} \right]$	VI+8F,2]	=1.65	
	72 = 1.85 4, 72 = 1.24m	= 1.65 (0.6		

5.5

Given: Rectangular channel

Q (m²/s) 0.92 17.00 1.31

6.1 m

0.014 n=

y, (m)

0.93

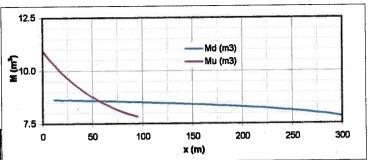
0.001 S_o= 300 m upstream from overfall

0.47 m

17 m³/sec Q= Find: Water surface profiles and location of hydraulic jump Direct Step Method

∆y (m) = 0.02 m

Moving ups	iream from	overfall						·····			
y (m)	A (m²)	P (m)	R (m)	V (m/s)	E (m)	S,	Seber	ΔE (m)	Δx (m)	∑x (m)	M _d (m ³)
0.93	5.67	7.98	0.71	3.00	1.38769	0.002765				300.00	
0.95	5.80	8.00	0.72	2.93	1,38862	0.002593	0.002679	0.00093	-0.55	299.45	7.84
0.97	5.92	8.04	0.74	2.87	1,39072	0.002435	0.002514	0.00210	-1.39	298.06	
0.99	6.04	8,08	0.75	2.82	1,39390	0.002290	0.002382	0.00317	-2,33	295.73	
1.01	6.16	8,12	0.76	2.78	1.39806	0.002158	0.002223	0.00418	-3.40	292.33	
1.03	6.28	8.16	0.77	2.71	1.40313	0.002033	0.002095	0.00508	-4.64	287.69	
1.05	8.41	8.20	0.78	2.65	1.40905	0.001919	0.001976	0.00592	-8.08	281.63	
1.07	6.53	8.24	0.79	2.60	1.41576	0.001814	0.001887	0.00870	-7.73	273.89	
1.09	6.65	8.28	0.80	2.56	1.42319	0.001717	0.001765	0.00743	-9.70	284.19	
1.11	6.77	8.32	0.81	2.51	1.43129	0.001626	0.001671	0.00810	-12.07	252.12	
1.13	6.89	8.38	0.82	2.47	1.44001	0.001542	0.001584	0.00873	-14.94	237.18	
1.15		8.40	0.84	2.42	1.44933	0.001464	0.001503	0.00931	-18.52	218.66	
1.17	7.14	8.44	0.85	2.38	1.45918	0.001391	0.001427	0.00985	-23.07	195.59	
1.19	7.28	8.48	0.86	2.34	1.46954	0.001323	0.001357	0.01038	-29.05	168.54	
1.21	7.38	8.52	0.87	2.30	1.48038	0.001259	0.001291	0.01084	-37.26	129.27	8.4
1.23	7.50	8.56	0.88	2.27	1.49165	0.001200	0.001229	0.01128	-49.20	80.08	
1.25		8.60	0.89	2.23	1.50335	0.001144	0.001172	0.01169	-68.12	11.95	
1.27		8.64	0.90	2.19	1.51543	0.001092	0.001118	0.01208		-90.71	
1.29		8.68	0.91	2.16	1.52788	0.001043	0.001087	0.01245	-185.54	-278.26	
1.31		8.72	0.92	2.13	1.54067	0.000997	0.001020	0.01279	-853,34	-929.50	8.9



Moving downstream from sluice gate

WONING GOM	LIST GRANT IN	A11 SICACO	Hano								2.
y (m)	A (m²)	P (m)	R (m)	V (m/s)	E (m)	S,	Saber	ΔE (m)	∆x (m)	Σx (m)	M _u (m³)
0.47	2.87	7.04	0.41	5,93	2.26202	0.022829				0.00	10,95
0.49	2.99	7.08	0.42	5.69	2.13872	0.020019	0.021424	-0.12330	6.04	6.04	10.59
0.51	3.11	7.12	0.44	5.48	2.03194	0.017852	0.018836	-0.10878	6.99	12.02	10.26
0,53	3.23	7.16	0.45	5.26	1.93925	0.015844	0.016848	-0.09270	5.92	17.95	9.97
0.55	3.38	7.20	0.47	5.07	1.85862	0.013930	0.014787	-0.08063	5.85	23.80	9.70
0.57	3.48	7.24	0.48	4.89	1.78840	0.012458	0.013194	-0.07022	5.78	29.55	9.46
0.59	3.60	7.28	0.49	4.72	1.72720	0.011187	0.011823	-0.06120	5.66	35.21	9.25
0.61	3.72	7.32	0.51	4.57	1.87385	0.010084	0.010638	-0.05335	5.54	40.75	9.05
0.63	3.84	7.36	0.52	4.42	1.62737	0.009122	0.009803	-0.04847	5.40	48.15	8.88
0.65	3.97	7.40	0.54	4.29	1.58894	0.008278	0.008701	-0.04043	5.25	51.40	8.72
0.67	4.09	7.44	0.55	4.16	1.55184	0.007538	0.007908	-0.03510	5.08	56.48	
0.69	4.21	7.48	0.56	4.04	1.52148	0.006883	0.007210	-0.03038	4.89	61.37	8.45
0.71	4.33	7.52	0.58	3.83	1.49528	0.006302	0.006592	-0.02818	4.68	66.05	
0.73	4.45	7.56	0.59	3.82	1.47284	0.005785	0.006044	-0.02244		70.50	8.24
0.75	4.58	7.60	0.60	3.72	1.45375	0.005324	0.005555	-0.01909	4.19	74.69	
0.77	4.70	7.64	0.61	3.62	1.43766	0.004911	0.005118	-0.01608	3.91	78.60	
0.79	4.82	7.68	0.63	3.53	1.42429	0.004541	0.004728	-0.01338	3,59	82.19	
0.81	4.94	7.72	0.64	3.44	1.41335	0.004207	0.004374	-0.01094	3.24	85.43	
0.83	5.08	7.76	0.65	3.36	1.40462	0.003905	0.004056	-0.00873	2.88	88.29	
0.85	5.19	7.80	0.66	3.28	1.39790	0.003832	0.003768	-0.00872	2.43	90.72	
0.87	5.31	7.84	0.68	3.20	1.39300	0.003384	0.003508	-0.00490		92.67	
0.89	5.43	7.88	0.69	3.13	1.38976	0.00315B	0.003271	-0.00324	1.43	94.10	
0.91	5.55	7.92	0.70	3.06	1.38803	0.002953	0.003056	-0.00173	0.84	94.94	
0.93	5.67	7.98	0.71	3.00	1.38789	0.002785	0.002859	-0.00034	0.18	95.12	
0.95		8.00	0.72	2.93	1.38862	0.002593	0.002679	0.00093	-0.55	94.56	7.84

Ax (m) changes sign, because passed critical depth

Moving downstream from sluice gate

	ream from sluice
	y (m)
0.00	0.47
6.04	0.49
12.02	0.51
17.95	0.53
23.80	0.55
29.55	0.57
35.21	0.59
40.75	0.61
46.15	0.63
51.40	0.65
56.48	0.67
35.25	0.59
38.04	0.60
40.79	0.61
43.51	0.62
46.20	0.63
48.84	0.64
51.45	0.65
54.02	0.66
56.54	
56.55	
80.08	
129.27	1.21
166.54	1.19
195.59	1.17
218.66	1.15
237.18	
252.12	
264.19	
273.89	
281.63	
287.69	
292.33	
295.73	
298.06	
299.45	
300.00	0.93

