CE 4353/5360 October 10, 2016

Homework 5, Due October 19

Generate the Q/Q_{full}, V/V_{full} vs. y/d curves known as the hydraulic elements graph for
partially full flow in circular pipes. You can assume a pipe diameter, n, and slope. Use at
least 25 pairs of points to define the curves. You can show the graph on the same page as the
Excel table. Remember to show your name on your spreadsheet printout, and to provide
sample calculations along one row.

- 2. Problem 4.1 with Q = 3200 cfs.
- 3. Repeat 4.1 for a rectangular channel with b=40 ft
- 4. Problem 4.2 with 17 cfs.
- 5. Problem 4.11 with $Q_{max} = 1.2 \text{ m}^3/\text{sec}$ and $Q_{min} = 0.3 \text{ m}^3/\text{sec}$.

Hydraulic Elements Graph

Can assume the following

d = 1 ft n = 0.013 S = 0.005

								1	
y/d	y (ft)	θ (rad)	A (ft ²)	P (ft)	R (ft)	Q (cfs)	V (fps)	Q/Qfull	V/Vfull
0.00	0.00	0.000	0.000	0.000	0.000	0.000	0	0	0
0.02	0.02	0.568	0.004	0.284	0.013	0.002	0.453	0.001	0.141
0.04	0.04	0.805	0.011	0.403	0.026	0.008	0.714	0.003	0.222
0.06	0.06	0.990	0.019	0.495	0.039	0.018	0.930	0.007	0.289
0.08	0.08	1.147	0.029	0.574	0.051	0.033	1.119	0.013	0.348
0.10	0.10	1.287	0.041	0.644	0.064	0.053	1.290	0.021	0.401
0.12	0.12	1.415	0.053	0.707	0.075	0.077	1.447	0.031	0.450
0.14	0.14	1.534	0.067	0.767	0.087	0.106	1.593	0.042	0.495
0.16	0.16	1.646	0.081	0.823	0.099	0.140	1.729	0.056	0.538
0.18	0.18	1.753	0.096	0.876	0.110	0.179	1.857	0.071	0.577
0.20	0.20	1.855	0.112	0.927	0.121	0.221	1.978	0.088	0.615
0.22	0.22	1.953	0.128	0.976	0.131	0.268	2.093	0.106	0.651
0.24	0.24	2.048	0.145	1.024	0.142	0.319	2.201	0.126	0.684
0.26	0.26	2.140	0.162	1.070	0.152	0.374	2.305	0.148	0.717
0.28	0.28	2.230	0.180	1.115	0.161	0.433	2.403	0.171	0.747
0.30	0.30	2.319	0.198	1.159	0.171	0.495	2.496	0.196	0.776
0.32	0.32	2.405	0.217	1.203	0.180	0.560	2.585	0.222	0.804
0.34	0.34	2.490	0.235	1.245	0.189	0.629	2.670	0.249	0.830
0.36	0.36	2.574	0.255	1.287	0.198	0.700	2.751	0.277	0.855
0.38	0.38	2.657	0.274	1.328	0.206	0.775	2.828	0.307	0.879
0.40	0.40	2.739	0.293	1.369	0.214	0.851	2.902	0.337	0.902
0.42	0.42	2.820	0.313	1.410	0.222	0.930	2.971	0.368	0.924
0.44	0.44	2.901	0.333	1.451	0.229	1.011	3.038	0.400	0.944
0.46	0.46	2.981	0.353	1.491	0.237	1.094	3.101	0.433	0.964
0.48	0.48	3.062	0.373	1.531	0.243	1.178	3.160	0.466	0.983
0.50	0.50	3.142	0.393	1.571	0.250	1.263	3.216	0.500	1.000
0.52	0.52	3.222	0.413	1.611	0.256	1.349	3.269	0.534	1.016
0.54	0.54	3.302	0.433	1.651	0.262	1.436	3.319	0.568	1.032
0.56	0.56	3.382	0.453	1.691	0.268	1.523	3.366	0.603	1.046
0.58	0.58	3.463	0.472	1.731	0.273	1.610	3.409	0.637	1.060
0.60	0.60	3.544	0.492	1.772	0.278	1.697	3,449	0.672	1.072
0.62	0.62	3.626	0.512	1.813	0.282	1.783	3.486	0.706	1.084
0.64	0.64	3.709	0.531	1.855	0.286	1.869	3.520	0.740	1.094
0.66	0.66	3.793	0.550	1.897	0.290	1.953	3.551	0.773	1.104
0.68	0.68	3.878	0.569	1.939	0.293	2.035	3.578	0.806	1.112
0.70	0.70	3.965	0.587	1.982	0.296	2.115	3.602	0.837	1.120
0.72	0.72	4.053	0.605	2.026	0.299	2.193	3.622	0.868	1.126
0.74	0.74	4.143	0.623	2.071	0.301	2.267	3.639	0.898	1.131
0.76	0.76	4.235	0.640	2.118	0.302	2.339	3.652	0.926	1.135
0.78	0.78	4.330	0.657	2.165	0.304	2.406	3.661	0.953	1.138
0.80	0.80	4.429	0.674	2.214	0.304	2.469	3.666	0.977	1.140
0.82	0.82	4.531	0.689	2.265	0.304	2.527	3.666	1.000	1.140
0.84	0.84	4.637	0.704	2.319	0.304	2.579	3.662	1.021	1.139
0.86	0.86	4.749	0.719	2.375	0.303	2.625	3.653	1.039	1.136
0.88	0.88	4.868	0.732	2.434	0.301	2.663	3.638	1.054	1.131
0.90	0.90	4.996	0.745	2.498	0.298	2.692	3.616	1.066	1.124
0.92	0.92	5.136	0.756	2.568	0.294	2.711	3.586	1.073	1.115
0.94	0.94	5.293	0.766	2.647	0.289	2.717	3.547	1.076	1.103
0.96	0.96	5.478	0.775	2.739	0.283	2.706	3.493	1.071	1.086
0.98	0.98	5.716	0.782	2.858	0.274	2.669	3.415	1.057	1.062
1.00	1.00	6.283	0.785	3.142	0.250	2.526	3.216	1.000	1.002
1.00	1.00	0.203	0.703	J. 14Z	0.230	Q _{full}	V _{full}	1.000	1.000
						≪tull	* full	l	

$$\theta = 2 \cos^{-1} \left(1 - 2 \frac{y}{d} \right)$$

$$A = \left(\theta - \sin \theta \right) \frac{d^2}{8}$$

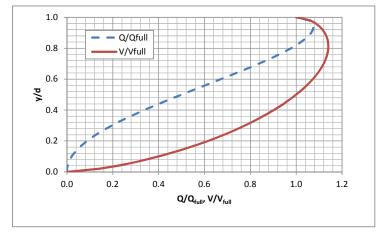
$$P = \frac{\theta d}{2}$$

$$R = \frac{A}{P}$$

$$Q = \frac{1.49}{n} A R^{\frac{1}{2} 3} S^{\frac{1}{2} 2}$$

$$V = \frac{Q}{A}$$

20 points 16 for calculations 4 for graph



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214.1 Gwan: Tray	pozoidal channel	6=40H, m=3, 50	= 0.002	
T T	0.025 D= 3200	عد اء		
E Zina	Au Slore S	teep or mild:	,	F # #=
(1) Re	pear for n=0,012	. Does ye change	6	
(i) 40: Q=!	149 AR2356			
42'	45 - 40			1-1
24	10 24 5/2	14-16+ny 173	no	
C ARB = A	告)3 = 台計 =	[b+240 (1+m2)42] 2	IKn S. Y.	
[4] [40 (+04+	7. 75%	0,-		
[1 Lyo (4044 +	37011	1,49(0.002) 1/2	1201	سلي رمال ا
[40t+ 270C1	+3)23	1.49(0.002)/2		
w/60	~ Sick - 7/40:	6.8244		
		124		
42: Q B	= (
246	1-3 Ty (b	+my 13		
61 -2 =	A23 - [42 (b- B2 - b+3	yn y		
(224) (12	13 -	3 3 3	
3212 14/5	= [404	+ + 37e)]3 - [40	4c + 34c)	+
			7-642	
~/G0	alseck -> 19c=	5.10+4		
m y	ye shope is	mild		
(ii) Represe for	n=0.012			
4c do	es not change	, n is not in y	equation	
to ha	114 (0.002	576.3	1-1-1-1-1	
Rela	ate to Eq.[4]	-> Goal Seel		
	10 = 4.59 ft			
(I) 4.	0 < 42 , slope	c is steep		



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31 Given: Repeat 4.1 forv	ectangular K-section		
6=40 4t N=0	200 LTS 30=	0005	
Fund - (i) yo (ye, is slo			
(ii) Repeat for n =	2012		
(1) 4: () = 1.49 AR 3/3	5,2		
AR26 = Wn 49 5072			
AR 3 = 39 5-72			
1 2/2 - 15/3 (D 7) 5/3	_ ~ Q		-
AL2/3 = A5/2 (by) 5/3 (b+270)	42 Kusste		
754			
[A] [(40ft)(40)] 5/3 =	0.025 (3200 cts) = 120		
[6] [40ft+24.]2/3	1.49 (0.025) 12		
w/ooal seek 40			
T9272			-
7 c= Ye = [92] 1/2			
- (D) 3740	cts - an 4 2/		
6 9 5 40	ft = 80 ft 2/sec		
T(BOft2/s	12 7/2 = 5 Rs fa		
1c = 32.2 ft	1)2-]/3 = 5.84 fe		
TI 40 > 1/2, 540,	pe is mild		
(ii) repeat for n=0.01	2		
6) ncd = 0.0126	3200cts) = 576.3		
1.495042 - 1.496	0.002) 12		
	HS, use Goal Seek		
10=5.4	o ft (
ye does no	+ cheire		+
Te does no	- E- Carlo		
4 < 74	Slope is steep		
4			-
			+++
			1 1
	+		

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+ 14.2 modified Given; Concrete culvert, N=0.015, D=36in, S=0.002
Q = 17 cts
Fire City of 42 a Isslore Steep or mild?
(i) Repeat for 5=0.02
(1) 40: A123/3 - 1.4950/2
$A = (0 - \sin \theta) \frac{d^2}{8}$
P= 0d/2
AR213 = A(A)33 = A 5/3 P 7/3
(17) P P P P P P P P P P P P P P P P P P P
[A] A = 2 cos-1(1-24) = 2 cos-1[1-2(4)]
$\left[\left(\theta - s_{1} - \theta\right) \frac{d^{2}}{B}\right]^{s/g} = nQ$
$ \begin{array}{c c} (\theta - 5.56) \overline{B} & hQ \\ \hline (\theta - 5.56) \overline{B} & + (4.95)/2 \end{array} $
$\frac{(0-504)^{2}}{(0-504)^{2}} = (0.05)(17c45) = 3.83$
[B] F & C3(E) 7/3 1.49 (0.002) %
Used Gorl See1 40= 1.77ft 1 0= 3.51 and
4c Q2 A3
$\frac{4^{2}}{8} = \frac{A^{3}}{B^{2}}$
0 = 2 cus - 1 - 2 (4 c 3 f.)
[6] BL = d Sim & [3+4] 27 3
$\frac{(6)}{8} = \frac{(2 - \sin \theta)^{3+(1)^{2}}}{8} = \frac{(6 - \sin \theta)^{3+(1)^{2}}}{8}$
(ii) v-net 3-0.02
1.49 50 72 = 1.47 (0 02) 1/2 = 1.210
1,495072
The late to [A] & [B] above use 6 and seele Mo = 0.92 Ft], B = 2.36 red
1) YO LYZ, SLOPE KS STEED

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+ (1/25)
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'45 T	
5 4. Umodified Givens Concrete Sewer for	Quar = 1.2 m3/sec D (= Q3 m3/
Find: Diameter & solf-cleaning	7 7 7 7
Find: Diameter de	نمان المراوات المراوات المتعادلات
- check V for self-cleaning	
Cuzota V 10V 3	esi tent
11 Fatinate di muester	
check V for SEIT-cleaning (i) Estimate di ometer d = 1.56 [n Q] 38 = 1.56 [0.UIT) (1.24 Year) 73/8
d = 1,56/ = 1,56/	1,010,014/2 = 560,000
7107 3070 -	10320.0.0
14\ d= 1,13 m (3.28ft) = 3-71ft	1/12in /- dar
0 - 1113-11 (m)	(FF)-11.3 h
Say d = 48 in as nom	in 2 più size (ox 1.22 m)
ANZIS = NQ = 0.424 from.	160Ve
Kn 50 12	
D= 2005-1[1-2/4] = Z005-1	1-2/1
$\overline{(\theta)} A = (\theta - \sin \theta) \frac{d^2}{8} = (\theta - \sin \theta) $	1,22m JZ
(8)	8
P= 01 = 0 (1.22m)	
R= = > ARY = 0.424+	an fet
Use 6 and seek => 14 = 0.83	- A=0.843 - G=3.87 ad
Ware # = 1.2 m3/sec = .	1,42 m/sex > a61- Kee
max # 0,843 m2	
	OK at Wway
A+ amin = 0.3 m3/sec	
_ nd 6.015(0.3 m3/cc)	
(B) Kn 5072 = 6.01 (0.3 m3/2) = 0.11	06
100000	
Same Egs. Used book Seek	AR 13 tancet = 0,106
1/min = 0.37m Ami=0	200m2 U= 28 Syell
V = Q = 0.3 ~ Vsec -	01 2011
V A 030-2	unfsec 10,61 m/sec
	WOK at Qmis
	O OK AT OMIN

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