

ECSE 597: Circuit Simulation and Modelling
Assignment 3



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1. *dcsolvealpha.m*

```
function Xdc = dcsolvealpha(Xguess,alpha,maxerr)
% Compute dc solution using newton iteration for the augmented system
%  $G \cdot X + f(X) = \alpha \cdot b$ 
% Inputs:
% Xguess is the initial guess for Newton Iteration
% alpha is a paramter (see definition in augmented system above)
% maxerr defined the stopping criterion from newton iteration: Stop the
% iteration when  $\text{norm}(\text{deltaX}) < \text{maxerr}$ 
% Oupputs:
% Xdc is a vector containing the solution of the augmented system

global G C b DIODE_LIST npnBJT_List

converged = false;

delta_x = 1234567890;

% slides B45/48
while (norm(delta_x) >= maxerr)

    f = f_vector(Xguess);

    disp ('f=');
    disp (f);

    phi = G * Xguess + f - alpha * b;

    J = nlJacobian(Xguess);

    disp ('J=');
    disp (J);

    delta_x = -1 * J \ phi;

    Xguess = Xguess + delta_x;

    disp ('Xdc=');
    disp(Xguess);

    % if (delta_x >= maxerr)
    %     converged = true;
    %end

end

Xdc = Xguess;
```

2. *dcsolvecont.m*

Vi was set at different values and the following code was run to test this function.

Vi=10;

```
Sedra4_93  
Xdc = dcsolvecont(10,1e-6)
```

```
Vi=2;  
Sedra4_93  
Xdc = dcsolvecont(10,1e-6)
```

```
Vi=-8;  
Sedra4_93  
Xdc = dcsolvecont(10,1e-6)
```

At $V_i = 10V$

Xdc =

```
1.0000  
3.0702  
3.7895  
10.0000  
-2.0000  
-2.0000  
0.0021  
-0.0021  
0.0000
```

At $V_i = 2V$

Xdc =

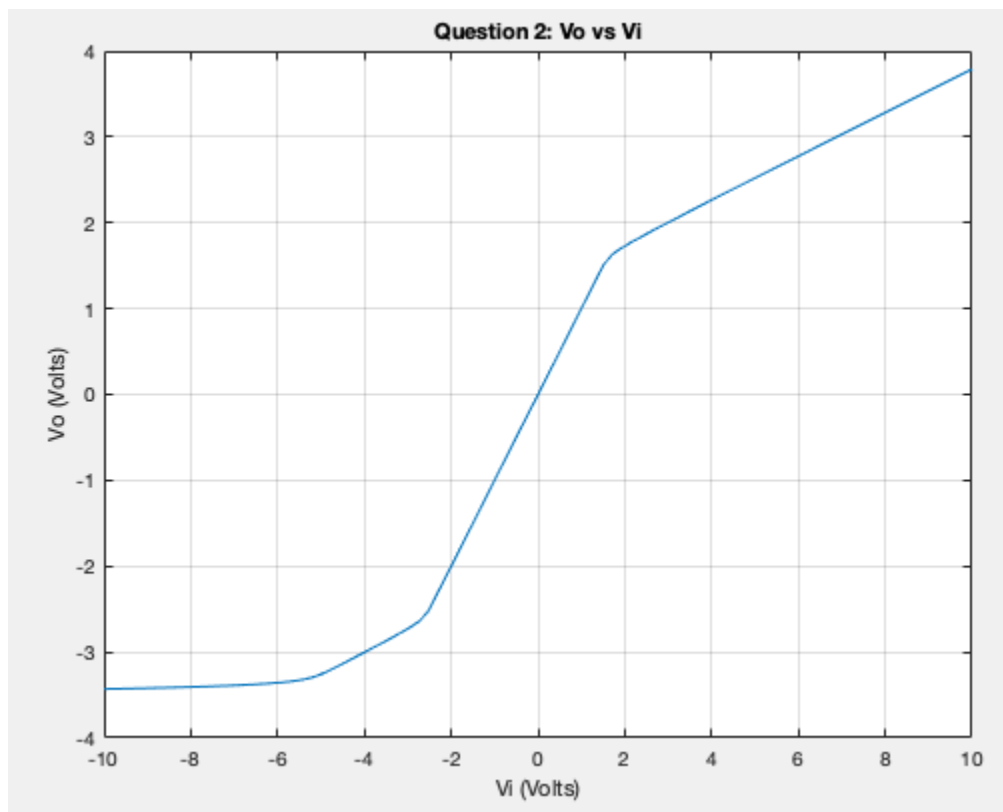
```
1.0000  
1.0905  
1.7284  
2.0000  
-2.0000  
-2.0000  
0.0001  
-0.0001  
0.0000
```

At $V_i = -8V$

$X_{dc} =$

1.0000
1.0000
-3.4072
-8.0000
-2.6957
-2.0000
-0.0000
0.0015
-0.0015

2. TestBenchDiodeckt4_93.m was run to compute and plot V_o as a function of V_i . Following plot was observed. The values observed in the plot align with DC values obtained in the output node (node 3) in the previous part.



```

function Xdc = dcsolvecont(n_steps,maxerr)
% Compute dc solution using newtwn iteration and continuation method
% (power ramping approach)
% inputs:
% n_steps is the number of continuation steps between zero and one that are
% to be taken. For the purposes of this assignments the steps should be
% linearly spaced (the matlab function "linspace" may be useful).
% maxerr is the stopping criterion for newton iteration (stop iteration
% when norm(deltaX)<maxerr

global G C b DIODE_LIST npnBJT_List

% Slides C00 10/15
sz = length(G);
Xdc = zeros(sz, 1);
%y = linspace(x1,x2,n) generates n points. The spacing between the points is (x2-x1)/(n-1).
steps = linspace(0,1,n_steps);

for i = 1 : n_steps
    Xdc = dcsolvealpha(Xdc, steps(i), maxerr);
end

```

3. BJT implementation

1. Run the BJT_CB.m using the dcsolve.m function you implemented in Assignment 1. Report your observations.

Without power ramping it keeps iterating forever and doesn't converge although I waited for a long term and set the error tolerance quite high.

2. Run the BJT_CB.m using the dcsolvecont.m function you implemented in Question II. Report the values of the nodal voltages obtained after using dcsolvecont.m.

Xdc =

```

10.0000
 5.3197
 6.0000
 5.2964
-0.0010
-0.0006

```

- 1) f_vector.m with BJT

```

function f = f_vector(X)
% Compute the nonlinear vector of the MNA equations as a function of x

global b DIODE_LIST npnBJT_LIST

N = size(b);
f = zeros(N); % Initialize the f vector (same size as b)

NbDiodes = size(DIODE_LIST,2);
Npnbjts = size(npnBJT_LIST,2);

%% Fill in the Fvector for Diodes
for I = 1:NbDiodes
    node_i = DIODE_LIST(I).node1
    node_j = DIODE_LIST(I).node2
    Vt = DIODE_LIST(I).Vt; % Vt of diode (part of diode model)
    Is = DIODE_LIST(I).Is; % Is of Diode (part of diode model)

    if (node_i ~= 0) && (node_j ~= 0)
        v1 = X(node_i); %nodal voltage at anode
        v2 = X(node_j); %nodal voltage at cathode
        diode_current = Is*(exp((v1-v2)/Vt)-1);
        f(node_i) = f(node_i) + diode_current;
        f(node_j) = f(node_j) - diode_current;
    elseif (node_i == 0)
        v2 = X(node_j); %nodal voltage at cathode
        diode_current = Is*(exp((-v2)/Vt)-1);
        f(node_j) = f(node_j) - diode_current;
    elseif (node_j == 0)
        v1 = X(node_i); %nodal voltage at anode
        diode_current = Is*(exp((v1)/Vt)-1);
        f(node_i) = f(node_i) + diode_current;
    end
end

%% Fill in the Fvector for BJTs
for I=1:Npnbjts

    %get Nodes Numbers
    cNode = npnBJT_LIST(I).collectorNode;
    bNode = npnBJT_LIST(I).baseNode;
    eNode = npnBJT_LIST(I).emitterNode;

    % get other parameters
    Vt = npnBJT_LIST(I).Vt;
    Is = npnBJT_LIST(I).Is;
    alphaR = npnBJT_LIST(I).alphaR;
    alphaF = npnBJT_LIST(I).alphaF;

    % if both nodes not grounded

    if (cNode~=0) && (bNode~=0) && (eNode~=0) % all nodes present
        % get nodal voltages

        Vbe = X(bNode) -X(eNode);
        Vbc = X(bNode) -X(cNode);
        % diode currents
        If = Is*(exp(Vbe/Vt)-1);
        Ir = Is*(exp(Vbc/Vt)-1);
    end
end

```

```

f(cNode) = f(cNode) -Ir + alphaF*If ;
f(bNode) = f(bNode) +Ir*(1-alphaR) + If*(1-alphaF);
f(eNode) = f(eNode) +Ir*alphaR - If;

elseif (cNode~=0) && (bNode==0) && (eNode~=0) % Base is Grounded

Vbe = -1*X(eNode);
Vbc = -1*X(cNode);
% diode currents
If = Is*(exp(Vbe/Vt)-1);
Ir = Is*(exp(Vbc/Vt)-1);

f(cNode) = f(cNode) -Ir + alphaF*If ;
%f(bNode) = f(bNode) +Ir*(1-alphaR) + If*(1-alphaF);
f(eNode) = f(eNode) +Ir*alphaR - If;

elseif (cNode~=0) && (bNode~=0) && (eNode==0) % Emitter is Grounded
% fill this up

Vbe = X(bNode);
Vbc = X(bNode) -X(cNode);
% diode currents
If = Is*(exp(Vbe/Vt)-1);
Ir = Is*(exp(Vbc/Vt)-1);

f(cNode) = f(cNode) -Ir + alphaF*If ;
f(bNode) = f(bNode) +Ir*(1-alphaR) + If*(1-alphaF);
%f(eNode) = f(eNode) +Ir*alphaR - If;

elseif (cNode==0) && (bNode~=0) && (eNode~=0) % Collector is Grounded
% fill this up

% get nodal voltages

Vbe = X(bNode) -X(eNode);
Vbc = X(bNode);
% diode currents

If = Is*(exp(Vbe/Vt)-1);
Ir = Is*(exp(Vbc/Vt)-1);

f(bNode) = f(bNode) +Ir*(1-alphaR) + If*(1-alphaF);
f(eNode) = f(eNode) +Ir*alphaR - If;

elseif (cNode~=0) && (bNode==0) && (eNode==0) % Base and Emitter are grounded
% get nodal voltages
Vbe = 0;
Vbc = -X(cNode);
% diode currents
If = Is*(exp(Vbe/Vt)-1);
Ir = Is*(exp(Vbc/Vt)-1);

f(cNode) = f(cNode) -Ir + alphaF*If ;

end
end %end Forloop for BJTs

```

2) nlJacobian.m with BJT

```
function J = nlJacobian(X)
% Compute the jacobian of the nonlinear vector of the MNA equations as a
% function of X
% input: X is the current value of the unknown vector.
% output: J is the jacobian of the nonlinear vector f(X) in the MNA
% equations. The size of J should be the same as the size of G.

global G DIODE_LIST npnBJT_LIST
N = size(G);
J = zeros(N);
d_diode = zeros(N);
d_BJT = zeros(N);

%% Add the Jacobian for diode --
%copy paste the one you implemented in your previous assignment

NbDiodes = size(DIODE_LIST,2);

if (NbDiodes ~= 0)

for I = 1:NbDiodes
    node_i = DIODE_LIST(I).node1;
    node_j = DIODE_LIST(I).node2;
    v1 = X(node_i); %nodal voltage at anode
    v2 = X(node_j); %nodal voltage at cathode
    Vt = DIODE_LIST(I).Vt; % Vt of diode
    Is = DIODE_LIST(I).Is; % Is of Diode

    if (node_i ~= 0) && (node_j ~= 0)

        %diode_current = Is*(exp((v1-v2)/Vt)-1);
        % derivative of diode current wrt v1
        d_I_v1 = (Is/Vt)*exp((v1-v2)/Vt);
        % derivative of diode current wrt v2
        d_I_v2 = -(Is/Vt)*exp((v1-v2)/Vt);

        % f(node_i) = f(node_i) + diode_current;
        % differentiate f(node_i) wrt v1
        d_diode(node_i, node_i) = d_diode(node_i, node_i) + d_I_v1;
        % f(node_i) = f(node_i) + diode_current;
        % differentiate f(node_i) wrt v2
        d_diode(node_i, node_j) = d_diode(node_i, node_j) + d_I_v2;
        %f(node_j) = f(node_j) - diode_current;
        % differentiate f(node_j) wrt v1
        d_diode(node_j, node_i) = d_diode(node_j, node_i) - d_I_v1;
        %f(node_j) = f(node_j) - diode_current;
        % differentiate f(node_j) wrt v2
        d_diode(node_j, node_j) = d_diode(node_j, node_j) - d_I_v2;

    elseif (node_i == 0)

        % diode_current = Is*(exp((v1-v2)/Vt)-1);
        % derivative of diode current wrt v2
        d_I_v2 = -(Is/Vt)*exp((v1-v2)/Vt);
        %f(node_j) = f(node_j) - diode_current;
        % differentiate f(node_j) wrt v2
```



```

        d_diode(node_j, node_j) = d_diode(node_j, node_j) - d_I_v2;

elseif (node_j == 0)
    % diode_current = Is*(exp((v1-v2)/Vt)-1);
    % derivative of diode current wrt v1
    d_I_v1 = (Is/Vt)*exp((v1-v2)/Vt);
    % f(node_i) = f(node_i) + diode_current;
    % differentiate f(node_i) wrt v1
    d_diode(node_i, node_i) = d_diode(node_i, node_i) + d_I_v1;

end
end

end

%% Add the Jacobian for BJT

NbBJTs = size(npnBJT_LIST,2);

if (NbBJTs ~= 0)

for I=1:NbBJTs

    %get Nodes Numbers
    cNode = npnBJT_LIST(I).collectorNode;
    bNode = npnBJT_LIST(I).baseNode;
    eNode = npnBJT_LIST(I).emitterNode;

    % get other parameters
    Vt = npnBJT_LIST(I).Vt;
    Is = npnBJT_LIST(I).Is;
    alphaR = npnBJT_LIST(I).alphaR;
    alphaF = npnBJT_LIST(I).alphaF;

    if(cNode~=0) && (bNode~=0) && (eNode~=0) % all nodes present

        % get nodal voltages
        Vbe = X(bNode) -X(eNode);
        Vbc = X(bNode) -X(cNode);

        % diode currents
        % If = Is*(exp(Vbe/Vt)-1);
        % derivative of If wrt Vc
        delta_If_c = 0;
        % derivative of If wrt Vb
        delta_If_b = Is/Vt*exp(Vbe/Vt);
        % derivative of If wrt Ve
        delta_If_e = -Is/Vt*exp(Vbe/Vt);

        % Ir = Is*(exp(Vbc/Vt)-1);
        % derivative of Ir wrt Vc
        delta_Ir_c = -Is/Vt*exp(Vbc/Vt);
        % derivative of Ir wrt Vb
        delta_Ir_b = Is/Vt*exp(Vbc/Vt);
        % derivative of Ir wrt Ve
        delta_Ir_e = 0;

        %f(cNode) = f(cNode) -Ir + alphaF*If ;
        % derivative f(cNode) wrt Vc
        d_BJT(cNode, cNode) = d_BJT(cNode, cNode) - delta_Ir_c + alphaF * delta_If_c;
        % derivative f(cNode) wrt Vb

```

```

d_BJT(cNode, bNode) = d_BJT(cNode, bNode) - delta_Ir_b + alphaF * delta_If_b;
% derivative f(cNode) wrt Ve
d_BJT(cNode, eNode) = d_BJT(cNode, eNode) - delta_Ir_e + alphaF * delta_If_e;

%f(bNode) = f(bNode) +Ir*(1-alphaR) + If*(1-alphaF);
d_BJT(bNode,cNode) = d_BJT(bNode, cNode) + delta_Ir_c *(1-alphaR) +
delta_If_c*(1-alphaF);
d_BJT(bNode,bNode) = d_BJT(bNode, bNode) + delta_Ir_b *(1-alphaR) +
delta_If_b*(1-alphaF);
d_BJT(bNode,eNode) = d_BJT(bNode, eNode) + delta_Ir_e *(1-alphaR) +
delta_If_e*(1-alphaF);

%f(eNode) = f(eNode) +Ir*alphaR - If;
d_BJT(eNode,cNode) = d_BJT(eNode, cNode) + delta_Ir_c *(alphaR) - delta_If_c;
d_BJT(eNode,bNode) = d_BJT(eNode, bNode) + delta_Ir_b *(alphaR) - delta_If_b;
d_BJT(eNode,eNode) = d_BJT(eNode, eNode) + delta_Ir_e *(alphaR) - delta_If_e;

elseif (cNode~=0) && (bNode==0) && (eNode~=0) % Base is Grounded

Vbe = -1*X(eNode);
Vbc = -1*X(cNode);

delta_If_c = 0;
%delta_If_b = Is/Vt*exp(Vbe/Vt);
delta_If_e = -Is/Vt*exp(Vbe/Vt);

delta_Ir_c = -Is/Vt*exp(Vbc/Vt);
%delta_Ir_b = Is/Vt*exp(Vbc/Vt);
delta_Ir_e = 0;

d_BJT(cNode, cNode) = d_BJT(cNode, cNode) - delta_Ir_c + alphaF * delta_If_c;
d_BJT(cNode, eNode) = d_BJT(cNode, eNode) - delta_Ir_e + alphaF * delta_If_e;

d_BJT(eNode,cNode) = d_BJT(eNode, cNode) + delta_Ir_c *(alphaR) - delta_If_c;
d_BJT(eNode,eNode) = d_BJT(eNode, eNode) + delta_Ir_e *(alphaR) - delta_If_e;

elseif (cNode~=0) && (bNode~=0) && (eNode==0) % Emitter is Grounded

% fill this up

Vbe = X(bNode);
Vbc = X(bNode) -X(cNode);

delta_If_c = 0;
delta_If_b = Is/Vt*exp(Vbe/Vt);
%delta_If_e = -Is/Vt*exp(Vbe/Vt);

delta_Ir_c = -Is/Vt*exp(Vbc/Vt);
delta_Ir_b = Is/Vt*exp(Vbc/Vt);
%delta_Ir_e = 0;

d_BJT(cNode, cNode) = d_BJT(cNode, cNode) - delta_Ir_c + alphaF * delta_If_c;
d_BJT(cNode, bNode) = d_BJT(cNode, bNode) - delta_Ir_b + alphaF * delta_If_b;

d_BJT(bNode,cNode) = d_BJT(bNode, cNode) + delta_Ir_c *(1-alphaR) +
delta_If_c*(1-alphaF);
d_BJT(bNode,bNode) = d_BJT(bNode, bNode) + delta_Ir_b *(1-alphaR) +
delta_If_b*(1-alphaF);

```

```

elseif (cNode==0) && (bNode~=0) && (eNode~=0) % Collector is Grounded

    Vbe = X(bNode) -X(eNode);
    Vbc = X(bNode);

    % diode currents

    %delta_If_c = 0;
    delta_If_b = Is/Vt*exp(Vbe/Vt);
    delta_If_e = -Is/Vt*exp(Vbe/Vt);

    %delta_Ir_c = -Is/Vt*exp(Vbc/Vt);
    delta_Ir_b = Is/Vt*exp(Vbc/Vt);
    delta_Ir_e = 0;

    d_BJT(bNode,bNode) = d_BJT(bNode, bNode) + delta_Ir_b *(1-alphaR) +
delta_If_b*(1-alphaF);
    d_BJT(bNode,eNode) = d_BJT(bNode, eNode) + delta_Ir_e *(1-alphaR) +
delta_If_e*(1-alphaF);

    d_BJT(eNode,bNode) = d_BJT(eNode, bNode) + delta_Ir_b *(alphaR) -    delta_If_b;
    d_BJT(eNode,eNode) = d_BJT(eNode, eNode) + delta_Ir_e *(alphaR) -    delta_If_e;

elseif (cNode~=0) && (bNode==0) && (eNode==0) % Base and Emitter are grounded

    %Vbe = 0;
    Vbc = -X(cNode);
    % diode currents

    delta_If_c = 0
    delta_Ir_c = -1*Is/Vt*exp(Vbc/Vt)

    d_BJT(cNode, cNode) = d_BJT(cNode, cNode) -    delta_Ir_c          +
alphaF*delta_If_c ;

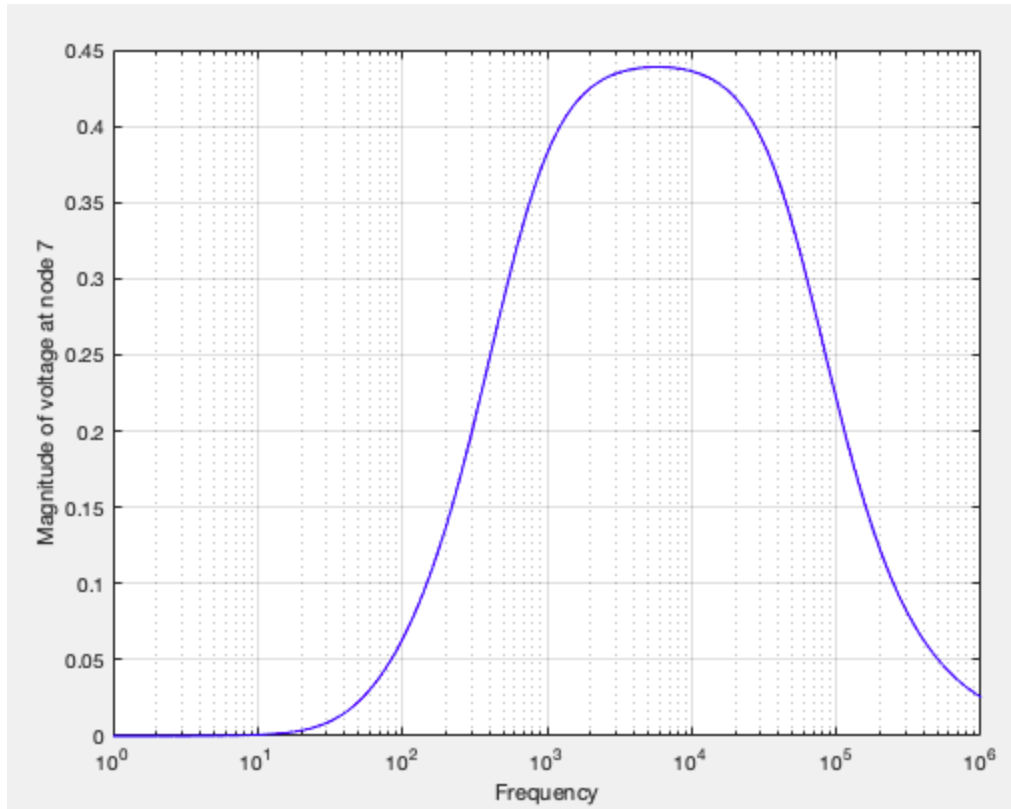
end
end %end Forloop for BJTs

end
J = G + d_BJT + d_diode;
end

```

4. nlACresponse.m

1. Run the BJT_CE.m and plot the gain at node 7 for the frequencies between 0 to 10^6 Hz obtained and include it in the assignment.



```
function r = nonlinear_fsolve(Xdc, fpoints ,out)
% nonlinear_fsolve(fpoints ,out)
% Obtain frequency domain response
% global variables G C b bac
% Inputs: fpoints is a vector containing the fequency points at which
%         to compute the response in Hz
%         out is the output node
% Outputs: r is a vector containing the value of
%         of the response at the points fpoint

global G C b bac

% book page 148
sz = size(fpoints, 2);
r = zeros(1, sz);

for i = 1:sz
    % (G + jwC) * X = b
    %Xdc = (G + 1j * 2 * pi * fpoints(i) * C) \ (b + bac);

    %Xs*(G+Jdc) + CXs = bs

    J = nlJacobian(Xdc);
    Xac = (G + J + 1j * 2 * pi * fpoints(i) * C) \ (bac);

    r(1, i) = Xac(out);
end

end
```

