

1. Code a numerical solution to the RP equation (1).

MATLAB was used to generate a solution to the Rayleigh-Plesset Equation. Variables were re-defined such that $y_1 = R$ and $y_2 = \dot{R}$. This allowed the single 2nd order ODE to become 2 coupled 1st order ODEs. Redefinition of variables resulted in:

$$\dot{y}_1 = y_2 \quad \dot{y}_2 = \ddot{R}$$

with

$$\ddot{R} = \left[\frac{P(R, \dot{R}, t)}{\rho} - \frac{3}{2} \dot{R}^2 \right] \frac{1}{R}$$

where

$$P(R, \dot{R}, t) = P_g^e \left(\frac{R_o}{R} \right)^{3k} + P_v - P_\infty - \frac{2\sigma}{R} - \frac{4\mu\dot{R}}{R}$$

$$P_g^e = P_\infty^e - P_v + \frac{2\sigma}{R_o}$$

$$P_\infty = P_\infty^e + P_a \sin(\omega t)$$

Shown below are the codes used to obtain solutions to the RP equation

```

1 % This script will model the Rayleigh Plesset Equations
2 % Author: Dorien Villafranco
3 % Department of Mechanical Engineering, Boston University
4 % Requirements for ME721: Acoustic Bubble Dynamics ~ HW1
5 clear
6 clc
7 close all
8 %% Define Variables
9 % rho = 998; % kg/m^3
10 % P_a = 1*10^4 ; % Acoustic Pressure amplitude (Pascals)
11 % w = 2*pi*20*10^3; % Acoustic Driving Frequency (2*pi*20 kHz)
12 % Pv = 2.33*10^3; % Vapor Pressure (Water/Air) Boundary
13 % P_inf_e = 1*10^5; % Pressure far away from the bubble at
    equil ~ Pa

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14 % k = 1.4; % Polytropic Exponent of gas (air
    adiabatic approx.)
15 % sigma = 0.072; % Surface Tension for Air/Water
16 % nu = 0.001; % Shear (dynamic) liquid viscosity for
    water in Pa*s
17 Ro = 1*10^-5; % Equilibrium Bubble Radius in meters
18 % %tspan= [0 0.0001]; % Time vector in seconds
19 %
20 t0 = 0;
21 tf = 0.001;
22 y0 = [1.5*Ro, 0]';
23 [t,y] = ode23(@Rayleigh2,[t0,tf],y0);
24 t1 = t;
25 % tplot = t-t0;
26
27 figure(1)
28 hp = plot(t,y(:,1));
29 grid on
30 set(hp,'LineWidth',2)
31 set(gca,'FontSize',12)
32 xlabel('Time (s)')
33 ylabel('Bubble Radius (m)')
34
35 % Question 3
36 % Lauterborn's Figure 2 was digitized and points imported into
    data set
37 % format long
38 % LAT = dlmread('Lauterborn-Figure2.txt');
39 % t_lat = LAT(:,1);
40 % R_Ro_lat = LAT(:,2);
41 % figure(2)
42 % hp2 = plot(tplot,y(:,1)/Ro,'x');
43 % hold on;
44 % hp3 = plot(t_lat,R_Ro_lat);
45 % leg1 = legend('Computed Results','Lauterborn Results');
46 % set(leg1,'FontSize',13)
47 % xlim([0 17*10^-6])
48 % ylim([0 2])
49 % grid on
50 % set(hp2,'LineWidth',2)
51 % set(hp3,'LineWidth',2)
52 % set(gca,'FontSize',13)
53 % xlabel('Time (s)')
54 % ylabel('R/Ro')
55
56 % Question 4

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57 clear t
58 tf = 0.001;
59 [T,Y] = ode45(@Runge_Kutta, [t0,tf],y0);
60 figure(3)
61 hp4 = plot(T,Y(:,1)+Ro);
62 set(gca,'FontSize',12)
63 set(hp4,'LineWidth',2)
64 xlabel('Time (s)')
65 ylabel('Bubble Radius (m)')
66 grid on
67
68
69 % Quesiton 5
70 rho = 998; % kg/m^3
71 P_a = 1*10^2 ; % Acoustic Pressure amplitude (Pascals)
72 w = 2*pi*20*10^3; % Acoustic Driving Frequency (2*pi*20 kHz)
73 Pv = 2.33*10^3; % Vapor Pressure (Water/Air) Boundary
74 P_inf_e = 1*10^5; % Pressure far away from the bubble at
    equil ~ Pa
75 k = 1.4; % Polytropic Exponent of gas (air adiabatc
    approx.)
76 sigma = 0.072; % Surface Tension for Air/Water
77 nu = 0.001;
78 tspan= [0:0.000001:0.001]; % Time vector in seconds
79
80 w_sq = (3*k*P_inf_e)/(rho*Ro^2);
81 damp = (2*nu)/(sqrt(rho*Ro^2*3*k*P_inf_e));
82 M = ((1-w.^2/w_sq)).^2 + (2*damp*w.^2/w_sq)^(-0.5);
83 phi = -atan((2*damp*w/w_sq.^0.5)/(1-(w.^2/w_sq)));
84 y_approx = -P_a/(rho*Ro*w_sq)*M*sin(w*tspan+phi);
85
86 figure(4)
87 plot(tspan,y_approx)
88
89 figure(5)
90 hp10 = plot(t1,y(:,1),'x');
91 hold on;
92 hp20 = plot(T,Y(:,1)+Ro);
93
94 hp30 = plot(tspan,y_approx+Ro);
95 xlim([0 0.001])
96 set(gca,'FontSize',14)
97 grid on
98 leg2 = legend('Equation 1','Equation 3','Equation 5');
99 xlabel('Time (s)')
100 ylabel('Bubble Radius (m)')

```

```
101 set(leg2,'FontSize',14)
102 set(hp10,'LineWidth',1)
103 set(hp20,'LineWidth',1)
104 set(hp30,'LineWidth',2)

1 function Rdot2 = Rayleigh(t,y)
2 rho = 998;           % kg/m^3
3 P_a = 0 ;           % Acoustic Pressure amplitude (Pascals)
4 w = 2*pi*20*10^3; % Acoustic Driving Frequency (2*pi*20 kHz)
5 Pv= 2.33*10^3;      % Vapor Pressure (Water/Air) Boundary
6 P_inf_e=1*10^5;     % Pressure far away from the bubble at equil(Pa)
7 k = 1.4;            % Polytropic Exponent of gas (air adiabatic)
8 sigma = 0.072;      % Surface Tension for Air/Water
9 nu = 0.001;         % Shear(dynamic) liquid viscosity for water(Pas)
10 Ro = 1*10^-5;       % Equilibrium Bubble Radius in meters
11 Rdot = y(2);
12 R = y(1);
13 % Pressure in the gas @ equilibrium
14 P_ge = P_inf_e - Pv + (2*sigma/Ro);
15
16 % Pressure far away from the bubble
17 P_inf = P_inf_e + P_a.*sin(w*t);
18 P = P_ge*(Ro/R)^(3*k) + Pv - P_inf - (2*sigma/R) - (4*nu*Rdot/R);
19 Rdot2 = [y(2); (P/rho - (3/2)*y(2).^2)*(1./y(1))];
```

2. Perform the following sanity checks on your code:

- i. Equilibrium: Set $P_a = 0$; $\dot{R}(t=0) = 0$; $R(t=0) = R_o$ and run the code with these initial conditions for at least $t = 0.001$ s. Plot $R(t)$; is it stable?

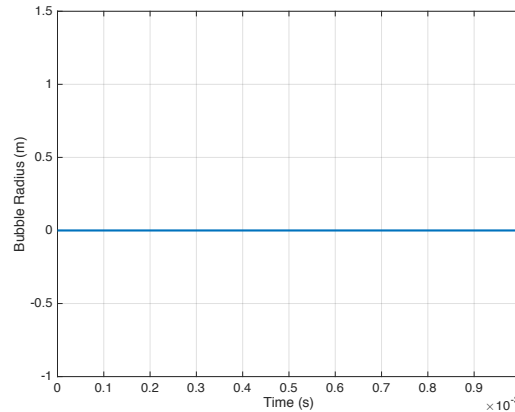


Figure 1: Equilibrium Solution for the Rayleigh Plesset Equation

- ii. Ring down: Set run your code for each initial condition. Plot $R(t)$ does it decay to R_0 ? What is the frequency of the ringing? How does it compare with the linear natural frequency.

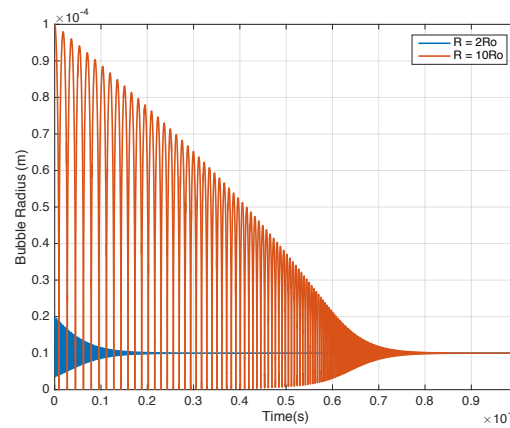


Figure 2: Ring Down test for Rayleigh Plesset Code

iii. Step drive: Set $\dot{R}(t=0) = 0$; $R(t=0) = R_0$; $P_\infty = P_\infty^e + P_c H(t - t_o)$ where P_c is 1×10^5 Pa and $H(t)$ is the unit step function (Heaviside). Plot $R(t)$ does it make sense?

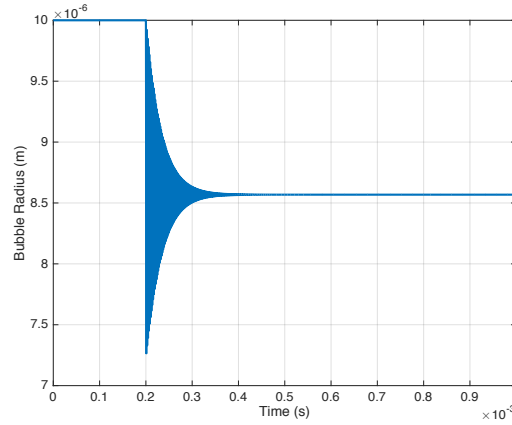


Figure 3: Step Drive test for Rayleigh Plesset Code

3. Benchmark your code against a previously published solution, using their parameter values. You may choose anything nontrivial* in the literature of the past 50 years, but be careful to compare results of the same equation at the same parameters, since there are a variety of Rayleigh-Plesset equations.

I used the parameters laid out in the paper by Lauterborn. The figure below shows the comparison of the results. Not sure why they do not align properly. It may be an incorrect use of his parameters in the papers or a sign difference in the equation - will double check later and update.

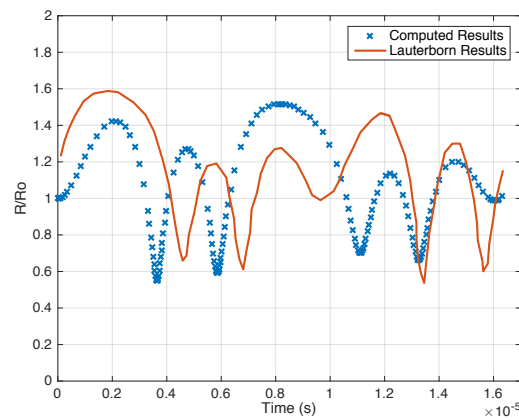


Figure 4: Comparison of Computational Results with those obtained by Lauterborn

4. Recall the linear EOM we derived in class for $R(t) = R_o + y(t)$, $y \ll R_o$

$$\ddot{y} + \left(\frac{4\mu}{\rho R_o^2} \right) \dot{y} + \frac{1}{\rho R_o^2} \left(3k \left(P_\infty^e - P_v + \frac{2\sigma}{R_o} \right) - \frac{2\sigma}{R_o} \right) y = \frac{-P}{\rho R_o} \sin(\omega t)$$

- i. Code a numerical integration solution to (3)

```

1 function dy = Runge_Kutta(t,y)
2
3 rho = 998; % kg/m^3
4 P_a = 0 ; % Acoustic Pressure amplitude (Pascals)
5 w = 2*pi*20*10^3; % Acoustic Driving Frequency (2*pi*20 kHz)
6 P_v = 2.33*10^3; % Vapor Pressure (Water/Air) Boundary
7 P_inf_e = 1*10^5; % Pressure far away from the bubble at equilibrium Pa
8 k = 1.4; % Polytropic Exponent of gas (air adiabatic approx.)
9 sigma = 0.072; % Surface Tension for Air/Water
10 nu = 0.001; % Shear (dynamic) liquid viscosity for water in Pa*s
11 Ro = 1*10^-5; % Equilibrium Bubble Radius in meters
12 dy = zeros(2,1);
13 dy(1) = y(2);
14 dy(2) = -P_a/(rho*Ro).*sin(w*t) - ((4*nu)/(rho*Ro^2))*y(2) - (1/(rho*Ro^2))*...
15 (3*k*(P_inf_e - P_v + (2*sigma/Ro)) - (2*sigma/Ro))*y(1);

```

- ii. Benchmarks Works for all similar cases. See comparison in Problem 5

5. For the linearized EOM in problem 4, we can approximate the natural frequency as:

$$\omega_o^2 = \frac{3kP_\infty^e}{\rho R_o^2}$$

and the damping ratio as:

$$\xi = \frac{2\mu}{(\rho R_o^2 3kP_\infty^2)^{0.5}}$$

with the usual solution to sine forcing given as:

$$y(t) = \frac{-P_a}{\rho R_o \omega_o^2} M(\omega) \sin(\omega t + \phi(\omega))$$

-
- i. Compare results of all there developments of R(t)

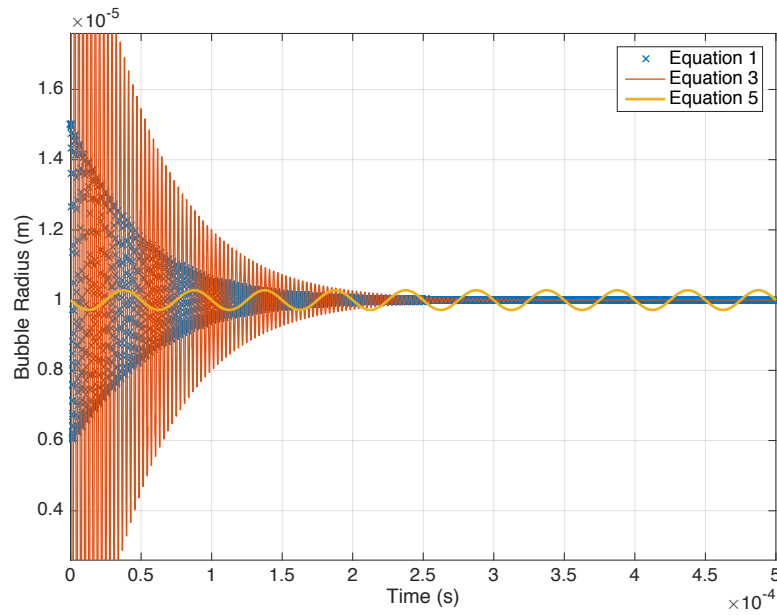


Figure 5: Comparison of all developments of R(t)