Control Of A Quadcopter

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1 Generalized Coordinates

In order to properly define the dynamics of a quadcopter, two coordinate systems will be defined, body & inertial coordinate systems. In the inertial frame the position will be defined by X_G , Y_G , Z_G with angles of rotation in the body frame defined as ψ, θ, ϕ , which allows to define the generalized coordinates q:

$$q = [\begin{array}{cccc} X_G & Y_G & Z_G & \psi & \theta & \phi \end{array}]$$

The vector defined from the origin of the inertial frame to the certain of the body is as follows:

$$\overrightarrow{r_G} = \left[egin{array}{c} X_G \ Y_G \ Z_G \end{array}
ight]$$

In the case of the quadcopter where there are four motors, there are four forces produced by the motors defined in the positive \overrightarrow{k} direction of the body frame, in general the forces are defined as:

$$\overrightarrow{F_i} = \left[egin{array}{c} 0 \\ 0 \\ F_i \end{array}
ight] i = 1:4$$

Which will veild a resultant force in the body frame of:

$$\overrightarrow{F_R} = \sum_{i=1}^{4} \overrightarrow{F_i} - mg$$

These forces will also need to be defined in the inertial frame, this is acheived by the rotation matrix:

$$\overrightarrow{F_R} = R(\psi, \theta, \phi) \cdot \overrightarrow{F_R}$$

Where the rotation matrix is defined as:

$$R(\psi,\theta,\phi) = \begin{bmatrix} cos\psi cos\theta & cos\theta sin\psi & -sin\theta \\ cos\psi sin\phi sin\theta - cos\phi sin\psi & cos\phi cos\psi + sin\phi sin\psi sin\theta & cos\theta sin\phi \\ sin\phi sin\psi + cos\phi cos\psi sin\theta & cos\phi sin\psi sin\theta - cos\psi sin\phi & cos\phi cos\theta \end{bmatrix}$$

Which can be expressed in terms of the generalized coordinates q as:

$$R(q) = \begin{bmatrix} \cos(q_4)\cos(q_5) & \cos(q_5)\sin(q_4) & \sin(q_5) \\ \cos(q_4)\sin(q_6)\sin(q_5)\cos(q_6)\sin(q_4) & \cos(q_6)\cos(q_4) + \sin(q_6)\sin(q_4)\sin(q_5) & \cos(q_5)\sin(q_6) \\ \sin(q_6)\sin(q_4) + \cos(q_6)\cos(q_4)\sin(q_5) & \cos(q_6)\sin(q_4)\sin(q_5) - \cos(q_4)\sin(q_6) & \cos(q_6)\cos(q_5) \end{bmatrix}$$

which yields the force resultant in the inertial frame as:

$$\overrightarrow{F_R}(q) = \begin{bmatrix} -\sin(q_5) \cdot (F_1 + F_2 + F_3 + F_4 - mg) \\ \cos(q_5) \sin(q_6) \cdot (F_1 + F_2 + F_3 + F_4 - mg) \\ \cos(q_6) \cos(q_5) \cdot (F_1 + F_2 + F_3 + F_4 - mg) \end{bmatrix}$$

The position of the forces in the body frame are defined by the position vectors $\overrightarrow{r_i}$ (i=1:4) as follows:

$$\overrightarrow{r_1} = \frac{a}{2}\overrightarrow{i} + \frac{b}{2}\overrightarrow{j} + 0\overrightarrow{k}$$

$$\overrightarrow{r_2} = -\frac{a}{2}\overrightarrow{i} + \frac{b}{2}\overrightarrow{j} + 0\overrightarrow{k}$$

$$\overrightarrow{r_3} = \frac{a}{2}\overrightarrow{i} - \frac{b}{2}\overrightarrow{j} + 0\overrightarrow{k}$$

$$\overrightarrow{r_4} = -\frac{a}{2}\overrightarrow{i} - \frac{b}{2}\overrightarrow{j} + 0\overrightarrow{k}$$

Using the forces and their position vectors the moment about origin G in the body frame is defined as:

$$\overrightarrow{M_G} = \sum_{i=1}^4 (\overrightarrow{r_i} \times \overrightarrow{F_i})$$

this will also need to be rotated into the inertial frame yielding:

$$\overrightarrow{M_G} = \begin{bmatrix} cosq_4cosq_5M_1 + cosq_5sinq_4M_2 \\ -(cosq_6sinq_4 - cosq_4sinq_6sinq_5)M_1 + (cosq_6cosq_4 + sinq_6sinq_4sinq_5)M_2 \\ (sinq_6sinq_4 + cosq_6cosq_4sinq_5)M_1 - (cosq_4sinq_6 - cosq_6sinq_4sinq_5)M_2 \end{bmatrix}$$

$$M_1 = \frac{b}{2}F_1 + \frac{b}{2}F_2 - \frac{b}{2}F_3 - \frac{b}{2}F_4$$

$$M_2 = \frac{a}{2}F_1 - \frac{a}{2}F_2 + \frac{a}{2}F_3 - \frac{a}{2}F_4$$

For a full depiction of the dynamics of the system in the global frame first we start with looking at the local angular velocities as expressed in the body frame:

$$\omega_{body} = \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} -sin\theta & 0 & 1 \\ cos\theta cos\phi & cos\phi & 0 \\ cos\phi cos\theta & -sin\phi & 0 \end{bmatrix} \begin{bmatrix} \dot{\psi} \\ \dot{\theta} \\ \dot{\phi} \end{bmatrix}$$

Expressing these in the generalized coordinates of q yields:

$$\omega(q) = R(q) \cdot \omega_{body}$$

With the local angular velocities and the moments in the body frame rotated into the inertial, the generalized forces Q_i can be defined by:

$$Q_i = \overrightarrow{F}_R \frac{\partial \overrightarrow{r_G}}{\partial q_i} + \overrightarrow{M}_G \frac{\partial \overrightarrow{\omega}}{\partial \dot{q_j}}, i = 1:6, j = 4:6$$

The Kinetic Energy and the Equations of Motion

The kinetic energy of the quadcopter is defined as:

$$T(q) = \frac{1}{2}\dot{q}^T M(q)\dot{q}$$

where M(q) is defined as:

$$M(q) = J_v(q)^T m_{rr} J_v(q) + J_w(q)^T m_{\theta\theta} J_w(q)$$

with:

$$J_{v}(q) = \begin{bmatrix} \frac{\partial q_{1}}{\partial q_{1}} & \frac{\partial q_{1}}{\partial q_{2}} & \frac{\partial q_{1}}{\partial q_{3}} & 0 & 0 & 0 \\ \frac{\partial q_{2}}{\partial q_{1}} & \frac{\partial q_{2}}{\partial q_{2}} & \frac{\partial q_{2}}{\partial q_{3}} & 0 & 0 & 0 \\ \frac{\partial q_{3}}{\partial q_{1}} & \frac{\partial q_{3}}{\partial q_{1}} & \frac{\partial q_{3}}{\partial q_{1}} & 0 & 0 & 0 \end{bmatrix}$$

$$J_{w}(q) = \begin{bmatrix} 0 & 0 & 0 & -\sin q_{5} & 0 & 1 \\ 0 & 0 & 0 & \cos q_{5}\sin q_{6} & \cos q_{6} & 0 \\ 0 & 0 & 0 & \cos q_{5}\cos q_{6} & -\sin q_{6} & 0 \end{bmatrix}$$

$$m_{rr} = \begin{bmatrix} m & 0 & 0 \\ 0 & m & 0 \\ 0 & 0 & m \end{bmatrix}$$

$$m_{\theta\theta} = \left[\begin{array}{ccc} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{array} \right]$$

which expands to:

$$T(q) = \frac{1}{2}(m\dot{q_1}^2 + m\dot{q_2}^2 + m\dot{q_3}^2 + \dot{q_4}^2((I_{yy} + I_{zz})\cos(q_5)^2\cos(q_6)^2 + I_{xx}\sin(q_5)^2) + \dots$$

$$\ldots + \dot{q_5}^2 (I_{yy} cos(q_6)^2 + I_{zz} sin(q_6)^2) + 2\dot{q_5} \dot{q_4} \sigma + \dot{q_6}^2 I_{xx} - 2\dot{q_6} \dot{q_4} I_{xx} sin(q_5))$$

where:

$$\sigma = \frac{1}{2}(I_{yy} - I_{zz})cos(q_5)sin(2q_6)$$

The potential energy of the drone is defined as:

$$\overrightarrow{V}(q) = mgq_3$$

which allows for the lagrangian to be:

$$\mathcal{L}(q) = T(q) - V(q)$$

yielding,

$$\mathcal{L}(q) = \frac{1}{2}m\dot{q}_1^2 + \frac{1}{2}m\dot{q}_2^2 + \frac{1}{2}m\dot{q}_3^2 +$$

$$\dots(\frac{1}{2}I_{xx}sin^2(q_5) + \frac{1}{2}I_{yy}cos^2(q_6) - (\frac{1}{2}I_{yy} - \frac{1}{2}I_{zz})cos^2(q_5)cos^2(q_6))\dot{q}_4^2 +$$

$$\dots(\frac{1}{2}I_{zz} + \frac{1}{2}(I_{yy} - I_{zz})cos^2(q_6))\dot{q}_5^2 + \frac{1}{2}I_{xx}\dot{q}_6^2 - I_{xx}sin(q_5)\dot{q}_4\dot{q}_6$$

$$\dots + \frac{1}{2}(I_{yy} + I_{zz})cos(q_5)sin(2q_6)\dot{q}_4\dot{q}_5 + gmq_3$$

with $\mathcal{L}(q)$ defined this allows us to find the corresponding Euler-Lagrange equations of motions from the following equation:

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}(q)}{\partial \dot{q}_j} \right) - \frac{\partial \mathcal{L}(q)}{\partial q_j} = Q_j(q)$$
$$Q_1(q) = m\ddot{q}_1$$

$$Q_3(q) = m\ddot{q}_3 - mg$$

 $Q_2(q) = m\ddot{q}_2$

$$Q_4(q) = -I_{xx}sin(q_5)\ddot{q}_6 + (-I_{xx} + (I_{yy} - I_{zz})cos^2(q_5))sin(q_6)cos(q_6)\dot{q}_4\dot{q}_6 + \dots 2(I_{xx} + (I_{yy} - I_{zz})cos^2(q_6))sin(q_5)cos(q_5)\dot{q}_4\dot{q}_5 + (-0.5I_{yy} + 0.5I_{zz})cos^2(q_5)cos^2(q_6)\ddot{q}_4 + \dots (I_{yy} + I_{zz})cos(q_5)sin(2q_6)\ddot{q}_5$$

$$Q_5(q) = (I_{xx} + (I_{yy} - I_{zz})cos^2(q_6))sin(q_5)cos(q_5)\dot{q}_4^2 + (I_{xx} + (I_{yy} + I_{zz})cos(2q_6))cos(q_5)\dot{q}_4\dot{q}_6 + \dots (I_{yy} + I_{zz})cos(q_5)sin(2q_6)\ddot{q}_4 - (2I_{yy} - 2I_{zz})sin(q_6)cos(q_6)\dot{q}_5\dot{q}_6 + (I_{zz} + (I_{yy} - I_{zz})cos^2(q_6))\ddot{q}_5$$

$$Q_{6}(q) = -I_{xx}sin(q_{5})\ddot{q}_{4} + I_{xx}\ddot{q}_{6} - (I_{xx} + (I_{yy} + I_{zz})cos(2q_{6}))cos(q_{5})\dot{q}_{4}\dot{q}_{5} + \dots (I_{yy} - I_{zz})sin(q_{6})cos(q_{6})\dot{q}_{5}^{2} - (I_{yy} + (I_{yy} - I_{zz})cos^{2}(q_{5}))sin(q_{6})cos(q_{6})\dot{q}_{4}^{2}$$

State Space Representation

To define a controller, the dynamics of the system must be first put into state space form:

 $x = [q, \dot{q}]^T$

and,

$$\dot{x} = \left[\frac{dq}{dt}, \frac{d\dot{q}}{dt}\right]^T$$

where,

$$\frac{d\dot{q_1}}{dt} = \frac{Q_1}{m}$$

$$\frac{d\dot{q_2}}{dt} = \frac{Q_2}{m}$$

$$\frac{d\dot{q}_3}{dt} = g + \frac{Q_3}{m}$$

$$\frac{d\dot{q}_4}{dt} = \frac{A_1}{(I_{zz} + (I_{yy} - I_{zz})cos^2(q_6))(2I_{xx}sin^2(q_5) + (I_{yy} - I_{zz})cos^2(q_5)cos^2(q_6))}$$

where:

$$A_{1} = -(I_{yy} + I_{zz})((I_{xx} + (I_{yy} - I_{zz})\cos^{2}(q_{6}))\sin(q_{5})\cos(q_{6})\dot{q}_{4}^{2} + \\ \dots (I_{xx} + (I_{yy} + I_{zz})\cos(2q_{6}))\cos(q_{5})\dot{q}_{4}\dot{q}_{6} + \\ \dots (-I_{yy} + I_{zz})\sin(2q_{6})\dot{q}_{5}\dot{q}_{6} - Q_{5})\sin(2q_{6})\cos(q_{5}) - \\ \dots (2I_{zz} + 2(I_{yy} - I_{zz})\cos^{2}(q_{6}))((-I_{xx} + (I_{yy} - I_{zz})\cos^{2}(q_{6}))\sin(2q_{5})\dot{q}_{4}\dot{q}_{5} + \\ (I_{xx} + (I_{yy} - I_{zz})\cos^{2}(q_{5}))\sin(q_{6})\cos(q_{6})\dot{q}_{4}\dot{q}_{6} + Q_{4})\sin(q_{5}) - \\ \dots (2I_{zz} + 2(I_{yy} - I_{zz})\cos^{2}(q_{6}))((I_{xx} + (I_{yy} + I_{zz})\cos(2q_{6}))\cos(q_{5})\dot{q}_{4}\dot{q}_{5} + (-0.5I_{yy} + 0.5I_{zz})\sin(2q_{6})\dot{q}_{5}^{2} + \\ (-0.125I_{yy} + 0.125I_{zz})\sin(2q_{5} - 2q_{6}) + (0.125I_{yy} - 0.125I_{zz})\sin(2q_{5} + 2q_{6}) + (1.5I_{yy} - 0.5I_{zz})\sin(q_{5})\cos(q_{5})\dot{q}_{4}^{2}$$

$$\frac{d\dot{q}_5}{dt} = \frac{A_2}{2I_{xx}sin^2(q_5)(I_{yy}cos^2(q_6) + I_{zz}sin^2(q_6)) + cos^2(q_5)cos^2(q_6)(I_{yy}^2(sin^2(q_6) + 1) + I_{yy}I_{zz}(6sin^2(q_6) - 1)) + I_{zz}^2sin^2(q_6)}$$

where.

$$A_{2} = (0.5I_{yy} + 0.5I_{zz})((-0.5I_{yy} + 0.5I_{zz})sin(2q_{6})\dot{q}_{5}^{2} + (I_{xx}cos(q_{5}) + (0.5I_{yy} + 0.5I_{zz})cos(q_{5})cos(2q_{6}))\dot{q}_{4}\dot{q}_{5} + \\ \dots ((-0.125I_{yy} + 0.125I_{zz})sin(2q_{5} - 2q_{6}) + (0.125I_{yy} - 0.125I_{zz})sin(2q_{5} + 2q_{6}) + \\ \dots (0.75I_{yy} - 0.25I_{zz})sin(2q_{6}))\dot{q}_{4}^{2} + Q_{6})sin(2q_{5})sin(2q_{6}) + (I_{yy} + I_{zz})((-I_{xx} + (-I_{yy} + I_{zz})cos^{2}(q_{6}))sin(2q_{5})\dot{q}_{4}\dot{q}_{5} + \\ \dots (I_{xx} + (-0.5I_{yy} + 0.5I_{zz})cos^{2}(q_{5}))sin(2q_{6})\dot{q}_{4}\dot{q}_{6} + Q_{4})sin(2q_{6})cos(q_{5}) - \\ \dots (2I_{xx}sin^{2}(q_{5}) + (I_{yy} - I_{zz})cos^{2}(q_{5})cos^{2}(q_{6}))((0.5I_{xx} + (0.5I_{yy} - 0.5I_{zz})cos^{2}(q_{6}))sin(2q_{5})\dot{q}_{4}^{2} + \\ \dots (-I_{yy} + I_{zz})sin(2q_{6})\dot{q}_{5}\dot{q}_{6} + (I_{xx}cos(q_{5}) + (I_{yy} + I_{zz})cos(q_{5})cos(2q_{6}))\dot{q}_{4}\dot{q}_{6} - Q_{6})$$

$$\frac{d\dot{q}_{6}}{dt} = \frac{A_{3}}{I_{xx}(2I_{xx}((I_{yy} - I_{zz})cos^{2}(q_{6}) + I_{zz})sin^{2}(q_{5}) + (I_{yy} - I_{zz})((I_{yy} - I_{zz})cos^{2}(q_{6}))}{I_{xx}(2I_{xx}((I_{yy} - I_{zz})cos^{2}(q_{6}) + I_{zz})sin^{2}(q_{5}) + (I_{yy} - I_{zz})((I_{yy} - I_{zz})cos^{2}(q_{6}))}$$

 $I_{zz}\cos^2(q_5)\cos^2(q_6) + 2(I_{yy} + I_{zz})^2\sin^2(q_6)\cos^2(q_5)\cos^2(q_6)$

where,

$$A_{3} = -0.25I_{xx}(I_{yy} + I_{zz})((-I_{yy} + I_{zz})sin(2q_{6})\dot{q}_{5}\dot{q}_{6} + (0.5I_{xx}sin(2q_{5}) + (I_{yy} - I_{zz})sin(q_{5})cos(q_{5})cos^{2}(q_{6}))\dot{q}_{4}^{2} + \\ \dots (I_{xx}cos(q_{5}) + (I_{yy} + I_{zz})cos(q_{5})cos(2q_{6}))\dot{q}_{4}\dot{q}_{6} - Q_{5})sin(2q_{5})sin(2q_{6}) - \\ \dots 2I_{xx}(I_{zz} + (I_{yy} - I_{zz})cos^{2}(q_{6}))((-0.5I_{xx} + (-I_{yy} + I_{zz})cos^{2}(q_{6}))sin(2q_{5})\dot{q}_{4}\dot{q}_{5} + \\ \dots (I_{xx} + (-0.5I_{yy} + 0.5I_{zz})cos^{2}(q_{5}))sin(2q_{6})\dot{q}_{4}\dot{q}_{6} + Q_{4})sin(q_{5}) +$$

$$\dots ((I_{yy} - I_{zz})(I_{zz} + (I_{yy} - I_{zz})cos^{2}(q_{6})) + 2(I_{yy} + I_{zz})^{2}sin(q_{6}))((I_{xx} + (I_{yy} + I_{zz})cos(2q_{6}))cos(q_{5})\dot{q}_{4}\dot{q}_{5} + (-0.5I_{yy} + 0.5I_{zz})sin(2q_{6})\dot{q}_{5}^{2} + ((-0.25I_{yy} + 0.25I_{zz})sin(2q_{5} - 2q_{6}) + (0.25I_{yy} + 0.25I_{zz})sin(2q_{5} + 2q_{6}) + (0.75I_{yy} - 0.25I_{zz})sin(2q_{6}))\dot{q}_{4}^{2} + Q_{6})cos^{2}(q_{5})cos^{2}(q_{6})$$

To control the dynamics of the system the state space needs to be written in the following form:

$$\dot{x} = F(q, \dot{q}) + G(q, \dot{q})Q$$

where $G(q,\dot{q})$ is a function of the states, and the generalized forces Q_{1x12} are the system inputs.

where,

$$\begin{split} g_{1010} &= \frac{(I_{yy} - I_{zz})cosq_6^2 + I_{zz}}{(I_{zz} + (I_{yy} - I_{zz})cos^2(q_6))(2I_{xx}sin^2(q_5) + (I_{yy} - I_{zz})cos^2(q_5)cos^2(q_6))} \\ g_{1011} &= \frac{(I_{yy} + I_{zz})cosq_5sin2q_6}{(I_{zz} + (I_{yy} - I_{zz})cos^2(q_6))(2I_{xx}sin^2(q_5) + (I_{yy} - I_{zz})cos^2(q_5)cos^2(q_6))} \\ g_{1012} &= \frac{2sinq_5((I_{yy} - I_{zz})cosq_6^2 + I_{zz})}{(I_{zz} + (I_{yy} - I_{zz})cos^2(q_6))(2I_{xx}sin^2(q_5) + (I_{yy} - I_{zz})cos^2(q_5)cos^2(q_6))} \end{split}$$

$$g_{1110} = \frac{(I_{yy} + I_{zz})cos(q_5)sin(2q_6)}{2I_{xx}sin^2(q_5)(I_{yy}cos^2(q_6) + I_{zz}sin^2(q_6)) + cos^2(q_5)cos^2(q_6)(I_{yy}^2(sin^2(q_6) + 1) + I_{yy}I_{zz}(6sin^2(q_6) - 1)) + I_{zz}^2sin^2(q_6)}$$

$$g_{1111} = \frac{2I_{xx}sin^2(q_5) + (I_{yy} - I_{zz})cos^2(q_5)cos^2(q_6)}{2I_{xx}sin^2(q_5)(I_{yy}cos^2(q_6) + I_{zz}sin^2(q_6)) + cos^2(q_5)cos^2(q_6)(I_{yy}^2(sin^2(q_6) + 1) + I_{yy}I_{zz}(6sin^2(q_6) - 1)) + I_{zz}^2sin^2(q_6)}$$

$$g_{1112} = \frac{\frac{1}{2}(I_{yy} + I_{zz})sin(2q_5)sin(2q_6)}{2I_{xx}sin^2(q_5)(I_{yy}cos^2(q_6) + I_{zz}sin^2(q_6)) + cos^2(q_5)cos^2(q_6)(I_{yy}^2(sin^2(q_6) + 1) + I_{yy}I_{zz}(6sin^2(q_6) - 1)) + I_{zz}^2sin^2(q_6)}$$

$$g_{1210} = \frac{2sin(q_5)((I_{yy} - I_{zz})cos^2(q_6) + I_{zz})}{I_{xx}(2I_{xx}((I_{yy} - I_{zz})cos^2(q_6) + I_{zz})sin^2(q_5) + (I_{yy} - I_{zz})((I_{yy} - I_{zz})cos^2(q_6) + I_{zz})cos^2(q_6) + 2(I_{yy} + I_{zz})^2sin^2(q_6)cos^2(q_5)cos^2(q_6))}$$

$$g_{1211} = \frac{\frac{1}{2}(I_{yy} + I_{zz})sin(2q_5)sin(2q_6)}{I_{xx}(2I_{xx}((I_{yy} - I_{zz})cos^2(q_6) + I_{zz})sin^2(q_5) + (I_{yy} - I_{zz})((I_{yy} - I_{zz})cos^2(q_6) + I_{zz})cos^2(q_6) + (I_{yy} - I_{zz})cos^2(q_6) + (I_{yy}$$

$$g_{1212} = \frac{(I_{yy} - I_{zz})^2 cos^2(q_5) cos^4(q_6) + 2(I_{yy} + I_{zz})^2 sin^2(q_6) cos^2(q_5) cos^2(q_6) + I_{zz} cos^2(q_5) cos^2(q_6)(I_{yy} - I_{zz})}{I_{xx}(2I_{xx}((I_{yy} - I_{zz}) cos^2(q_6) + I_{zz}) sin^2(q_5) + (I_{yy} - I_{zz})((I_{yy} - I_{zz}) cos^2(q_6) + I_{zz}) cos^2(q_6) + 2(I_{yy} + I_{zz})^2 sin^2(q_6) cos^2(q_5) cos^2(q_6))}$$