**Using Software A\*\*\* and Algorithm Testing to Verify a One-dimensional Transport Model**

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**ABSTRACT**

In this paper we describe a framework for software verification of a transport model. The framework is crafted according to principles from both the software \*\*\* and numerical testing fields. Herein, we describe the components and implementation of the suite, emphasizing the incremental nature of the tests, quantitative criteria for testing, and the tension between the silent, automatic perspective of software testing and the verbose, graphical outputs required for public reporting of numerical verification results. Our experience might result in a useful starting point for researchers and practitioners wanting to verify codes in similar situations. WE CAN GO AS FAR AS 150 WORDS

**INTRODUCTION**

In this paper, we describe our approach and experiences developing a software verification framework for a one dimensional transport model of advection, diffusion and reactions or sources. We begin by describing the motivation and requirements for testing. Our acceptance criteria are driven by the requirements for the model, but are crafted according to principles from both the software and numerical testing fields. We then describe the components and implementation of the suite, emphasizing the incremental nature of the tests, quantitative criteria for testing and the tension between the silent, automatic perspective of software testing and the verbose, graphical outputs required for public reporting of numerical verification results.

**Description of requirements and motivation of the testing.**

The California Department of Water Resources maintains the Delta Simulation Model 2 (DSM2), a one-dimensional (1D) hydrodynamic and transport model for rapidly simulating flow and water quality in the Sacramento-San Joaquin Delta. Recently, the authors commenced work on a flexible and more rigorously verified transport component for this suite. Our target problems include river and estuary advection, 1D approximations of common mixing mechanisms and source terms associated with sediment, radiation and non-conservative water quality kinetics.

The formulation of our problem, scaling of our target modeling applications and choice of algorithm influence the components of our test suite. The model is based on the 1D transport equations in conservative form:



where *A* is the wetted area, *C* is the scalar concentration, *u* is the flow velocity, *K* is the longitudinal dispersion coefficient, and *R* is the source term (deposition, erosion, lateral inflow and other forms of sources and sinks). Equation (1) describes the mass conservation of a given pollutant in dissolved phase, or suspended sediment away from the streambed.

The problem domain includes estuaries and river channels and even some open water areas grossly approximated as channels (Fig. 1). The main transport process is advection, and the mixing mechanisms we anticipate are turbulent diffusion, gravitational circulation, and shear dispersion. We anticipate the shear dispersion to obviously dominate over the turbulent diffusion, but we also expect the gravitational circulation to exert an important role in mixing. We additionally contemplate significant, non-linear source terms, though none of the above processes are so quickly varying as to constitute truly stiff reactions.

Our algorithms include an explicit scheme for advection based on the finite-volumes method (FVM) and the Lax, two-step method with van Leer flux limiter; it also includes an implicit, time-centered Crank-Nicolson scheme for dispersion. The advection and reaction solver are coupled as a predictor corrector pair, and diffusion is implemented using operator splitting. Two features of the algorithm are particularly important. First, the scheme requires a flow field (flow discharges and flow areas) that preserves mass continuity. In some cases tests from the literature were written in non-conservative or primitive form in terms of a velocity and had to be reworked in conservative form. Second, we employ operator splitting and wanted to exercise the equations with and without known vulnerabilities (such as time-varying boundaries and nonlinear source terms) of this class of algorithm.

The target accuracy is strict second order for individual operators and near second-order for the algorithm as a whole. Second order allows coarser discretization for a modest increase in work. A second-order algorithm gives us a buffer of accuracy as details like networks of channels and coarse boundary data are added. At the time of writing this paper, our splitting is first order Godunov splitting. Numerous authors (e.g. Leveque 1986) have observed that near second-order accuracy can be achieved with first order splitting, and the design of the tests probes this point.

**TESTING PRINCIPLES**

Flow and transport codes inherently comprise both numerical algorithms and pieces of software. Well-developed testing literature exists for both. Oberkampf and Trucano (2002) describe some elements of “software quality engineering” in the context of numerical verification, and notes some cultural reasons why it is seldom implemented.

We incorporate both numerical and software principles testing in our suite. We regard numerical verification as our key responsibility and the numerical verification toolset as our greatest asset. Nonetheless, we also comment on how these tools feature as tests; we find that the reporting requirements for verification are in fact sometimes in tension with the principles of good testing.

**Software Assurance Testing Principles.**

Numerical verification is the standard of success of the underlying code, however there are certain software testing principles that we feel help create a framework for the numerical testing. The principles that we want to emphasize are:

1. Testing should be automatic and continuous.
2. The approach should foster exact specification of every unit of code.

One goal of tests is that they be a continuous assessment of the code. The tests themselves stay static, and establish a gauntlet of through which future changes must be passed. A consequence of automation and regression is that test suites must be based on binary *assertions,* true and false statements that can be tested without human intervention and that reveal whether the aspect of the code under consideration is correct. Convergence criteria are a rigorous basis for assertions, either by requiring strict convergence criteria (“the algorithm is O(2) in time and space”) or a *regression* criterion (“convergence will not get any worse on this test”).

The software testing literature further distinguishes between “unit tests” of atomic routines and “system tests” of larger subtasks. For example, the evaluation of a gradient might be a unit of code and the integration of diffusion might be a small system. The software testing point of view is that code must be exercised over a range of inputs that covers every line. For instance, to test a gradient routine with a slope limiter, a developer would want to cover:

1. well-behaved cases in the middle of the mesh.
2. behavior near the edges of the mesh, where one-sided differences may be used instead of central differences.
3. cases that test the limiters with steep or zero gradients in both directions.

Convergence tests will always exercise the central cases, which in any event can seldom be wrong without being obvious. A system test might, on the other hand, miss a bug in the limiter for the case of steep decreasing slopes for several reasons. First, convergence is often assessed with limiters turned off, as they are locally order reducing. Second, it is hard to fiddle with the problem in just the right way to make sure the left, right, and center cases of the gradient limiter are all triggered. This is particularly true when trying to exercise all the other units of code the same way – parameter changes made to fully exercise one unit of code may lessen the coverage of another unit.

Overall, we agree with the conclusions of \*\*\*\* that system tests expose bugs well, particularly when an attempt is made to test symmetrically and over special cases. We feel that the hierarchical approach we describe in the next section further helps to isolate problems. Nevertheless, we began our coding with near-100% coverage by unit tests and discoveries made in the context of system tests are analyzed and pushed back into unit tests whenever possible.

**Numerical Verification.**

One of the well-recognized and the standard verification methods of computational-fluid-dynamics (CFD) codes is based on the notion of mesh convergence. This method provides a quantitative check on how the code responds to changes in spatial and time steps, and \*\*\*\*

The ratio of consecutive error norms is also a proven means to discover coding error/algorithm problems. \*\*\*\*OTHER SANDIA\*\*\* found that convergence error tests on manufactured solutions were able to expose 21 different synthesized coding mistakes.

The \*\*\*\*\*\*\*\*\*\*\*\*\*\*What is a convergence test?\*\*\*\* 1 paragraph plus picture showing what grid refinement is and how a numerical result looks as it is being refined (err on the coarse side) \*\*\*\*\*\*

The points needed to be considered in any mesh-convergence study include:

* Norms: L∞[[1]](#footnote-1) should be included as an ultimate diagnostic tool for local errors and worst case scenario. L2 is a more forgiving norm compared to the first error norm L1. We recommend L1 as an appropriate global metric of error.[[2]](#footnote-2)
* The convergence ratio in a very coarse grid oscillates around its main value; as the grid size is refined, convergence becomes monotonic until the mesh size reaches a point where the machine precision overtakes the truncation error of the numerical scheme. At this point error norms do not change and convergence rate is zero. Thus, convergence ratios should be checked for intermediate grid sizes (preferably at the scale of the real phenomenon).
* Although the convergence is a reliable warning of a defect, it should not be forgotten that the main goal in practice is a more accurate solver. Therefore, the superiority of methods should be assessed based on both convergence and accuracy. Accuracy metrics similarly are error norms as is discussed above, however for evaluating the accuracy error norms should be normalized by an appropriate scale of the solution.
* All of the convergence tests such as MMS, Richardson Extrapolation, could be run by a same driver. The post processing of the convergence test also could carry out with a same code for all the tests.
* Visualization of time evolution of error and results in the solution domain is a recommended strategy for debugging in cases where the source of inaccuracy is obscure.

The question here is: if one wants to find accuracy and convergence ratio of a scheme in which the analytical solution is unknown (absence of analytical solution is the main motivator towards all numerical methods), what should be done? It is ideal to test a model’s correctness by comparing its numerical results with analytical solutions; however the difficulty is that there is not a general solution for the non-linear IBVP in water quality. There are some ways to deal with this problem from the simplest to the most sophisticated:

a) Comparing with a higher order code/run on a dense mesh. Downside of the method is: the benchmark code requires verification prior to the code that is subjected to the verification process.

b) Richardson Extrapolation: it is the common method for dealing with commercial packages and multidimensional complex systems (Roache and Knupp, 1993). However the drawback is that the method only checks if the solver converges and it is not able to measure where it is converging to.

Difficulties arise in Richardson EXTRAPOLATION???(BC/IC incompatibility?)

c) Method of Manufactured Solutions (MMS) (Wang and Jia, 2009), and Prescribed Solution Forcing Method (PSF) (Dee and Da Silva, 1986). The basic concept of the MMS and PSF is to compare the correctness of numerical solvers using an arbitrary manufactured function. MMS and PSF are conceptually following the same idea, although the former is more general than the latter. PSF have been used for the verification cases in which the user can not access the source code to define boundary conditions such as some groundwater codes.

**TEST SUITE DESIGN**

**General approach.** Our test suite is based on four hierarchical steps, as follows:

1) Testing of the basic components of each physical process (units) for correctness. This involves testing each sub-routine, such as the routine which coarsens the values on the mesh. One of the obvious tests is to check that the coarsen process is correctly undertaken. CCCC

2) System testing of physical processes at level 1: advection, dispersion and reaction.

3) System testing of physical processes at level 2: advection-dispersion, advection-reaction, and dispersion-reaction,

4) System testing of physical processes at level 3: advection-dispersion-reaction.

It is worth mentioning that in each category, we tested two conditions for the boundaries: a) Boundaries close to the main transport events, b) boundaries far from those events.

**Detail of tests.** We detail below the tests developed, and comment on the results.

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**Results.** FABIAN AND KAVEH

**LESSONS LEARNED AND CHALLENGES**

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**CONCLUSIONS AND FINAL REMARKS**

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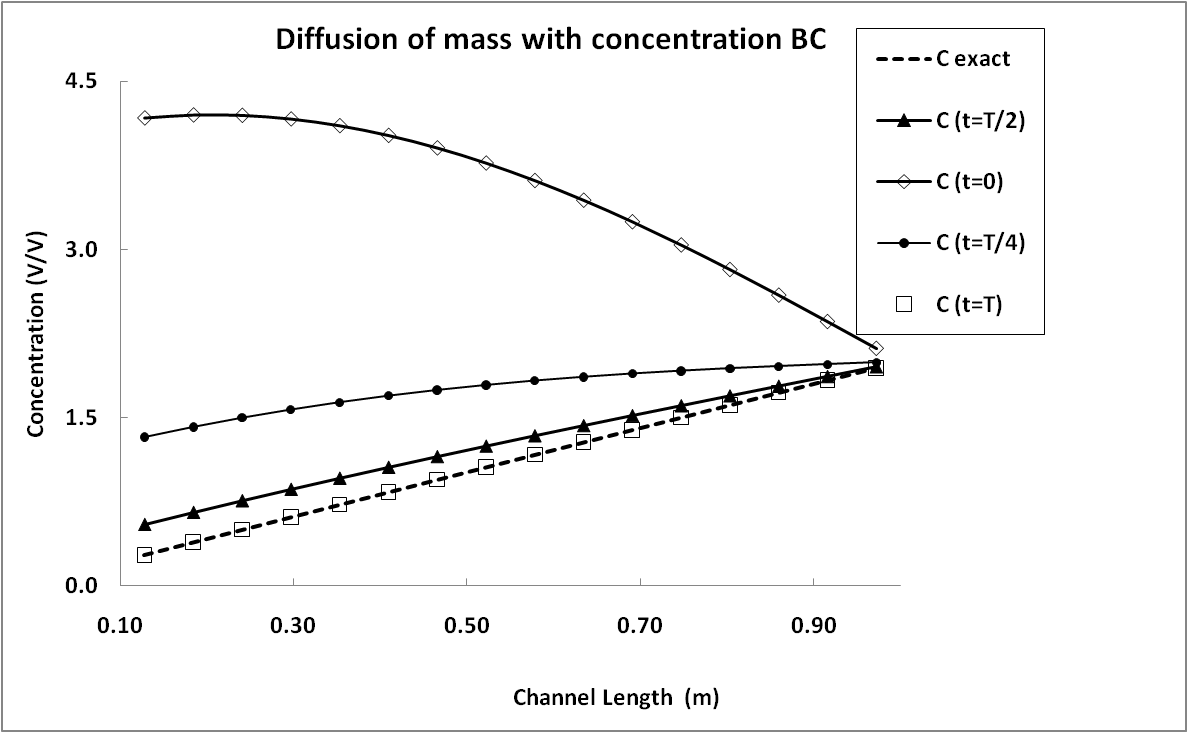
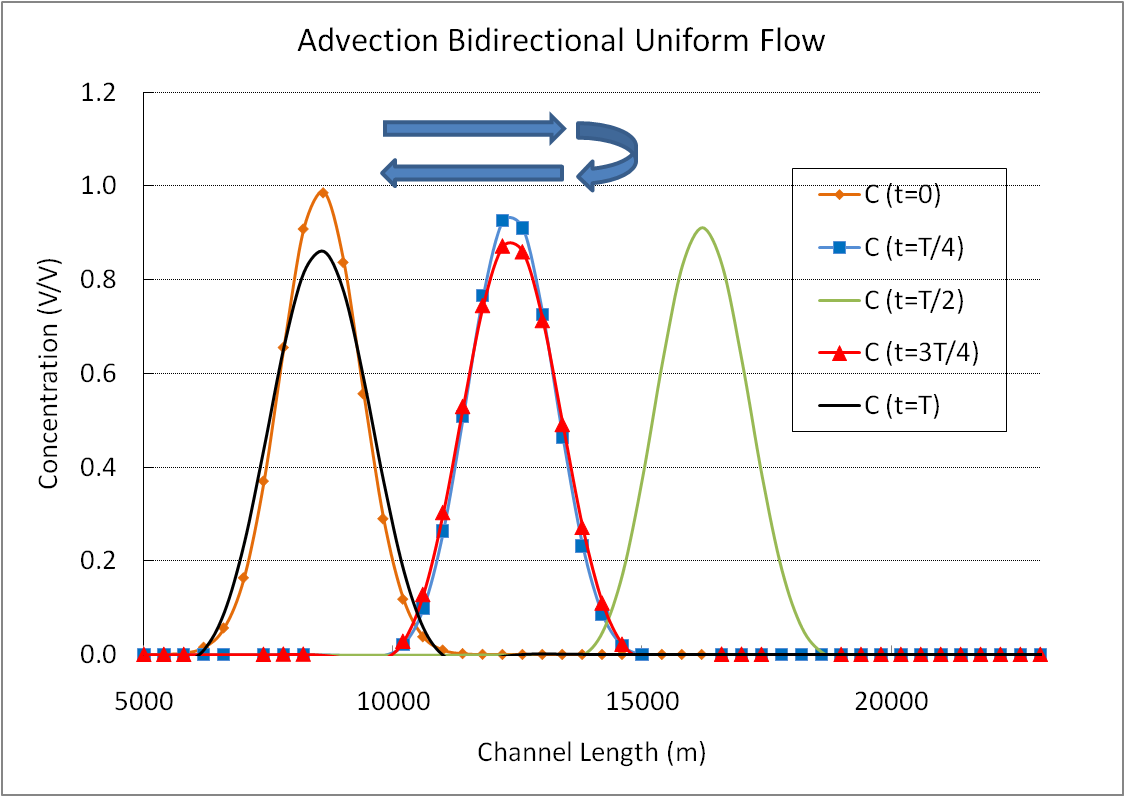
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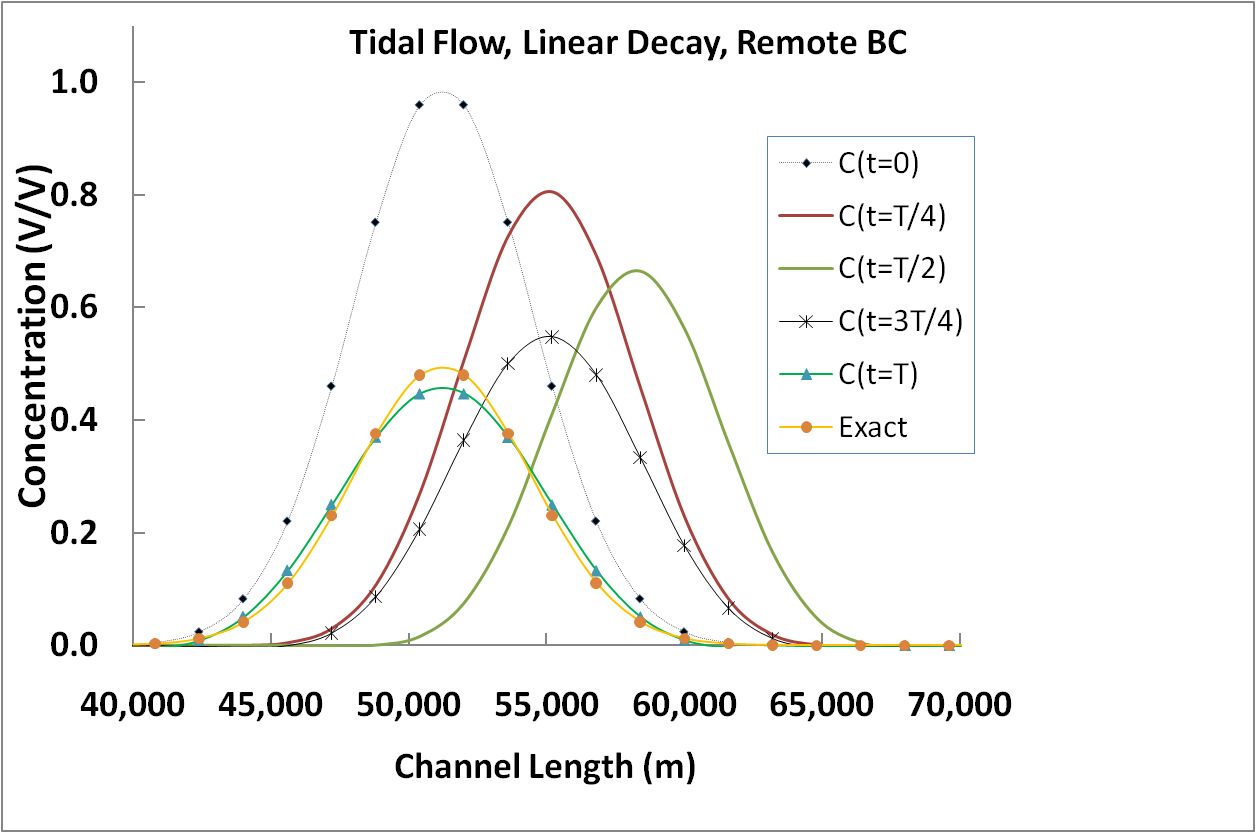
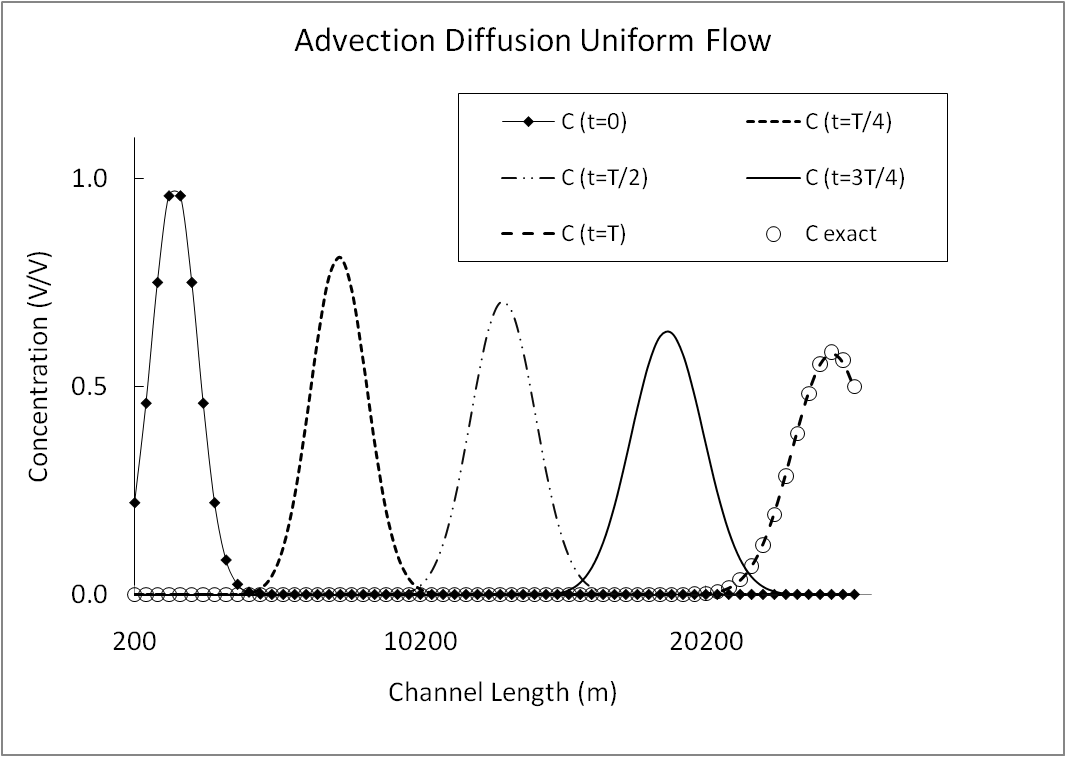
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**SCALING OF THE PROBLEM FOR AN ESTUARY**

The ADR solver is only working in the feasible ranges of dimensionless numbers (Peclet number and Damkohler number,) so in case the reaction rate in equation (1) should not exceed a certain limit, and generally speaking the test suit has to be designed within the natural scales of the physical problem. The assumed scales and ranges are as follows: Area~ 1000 [m2], C (0 – 0.05) [vol/vol=1], u (±0.2-2) [m/s], *u*\* isshear velocity is scaled based on where g is gravitational acceleration, *Rh* is hydraulic radius and *S* is bed slope. The longitudinal dispersion coefficient scales with:  Where *B* is width, *H* is depth and is average velocity (Abbott 1993), *K*s ~[2-150 m2/s]. Finally based on the formula suggested by Garcia and Parker (1991) reaction variation range for non-cohesive sediment in an estuary will be ( +1.0×10-3 to -3.7×10-4 [1/s]). That is to mention the length scale in the scaling process assumed the same length of spatial discretization where needed.





1. ,,, where *v*= U num - U exact [↑](#footnote-ref-1)
2. It is proven that kL∞ ≤ L2 ≤ L1 ≤ L∞ where k is a constant and 0<k<1, here norms are assumed to be scaled. [↑](#footnote-ref-2)