

第九章

正弦稳态电路的分析

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9.1 阻抗和导纳

① 欧姆定律的向量形式 阻抗模 阻抗角
$$\dot{U} = Z \dot{I} \quad Z = \frac{\dot{U}}{\dot{I}} = |Z| \angle \varphi_Z \quad (Z) \quad |Z| = \frac{U}{I} \quad \varphi_Z = \varphi_u - \varphi_i$$

电阻 $Z=R$ 电容 $Z = -j\frac{1}{\omega C} = jX_C$ 电感 $Z = j\omega L = jX_L$
容抗 感抗

② RLC串联电路 $Z = R + j\omega L - j\frac{1}{\omega C} = R + jX = |Z| \angle \varphi_Z$

$|Z| = \sqrt{R^2 + X^2}$ (X为电抗, R为电阻) $\varphi_Z = \arctan \frac{X}{R}$ 阻抗三角形

相量图: 串联(KVL)选电流为参考, $\varphi_i = 0$

① $\dot{U}_R = R\dot{I}$ $\dot{U}_L = j\omega L\dot{I}$ $\dot{U}_C = -j\frac{1}{\omega C}\dot{I}$ $\dot{U} = \sqrt{U_R^2 + (U_L - U_C)^2}$

② $\dot{U} = \sqrt{U_R^2 + (U_L - U_C)^2}$ $\dot{U}_R = R\dot{I}$ $\dot{U}_L = j\omega L\dot{I}$ $\dot{U}_C = -j\frac{1}{\omega C}\dot{I}$

③ 导纳 $Y = \frac{\dot{I}}{\dot{U}} = |Y| \angle \varphi_Y (S) \quad |Y| = \frac{I}{U} \quad \varphi_Y = \varphi_i - \varphi_u$
电导 电纳 容纳 感纳

④ RLC并联电路 $Y = G + j\omega C - j\frac{1}{\omega L} = G + jB = |Y| \angle \varphi_Y$
 $|Y| = \sqrt{G^2 + B^2}$ $\varphi_Y = \arctan \frac{B}{G}$ $|Y|$ 为电纳模 G 为电导 B 为电纳 Δ 为电导角

相量图 ① $\dot{I}_L = j\omega C\dot{U}$ $\dot{I}_C = -j\frac{1}{\omega L}\dot{U}$ $\dot{I} = \sqrt{I_G^2 + (I_L - I_C)^2}$ 分电流可大于总电流

② $\dot{I}_G = G\dot{U}$ $\dot{I}_L = j\omega C\dot{U}$ $\dot{I}_C = -j\frac{1}{\omega L}\dot{U}$ $\dot{I} = \sqrt{I_G^2 + (I_L - I_C)^2}$

③ $\dot{I}_L = j\omega C\dot{U}$ $\dot{I}_C = -j\frac{1}{\omega L}\dot{U}$ $\dot{I} = \sqrt{I_G^2 + (I_L - I_C)^2}$

⑤ 阻抗和导纳的等效互换

$Z = R + jX \quad Y = G + jB$ $Z = \frac{1}{Y} \quad Y = \frac{1}{Z}$ $|Z| \angle \varphi_Z = \frac{1}{|Y| \angle \varphi_Y}$ $|Z| = \frac{1}{|Y|} \quad \varphi_Z = -\varphi_Y$

$G = \frac{R}{R^2 + X^2} \quad B = \frac{-X}{R^2 + X^2} \quad |Y| = \frac{1}{|Z|} \quad \varphi_Y = -\varphi_Z$

1) 一端口的阻抗/导纳是由其内部参数、结构物、正弦电源频率决定的, 在一般情况下, 其每一部分均有频率依赖

2) 一端口不含受控源, 有 $|\varphi_Z| \leq 90^\circ$ 或 $|\varphi_Y| \leq 90^\circ$

有受控源时 $|\varphi_Z| > 90^\circ$ 或 $|\varphi_Y| > 90^\circ$ (R, G为正值)

3) Z和Y在一端口有同等效果, 并有 $ZY = 1$

$|Z||Y| = 1 \quad \varphi_Z + \varphi_Y = 0$

⑥ 阻抗(导纳)的串联和并联

① 阻抗串联 $Z = \sum_{k=1}^n Z_k \quad \dot{I}_i = \frac{Z_i}{Z} \dot{I}$ (分压公式)

② 导纳并联 $Y = \sum_{k=1}^n Y_k \quad \dot{I}_i = \frac{Y_i}{Y} \dot{I}$ (分流公式)

③ 阻抗并联 $\frac{1}{Z} = \sum_{k=1}^n \frac{1}{Z_k}$

④ 导纳串联 $\frac{1}{Y} = \sum_{k=1}^n \frac{1}{Y_k}$

感性容性: $Z = R + jX \quad X < 0$ 容性 $X > 0$ 感性

若 $R=0$, 则纯电感/电容

9.2 电路的相量图 一电压电流在复平面

1. 判断电路框架 (KVL, KCL)

2. 确定参考相量 (I/U 为 0° 相量)

3. 不分顺序, 依次绘制方程相量 (合理选择顺序)

9.3 正弦稳态电路的分析

9.4 正弦稳态电路的功率

1. 瞬时功率 $u(t) = \sqrt{2} U \cos \omega t \quad i(t) = \sqrt{2} I \cos (\omega t - \varphi) \quad p(t) = UI [\cos \varphi + \cos (2\omega t - \varphi)]$

第一种分解法 $p(t) = UI [\cos \varphi + \cos (2\omega t - \varphi)]$ $\therefore p$ 时正时负, $p > 0$ 吸收, $p < 0$ 发出

第二种分解法 $p(t) = UI \cos \varphi (1 + \cos 2\omega t) + UI \sin \varphi \sin 2\omega t$ 有源部分能在 $0 \sim 2\pi \cos \varphi$ 间 $-UI \sim +UI$ 电源、一端口间来回交换

2. 平均功率 $P = \frac{1}{T} \int_0^T p dt = UI \cos \varphi (W)$

$\varphi = \varphi_u - \varphi_i$: 功率因数角。对无源网络, 为其等效阻抗的阻抗角

$\cos \varphi$: 功率因数

$\cos \varphi = 1$: 纯电阻 $\cos \varphi = 0, \varphi = \pm 90^\circ$: 纯电抗 (电感/电容)

$X > 0, \varphi > 0$ 感性 $X < 0, \varphi < 0$ 容性

平均功率是电阻消耗的功率, 亦称有功功率, 表示电路实际消耗的功率

3. 无功功率 Q

$Q \triangleq UI \sin \varphi$, 单位 var $Q > 0$: 网络吸收无功功率 $Q < 0$: 网络发出无功功率

Q大小反映网络与外电路交换功率的速率, 由 L 决定

4. 视在功率 S

$S \triangleq UI$ 单位 VA (伏安) 电气设备的容量

5. $\sqrt{P^2 + Q^2} = S \quad \tan \varphi = \frac{Q}{P}$ 功率三角形

功率因数 $\lambda = \cos \varphi \leq 1 = \frac{P}{S}$ 一般整个电路 P 守恒 S 守恒

电阻: 电压电流同相 电感: 电压正超前电流 电容: 电流超前电压

$P_R = UI \cos 0 = U^2/R \quad P_L = UI \cos 90^\circ = 0 \quad P_C = UI \cos (-90^\circ) = 0$

(阻抗角) $Q_R = UI \sin 0 = 0 \quad Q_L = UI \sin 90^\circ = I^2 X_L = U^2/X_L \quad Q_C = -UI \sin (-90^\circ) = U^2/X_C$

6. 任意阻抗的功率计算

$P_Z = UI \cos \varphi = I^2 |Z| \cos \varphi = I^2 R \quad Q_Z = UI \sin \varphi = I^2 X = I^2 (X_L + X_C)$

$Q_L = I^2 X_L > 0$ 吸收无功为正 $Q_C = I^2 X_C < 0$ 吸收无功为负 $S = \sqrt{P^2 + Q^2} = I^2 \sqrt{R^2 + X^2} = I^2 |Z|$

$\therefore \frac{S}{P} = \frac{1}{\cos \varphi} \quad \frac{|Z|}{R} = \frac{1}{\cos \varphi} \quad X$ 相似于 $\frac{|Z|}{R}$ 外界补 $P_L + P_C$

电感、电容的无功补偿作用: L发出功率时, C吸收功率, L、C无功互补

电压电流的有功分量和无功分量, 以感性负载为例

$\dot{U} = U_R \angle 0^\circ \quad \dot{I} = I \angle -\varphi$ $P = U_R I \quad Q = U I \sin \varphi$ U_R 为有功分量 $U \sin \varphi$ 为无功分量

$\dot{U} = U \angle 0^\circ \quad \dot{I} = I \angle -\varphi$ $P = UI \cos \varphi \quad Q = UI \sin \varphi$ $I \cos \varphi$ 为有功分量, $I \sin \varphi$ 为无功分量

9.5 复功率

功率因数 $\lambda = \cos \varphi$ 低带来的问题是, 解决?

① 设备不能充分利用, 电流到额定值, 功率容量还有

$(P = UI \cos \varphi)$, 设备 S 向负载送多少有功功率

要由负载的阻抗角决定

② 输出有功功率相同时, 电流大, $I = P / U \cos \varphi$, 压降损耗大

解决: (1) 高压 (2) 改进设备 ($\cos \varphi \uparrow$) (3) 并联电容 (感性抵消感性)

并联电容后, 原负载电压电流不变, P 不变, 但 $\cos \varphi \uparrow$

电容大小: $Z_C = I_L \sin \varphi_1 - I \sin \varphi_2$

$C = \frac{P}{\omega U^2} (\tan \varphi_1 - \tan \varphi_2)$

欠补偿 临界补偿 过补偿 (一般只欠补偿) 0 补偿

复功率: 用相量 \dot{U} 来计算功率

定义 $\bar{S} = \dot{U} \dot{I}^*$ 单位 VA, \dot{I}^* 为 \dot{I} 的共轭

$\bar{S} = UI \angle (\varphi_u - \varphi_i) = S \angle \varphi = UI \cos \varphi + j UI \sin \varphi$

$= P + jQ = Z I^2 = R I^2 + j X I^2 = U^2 Y^*$

\bar{S} 是复数, 不是相量, 复功率守恒, 视在功率不守恒

9.6 最大功率传输

$Z_i = R_i + jX_i \quad Z_L = R_L + jX_L$

$\dot{I} = \frac{\dot{U}_s}{Z_i + Z_L} \quad I = \frac{U_s}{\sqrt{(R_i + R_L)^2 + (X_i + X_L)^2}}$ 有功功率 $P = R_L I^2$

$R_L = R_i \quad X_L = -X_i \rightarrow Z_L = Z_i^*$ 如果 $Z_L = R_L$, 则 $|Z_L| = |Z_i|$ 时 P 最大 (共轭匹配)

此时 $P_{max} = \frac{U_s^2}{4R_i}$

电阻 $Z = \frac{\dot{U}}{\dot{I}}$ $\dot{U}_R = R\dot{I}$ $\dot{U}_L = j\omega L\dot{I}$ $\dot{U}_C = -j\frac{1}{\omega C}\dot{I}$ $\dot{U} = \sqrt{U_R^2 + (U_L - U_C)^2}$ $\dot{I} = \frac{\dot{U}}{Z}$ $Z = R + jX$ $X = \omega L - \frac{1}{\omega C}$ $\dot{U} = jX_L \dot{I}$ $\dot{I} = jB_C \dot{U}$ $U = \omega L I \angle \varphi_i + \frac{\pi}{2}$ $I = \omega C U \angle \varphi_u + \frac{\pi}{2}$

导纳 $Y \triangleq \frac{\dot{I}}{\dot{U}}$ $\dot{I}_G = G\dot{U}$ $\dot{I}_L = j\omega C\dot{U}$ $\dot{I}_C = -j\frac{1}{\omega L}\dot{U}$ $\dot{I} = \sqrt{I_G^2 + (I_L - I_C)^2}$ $Y = G + jB$ $B = \omega C - \frac{1}{\omega L}$ $\dot{U} = jX_L \dot{I}$ $\dot{I} = jB_C \dot{U}$ $U = \omega L I \angle \varphi_i + \frac{\pi}{2}$ $I = \omega C U \angle \varphi_u + \frac{\pi}{2}$

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