

# Optimal strategies of liquid CO<sub>2</sub> transportation for geological carbon storage : A case study of South Korea

강현진<sup>a,b</sup>, 이석구<sup>c</sup>, 조형태<sup>d</sup>, 이재원<sup>a</sup>

<sup>a</sup> 한국생산기술연구원 저탄소에너지그룹, <sup>b</sup> 부산대학교 응용화학공학부 <sup>c</sup> 한국에너지기술연구원 탄소전환연구실, <sup>d</sup> 경희대학교 화학공학과

(j.lee@kitech.re.kr)



## Abstract

Geological CO<sub>2</sub> storage, a prominent facet among carbon capture and storage technologies aiming for net-zero emissions, has received substantial attention. Existing studies have investigated liquid CO<sub>2</sub> transportation conditions based on CO<sub>2</sub> emissions from individual plants through a central CO<sub>2</sub> hub terminal. Nevertheless, a misalignment persists between the CO<sub>2</sub> capture assumptions made in previous studies and the actual quantities necessitated for capture from various industrial sources. To address these challenges, we propose comprehensive liquid CO<sub>2</sub> transportation strategies incorporating numerous CO<sub>2</sub> emission sites and multiple CO<sub>2</sub> hub terminals in South Korea. Furthermore, we ascertain the optimal conditions for large-scale liquid CO<sub>2</sub> transportation. The results of this study are expected to contribute to the achievement of net-zero emissions by providing insights into the optimal conditions and transportation strategies for liquid CO<sub>2</sub> in South Korea.

**Keywords:** Carbon Capture and Storage (CCS), Geological CO<sub>2</sub> storage, CO<sub>2</sub> transportation, CO<sub>2</sub> hub terminal, Techno-economic analysis

## Method and Results

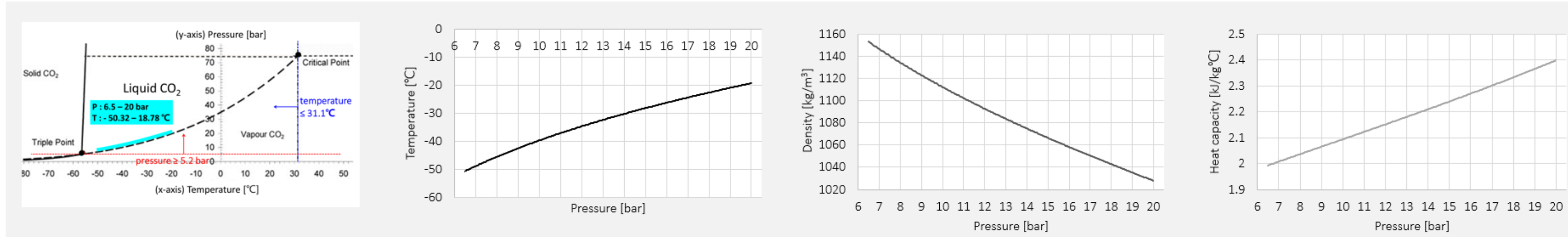
### 1. Introduction

#### ■ MOTIVATION

- With the growing severity of global warming attributed to greenhouse gas emissions, the implementation of post-combustion CO<sub>2</sub> capture processes is on the rise in diverse industries, including power generation, steel production, and petrochemicals.
- If the substantial volume of CO<sub>2</sub> gas, continuously separated from the capture process, is not directly integrated into utilization processes, a volume reduction process is necessary for efficient storage and transportation.
- Liquefaction results in higher density compared to compressing it into high-pressure gas.

	Pressure [bar]	Temperature [°C]	Density [kg/m <sup>3</sup> ]
High-pressure gas	300	30	870
Liquid	20	-20	1030

- Then why do we need to ponder about the pressure conditions of liquid CO<sub>2</sub>?



- : Liquid CO<sub>2</sub> has a higher density at lower pressures than at higher pressures.
- : Liquefaction and boil-off gas re-liquefaction energy depending on pressure can vary significantly.
- : Under low pressure conditions, the equilibrium temperature and heat capacity are lower, so the amount of boil-off gas produced during storage is higher.
- The development of ships to transport captured CO<sub>2</sub> to utilization and storage sites is actively underway.

#### ■ CCS VALUE CHAIN

- Capture → Liquefaction → Buffer Tank → Ship Transport → Injection

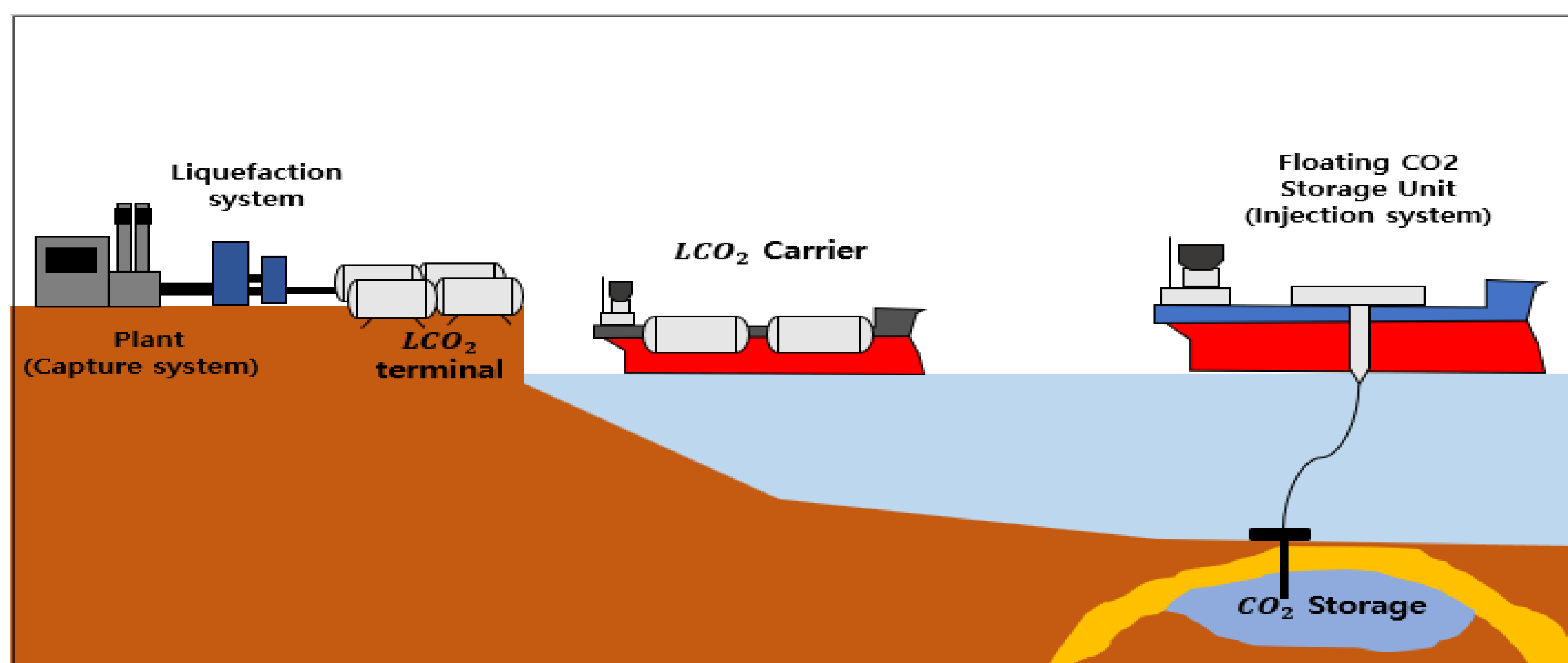


Figure 1. CCS value chain

#### ■ OBJECTIVE

- A comparative analysis of CO<sub>2</sub> transport pressures (6.5 bar, 7 bar, 10 bar, 15 bar, 20 bar) was conducted to determine the optimal pressure.

## Conclusion

- Density differences, liquefaction and re-liquefaction energy, the amount of boil-off gas, domestic CO<sub>2</sub> emission and captured CO<sub>2</sub>, and expected capacity of storage site are considered to determine optimal liquid pressure for efficient transport and intermediate storage.
- Currently, the results of liquefaction energy have been derived, and the results of boil-off gas and re-liquefaction energy are being derived. By combining these results, we will present the optimal pressure for each scenario we set.

### 2. Methodology

- DEFINE OF MASS FLOW RATE

$$W_c = \mathbf{m}[H_v(P_2, T_2) - H_v(P_1, T_1)] \quad - \text{If } \mathbf{m} \text{ is defined, } W_c \text{ is a function of } \mathbf{P}$$

- CALCULATION BASIS

$$(\text{CO}_2 \text{ capture amount}) = (\text{CO}_2 \text{ emission from sources}) - (\text{free quota})$$

- THE AMOUNT OF CO<sub>2</sub> EMISSION

- The CO<sub>2</sub> capture sources are assumed to be domestic power plants, steel mills, oil refineries and petrochemicals.

i) Power plant – coal-fired power plant (based on generated electricity)

ii) Petrochemicals – naphtha cracking facilities (based on annual ethylene production)

iii) Steel mills – furnace facilities (based on annual crude steel production)

Annual amount of CO <sub>2</sub> entering the terminal [m <sup>3</sup> /h]	6.5 bar	7 bar	10 bar	15 bar	20 bar
Ulsan	742	746	770	804	835
Yeosu	1,257	1,265	1,305	1,363	1,416
Daesan	2,619	2,634	2,719	2,839	2,949

### 3. Results & discussion

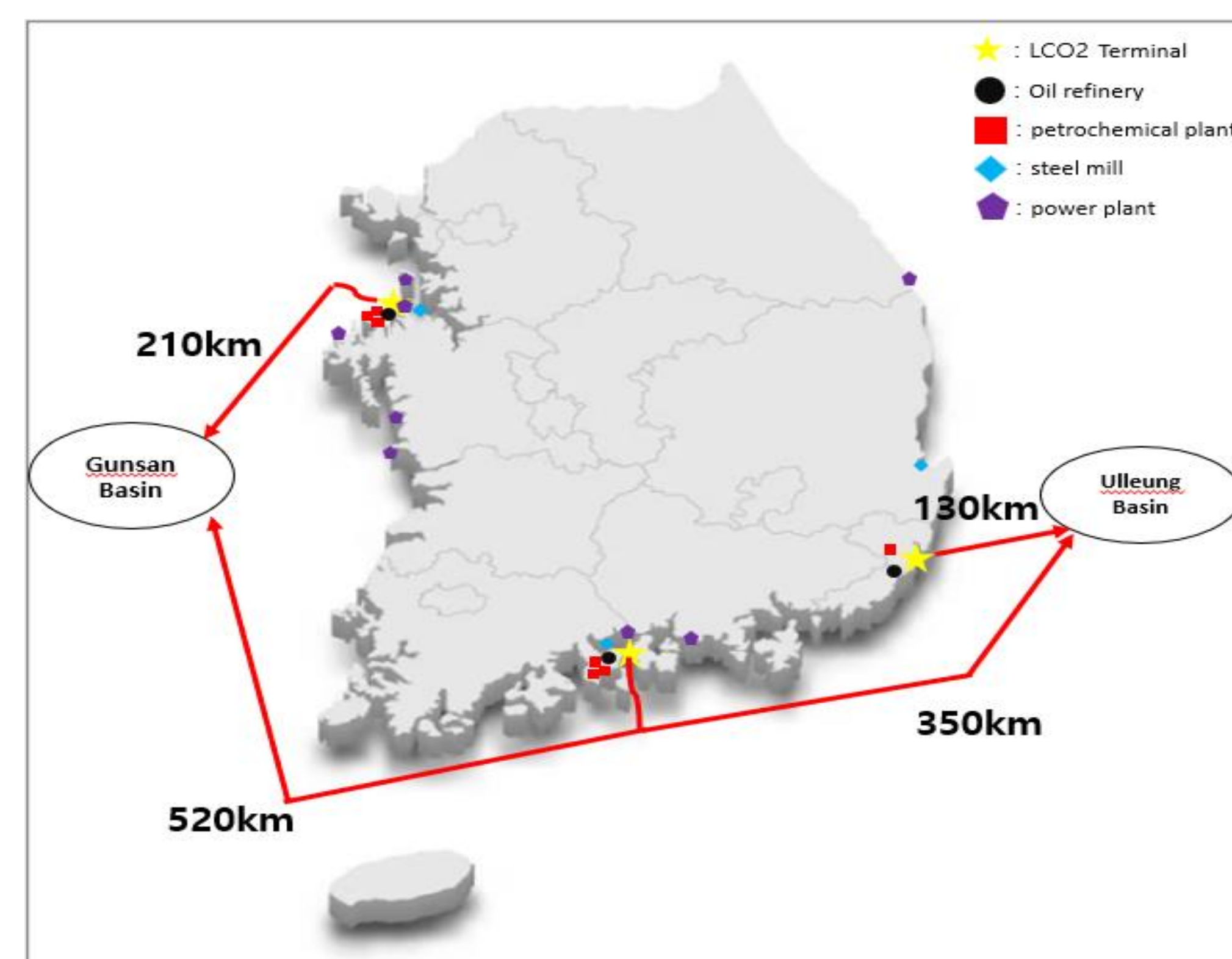
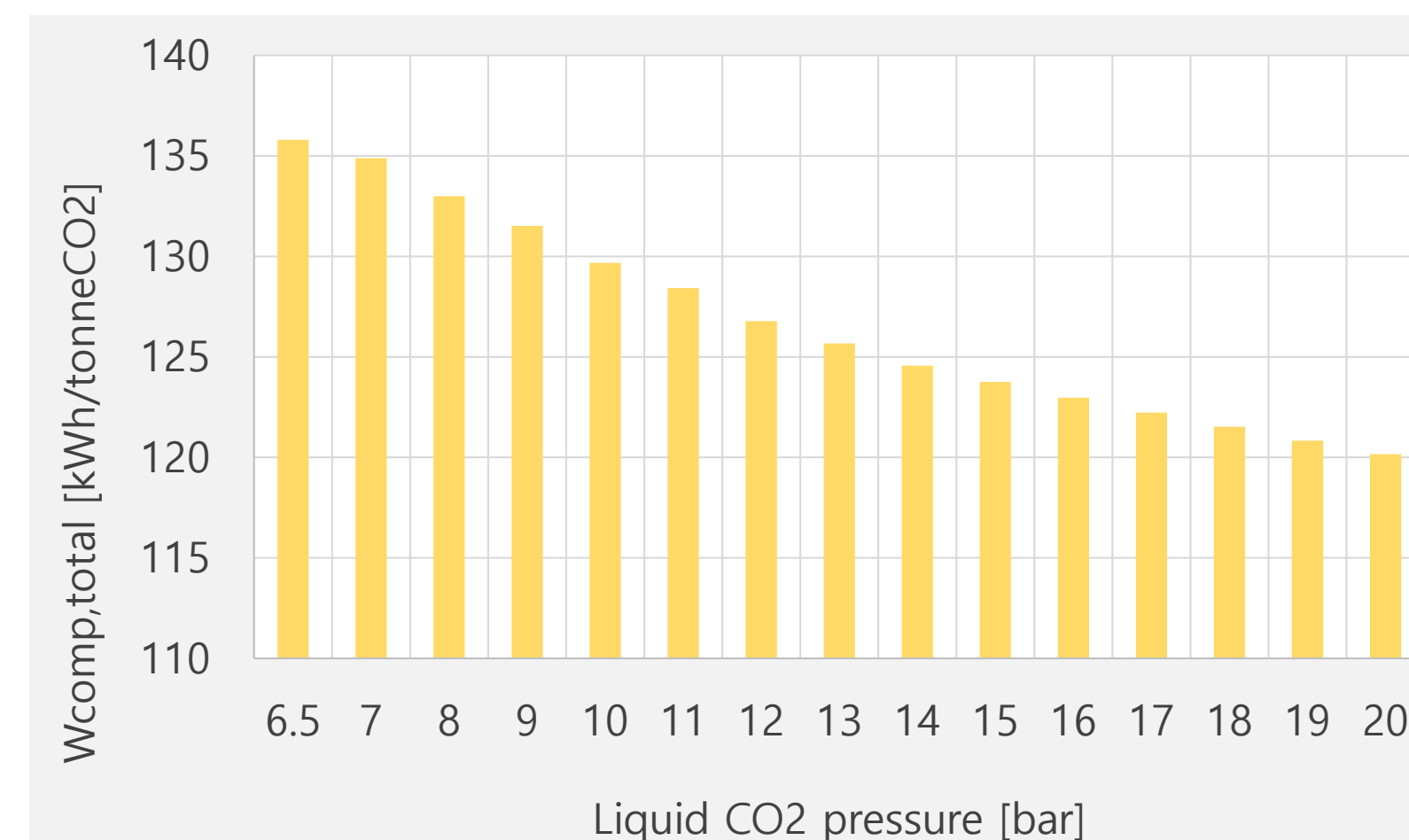


Figure 2. Distance between CO<sub>2</sub> emission source and Storage

- DETERMINATION OF BUFFER TANK SIZE AND NUMBER

Liquid CO <sub>2</sub> terminal	Ulsan	Yeosu	Daesan
Time required shipping [hr]	62	77	67
Minimum number of ships	1	2	4
Buffer tank size [m <sup>3</sup> ]	5,000 X 16	5,000 X 17	5,000 X 16

- COMPARISON OF (RE-)LIQUEFACTION ENERGY



- Liquefaction and re-liquefaction energy tends to decrease linearly as pressure increases.

- Currently, liquefaction energy has been derived, and the amount of boil-off gas and re-liquefaction energy are being derived.