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Miura-Ori Inspired Smooth Sheet Attachments for Zipper-Coupled Tubes

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Abstract: Zipper-coupled tubes are a broadly applicable, deployable mechanism with an angular surface that can be smoothed by attaching an additional smooth sheet pattern. The existing design for the smooth sheet attachment, however, leaves small gaps that can only be covered by adding flaps that unfold separately, limiting applicability in situations requiring a seamless surface and simultaneous deployment. We provide a novel construction of the smooth sheet attachment that unfolds simultaneously with zipper-coupled tubes to cover the entire surface without requiring additional actuation and without inhibiting the tubes' motion up to an ideal, unfolded state of stability. Furthermore, we highlight the mathematics underlying the design and motion of the new smooth sheet pattern, thereby demonstrating its rigid-foldability and compatibility with asymmetric zipper-coupled tubes.



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1. Introduction

Origami is the basis for many deployable mechanisms, including self-scaling, modular robots [1], satellite reflectarray antennas that pack efficiently [2], and multimodal biomedical devices that actuate electromagnetically [3]. Zipper-coupled tubes are multistable origami structures that fold up compactly and unfold bidirectionally to fill space and resist compression [4]. An asymmetric generalization of zipper-coupled tubes with smooth sheet attachments was introduced previously [5]. Together, these origami-based mechanisms form a deployable device with a smooth surface that is advantageous in applications, such as prefab architecture, when drivability and walkability are important, and in smooth medical devices, when sharp edges could harm the body. The smooth sheet attachment we presented previously, however, does not fully cover the surface of zipper-coupled tubes without additional flaps that actuate separately [5]. We rectify this problem by offering an alternative, Miura-ori inspired [6–8], construction of a smooth sheet attachment that fully covers the surface of, and deploys simultaneously with, asymmetric zipper-coupled tubes.

In this paper we briefly review the design of asymmetric zipper-coupled tubes and then demonstrate how to (1) construct a Miura-ori inspired smooth sheet attachment without gaps that attaches to the mountain folds of asymmetric zipper-coupled tubes and (2) handle design variations in the symmetric case. We present a mathematically robust design method, decomposing the attachment into pairs of compatible, tessellating cells inspired by the Miura-ori pattern and then defining the cells' vertices throughout the folding motion, thereby confirming rigid-foldability of the smooth sheet attachment and highlighting the mathematical processes involved in mechanism design. Our Miura-ori-based smooth sheet attachment expands the utility of asymmetric zipper-coupled tubes;

combined, these origami-inspired mechanisms are ideal for applications requiring a rigidly deployable structure with a smooth surface.

2. Zipper-Coupled Tubes Review

Zipper-coupled tubes are an origami pattern consisting of two or more deployable tubes coupled together in a zipper fashion that makes their motion compatible. Designed by Filipov et al., this structure is remarkable for its ability to deploy from a flat, stowable form into a stable, space-filling structure with only one degree of freedom [4]. In this section we review briefly the construction of asymmetric zipper-coupled tubes from two tube segments that are each, in turn, composed of two degree-four vertex cells; the interested reader may refer to our previous work for a thorough treatment of the construction [5].

Throughout this paper we use the notational convention that an arbitrary vector \mathbf{x} has unit length direction vector $\hat{\mathbf{x}}$ with length x , and hence

$$\mathbf{x} = x\hat{\mathbf{x}}$$

Thus, the notation $\hat{\mathbf{x}}$ always represents a unit length vector associated with a vector denoted \mathbf{x} , where $\mathbf{x} = x\hat{\mathbf{x}}$.

The building blocks for zipper-coupled tubes are the compatible degree-four vertex cells \mathcal{C}_1 and \mathcal{C}_2 illustrated in Figures 1 and 2. When combined, they form a single tube segment [5]. To couple correctly and satisfy rigid and flat-foldability [9], the design constraints of these degree-four vertex cells include:

$$\begin{array}{lll} \alpha_3 = \pi - \alpha_1 & \alpha_1 + \alpha_3 = \alpha_2 + \alpha_4 & \alpha_1 < \alpha_2 \\ \alpha_4 = \pi - \alpha_2 & d \sin \alpha_4 = b \sin \alpha_1 & \alpha_1 + \alpha_2 \leq \pi \end{array}$$

If $\alpha_1 + \alpha_2 < \pi$, the zipper-coupled tubes are called *asymmetric*, having a characteristic tilt and a customizable unfolding motion. In the special case that $\alpha_1 + \alpha_2 = \pi$ and $c = a$, the two cells in Figure 1 are congruent, symmetric Miura-ori cells and the resulting zipper-coupled tubes are those constructed by Filipov et al. [4].

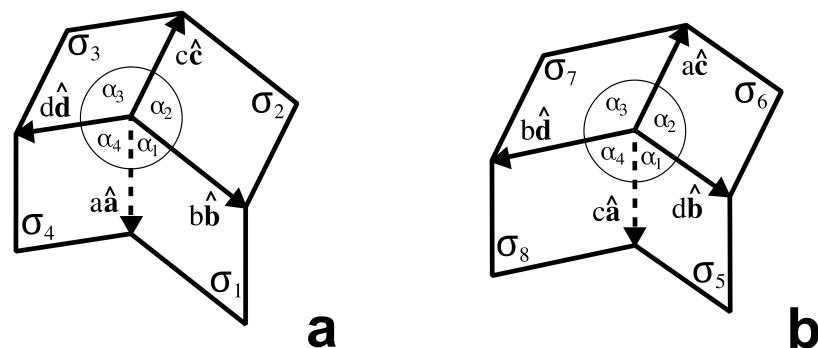


Figure 1. (a) Vectors defining the basic asymmetric degree-four vertex cell, \mathcal{C}_1 . (b) Vectors defining the complementary degree-four vertex cell, \mathcal{C}_2 . (Adapted from [5]).

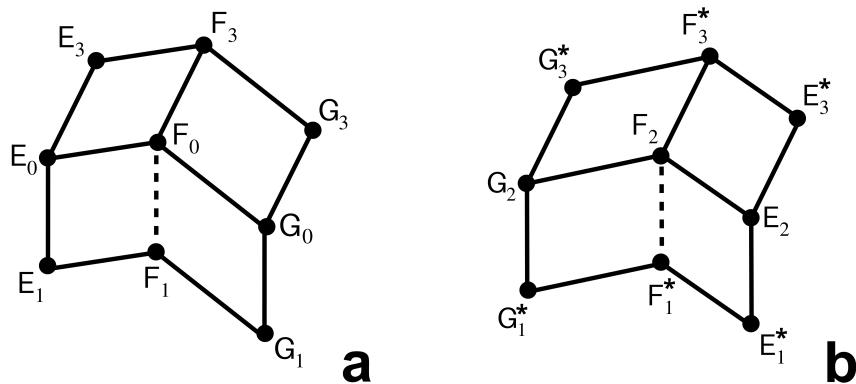


Figure 2. (a) Vertices of the basic asymmetric degree-four vertex cell, C_1 . (b) Vertices of the complementary degree-four vertex cell, C_2 . The points X_i^* identify with X_i . (Adapted from [5]).

Like a Miura-ori cell, the basic degree-four vertex cell has one degree of freedom in its motion. Let the basic and complementary cells lie flat in the xz -plane when unfolded, as depicted in Figures 1 and 2, and let the angles between the xz -plane and panels σ_1 and σ_4 , respectively, be equal as σ_1 and σ_4 fold toward each other (see Figure 1a). Call this motion parameter γ . Then, placing F_0 at the origin and fixing F_1 on the negative z -axis in \mathbb{R}^3 (see Figure 2a), the motion of the basic cell is determined by the following vector paths:

$$\begin{aligned}\hat{\mathbf{a}}(\gamma) &= [0, 0, -1]^T \\ \hat{\mathbf{b}}(\gamma) &= [-\sin \alpha_1 \cos \gamma, \sin \alpha_1 \sin \gamma, -\cos \alpha_1]^T \\ \hat{\mathbf{c}}(\gamma) &= \left[\frac{a_x c_3 + b_x}{k \cos \gamma}, \frac{a_y c_3 + b_y}{k \sin \gamma}, -\frac{a_x b_x \sin^2 \gamma + a_y b_y \cos^2 \gamma + k^2 \sin^2 \gamma \cos^2 \gamma}{a_x^2 \sin^2 \gamma + a_y^2 \cos^2 \gamma + k^2 \sin^2 \gamma \cos^2 \gamma} \right]^T \\ \hat{\mathbf{d}}(\gamma) &= [\sin \alpha_4 \cos \gamma, \sin \alpha_4 \sin \gamma, -\cos \alpha_4]^T\end{aligned}$$

where

$$\begin{aligned}a_x &= \sin \alpha_1 \cos \alpha_4 - \sin \alpha_4 \cos \alpha_1 & b_x &= \sin \alpha_1 \cos \alpha_3 - \sin \alpha_4 \cos \alpha_2 \\ a_y &= \sin \alpha_1 \cos \alpha_4 + \sin \alpha_4 \cos \alpha_1 & b_y &= \sin \alpha_1 \cos \alpha_3 + \sin \alpha_4 \cos \alpha_2 \\ k &= 2 \sin \alpha_1 \sin \alpha_4 & \hat{\mathbf{c}} &= \langle c_1, c_2, c_3 \rangle\end{aligned}$$

The same vectors define the motion of both basic and complementary cells. By combining one basic cell (C_1) and one complementary cell (C_2), we obtain the first tube segment in a zipper-coupled pair, illustrated in Figure 3a. Its vertices, identified with their corresponding position vectors, are given by:

$$\begin{array}{lll}E_0(\gamma) = \mathbf{d}(\gamma) & F_0(\gamma) = \mathbf{0} & G_0(\gamma) = \mathbf{b}(\gamma) \\ E_1(\gamma) = \mathbf{a}(\gamma) + \mathbf{d}(\gamma) & F_1(\gamma) = \mathbf{a}(\gamma) & G_1(\gamma) = \mathbf{a}(\gamma) + \mathbf{b}(\gamma) \\ E_2(\gamma) = \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) & F_2(\gamma) = \mathbf{a}(\gamma) + \mathbf{c}(\gamma) & G_2(\gamma) = \mathbf{a}(\gamma) + \mathbf{b}(\gamma) + \mathbf{c}(\gamma) \\ E_3(\gamma) = \mathbf{c}(\gamma) + \mathbf{d}(\gamma) & F_3(\gamma) = \mathbf{c}(\gamma) & G_3(\gamma) = \mathbf{b}(\gamma) + \mathbf{c}(\gamma)\end{array}$$

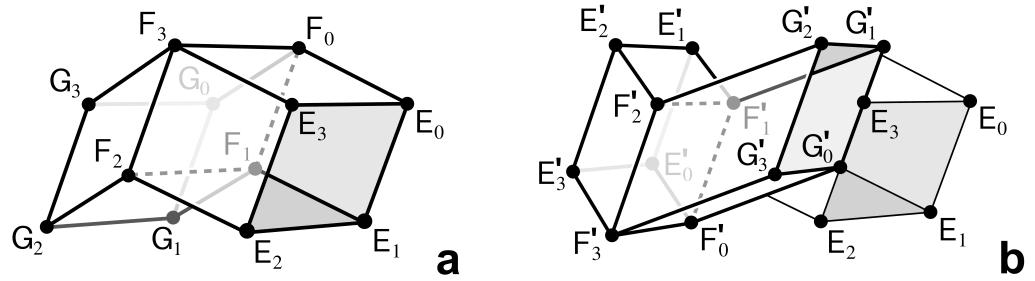


Figure 3. (a) The vertices in the first origami tube segment in the construction of an asymmetric zipper-coupled tube segments pair. (b) The vertices in the second origami tube segment in the construction of an asymmetric zipper-coupled tube segments pair. (Adapted from [5]).

The second tube segment is a copy of the first, but rotated 180° about the y -axis and then shifted by an offset vector so that it attaches to the first tube segment along the vertical creases (illustrated in Figure 3b). Let \mathcal{C}_3 and \mathcal{C}_4 denote the copies of \mathcal{C}_1 and \mathcal{C}_2 , respectively, comprising the second tube segment. To define the motion of the second tube segment, let $\bar{\mathbf{x}}$ denote the 180° rotation of a vector \mathbf{x} about the y -axis and define the offset vector:

$$\mathbf{s}(\gamma) = \left(1 + \frac{b \cos \alpha_1 + d \cos \alpha_4}{2a}\right) \mathbf{a}(\gamma) + \mathbf{c}(\gamma)$$

Then the vertices of the second tube segment are defined by:

$$\begin{aligned} E'_0(\gamma) &= \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) & F'_0(\gamma) &= \mathbf{s}(\gamma) & G'_0(\gamma) &= \bar{\mathbf{b}}(\gamma) + \mathbf{s}(\gamma) \\ E'_1(\gamma) &= \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) & F'_1(\gamma) &= \bar{\mathbf{a}}(\gamma) + \mathbf{s}(\gamma) & G'_1(\gamma) &= \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{b}}(\gamma) + \mathbf{s}(\gamma) \\ E'_2(\gamma) &= \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) & F'_2(\gamma) &= \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) & G'_2(\gamma) &= \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{b}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) \\ E'_3(\gamma) &= \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) & F'_3(\gamma) &= \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) & G'_3(\gamma) &= \bar{\mathbf{b}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) \end{aligned}$$

The pair of tube segments, with vertices positioned as indicated above, form a single component in a pair of zipper-coupled tubes (Figure 3b), which will be denoted as \mathcal{Z}_0 . The zipper-coupled tubes can be extended by taking multiple copies of \mathcal{Z}_0 and attaching them end-to-end. In particular, for $i = 1 \dots n$, let

$$\mathcal{Z}_i = \mathcal{Z}_0 + i(\mathbf{d} - \mathbf{b})$$

Then

$$\mathcal{Z} = \bigcup_{i=0}^n \mathcal{Z}_i$$

denotes zipper-coupled tubes with $n + 1$ components.

Of critical importance, at a certain point in the motion of \mathcal{Z} , the upper (or lower) creases simultaneously become coplanar, as bolded in Figure 4b. This state is the *ideal state*, and it occurs at a parameter value:

$$\gamma_0 = \cos^{-1} \left(\sqrt{\frac{a_y b_y - a_x^2 + k^2 + \sqrt{(a_y b_y + a_x^2 + k^2)^2 - 4 a_y^2 a_x b_x}}{2k^2}} \right)$$

The value γ_0 will be the terminal value for the deployment of \mathcal{Z} with a smooth sheet attachment. Thus, by construction, the smooth sheet attachment lies flat on the surface of the zipper-coupled tubes when $\gamma = \gamma_0$ and folds up with the zipper-coupled tubes until $\gamma = \pi/2$, at which point the entire structure lies in a plane and has no volume.

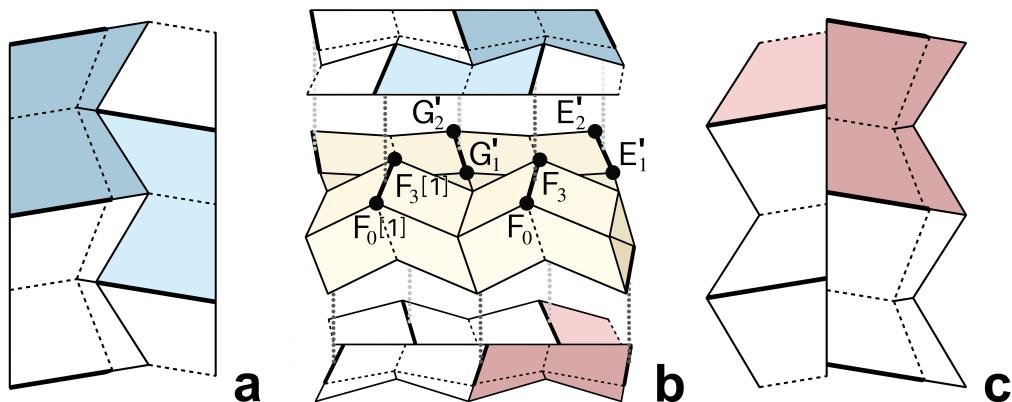


Figure 4. (a) The top smooth sheet attachment (S_1 is lightly shaded, S_4 is darkly shaded, and co-planar ridges are bolded). (b) Adding the top and bottom smooth sheet attachments to asymmetric zipper-coupled tubes (co-planar ridges are bolded). (c) The bottom smooth sheet attachment (S_3 is lightly shaded, S_2 is darkly shaded, co-planar ridges are bolded).

3. Asymmetric Smooth Sheet Attachment

In this section we design a Miura-ori inspired smooth sheet attachment that actuates simultaneously with the asymmetric zipper-coupled tubes pattern, folding up flat and unfolding into a rigid sheet without gaps in the ideal state. This additional pattern broadens the potential applications of the zipper-coupled tubes structure and expands on the design of the attachment described previously [5]. As with the zipper-coupled tubes, we decomposed the overall structure into its basic units: four distinct smooth sheet cells that tessellate. We define the vectors used to construct each cell to describe the motion of the cell's vertices and confirm its compatibility with the zipper-coupled tubes structure.

The seamless smooth sheet attachment consists of four distinct cells denoted S_i , for $i = 1, 2, 3, 4$. In Figure 4a, the lightly shaded cell is S_1 and the darkly shaded cell is S_4 , while in Figure 4c, the lightly shaded cell is half of S_3 and the darkly shaded cell is S_2 . Cells S_1 and S_3 share the same configuration, but like the zipper-coupled tube segments, one is rotated 180° about the y -axis; the same is true of S_2 and S_4 . The manner in which the smooth sheet cells attach to \mathcal{Z} in the ideal state ($\gamma = \gamma_0$) is highlighted in Figure 4b. When the mechanism is fully deployed, cells on the top sheet meet along their jagged edges, as seen in Figure 4a. The cells on the bottom sheet, however, meet along their straight edges, as seen in Figure 4c—this is a key feature in defining a design that will cover zipper-coupled tubes without gaps and deploy without restricting the tubes' motion up to the ideal state.

Regarding the single component \mathcal{Z}_0 , the cell S_i attaches to \mathcal{C}_i . However, whereas the cells S_2 and S_4 form a bridge between a pair of creases in \mathcal{Z}_0 , the cells S_1 and S_3 form a bridge between a crease of \mathcal{Z}_0 and a crease of \mathcal{Z}_1 (bolded in Figure 4b). Upon careful examination of the zipper-coupled tubes, we observed that S_1 can be designed as though it bridged two creases of \mathcal{C}_4 and then moved to bridge creases of the copies of \mathcal{C}_1 in \mathcal{Z}_0 and \mathcal{Z}_1 ; this strategy eliminates some complexity in defining S_1 . In contrast, S_4 is designed directly, transversing the two creases of \mathcal{C}_4 where it attaches. Designing both cells atop \mathcal{C}_4 allows us to re-use the same vectors and enables the interested reader to easily compare the Miura-ori inspired cells and the original smooth sheet cells with gaps [5].

3.1. Design of S_1

The first smooth sheet cell, S_1 , has two panels that fold toward each other as the zipper-coupled tubes fold up. We first discuss the design of S_1 when built atop \mathcal{C}_4 —the desired relation between S_1 and \mathcal{C}_4 is shown in Figure 5a. The vectors that define S_1 in this temporary configuration will be re-used to define S_4 , allowing the edges of these two cells to mesh when placed opposite each other. After construction, the smooth sheet cell S_1 will be moved to attach to \mathcal{C}_1 , as seen in Figure 5b.

In preparation of the design of \mathcal{S}_1 , let the displacement between $G'_2(\gamma)$ and $E'_2(\gamma)$ be described by

$$\bar{\mathbf{q}}(\gamma) = \bar{\mathbf{d}}(\gamma) - \bar{\mathbf{b}}(\gamma)$$

and

$$\bar{\mathbf{q}}_{\perp}(\gamma) = \bar{\mathbf{q}}(\gamma) - (\bar{\mathbf{q}}(\gamma) \cdot \hat{\mathbf{c}}(\gamma)) \hat{\mathbf{c}}(\gamma)$$

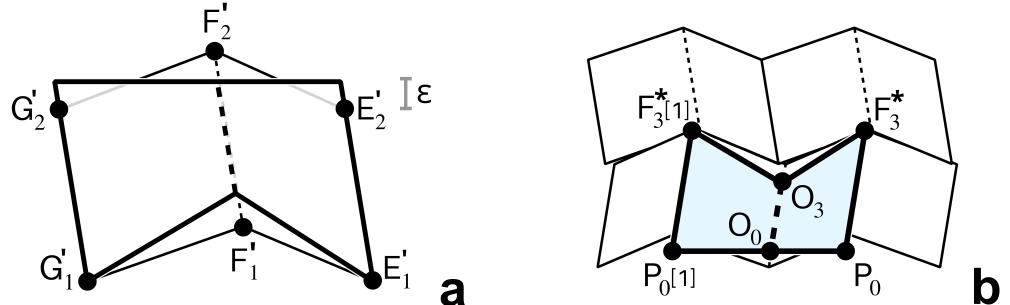


Figure 5. (a) Placing \mathcal{S}_1 on \mathcal{C}_4 . (b) Attaching \mathcal{S}_1 to asymmetric zipper-coupled tubes.

As depicted in Figure 6a,b, $\bar{\mathbf{q}}_{\perp}(\gamma)$ is the component vector of $\bar{\mathbf{q}}(\gamma)$ orthogonal to $\bar{\mathbf{c}}(\gamma)$, the displacement between $E'_1(\gamma)$ and $E'_2(\gamma)$ (or equivalently, the displacement between $G'_1(\gamma)$ and $G'_2(\gamma)$). In the ideal state of the zipper-coupled tubes, the distance between the ridges of \mathcal{Z} on which the smooth sheet will be attached is

$$\Delta = \|\bar{\mathbf{q}}_{\perp}(\gamma_0)\|$$

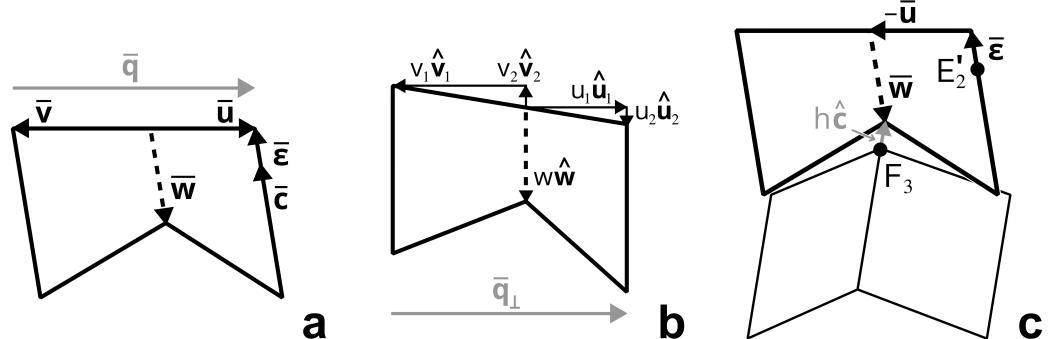


Figure 6. (a) Vectors in \mathcal{S}_1 . (b) Vector components of $\bar{\mathbf{u}}$ and $\bar{\mathbf{v}}$. (c) Relation between h and w in the ideal state.

Note that, of necessity and by design, the top edges of both \mathcal{S}_1 and \mathcal{S}_4 are parallel with $\bar{\mathbf{q}}(\gamma_0)$. To remove gaps between zipper-coupled tubes stacked laterally to \mathcal{Z}_0 and in anticipation of the behavior depicted in Figure 4c, we extended the side edges of \mathcal{S}_1 in the direction of $\bar{\mathbf{c}}$ by the length ε , as shown in Figures 5a and 6a, where

$$\varepsilon = \frac{b \sin \alpha_1 \sin \gamma_0}{2 |c_2(\gamma_0)|}$$

Toward this end, let

$$\bar{\mathbf{e}}(\gamma) = \varepsilon \hat{\mathbf{c}}$$

The smooth sheet cell is determined by the vectors $\bar{\mathbf{u}}$, $\bar{\mathbf{v}}$, and $\bar{\mathbf{w}}$ illustrated in Figure 6a. As highlighted in Figure 6b, let

$$u_1 = \frac{d \sin \alpha_1 - b \sin \alpha_4 + \Delta}{2} \quad (1)$$

$$v_1 = \frac{b \sin \alpha_4 - d \sin \alpha_1 + \Delta}{2} \quad (2)$$

Note that $\Delta = u_1 + v_1$. Examining the components of $\bar{\mathbf{u}}$ and $\bar{\mathbf{v}}$ in the ideal state, as shown in Figure 6a,b, we see that $u_2 + v_2 = ||\bar{\mathbf{q}}(\gamma_0) - \bar{\mathbf{q}}_\perp(\gamma_0)||$. Since

$$\frac{u_2}{u_2 + v_2} = \frac{u_1}{u_1 + v_1} = \frac{u_1}{\Delta} \quad \text{and} \quad \frac{v_2}{v_1} = \frac{u_2}{u_1}$$

it follows that

$$u_2 = \frac{u_1}{\Delta} ||\bar{\mathbf{q}}(\gamma_0) - \bar{\mathbf{q}}_\perp(\gamma_0)|| \quad (3)$$

$$v_2 = v_1 \frac{u_2}{u_1} \quad (4)$$

Rodrigues' rotation formula [10] rotates a vector \mathbf{x} by angle θ in a counter-clockwise direction about a unit vector \mathbf{k} , and is given by:

$$R[\mathbf{k}, \theta](\mathbf{x}) = \mathbf{x} \cos \theta + (\mathbf{k} \times \mathbf{x}) \sin \theta + \mathbf{k} \langle \mathbf{k}, \mathbf{x} \rangle (1 - \cos \theta)$$

Let

$$\begin{aligned} \hat{\mathbf{u}}_1(\gamma) &= R[-\hat{\mathbf{c}}(\gamma), \lambda(\gamma)](\hat{\mathbf{q}}_\perp(\gamma)) \\ \hat{\mathbf{u}}_2(\gamma) &= -\hat{\mathbf{c}}(\gamma) \end{aligned}$$

where

$$\lambda(\gamma) = \cos^{-1} \left(\frac{\|\bar{\mathbf{q}}_\perp(\gamma)\|^2 + u_1^2 - v_1^2}{2\|\bar{\mathbf{q}}_\perp(\gamma)\|u_1} \right)$$

Then we define $\bar{\mathbf{u}}(\gamma)$ and $\bar{\mathbf{v}}(\gamma)$ as

$$\begin{aligned} \bar{\mathbf{u}}(\gamma) &= u_1 \hat{\mathbf{u}}_1(\gamma) + u_2 \hat{\mathbf{u}}_2(\gamma) \\ \bar{\mathbf{v}}(\gamma) &= \bar{\mathbf{u}}(\gamma) - \bar{\mathbf{q}}(\gamma) \end{aligned}$$

In order to satisfy flat-foldability, the direction of the vector $\bar{\mathbf{w}}$ must be the same as the direction of $-\hat{\mathbf{c}}$. Thus, for some positive constant w :

$$\bar{\mathbf{w}}(\gamma) = -w \hat{\mathbf{c}}(\gamma)$$

The primary concern in choosing the length w was to avoid intersections with the zipper-coupled tubes during deployment. So that the smooth sheet cells S_1 and S_4 lined up correctly, we defined w and h to be the lengths necessary so that in the ideal state, the tips of the vectors $\bar{\mathbf{w}}$ ($-w \hat{\mathbf{c}}$) and $h \hat{\mathbf{c}}$ meet, as shown in Figure 6c. In particular, we set

$$h \hat{\mathbf{c}}(\gamma_0) + F_3(\gamma_0) = -w \hat{\mathbf{c}}(\gamma_0) + (E'_2(\gamma_0) + \bar{\mathbf{e}}(\gamma_0) - \bar{\mathbf{u}}(\gamma_0))$$

Then, w (and h) can be obtained as follows:

$$[h, w]^T = [\text{proj}(\hat{\mathbf{c}}(\gamma_0)), \text{proj}(\hat{\mathbf{c}}(\gamma_0))]^{-1} \text{proj}(\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\mathbf{e}} - \bar{\mathbf{u}} - \mathbf{c})(\gamma_0) \quad (5)$$

where the function $\text{proj} : \mathbb{R}^3 \rightarrow \mathbb{R}^2$ is defined such that

$$\text{proj}[x, y, z]^T = [x, y]^T$$

Remark 1. Note that the matrix that is inverted in Equation (5) will be singular only in the symmetric case when $\bar{\mathbf{c}}$ has the same direction as $-\mathbf{c}$.

We have now stipulated all three vectors— $\bar{\mathbf{u}}$, $\bar{\mathbf{v}}$, and $\bar{\mathbf{w}}$ —which define \mathcal{S}_1 when it is attached to \mathcal{C}_4 . What remains is to move \mathcal{S}_1 so that it attaches to \mathcal{C}_1 . The desired placement is depicted in Figure 5b, where \mathcal{S}_1 is positioned on top of \mathcal{C}_1 and bridges \mathcal{Z}_0 and \mathcal{Z}_1 ; note that the zipper-coupled tubes have been rotated about the y -axis in this figure so that \mathcal{S}_1 lies parallel with the xy -plane (see [5] for further details). Let $X[i]$ denote the point in \mathcal{Z}_i that is a copy of X in \mathcal{Z}_0 , for $i \geq 1$. Then, the vertex F_3^* in \mathcal{S}_1 attaches to F_3 in \mathcal{Z}_0 and the vertex $F_3^*[1]$ in \mathcal{S}_1 attaches to $F_3[1]$ in \mathcal{Z}_1 . More particularly, the edge $\overline{P_0 F_3^*}$ attaches to $\overline{F_0 F_3}$ and $\overline{P_0[1] F_3^*[1]}$ attaches to $\overline{F_0[1] F_3[1]}$.

Recall that the 180° rotation of a vector $\bar{\mathbf{x}}$ about the y -axis is denoted \mathbf{x} . Thus, the vertices in \mathcal{S}_1 when attached to \mathcal{C}_1 as desired are:

$$\begin{aligned} F_3(\gamma) &= \mathbf{c}(\gamma) & O_0(\gamma) &= -\mathbf{e}(\gamma) + \mathbf{u}(\gamma) & F_3[1](\gamma) &= \mathbf{c}(\gamma) - \mathbf{b}(\gamma) + \mathbf{d}(\gamma) \\ P_0(\gamma) &= -\mathbf{e}(\gamma) & O_3(\gamma) &= -\mathbf{e}(\gamma) + \mathbf{u}(\gamma) - \mathbf{w}(\gamma) & P_0[1](\gamma) &= -\mathbf{e}(\gamma) - \mathbf{b}(\gamma) + \mathbf{d}(\gamma) \end{aligned}$$

3.2. Design of \mathcal{S}_3

The cell \mathcal{S}_3 is a rotated copy of \mathcal{S}_1 attached to \mathcal{C}_3 , so the vectors that define \mathcal{S}_3 are rotated copies of the vectors that define \mathcal{S}_1 , shifted by \mathbf{s} . Let the vertices on smooth sheet cells attached to the rotated tube segment in \mathcal{Z}_0 —i.e., the vertices in \mathcal{S}_2 and \mathcal{S}_3 —be denoted with primes. Note that the smooth sheet cell \mathcal{S}_3 bridges \mathcal{Z}_0 and \mathcal{Z}_{-1} , so the smooth sheet cell contains the vertices F'_3 and $F'_3[-1]$. Thus, the vertices of \mathcal{S}_3 when attached to \mathcal{C}_3 are:

$$\begin{aligned} F'_3(\gamma) &= \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) & O'_0(\gamma) &= \mathbf{s}(\gamma) - \bar{\mathbf{e}}(\gamma) + \bar{\mathbf{u}}(\gamma) & F'_3[-1](\gamma) &= \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) - \bar{\mathbf{b}}(\gamma) + \bar{\mathbf{d}}(\gamma) \\ P'_0(\gamma) &= \mathbf{s}(\gamma) - \bar{\mathbf{e}}(\gamma) & O'_3(\gamma) &= \mathbf{s}(\gamma) - \bar{\mathbf{e}}(\gamma) + \bar{\mathbf{u}}(\gamma) - \bar{\mathbf{w}}(\gamma) & P'_0[-1](\gamma) &= \mathbf{s}(\gamma) - \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{b}}(\gamma) + \bar{\mathbf{d}}(\gamma) \end{aligned}$$

3.3. Design of \mathcal{S}_4

The smooth sheet cell \mathcal{S}_4 attaches on top of \mathcal{C}_4 and fits together with \mathcal{S}_1 in the ideal state, as illustrated in Figure 7. We make the edge of \mathcal{S}_4 opposite of \mathcal{S}_1 straight in the ideal state so that zipper-coupled tubes with smooth sheet attachments can be stacked laterally without gaps. From another point of view, the edge is made straight in preparation of the design of \mathcal{S}_2 , a copy of \mathcal{S}_4 attached to the bottom of \mathcal{Z}_0 —the straight edges of \mathcal{S}_2 and \mathcal{S}_3 meet in the ideal state, as illustrated in Figure 4c.

The smooth sheet cell \mathcal{S}_4 has a degree-four vertex folding pattern inspired by the Miura-ori cell, as shown in Figure 8a. This allows the cell to close the gap on the top of \mathcal{Z}_0 in the ideal state and fold up without intersecting the adjacent tube segment. For flat-foldability of the cell, we require the sum of opposite angles at the interior vertex to be 180° (see Kawasaki-Justin theorem [11,12]). The pattern in Figure 8a is described by the previously defined vectors $\bar{\mathbf{u}}$, $\bar{\mathbf{v}}$, and $\bar{\mathbf{w}}$ and the yet-to-be-defined vectors $\bar{\mathbf{r}}$, $\bar{\mathbf{t}}$, $\bar{\mathbf{h}}$, $\bar{\mathbf{f}}$, and $\bar{\mathbf{g}}$.

In the ideal state, $\bar{\mathbf{r}}$ and $\bar{\mathbf{t}}$ are the projections of \mathbf{b} and \mathbf{d} , respectively, into the xy -plane; this is necessary to ensure flat foldability. Thus (see Figures 3 and 8a),

$$\beta_2 = \angle P'_1 Q'_1 Q'_2 = \angle F_3 G'_1 G'_2 \quad \text{and} \quad \beta_3 = \angle P'_1 O'_1 O'_2 = \angle F_3 E'_1 E'_2$$

In particular,

$$\begin{aligned} \beta_2 &= \cos^{-1} \left(-\hat{\mathbf{c}}(\gamma_0) \cdot \frac{\mathbf{d}(\gamma_0) - s_0 \mathbf{a}(\gamma_0)}{\|\mathbf{d}(\gamma_0) - s_0 \mathbf{a}(\gamma_0)\|} \right) \\ \beta_3 &= \cos^{-1} \left(-\hat{\mathbf{c}}(\gamma_0) \cdot \frac{\mathbf{b}(\gamma_0) - s_0 \mathbf{a}(\gamma_0)}{\|\mathbf{b}(\gamma_0) - s_0 \mathbf{a}(\gamma_0)\|} \right) \end{aligned}$$

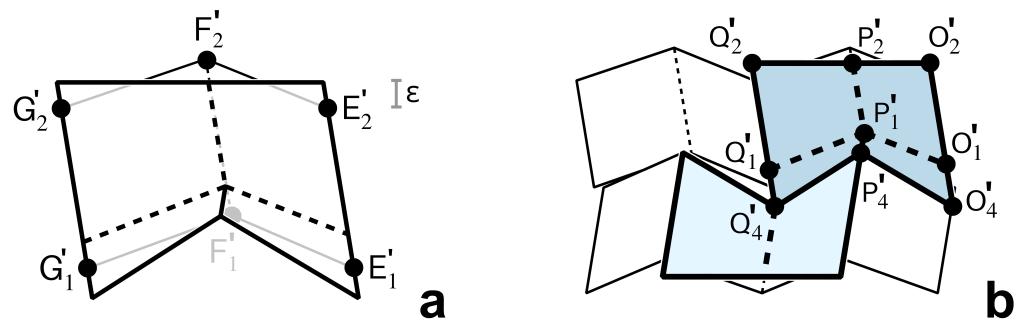


Figure 7. (a) Placing S_4 on C_4 . (b) Attaching S_4 to asymmetric zipper-coupled tubes.

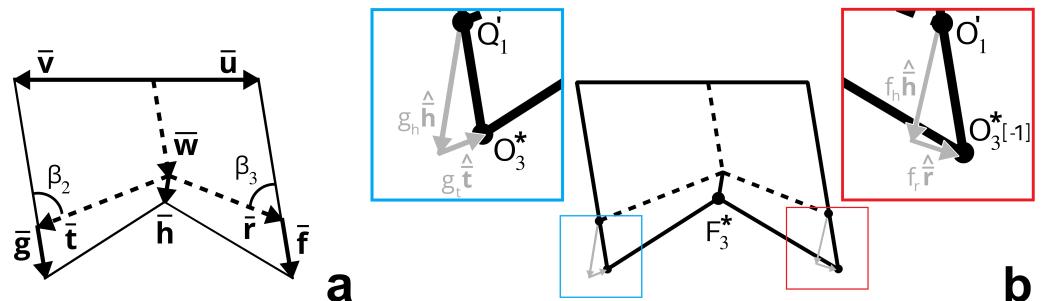


Figure 8. (a) Vectors in S_4 . (b) Vector components of \bar{f} and \bar{g} .

Having derived these angles, we are now ready to define \bar{r} and \bar{t} as follows (see Equations (1)–(4)):

$$\begin{aligned}\bar{r}(\gamma) &= -\left(\frac{u_1}{\tan \beta_3} - u_2\right) \hat{c}(\gamma) + \bar{u}(\gamma) \\ \bar{t}(\gamma) &= -\left(\frac{v_1}{\tan \beta_2} + v_2\right) \hat{c}(\gamma) + \bar{v}(\gamma)\end{aligned}$$

Observing Figure 8a, note that r and t can be expressed simply as:

$$r = \frac{u_1}{\sin \beta_3} \quad t = \frac{v_1}{\sin \beta_2}$$

In the ideal state, the crease defined by \bar{h} must have the same direction as $-c$ to satisfy flat-foldability. Moreover, so that there are no gaps when S_1 and S_4 come together in the ideal state, the length of \bar{h} should be the value h given by Equation (5), according to the premise upon which Equation (5) was derived (see also Figure 6c). Thus,

$$\bar{h}(\gamma_0) = -h \hat{c}(\gamma_0)$$

For an arbitrary parameter value γ , the unit vectors adjacent to $\hat{h}(\gamma)$ that emanate from the degree-four vertex in the interior of S_4 are $\hat{r}(\gamma)$ and $\hat{t}(\gamma)$. Because opposite angles in a degree-four vertex sum to 180° [11,12] and we require a rigid folding, $\hat{h}(\gamma)$ is determined by the following system of equations:

$$\begin{aligned}\hat{h}(\gamma) \cdot \hat{r}(\gamma) &= \cos(\pi - \cos^{-1}(\hat{c}(\gamma) \cdot \hat{t}(\gamma))) \\ \hat{h}(\gamma) \cdot \hat{t}(\gamma) &= \cos(\pi - \cos^{-1}(\hat{c}(\gamma) \cdot \hat{r}(\gamma))) \\ \hat{h}(\gamma) \cdot \hat{h}(\gamma) &= 1\end{aligned}$$

The first two equations are linear and the third is quadratic. Hence, there are precisely two solutions: one corresponding to a valley fold assignment and one corresponding to a mountain fold assignment. The solution corresponding to a mountain fold is the correct solution.

Because $\bar{\mathbf{g}}$ corresponds to an edge of the panel defined by $\hat{\mathbf{h}}$ and $\hat{\mathbf{t}}$, we can define it in terms of these vectors. We want the position of vertex Q'_4 in \mathcal{S}_4 to equal that of O_3 in \mathcal{S}_1 when in the ideal state. This is equivalent to saying that $g_h \hat{\mathbf{h}}$ and $-g_t \hat{\mathbf{t}}$ define the same point when the former is extended from Q'_1 and the latter is extended from O_3 in the ideal state, as shown in Figure 8b. The reader will recognize that this problem is formulated similarly to that in the end of Section 3.1, where the lengths h and w were computed using a system of equations based on two intersecting vectors. We employ the same technique, with the following system of equations:

$$g_h \hat{\mathbf{h}}(\gamma_0) + Q'_1(\gamma_0) = -g_t \hat{\mathbf{t}}(\gamma_0) + O_3(\gamma_0)$$

giving us

$$[g_h, g_t]^T = \left[\text{proj}(\hat{\mathbf{h}}(\gamma_0)), \text{proj}(\hat{\mathbf{t}}(\gamma_0)) \right]^{-1} \text{proj}(-\mathbf{e} + \mathbf{u} - \mathbf{w} - \bar{\mathbf{a}} - \bar{\mathbf{c}} - \bar{\mathbf{d}} - \mathbf{s} - \bar{\mathbf{e}} + \bar{\mathbf{u}} - \bar{\mathbf{w}} - \bar{\mathbf{t}})(\gamma_0)$$

We solve for g_h and g_t and use these components of projection to define $\bar{\mathbf{g}}$, using $\hat{\mathbf{h}}$ and $\hat{\mathbf{t}}$ as a basis:

$$\bar{\mathbf{g}}(\gamma) = g_h \hat{\mathbf{h}}(\gamma) + g_t \hat{\mathbf{t}}(\gamma)$$

We define $\bar{\mathbf{f}}$ similarly, solving for f_h and f_r via the same method and another system of equations:

$$f_h \hat{\mathbf{h}}(\gamma_0) + O'_1(\gamma_0) = -f_r \hat{\mathbf{r}}(\gamma_0) + O_3[-1](\gamma_0)$$

This gives us

$$[f_h, f_r]^T = \left[\text{proj}(\hat{\mathbf{h}}(\gamma_0)), \text{proj}(\hat{\mathbf{r}}(\gamma_0)) \right]^{-1} \text{proj}(-\mathbf{e} + \mathbf{u} - \mathbf{w} - \bar{\mathbf{a}} - \bar{\mathbf{b}} - \bar{\mathbf{c}} - \mathbf{s} - \bar{\mathbf{e}} + \bar{\mathbf{u}} - \bar{\mathbf{w}} - \bar{\mathbf{r}})(\gamma_0)$$

Thus, we have

$$\bar{\mathbf{f}}(\gamma) = f_h \hat{\mathbf{h}}(\gamma) + f_r \hat{\mathbf{r}}(\gamma)$$

Now that we have defined all the essential vectors in \mathcal{S}_4 , we are ready to attach the degree-four vertex to \mathcal{C}_4 in the zipper-coupled tubes structure. In the ideal state, this smooth sheet cell matches exactly with the edges of \mathcal{S}_1 , providing a smooth surface devoid of gaps on the top of asymmetric zipper-coupled tubes (Figure 4a). In particular, the edge $\overline{O'_1 O'_2}$ attaches to $\overline{E'_1 E'_2}$ and $\overline{Q'_1 Q'_2}$ attaches to $\overline{G'_1 G'_2}$. Likewise, the edges $\overline{O'_1 O'_4}$ and $\overline{Q'_1 Q'_4}$ align perfectly with adjacent cells in the ideal state and fold up at different rates to avoid intersections. The vertices in \mathcal{S}_4 identified with their corresponding position vectors are:

$$O'_1(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma) + \bar{\mathbf{r}}(\gamma)$$

$$O'_2(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma)$$

$$O'_4(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma) + \bar{\mathbf{r}}(\gamma) + \bar{\mathbf{f}}(\gamma)$$

$$P'_1(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma)$$

$$P'_2(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma)$$

$$P'_4(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma) + \bar{\mathbf{h}}(\gamma)$$

$$Q'_1(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma) + \bar{\mathbf{t}}(\gamma)$$

$$Q'_2(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{b}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma)$$

$$Q'_4(\gamma) = \bar{\mathbf{a}}(\gamma) + \bar{\mathbf{c}}(\gamma) + \bar{\mathbf{d}}(\gamma) + \mathbf{s}(\gamma) + \bar{\mathbf{e}}(\gamma) - \bar{\mathbf{u}}(\gamma) + \bar{\mathbf{w}}(\gamma) + \bar{\mathbf{t}}(\gamma) + \bar{\mathbf{g}}(\gamma)$$

3.4. Design of \mathcal{S}_2

The smooth sheet cell \mathcal{S}_2 is a rotated copy of \mathcal{S}_4 that attaches to \mathcal{C}_2 . The vertices in this smooth sheet cell are

$$\begin{aligned} O_1(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) + \mathbf{r}(\gamma) \\ O_2(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) \\ O_4(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) + \mathbf{r}(\gamma) + \mathbf{f}(\gamma) \\ P_1(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) \\ P_2(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) \\ P_4(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) + \mathbf{h}(\gamma) \\ Q_1(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) + \mathbf{t}(\gamma) \\ Q_2(\gamma) &= \mathbf{a}(\gamma) + \mathbf{b}(\gamma) + \mathbf{c}(\gamma) + \mathbf{e}(\gamma) \\ Q_4(\gamma) &= \mathbf{a}(\gamma) + \mathbf{c}(\gamma) + \mathbf{d}(\gamma) + \mathbf{e}(\gamma) - \mathbf{u}(\gamma) + \mathbf{w}(\gamma) + \mathbf{t}(\gamma) + \mathbf{g}(\gamma) \end{aligned}$$

We have now completed the details for the smooth sheet attachment in the asymmetric case; a summary of the edges and vertices in the attachment is given in Tables A1 and A2, suppressing γ for concision. This attachment folds up flat and actuates with the zipper-coupled tubes structure to form a smooth surface, leaving no gaps between the various asymmetric cells we have described. The symmetric case merits more discussion, however, because there are fewer constraints on the vectors in the \mathcal{S}_i , allowing for multiple rigidly foldable patterns given specific design parameters.

4. Symmetric Smooth Sheet Attachment

Unlike their asymmetric counterparts, symmetric zipper-coupled tubes have no tilt and fold parallel with the x -axis [5]. Furthermore, the center creases in \mathcal{S}_1 and \mathcal{S}_4 lie parallel with the y -axis in the ideal state, as illustrated in Figure 9. There are multiple valid lengths for these creases, therefore, in a design that covers all the gaps in the surface while maintaining rigid foldability without prohibitive intersections. In this section we comment on the diversity in symmetric, Miura-ori inspired smooth sheet cell construction and recommend values for certain lengths.

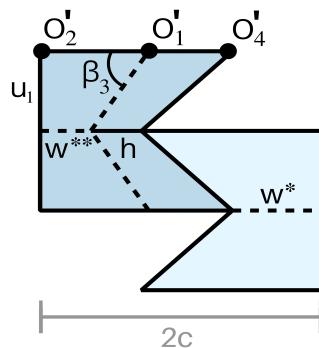


Figure 9. \mathcal{S}_1 and \mathcal{S}_4 in a symmetric smooth sheet attachment.

The design parameters for the smooth sheet cells \mathcal{S}_i are uniquely determined for all cases where $\alpha_1 + \alpha_2 < \pi$. When $\alpha_1 + \alpha_2 = \pi$, however, there is no longer a unique solution to Equation (5). In particular, $\bar{\mathbf{c}}(\gamma_0)$ has the same direction as $-\mathbf{c}(\gamma_0)$ in the symmetric case, so the matrix inverted in Equation (5) is singular and the values h and w are not uniquely defined. Similarly, β_2 and β_3 are no longer constrained, and we may define these features of the design problem advantageously by choosing a solution that minimizes the amount by which the smooth sheet attachment protrudes from the structure when folded.

In the design of \mathcal{S}_1 and \mathcal{S}_3 , let w^* replace the value of w . Likewise, in the design of \mathcal{S}_4 and \mathcal{S}_2 , let w^{**} replace the value of w . As highlighted in Figure 9, for the symmetric case we no longer require that $w^* = w^{**}$. In selecting a value for w^* , we set it as large as possible to maximize the surface area of \mathcal{S}_1 , thus minimizing the amount by which the edges of \mathcal{S}_4 can protrude from the zipper-coupled tubes structure. Applying the analysis given in [5] (see Section 7.1.3), the largest value for w^* can be shown to be

$$w^* = c - \frac{d \sin \alpha_1 + b \sin \alpha_4 - \Delta}{2 \tan(\alpha_2 - \alpha_1)} - \varepsilon$$

The only requirements for h , w^{**} , β_2 , and β_3 in the symmetric case are

$$h + w^{**} = c - \varepsilon \quad \text{and} \quad \beta_2 = \beta_3$$

Adjustments to the values h , w^{**} , β_2 , and β_3 can also assist in minimizing the protrusion of \mathcal{S}_4 from the zipper-coupled tubes. Optimal values can be determined by numerical methods according to the specific design application. However, care should be taken in making these adjustments to avoid intersections with the structure underneath.

On a final note, although $\bar{\mathbf{f}}$ and $\bar{\mathbf{g}}$ are determined after defining the previous quantities, a convenient simplification in their definition: because \mathcal{S}_4 is symmetric, the vectors $\bar{\mathbf{f}}$ and $\bar{\mathbf{g}}$ are parallel to $\bar{\mathbf{h}}$ and have equal lengths. Moreover, in the ideal state,

$$O'_1 O'_4 = O'_2 O'_4 - O'_1 O'_2$$

Therefore,

$$g_t = f_r = 0 \quad \text{and} \quad g_h = f_h = (2c - w^*) - \left(w^{**} + \frac{u_1}{\tan \beta_3} \right)$$

5. Conclusions

We have successfully defined a smooth sheet attachment that folds up with the zipper-coupled tubes and unfolds to the ideal state without inhibiting their motion to form a flat surface without any gaps (Figure 10). This pattern is defined for both the asymmetric and symmetric cases, and we provide access to code which the reader may use to visualize the origami structures described and print out the corresponding fold patterns: <https://github.com/dylanwebbc/azct> (accessed on 23 July 2022).

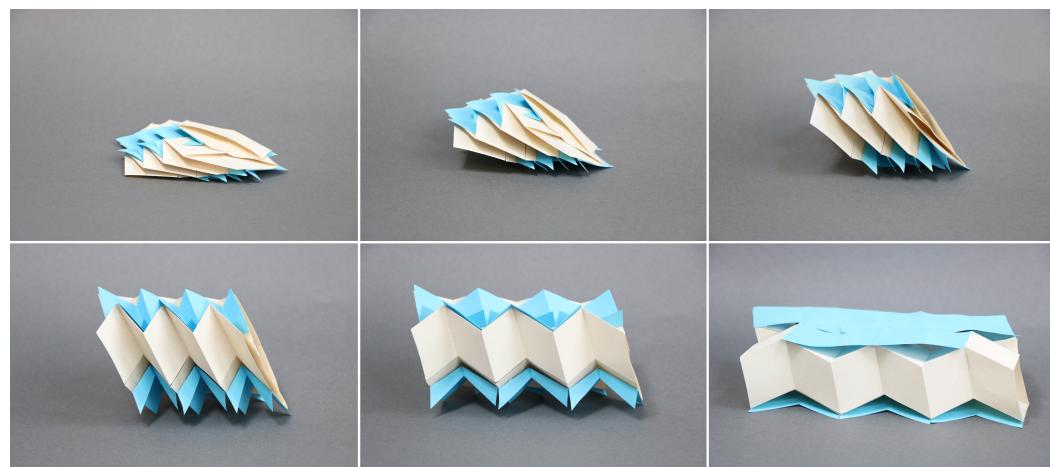


Figure 10. Model of asymmetric zipper-coupled tubes with a Miura-ori inspired smooth sheet attachment at different stages of unfolding; the nature of the deployment of the degree-four vertex cells is clearly observable on the bottom of the device. Parameters: $\alpha_1 = \frac{1}{3}\pi$, $\alpha_2 = \frac{5}{9}\pi$, $a = b = c$. Dimensions (inches): 4.9 by 3.3 when folded, 7.4 by 3.5 when unfolded.

Note that the smooth sheet cells protrude from the zipper-coupled tubes structure when folded. When gaps are tolerable and the folded state must be minimized for transportation, constraining the cells to fold up within the zipper-coupled tubes while maximizing surface area in the ideal state results in the smooth sheet attachment described previously [5]. Thus, the smooth sheet design can be tailored to the situation, much like zipper-coupled tubes themselves. To inform future applications of these structures, we suggest dynamic and quasi-static analyses. Constructing a device for architectural applications will likely require the use of thick origami and compliant hinges, and remote self-actuation via magnetism or heat could be useful in space or medical applications [13–15].

Miura-ori-inspired smooth sheet attachments enhance the utility of zipper-coupled tubes in various situations. The tubes are useful in architecture because they pack tight and deploy to a rigid state [4]; our gapless smooth sheet attachments improve existing designs by increasing drivability and walkability. If a local bridge collapses, for example, a prefabricated bridge based on zipper-coupled tubes with smooth sheet attachments can easily be transported on a single vehicle and swiftly deployed on-site to provide smooth, emergency transit. Space structures are another popular application of origami-inspired mechanisms—the Miura-ori pattern that the smooth sheet is based on is common in deployable space array design. Accommodating for material thickness, however, makes Miura-ori sheets challenging to deploy [16]. In contrast, a thin solar array constructed from Miura-ori inspired smooth sheet cells can deploy rigidly because it is supported by zipper-coupled tubes.

The design of smooth sheet attachments without gaps is key to the development of more versatile zipper-coupled tubes. We have communicated a clear design method for the origami-based structure, examining the mathematics of its motion in detail. By elucidating the possibility for further enhancements on the zipper-coupled tubes structure, we hope to spur many novel and exciting applications beyond those mentioned.

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Appendix A

Table A1. Defining the edges in Miura-ori based, smooth sheet attachments for a pair of asymmetric zipper-coupled tubes.

\mathcal{S}_1		\mathcal{S}_2		\mathcal{S}_3		\mathcal{S}_4	
$\overline{O_0P_0}$	$\overline{O_0P_0[1]}$	$\overline{O_1P_1}$	$\overline{O_2P_2}$	$\overline{O_4P_4}$	$\overline{O'_0P'_0}$	$\overline{O'_0P'_0[-1]}$	$\overline{O'_1P'_1}$
$\overline{O_3F_3}$	$\overline{O_3F_3[1]}$	$\overline{P_1Q_1}$	$\overline{P_2Q_2}$	$\overline{P_4Q_4}$	$\overline{O'_3F'_3}$	$\overline{O'_3F'_3[-1]}$	$\overline{P'_1Q'_1}$
$\overline{O_0O_3}$	$\overline{P_0F_3}$	$\overline{O_1O_2}$	$\overline{O_1O_4}$	$\overline{P_1P_2}$	$\overline{O'_0O'_3}$	$\overline{P'_0F'_3}$	$\overline{O'_1O'_2}$
$\overline{P_0[1]F_3[1]}$		$\overline{P_1P_4}$	$\overline{Q_1Q_2}$	$\overline{Q_1Q_4}$	$\overline{P'_0[-1]F'_3[-1]}$	$\overline{P'_1P'_4}$	$\overline{Q'_1Q'_2}$

Table A2. Defining the vertices in Miura-ori inspired smooth sheet attachments for a pair of asymmetric zipper-coupled tubes.

Vertex	Position	Vertex	Position
O_0	$-\boldsymbol{\epsilon} + \mathbf{u}$	O'_0	$\mathbf{s} - \bar{\boldsymbol{\epsilon}} + \bar{\mathbf{u}}$
O_1	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w} + \mathbf{r}$	O'_1	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}} + \bar{\mathbf{r}}$
O_2	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon}$	O'_2	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}}$
O_3	$-\boldsymbol{\epsilon} + \mathbf{u} - \mathbf{w}$	O'_3	$\mathbf{s} - \bar{\boldsymbol{\epsilon}} + \bar{\mathbf{u}} - \bar{\mathbf{w}}$
O_4	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w} + \mathbf{r} + \mathbf{f}$	O'_4	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}} + \bar{\mathbf{r}} + \bar{\mathbf{f}}$
P_0	$-\boldsymbol{\epsilon}$	P'_0	$\mathbf{s} - \bar{\boldsymbol{\epsilon}}$
P_1	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w}$	P'_1	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}}$
P_2	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u}$	P'_2	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}}$
P_4	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w} + \mathbf{h}$	P'_4	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}} + \bar{\mathbf{h}}$
Q_1	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w} + \mathbf{t}$	Q'_1	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}} + \bar{\mathbf{t}}$
Q_2	$\mathbf{a} + \mathbf{b} + \mathbf{c} + \boldsymbol{\epsilon}$	Q'_2	$\bar{\mathbf{a}} + \bar{\mathbf{b}} + \bar{\mathbf{c}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}}$
Q_4	$\mathbf{a} + \mathbf{c} + \mathbf{d} + \boldsymbol{\epsilon} - \mathbf{u} + \mathbf{w} + \mathbf{t} + \mathbf{g}$	Q'_4	$\bar{\mathbf{a}} + \bar{\mathbf{c}} + \bar{\mathbf{d}} + \mathbf{s} + \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{u}} + \bar{\mathbf{w}} + \bar{\mathbf{t}} + \bar{\mathbf{g}}$
F_3	\mathbf{c}	F'_3	$\bar{\mathbf{c}} + \mathbf{s}$
$F_3[1]$	$\mathbf{c} - \mathbf{b} + \mathbf{d}$	$F'_3[-1]$	$\bar{\mathbf{c}} + \mathbf{s} - \bar{\mathbf{b}} + \bar{\mathbf{d}}$
$P_0[1]$	$-\boldsymbol{\epsilon} - \mathbf{b} + \mathbf{d}$	$P'_0[-1]$	$\mathbf{s} - \bar{\boldsymbol{\epsilon}} - \bar{\mathbf{b}} + \bar{\mathbf{d}}$

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