



# Reactive Transport in the Hydrosphere

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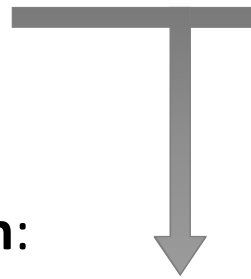
# Reaction-transport modeling

**Mass balance** equation:

$$\frac{\partial C}{\partial t} = -\frac{1}{A} \cdot \frac{\partial(A \cdot J)}{\partial x} + R$$

Expression for **transport flux**:

$$J = -D \frac{\partial C}{\partial x} + v \cdot C$$



**Reaction-transport equation:**

$$\frac{\partial C}{\partial t} = \frac{1}{A} \frac{\partial}{\partial x} \left( A \cdot D \cdot \frac{\partial C}{\partial x} \right) - \frac{1}{A} \frac{\partial}{\partial x} (A \cdot v \cdot C) + R$$

Modelling **early diagenesis** in aquatic sediments

- How to incorporate **porosity**?
- Modelling of **multiple components**



# Reaction-transport equation

**General form:**

$$\frac{\partial C}{\partial t} = \frac{1}{A} \frac{\partial}{\partial x} \left( A \cdot D \cdot \frac{\partial C}{\partial x} \right) - \frac{1}{A} \frac{\partial}{\partial x} (A \cdot v \cdot C) + R$$

assuming  $A \neq A(x)$

**Simplified form:**

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x} \left( D \cdot \frac{\partial C}{\partial x} \right) - \frac{\partial}{\partial x} (v \cdot C) + R$$

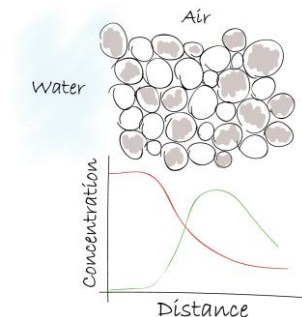
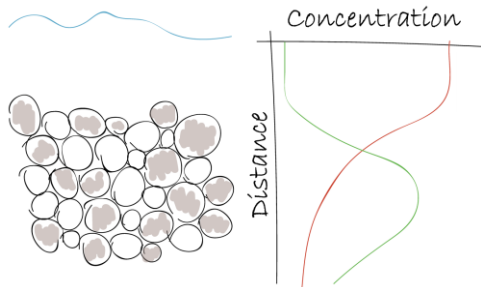
Rate of change

Diffusion term

Advection term

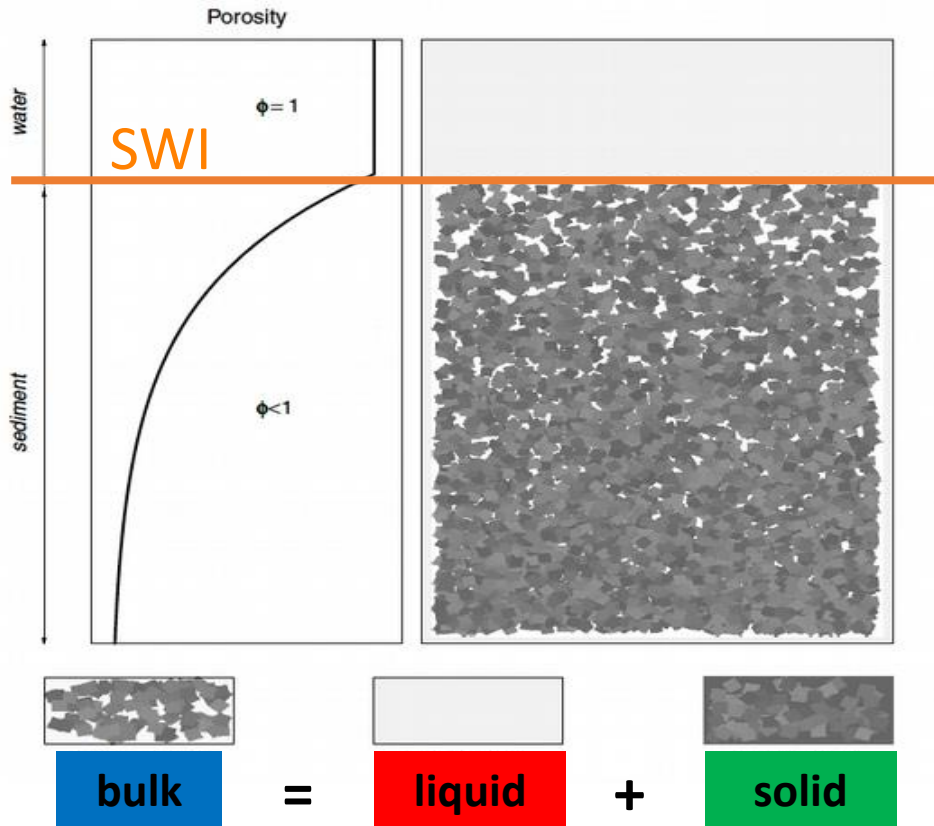
**Net** reaction term

**Solution:** A function of time and space:  $C(t,x)$



# Reaction-transport modeling in sediments

## Role of porosity



Porosity:

$$\phi = \frac{\text{liquid volume}}{\text{bulk volume}}$$

$$\text{unit} = \frac{m_L^3}{m_b^3}$$

Solid volume fraction :

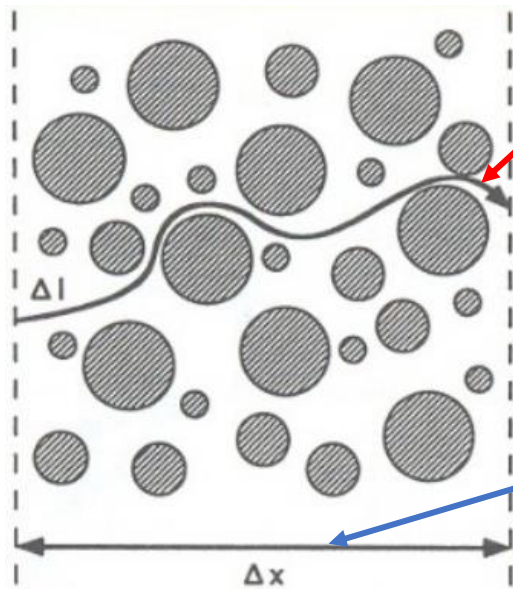
$$svf = \frac{\text{solid volume}}{\text{bulk volume}} = 1 - \phi$$

$$\text{unit} = \frac{m_s^3}{m_b^3}$$



# Reaction-transport modeling in sediments

## Role of porosity on molecular diffusion



True distance travelled

Tortuosity:  $\theta = \frac{\Delta l}{\Delta x}$   
(Path prolongation)

Effective distance travelled

Effective diffusion coefficient of solutes in porous media:

In bulk water

$$D_{eff} = \frac{D_{mol}}{\theta^2}$$

In sediments:

$$\theta^2 \approx 1 - \ln(\phi^2)$$

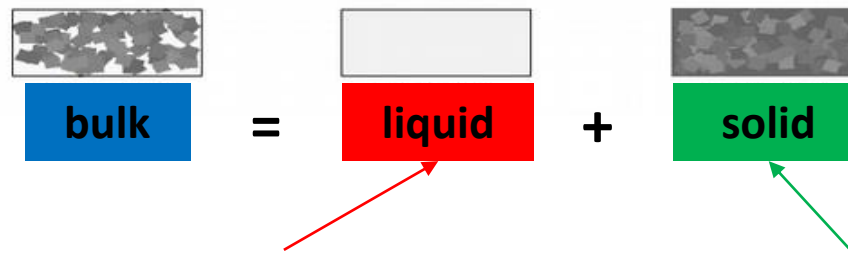
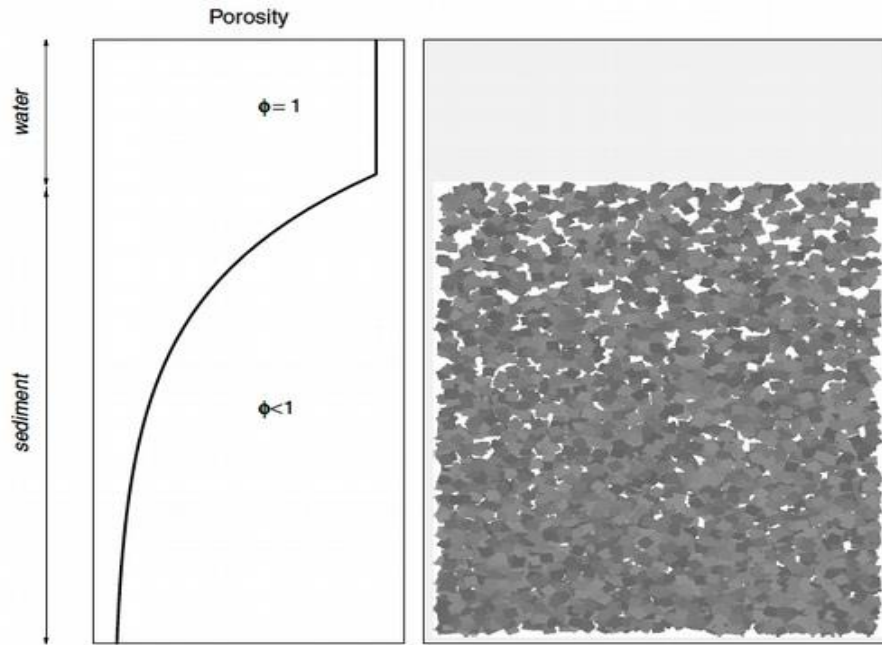


$$D_{sed} = \frac{D_{mol}}{1 - \ln(\phi^2)}$$



# Reaction-transport modeling in sediments

## Role of porosity on how we measure and report concentrations



Dissolved substances ( $C_L$ )

Solid substances ( $C_s$ )

Typically:

Dissolved substances ( $C_L$ )

**mol m<sup>-3</sup> of liquid**

Solid substances ( $C_s$ )

**mol m<sup>-3</sup> of solid**

= mol kg<sup>-1</sup> of dry solid

× **density** of bulk solid  
(kg m<sup>-3</sup> of solid)

# Reaction-transport modeling in sediments

## Role of porosity on the reaction-transport equation

Mass balance equation is formulated for:

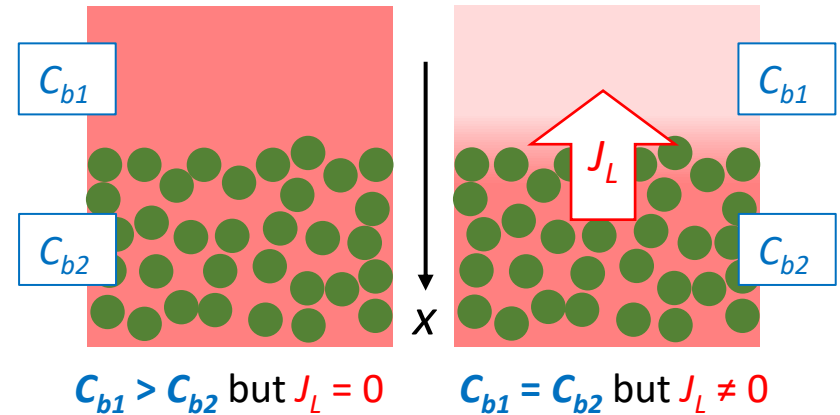
$$\frac{\partial C_b}{\partial t} = \dots \quad \leftarrow \text{mol m}^{-3} \text{ of bulk}$$

Transport fluxes of **solutes** are **determined** by concentrations in the **liquid phase**!

Not  $C_b$ !!!

$$J_L = v_L \cdot C_L - D_{sed} \frac{\partial C_L}{\partial x}$$

↑  
moles / **area of liquid phase** / time



If a reaction occurs between **solutes**:  $R_L$  ← moles / **volume of liquid phase** / time



# Conversions between liquid and bulk

Porosity:  $\phi = \frac{\text{liquid volume}}{\text{bulk volume}}$        $\text{unit} = \frac{m_L^3}{m_b^3}$

Conversion from liquid to bulk:

$$C_b = \phi \cdot C_L \qquad \frac{\text{mol}}{m_b^3} = \frac{m_L^3}{m_b^3} \cdot \frac{\text{mol}}{m_L^3}$$

$$J_b = \phi \cdot J_L \qquad \frac{\text{mol}}{\text{area}_b \cdot \text{time}} = \frac{m_L^3}{m_b^3} \cdot \frac{\text{mol}}{\text{area}_L \cdot \text{time}}$$

$$R_b = \phi \cdot R_L \qquad \frac{\text{mol}}{m_b^3 \cdot \text{time}} = \frac{m_L^3}{m_b^3} \cdot \frac{\text{mol}}{m_L^3 \cdot \text{time}}$$





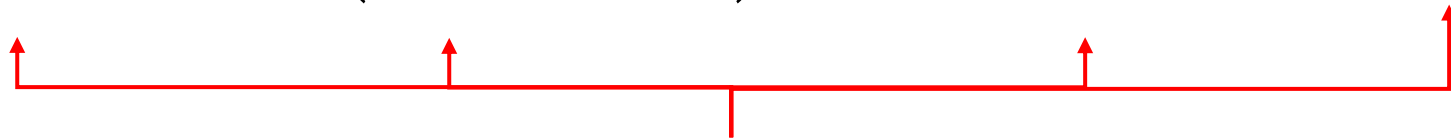
# Reaction-transport modeling in sediments

Reformulated for concentration in the liquid phase:

$$\frac{\partial C_b}{\partial t} = \frac{\partial(\Phi \cdot C_L)}{\partial t} = \frac{\partial}{\partial x} \left( \Phi \cdot D_{sed} \cdot \frac{\partial C_L}{\partial x} \right) - \frac{\partial}{\partial x} (\Phi \cdot v_L \cdot C_L) + \Phi \cdot R_L$$

assuming  $\Phi \neq \Phi(t)$

$$\frac{\partial C_L}{\partial t} = \frac{1}{\Phi} \cdot \frac{\partial}{\partial x} \left( \Phi \cdot D_{sed} \cdot \frac{\partial C_L}{\partial x} \right) - \frac{1}{\Phi} \cdot \frac{\partial}{\partial x} (\Phi \cdot v_L \cdot C_L) + R_L$$



All terms in mol m<sup>-3</sup> liquid s<sup>-1</sup>

Note:  $\phi$  changes in space (sediment compaction), so  $\phi$  cannot be taken out of the spatial derivative and cancelled out!



# Conversions between solid and bulk

Solid volume fraction:  $1 - \phi = \frac{\text{solid volume}}{\text{bulk volume}} \quad \text{unit} = \frac{m_s^3}{m_b^3}$

Conversion from liquid to bulk:

$$C_b = (1 - \phi) \cdot C_s \quad \frac{\text{mol}}{m_b^3} = \frac{m_s^3}{m_b^3} \cdot \frac{\text{mol}}{m_s^3}$$

$$J_b = (1 - \phi) \cdot J_s \quad \frac{\text{mol}}{\text{area}_b \cdot \text{time}} = \frac{m_s^3}{m_b^3} \cdot \frac{\text{mol}}{\text{area}_s \cdot \text{time}}$$

$$R_b = (1 - \phi) \cdot R_s \quad \frac{\text{mol}}{m_b^3 \cdot \text{time}} = \frac{m_s^3}{m_b^3} \cdot \frac{\text{mol}}{m_s^3 \cdot \text{time}}$$



# Reaction-transport modeling in sediments

Reformulated for porous media (sediments), assuming  $\phi \neq \phi(t)$ :

$$\frac{\partial C_f}{\partial t} = \frac{1}{f} \cdot \frac{\partial}{\partial x} \left( f \cdot D_f \cdot \frac{\partial C_f}{\partial x} \right) - \frac{1}{f} \cdot \frac{\partial}{\partial x} (f \cdot v_f \cdot C_f) + R_f$$

For dissolved substances:

$$f = \phi \quad C_f = C_L \quad D_f = D_{sed} \quad v_f = v_L$$

For concentrations of solids:

$$f = 1 - \phi \quad C_f = C_S \quad D_f = D_S \quad v_f = v_S$$

Note:  $\phi$  changes in space (sediment compaction), so **f cannot** be taken out of the spatial derivative and cancelled out!



# Reaction-transport modeling in sediments

Modeling multiple components:

Component **A**: 
$$\frac{\partial C_A}{\partial t} = \frac{1}{f_A} \cdot \frac{\partial}{\partial x} \left( f_A \cdot D_A \cdot \frac{\partial C_A}{\partial x} \right) - \frac{1}{f_A} \cdot \frac{\partial}{\partial x} (f_A \cdot v_A \cdot C_A) + R_A$$

Component **B**: 
$$\frac{\partial C_B}{\partial t} = \frac{1}{f_B} \cdot \frac{\partial}{\partial x} \left( f_B \cdot D_A \cdot \frac{\partial C_B}{\partial x} \right) - \frac{1}{f_B} \cdot \frac{\partial}{\partial x} (f_B \cdot v_A \cdot C_B) + R_B$$

⋮

⋮

⋮

If **A** and **B** react with each other, then  $R_A$  and  $R_B$  are **not independent!**

**Coupled** partial differential equations!!

How do we deal with the situation if **A** is a **dissolved** substance  
and **B** is a **solid** substance?



# Rate expressions for processes involving solute and solid substances



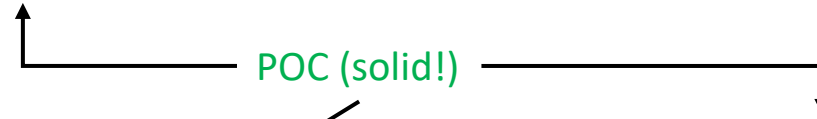
Rate expression:  $R = r_c \frac{[\text{O}_2]}{[\text{O}_2] + K_{\text{O}_2}} [\text{OM}]$

Units:  $[\text{OM}]: \frac{\text{mol C}}{\text{m}_s^3}$        $R: \frac{\text{mol C}}{\text{m}_s^3 \cdot \text{s}}$

Mass balance equation for OM:  $\frac{d[\text{OM}]}{dt} = -R + \dots$  ✓



# Rate expressions for processes involving solute and solid substances



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Mass balance equation for OM:  $\frac{d[\text{OM}]}{dt} = -R + \dots$  ✓

Mass balance equation for  $\text{O}_2$ :  $\frac{d[\text{O}_2]}{dt} = -R + \dots$  Units:  $[\text{O}_2]: \frac{\text{mol O}_2}{\text{m}_L^3}$        $R: \frac{\text{mol C}}{\text{m}_s^3 \cdot \text{s}}$

Based on stoichiometry



# Rate expressions for processes involving solute and solid substances



Rate expression:  $R = r_c \frac{[\text{O}_2]}{[\text{O}_2] + K_{\text{O}_2}} [\text{OM}]$  Units:  $[\text{OM}]: \frac{\text{mol C}}{\text{m}_s^3}$   $R: \frac{\text{mol C}}{\text{m}_s^3 \cdot \text{s}}$

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Based on stoichiometry

Based on stoichiometry & volume fraction correction!

$$\frac{d[\text{O}_2]}{dt} = -R \cdot \frac{1 - \phi}{\phi} + \dots$$

Units:  $\frac{\text{mol}}{\text{m}_L^3 \cdot \text{s}} = \frac{\text{mol}}{\text{m}_s^3 \cdot \text{s}} \cdot \frac{\text{m}_s^3}{\text{m}_b^3} \cdot \frac{\text{m}_b^3}{\text{m}_L^3}$



# Reaction-transport modeling in sediments

$$\frac{\partial C_f}{\partial t} = \frac{1}{f} \cdot \frac{\partial}{\partial x} \left( f \cdot D_f \cdot \frac{\partial C_f}{\partial x} \right) - \frac{1}{f} \cdot \frac{\partial}{\partial x} (f \cdot v_f \cdot C_f) + R_f$$

To formulate . . .

- For **dissolved** substances:  $f = \phi$        $C_L$  &  $R_L$       per m<sup>3</sup> of **liquid**!
- For **solid** substances:  $f = 1 - \phi$        $C_s$  &  $R_s$       per m<sup>3</sup> of **solid**!

**Do not forget** to account for porosity in the rate expressions for processes that involve **reactions of dissolved and solid substances**:

$$\frac{1 - \phi}{\phi} \left( \frac{m_s^3}{m_L^3} \right) \quad \text{vs.} \quad \frac{\phi}{1 - \phi} \left( \frac{m_L^3}{m_s^3} \right)$$







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