

Last Time:

- Calculus of Variations Pt. 2
- Dynamics from Energy
- Lagrangian Mechanics
- Least-Action Principle

Today:

- Interpretation of Least Action
- Manipulator Equation
- Non-Conservative
- Constraints + Coordinates

### Interpreting Least Action:

- Last time we saw the EL equation:

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = 0$$

- Is the FON condition for:

$$\min_{q(t)} S = \int_{t_0}^{t_f} \underbrace{L(q, \dot{q})}_{\text{Lagrangian}} dt$$

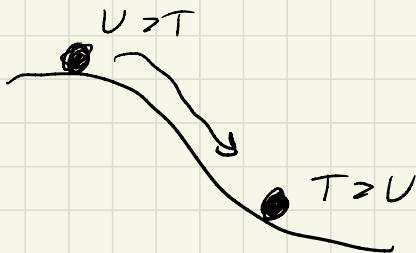
- If we define  $L = T - U$ , this gives:

$$\min_{q(t)} \left[ \int_{t_0}^{t_f} \underbrace{T(q, \dot{q})}_{\approx \text{Avg. Kinetic Energy}} dt \right] - \left[ \int_{t_0}^{t_f} \underbrace{U(q)}_{\approx \text{Avg. Potential Energy}} dt \right]$$

$\approx$  Avg. Kinetic  
Energy

$\approx$  Avg. Potential  
Energy

- System is conservative  $\Rightarrow$  can only trade  $V$  for  $T$  and vice-versa.
- Think about a ball rolling down hill:



- $V$  decreases,  $T$  increases  
 $\Rightarrow$  Dynamics tries to bring average  $V$  and  $T$  closer together.

- At a minimum of the action, we have:

$$\underbrace{\frac{d}{dq} \left[ \int_{t_0}^{t_f} T(q, \dot{q}) dt \right]}_{\text{Change in kinetic energy}} = \underbrace{\frac{d}{dq} \left[ \int_{t_0}^{t_f} V(q) dt \right]}_{\text{Change in Potential energy}}$$

- This is basically a re-statement of conservation of energy.
- This is only true at a local min of  $S$   
 $\Rightarrow$  True physical trajectories must minimize the action.

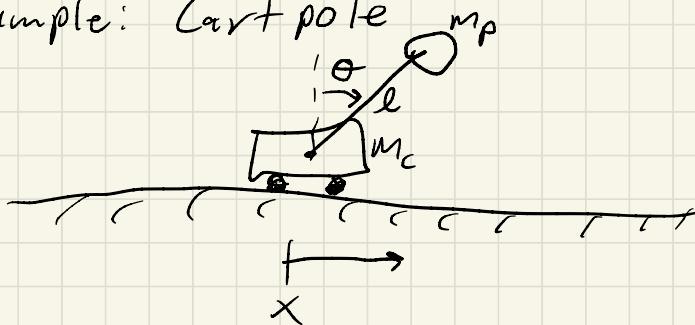
# The Manipulator Equation:

- All mechanical systems have a Lagrangian of the form:

$$L = T - U = \frac{1}{2} \dot{q}^T \underbrace{M(q)}_{\text{Mass Matrix}} \dot{q} - U(q)$$

"Generalized Inertia Tensor"

\* Example: Cart pole



Pole mass position:  $\begin{bmatrix} x + l \sin(\theta) \\ l \cos(\theta) \end{bmatrix}$

$$U = m_p g l \cos(\theta)$$

$$T = \frac{1}{2} m_c \dot{x}^2 + \frac{1}{2} m_p \begin{bmatrix} \dot{x} + l \cos(\theta) \dot{\theta} \\ -l \sin(\theta) \dot{\theta} \end{bmatrix}^T \begin{bmatrix} \cdot \\ \cdot \end{bmatrix}$$

$$= \frac{1}{2} (m_c + m_p) \dot{x}^2 + \frac{1}{2} m_p l^2 \dot{\theta}^2 + m_p \dot{x} l \cos(\theta) \dot{\theta}$$

$$T = \frac{1}{2} \begin{bmatrix} \dot{x} \\ \dot{\theta} \end{bmatrix}^T \underbrace{\begin{bmatrix} (m_c + m_p) & m_p l \cos(\theta) \\ m_p l \cos(\theta) & m_p l^2 \end{bmatrix}}_{M(q)} \begin{bmatrix} \dot{x} \\ \dot{\theta} \end{bmatrix}$$

- Let's plug this into EL equation:

$$L = \frac{1}{2} \dot{q}^T M(q) \dot{q} - V(q)$$

$$\Rightarrow \left\{ \begin{array}{l} \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) = \frac{d}{dt} (M(q) \dot{q}) = M(\dot{q}) \ddot{q} + \dot{M}(q) \dot{q} \\ \frac{\partial L}{\partial q} = -\frac{\partial V}{\partial q} + \frac{\partial}{\partial q} \left( \frac{1}{2} \dot{q}^T M(q) \dot{q} \right) \end{array} \right.$$

$$\Rightarrow M(q) \ddot{q} + \underbrace{\left[ \dot{M}(q) \dot{q} - \frac{\partial}{\partial q} \left( \frac{1}{2} \dot{q}^T M(q) \dot{q} \right) \right]}_{C(q, \dot{q})} + \frac{\partial V}{\partial q} = 0$$

"Coriolis term"  
(from  $\dot{q}$ -dependence of  $M$ )

$G(q)$   
"potential terms"

$$\Rightarrow M(q) \ddot{q} + C(q, \dot{q}) + G(q) = 0$$

"Manipulator Equation"

- Super common in robotics. Used in most dynamics software.
- Just a re-statement of EL eqn.
- Sometimes you will see:

$C(q, \dot{q})$   $\dot{q}$  ← this is not unique  
matrix

- Sometimes you'll see  $C(q\dot{q})$  include both Coriolis and potential. Called "dynamic bias" term.
- Manipulator form nicely shows worst-case computational complexity of computing dynamics:

$$\ddot{\vec{q}} = -M(\vec{q})^{-1} \underbrace{(C(q\dot{q}) + G(\vec{q}))}_{}$$

Solving an  $n \times n$  linear system  
 $\mathcal{O}(n^3)$

- 
- There's more to say about this ...

Example: Cartpole

$$L = \frac{1}{2}(m_c + m_p) \dot{x}^2 + m_p \dot{x} l \cos(\theta) \dot{\phi} + \frac{1}{2} m_p l^2 \dot{\phi}^2$$

$$\begin{aligned} \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}_i} \right) - \frac{\partial L}{\partial q_i} &= \begin{bmatrix} (m_c + m_p) & m_p l \cos(\theta) \\ m_p l \cos(\theta) & m_p l^2 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{\phi} \end{bmatrix} \\ &\quad + \begin{bmatrix} -m_p l \dot{\phi}^2 \sin(\theta) \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ -m_p g l \sin(\theta) \end{bmatrix} = 0 \end{aligned}$$

$M(\vec{q})$        $-m_p l \cos(\theta)$   
 $(\vec{q}, \dot{\vec{q}})$        $G(\vec{q})$

## Non-Conservative Forces:

- Conservative forces coming from  $F_C = -\nabla U$  are already included in the L eqn.
- From  $F = ma$ , we can guess what should happen with other forces:

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = F \quad \text{"Generalized Forces"}$$

$M(q)\ddot{q} + C(q, \dot{q}) + F(q) = F \quad \text{(defined in } q \text{ coordinates)}$

- From  $F_C = -\nabla U$  we know we need a term inside S that "integrates F" whose variational derivative w.r.t.  $q(t)$  is  $F$ :

$$\Rightarrow \frac{d}{dq(t)} \left[ \int_{t_0}^{t_f} L(q, \dot{q}) + F(q)^T q(t) dt \right] = 0$$

note that this is not a function of  $q(t)$ , just  $t$ .

$$\Rightarrow \int_{t_0}^{t_f} D_1 L(q, \dot{q}) \delta q + D_2 L(q, \dot{q}) \delta \dot{q} + F^T \delta q dt$$

$$\Rightarrow \int_{t_0}^{t_f} D_1 L(q, \dot{q}) \delta q - \frac{d}{dt} (D_2 L(q, \dot{q})) \delta q + F^T \delta q dt$$

$$\Rightarrow \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = F$$

- This is called "Lagrange-D'Alembert Principle" or "Principle of virtual work".
- The non-conservative term has units of work (force  $\times$  distance):

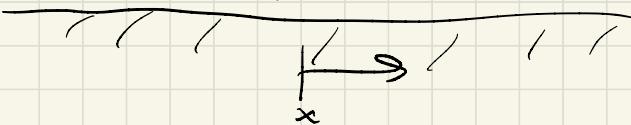
$$W = \int_{t_0}^{t_f} \mathbf{F}(t)^\top \mathbf{q}(t) dt$$

- Variational derivative of this term:

$$\delta W = \int_{t_0}^{t_f} \underbrace{\mathbf{F} \cdot \delta \mathbf{q}}_{\text{"Virtual work"} dt} \underbrace{\mathbf{q}}_{\text{"Virtual displacement"}}$$

$\Rightarrow$  Cartpole:

- Assume we have a motor that applies  $f_c$  to cart



$$M(x, \theta) \begin{bmatrix} \ddot{x} \\ \ddot{\theta} \end{bmatrix} + (\mathbf{q}\dot{\theta}) + \mathbf{G}(\theta) = \begin{bmatrix} f_c \\ 0 \end{bmatrix}$$

## Constraints + coordinates:

- So far we've been dealing with minimal coordinates.
- Often dynamics can be simpler with more coordinates.
- Now we have to deal with constraints to remove "fake" degrees of freedom.
- We've already seen how to handle constraints in the EL equation:

$$\min_{q(t)} \int_{t_0}^{t_f} L(q, \dot{q}) dt$$

$$\text{s.t. } C(q) = 0$$

$$\Rightarrow \frac{\partial}{\partial q(t)} \left[ \int_{t_0}^{t_f} L(q, \dot{q}) + \lambda^T(t) C(q) dt \right] = 0$$

$$\Rightarrow \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} - \lambda^T \frac{\partial C}{\partial q} = 0 \quad (\text{and } C(q)=0)$$

↑      ↗
"constraint force"
"constraint Jacobian"
  
 $J(q)$

$$\Rightarrow M(q)\ddot{q} + C(q, \dot{q}) + \lambda^T J(q) = F + \lambda^T J^T(q)$$

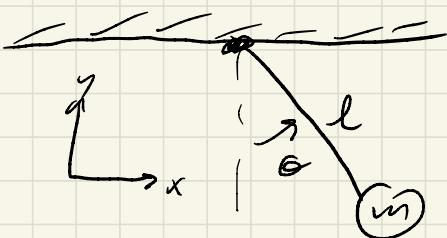
- We have to solve for both  $\ddot{q}$  and  $\lambda$  now
- To do this, differentiate  $C(q)$  twice w.r.t. time:

$$\frac{d^2 C}{dt^2} = \frac{d}{dt} \left( \frac{\partial C}{\partial q} \dot{q} \right) = J(q) \ddot{q} + \frac{\partial}{\partial q} (J(q) \dot{q}) \dot{q} = 0$$

- Now we can combine the acceleration constraint with the dynamics:

$$\begin{bmatrix} M(q) & -J(q)^T \\ J(q) & 0 \end{bmatrix} \begin{bmatrix} \ddot{q} \\ \lambda \end{bmatrix} = \begin{bmatrix} -C(q, \dot{q}) - b(q) \dot{q} + F \\ -\frac{\partial}{\partial q} (J(q) \dot{q}) \dot{q} \end{bmatrix}$$

\* Example: Pendulum



$$L = \frac{1}{2} m(\dot{x}^2 + \dot{y}^2) - mg y$$

$$C(x, y) = x^2 + y^2 - l^2 = 0$$

$$\underbrace{\begin{bmatrix} m & 0 \\ 0 & m \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}}_{M} + \begin{bmatrix} 0 \\ mg \end{bmatrix} = \underbrace{\begin{bmatrix} z_x \\ z_y \end{bmatrix}}_{J(q)^T} \lambda$$

$$\frac{d^2 C}{dt^2} = \frac{d}{dt} (J(q) \dot{q}) = \frac{d}{dt} ([z_x \ z_y] \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}) = [z_x \ z_y] \begin{bmatrix} \ddot{x} \\ \ddot{y} \end{bmatrix} + 2(z_x^2 + z_y^2) = 0$$

$$\Rightarrow \begin{bmatrix} M & -J_{(q)}^T \\ J_{(q)} & 0 \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{y} \\ \ddot{z} \end{bmatrix} = \begin{bmatrix} 0 \\ -mg \\ -2(\dot{x}^2 + \dot{y}^2) \end{bmatrix}$$