

Last Time:

- Stability of spinning bodies
- Numerical simulation w/ 3D Rotation

Today:

- Newton-Euler dynamics
- SE(3) group
- Quadrotors
- Airplanes

Newton-Euler Dynamics

- full translation + rotation dynamics for a rigid body
- combine $F = ma$ and Euler's equation

$$\frac{m^N v}{J_{\text{C}^N}^B} + \dot{\theta}_B^N \times J_{\text{C}^N}^B = \mathbf{F}$$

- Still some options. Two common choices of state:

$$x = \begin{bmatrix} {}^N r \\ {}^N q^B \\ {}^N V \\ {}^B \omega \end{bmatrix} \leftarrow \begin{array}{l} \text{position } (N \text{ frame}) \\ \leftarrow \text{ attitude } (B \rightarrow N) \\ \leftarrow \text{ velocity } (N \text{ frame}) \\ \leftarrow \text{ angular velocity } (B \text{-frame}) \end{array}$$

$$x = \begin{bmatrix} {}^N r \\ {}^N q^B \\ {}^B V \\ {}^B \omega \end{bmatrix} \leftarrow \begin{array}{l} {}^N r \\ {}^B V \\ \leftarrow \text{velocity } (B \text{-frame}) \end{array}$$

- For simulation really doesn't matter, but for control + estimation The 2nd one is often preferred.

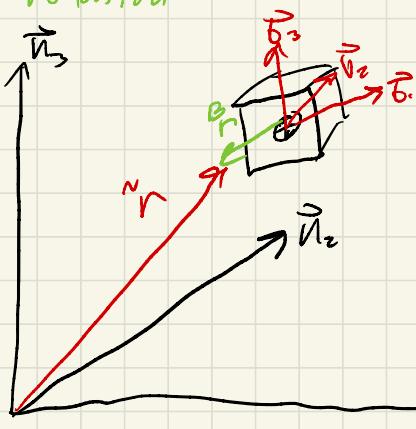
* Special Euclidean Group SE(3)

- Matrix Representation

$${}^N T^B = \begin{bmatrix} {}^N Q^B & {}^N d \\ 0 & 1 \end{bmatrix}$$

rotation

COM translation



$$\begin{bmatrix} {}^N Q^B & {}^N d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} {}^B r \\ 1 \end{bmatrix} = \begin{bmatrix} {}^B r \\ 1 \end{bmatrix}$$

- SE(3) Kinematics / Velocity:

$$\begin{aligned} T' &= T \Delta T = \begin{bmatrix} {}^N Q^B & {}^N d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \Delta Q & \Delta d \\ 0 & 1 \end{bmatrix} \\ &= \underbrace{\begin{bmatrix} Q O Q & 0 \\ 0 & 1 \end{bmatrix}}_{SO(3)} \underbrace{\begin{bmatrix} {}^N Q^B \Delta d \\ 1 \end{bmatrix}}_{\text{in } B \text{ frame!}} + \begin{bmatrix} {}^N d \\ 1 \end{bmatrix} \end{aligned}$$

Δd is in B frame!

- Taylor expand to 1st order:

$$OQ = \exp(\hat{\omega} h) \approx I + h \hat{\omega}$$

$$\text{od} \approx h^B V$$

$$\Rightarrow T' \approx \begin{bmatrix} Q & d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} (I + h \hat{\omega}) & h^B V \\ 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} Q + h Q^B \hat{\omega} & h Q^B V + d \\ 0 & 1 \end{bmatrix}$$

$$= \underbrace{\begin{bmatrix} Q & d \\ 0 & 1 \end{bmatrix}}_T + h \underbrace{\begin{bmatrix} Q & d \\ 0 & 1 \end{bmatrix}}_{\text{T}} \underbrace{\begin{bmatrix} \hat{\omega} & ^B V \\ 0 & 1 \end{bmatrix}}_{\hat{\omega}}$$

- Take limit: $h \rightarrow 0$

$$\underbrace{I' - I}_h \approx \dot{T} = T \hat{\omega}$$

that map for $se(3)$

$$w = \begin{bmatrix} {}^B V \\ \hat{\omega} \end{bmatrix} \in \mathbb{R}^6 \text{ is the Lie algebra } se(3)$$

- As with $SO(3)$, for constant w , we have

$$T(t) = T_0 \exp(t \hat{\omega})$$

* Full Newton-Euler Dynamics on SE(3)

$$\dot{\vec{x}} = \begin{bmatrix} {}^N\vec{r} \\ \dot{\vec{q}} \\ {}^B\vec{v} \\ {}^B\vec{\omega} \end{bmatrix} = \begin{bmatrix} {}^Q{}^B\vec{V} \\ \frac{1}{m} {}^L(q) H^B \vec{w} \\ \frac{1}{m} {}^B\vec{F} - {}^B\vec{\omega} \times {}^B\vec{V} \\ \mathcal{T}^{-1} ({}^B\vec{\gamma} - {}^B\vec{\omega} \times \mathcal{T}{}^B\vec{\omega}) \end{bmatrix}$$

$${}^N\vec{V} = {}^Q{}^B\vec{V} \Rightarrow {}^N\dot{\vec{V}} = \dot{{}^Q{}^B\vec{V}} + {}^Q{}^B\vec{\dot{V}} = {}^Q{}^B\vec{\omega} {}^B\vec{V} + {}^Q\vec{\dot{V}} = \frac{1}{m} {}^N\vec{F}$$

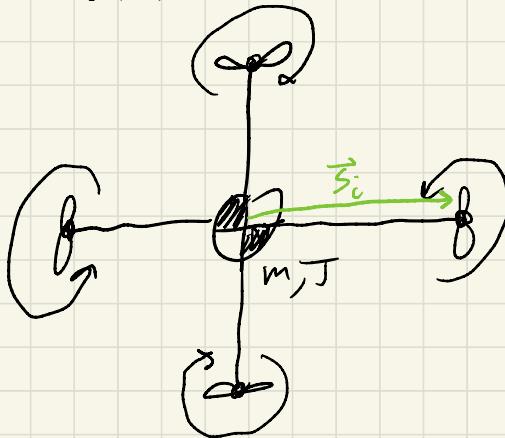
$$\Rightarrow \boxed{{}^B\dot{\vec{V}} = \frac{1}{m} {}^Q{}^T {}^N\vec{F} - {}^B\vec{\omega} \times {}^B\vec{V} = \frac{1}{m} {}^B\vec{F} - {}^B\vec{\omega} \times {}^B\vec{V}}$$

- Similarly, ${}^N\vec{V}$ instead of ${}^B\vec{V}$:

$$\dot{\vec{x}} = \begin{bmatrix} {}^N\vec{r} \\ \dot{\vec{q}} \\ {}^N\vec{v} \\ {}^B\vec{\omega} \end{bmatrix} = \begin{bmatrix} {}^N\vec{V} \\ \frac{1}{2} {}^L(q) H^B \vec{w} \\ \frac{1}{m} {}^N\vec{F} \\ \mathcal{T}^{-1} ({}^B\vec{\gamma} - {}^B\vec{\omega} \times \mathcal{T}{}^B\vec{\omega}) \end{bmatrix}$$

- Now we just need to compute F and \mathcal{Q} to simulate any rigid-body system.

Quadrrotors:



- Each prop exerts a force (thrust) in \vec{F}_i direction and torque surface $\pm \vec{\tau}_i$ direction due to drag

$$F_i = K_T u_i, \quad \tau_i = K_m u_i$$

"Thrust coefficient" "moment coefficient"

- Since F and τ are linear in $u \in \mathbb{R}^n$ we can write this as a matrix:

$${}^B F = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ u_1 & u_2 & u_3 & K_T \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} + Q^T \begin{bmatrix} 0 \\ 0 \\ -mg \end{bmatrix}$$

(
)
 gravity in
body frame

- Remember we also get $S_i \times F$ torque due to props being offset from C.M.:

$${}^B \tau = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ K_m & -K_m & K_m & -K_m \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} + \sum_i {}^B S_i \times \begin{bmatrix} 0 \\ 0 \\ K_T \end{bmatrix} u_i$$

- Assuming \mathbf{b}_S 's are aligned with \mathbf{b}_T axes:

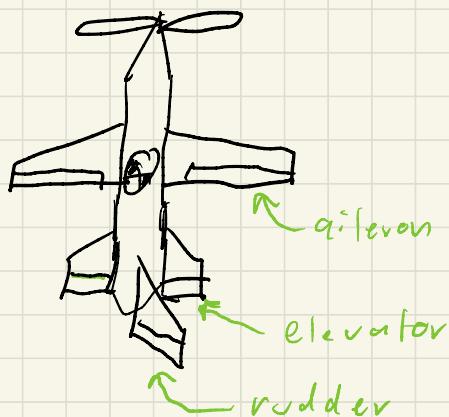
$$\mathbf{s}_1 = \begin{bmatrix} s_1 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{s}_2 = \begin{bmatrix} 0 \\ s_2 \\ 0 \end{bmatrix} \quad \mathbf{s}_3 = \begin{bmatrix} -s_3 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{s}_4 = \begin{bmatrix} 0 \\ -s_4 \\ 0 \end{bmatrix}$$

$$\Rightarrow \mathbf{B}_T = \begin{bmatrix} 0 & s_{KT} & 0 & -s_{KT} \\ -s_{KT} & 0 & s_{KT} & 0 \\ 0 & 0 & 0 & -K_m \\ K_m & -K_m & K_m & -K_m \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix}$$

- Now just plug into Newton-Euler dynamics.

- Note we ignored lots of aerodynamics; body drag, wake/boundary effects. These start to matter if you go fast and/or near walls/floor.

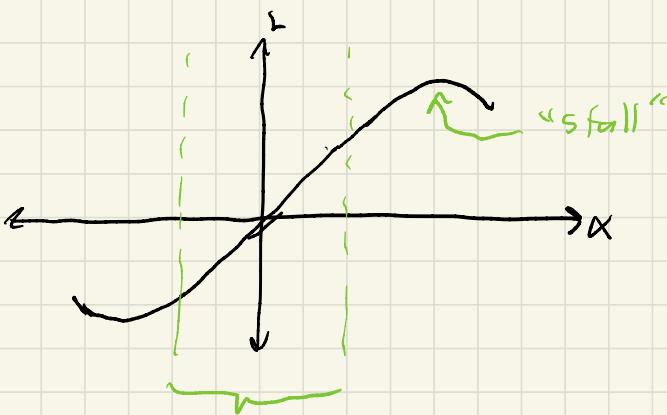
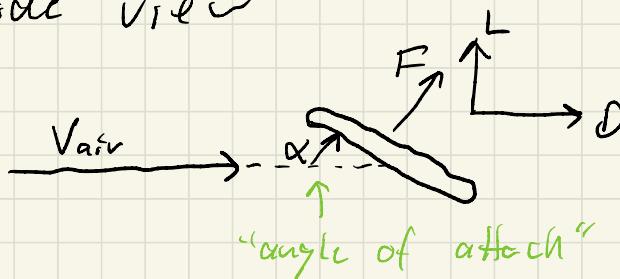
* Airplane:



$$\mathbf{u} = \begin{bmatrix} \text{throttle} \\ \text{aileron} \\ \text{elevator} \\ \text{rudder} \end{bmatrix} \in \mathbb{R}^4$$

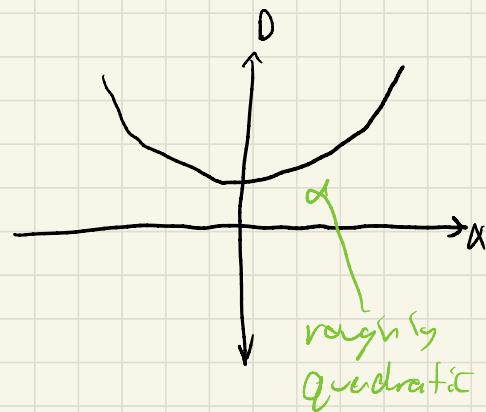
- Prop model is same as quadrotor
- Each lifting surface (wings, horizontal + vertical stabilizers) generate lift + drag:

side view



Linear region

$\approx \pm 10^\circ$



- For most applications, we can use linear approximations of $L(\alpha)$ and quadratic approximations of $D(\alpha)$

$$L \approx \frac{1}{2} \rho A v^2 C_L \alpha$$

Annotations for the equation:
 air density → ρ
 wing area → A
 velocity → v
 lift coefficient → C_L
 angle of attack → α

$$D \approx \frac{1}{2} \rho A V^2 [C_{D_0} + C_{D_2} \alpha^2]$$

↑
 Drag
 Coefficient

- Flaps just change effective α :

$$\alpha_{\text{eff}} = \alpha + \sum_i \epsilon_i \gamma_i$$

control input
 = flap deflection
 angle
 "flap effectiveness"

- Now just add up forces + torques from all lifting surfaces + prop
- Model breaks at high α (e.g. aerofastics)
- Also need to include prop wash
- * Other common (single) rigid-body systems

- Underwater robots
- Spacecraft
- Wheeled vehicles / cars
- Caged robots