Control & Estimation of Electrochemical Model-based Battery Management Systems

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April 6, 2012
Robert Bosch LLC
Research and Technology Center
Palo Alto, CA

Outline

- About Me
- PHEV Power Management
 - Models
 - Stochastic Optimal Control
 - Sample Results
- SOC/SOH Estimation
 - Single Particle Model
 - State Estimation via PDE Backstepping
 - Parameter Identification via Adaptive & Nonlinear Control
- 4 Outlook on Collaborative Efforts with Bosch

About Me: Education & Work Experience

Education

- Postdoctoral Fellow UC San Diego (July 2011 June 2013)
- Ph.D. & M.S.E. University of Michigan (Sept 2006 Apr 2011)
- B.S. UC Berkeley (Aug 2002 June 2006)

all in Mechanical Engineering

Industrial Work Experience

- DaimlerChrysler Corp Electrical Engineering (June 2006 Aug 2006)
- Ford Motor Company Manufacturing (June 2005 Aug 2005)
- Southern California Edison Staff Engineering (June 2004 Aug 2004)

About Me: Publications

Authored 20 peer-reviewed publications in energy systems and control

- Offline Parameter Identification of Electrochemical Models [ACC11, JPS]
- Charge Un-balancing in Battery Packs [DSCC09, IEEE TIE]
- Sensor Placement, Estimation, & Control of Battery Pack Thermal Dynamics [CDC12]
- Optimal PEV Charging on the Grid [DSCC10, JPS]
- Extremum Seeking with Application to Photovoltaic Systems [ACC09, IEEE TEC]
- Optimal Boundary Control of PDEs via Weak Variations [ACC11, ASME JDSMC]



About Me: Honors

- UC Presidential Postdoctoral Fellowship
- NSF Graduate Student Fellowship
- University of Michigan Distinguished Dissertation Honorable Mention
- University of Michigan Distinguished Leadership Award
- Best Student Paper Finalist
 - 2011 American Control Conference
 - 2009 ASME Dynamic Systems and Control Conference
- SHPE Conference Best Paper Award

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Open Problems in Battery Systems and Control

Cell Level

- Modeling & Design
- Optimal Control under Constraints
- SOC/SOH Estimation
- ...

Pack Level

- Change (Un)balancing
- Thermal Management
- Energy Management
- ...

Smart-Grid Level

- Renewable Energy Integration
- Optimal Power Flow
- PEV Power Management
- **.**...

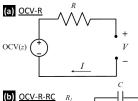


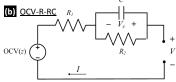


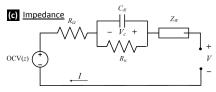


Battery Models

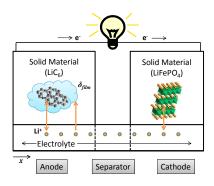
Equivalent Circuit Model







Electrochemical Model



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PHEV Power Management

Problem Statement

Design a supervisory control algorithm for plug-in hybrid electric vehicles (PHEVs) that splits engine and battery power in some optimal sense.



J. Voelcker, "Plugging Away in a Prius," IEEE Spectrum, vol. 45, pp. 30-48, 2008.



A Short History

Heuristic algorithms

A Short History

- Heuristic algorithms
- Rizzoni (2004) Equivalent Consumption Minimization Strategy
- Peng & Grizzle (2004) Deterministic Dynamic Programming
- Peng & Grizzle (2007) Stochastic Dynamic Programming
- Bemporad / Vahidi / Kolmanovsky (2010) Model Predictive Control

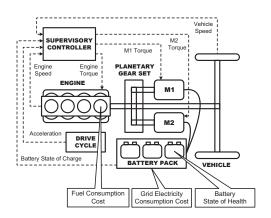
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- Moura (2011) SDP with Electrochemical Battery Model for Health

Power-Split PHEV Model

Ex: Toyota Prius, Ford Escape Hybrid

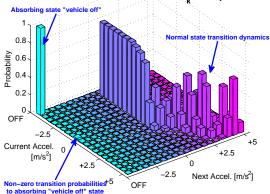
- Control Inputs
 - Engine Torque
 - M1 Torque
- State Variables
 - Engine speed
 - Vehicle speed
 - Battery SOC
 - Vehicle acceleration (Markov Chain)



State transition dynamics

$$p_{ijm} = \Pr(a_{k+1} = j | a_k = i, v_k = j)$$

Transition Probabilities for $v_{L} = 0$ mph

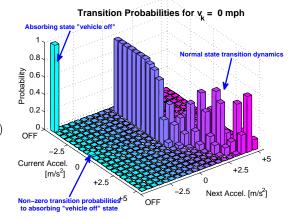


State transition dynamics

$$p_{ijm} = \Pr(a_{k+1} = j | a_k = i, v_k = j)$$

Transition to "vehicle off," denoted $a_{k+1} = t$

$$p_{itm} = \Pr(a_{k+1} = t | a_k = i, v_k = 0)$$



State transition dynamics

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Absorbing state "vehicle off"

$$1 = \Pr(a_{k+1} = t | \mathbf{a_k} = \mathbf{t}, v_k = 0)$$

Transition Probabilities for v = 0 mph Absorbing state "vehicle off" Normal state transition dynamics Probability 0.2 OFF Current Accel. +2.5 [m/s²] -2.5 Next Accel, [m/s²] Non-zero transition probabilit OFF to absorbing "vehicle off" state

State transition dynamics

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Transition Probabilities for v = 0 mph Absorbing state "vehicle off" Normal state transition dynamics Probability 9.0 0.2 OFF Current Accel. +2.5 [m/s²] Next Accel, [m/s2] Non-zero transition or OFF to absorbing "vehicle off" state

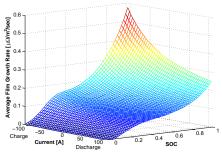
Identification data:

federal certification cycles, "naturalistic" driving data, 2009 NHTS

Two Battery Health Model Case Studies

Anode-side SEI Layer Growth

 Resistive film layer at solid/electrolyte interface

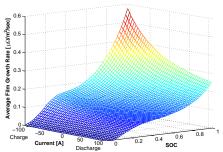


Ramadass, Haran, White, Popov (2003)

Two Battery Health Model Case Studies

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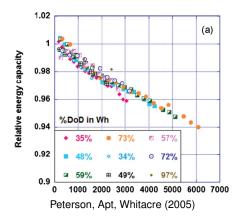
 Resistive film layer at solid/electrolyte interface



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Charge Processed

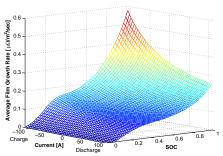
 \bullet Capacity fade \propto Ah into/out of cell



Two Battery Health Model Case Studies

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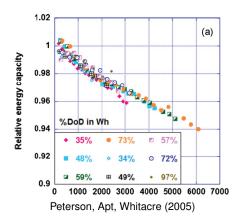
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Charge Processed

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^{*}Degradation depends on multitude of physical phenomena (e.g. temperature, stress, manufacturing, operating conditions, etc.)

Optimal Control Problem

Multiobjective Shortest-Path Stochastic Dynamic Program

Cost Functional:

Constraints:

Objective:

$$J^{g} = \lim_{N \to \infty} \mathbb{E} \left[\sum_{k=0}^{N} c(x_{k}, u_{k}) \right] \qquad x_{k+1} = f(x_{k}, u_{k}, w_{k})$$
$$x \in X$$

$$x_{k+1} = f(x_k, u_k, w_k)$$
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$$u \in U(x)$$

$$g^* = \arg\min_{g \in G} J^g$$

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$$x_{k+1} = f(x_k, u_k, w_k)$$
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Cost per time step: Convex sum of energy cost and battery health

$$c(x_k, u_k) = \alpha \cdot c_E(x_k, u_k) + (1 - \alpha) \cdot c_H(x_k, u_k)$$

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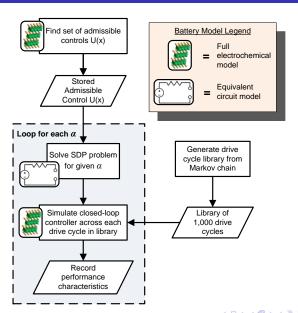
Cost per time step: Convex sum of energy cost and battery health

$$c(x_k, u_k) = \alpha \cdot c_E(x_k, u_k) + (1 - \alpha) \cdot c_H(x_k, u_k)$$

Energy:
$$c_E(x_k, u_k) = \beta W_{fuel} + \frac{-V_{oc}Q_{batt}SOC}{\eta_{EVSE}}$$

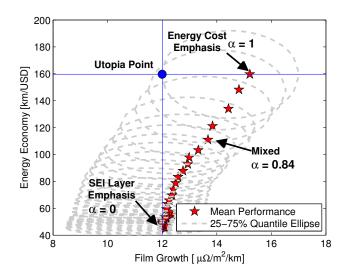
Health:
$$c_H(x_k, u_k) = \dot{\delta}_{film}(I, SOC)$$
 OR $|I/I_{max}|$

Optimization Procedure



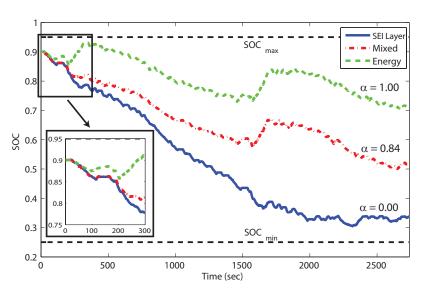
Pareto Set of Optimal Solutions

Anode-side SEI Layer Growth



SOC Trajectories

Anode-side SEI Layer Growth | UDDSx2



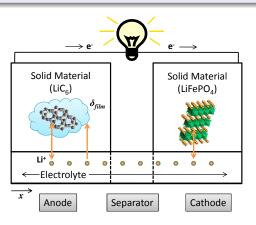
Outline

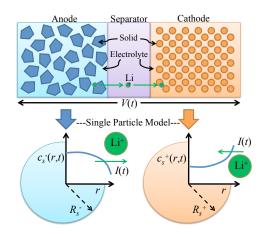
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SOC/SOH Estimation

Problem Statement

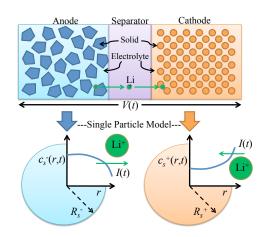
Simultaneously estimate SOC (states) and SOH (parameters) via an electrochemical model with measurements of voltage and current, only.





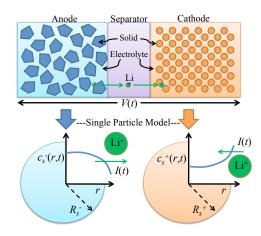
Mathematical Structure

- Two spherical diffusion PDEs
 - States: $c_s^-(r,t)$, $c_s^+(r,t)$



Mathematical Structure

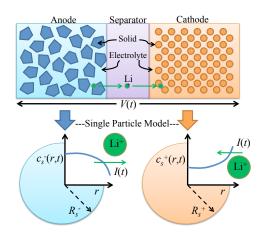
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 - Input: *I*(*t*)



Mathematical Structure

- Two spherical diffusion PDEs
 - States: $c_s^-(r,t)$, $c_s^+(r,t)$
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 - Input: *I*(*t*)
- Nonlinear output function of PDEs' boundary values
 - Output:

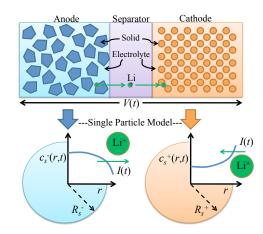
$$V(t) = h(c_{ss}^{-}(t), c_{ss}^{+}(t), I(t))$$



Mathematical Structure

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 - Output:

$$V(t) = h(c_{ss}^{-}(t), c_{ss}^{+}(t), I(t))$$



Definitions

- SOC: Bulk concentration SOC_{bulk} , Surface concentration $c_{ss}^-(t)$
- SOH: Physical parameters, e.g. ε, q, n_{Li}, R_f

The SOC Estimation Problem

Problem Statement

Estimate states $c_s^-(r,t),c_s^+(r,t)$ from measurements I(t),V(t) and SPM

The SOC Estimation Problem

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Estimate states $c_s^-(r,t), c_s^+(r,t)$ from measurements I(t), V(t) and SPM

Simplify the Math

- Model reduction to achieve observability
- Normalize time and space
- State transformation

The SOC Estimation Problem

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Estimate states $c_s^-(r,t), c_s^+(r,t)$ from measurements I(t), V(t) and SPM

Simplify the Math

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Observer Model Equations

$$\frac{\partial c}{\partial t}(r,t) = \varepsilon \frac{\partial^2 c}{\partial r^2}(r,t)$$

$$c(0,t) = 0$$

$$\frac{\partial c}{\partial r}(1,t) - c(1,t) = -q\rho I(t)$$
Measurement = $c(1,t)$

Heat PDE

Backstepping PDE Estimator

Estimator

$$\frac{\partial \hat{c}}{\partial t}(r,t) = \varepsilon \frac{\partial^2 \hat{c}}{\partial r^2}(r,t) + p_1(r)\tilde{c}(1,t)$$

$$\hat{c}(0,t) = 0$$

$$\frac{\partial \hat{c}}{\partial r}(1,t) - \hat{c}(1,t) = -q\rho I(t) + p_{10}\tilde{c}(1,t)$$

$$\tilde{c}(1,t) = c(1,t) - \hat{c}(1,t)$$

- Form error system $\tilde{c}(r,t)$
- Select target system $\tilde{w}(r,t)$ exponentially stable
- Find backstepping transformation: $\tilde{c}(r,t) \rightarrow \tilde{w}(r,t)$
- Derive kernels for transformation and solve analytically

$$p_1(r) = \frac{-\lambda r}{2\varepsilon z} \left[I_1(z) - \frac{2\lambda}{\varepsilon z} I_2(z) \right] \qquad \text{where} \quad z = \sqrt{\frac{\lambda}{\varepsilon} (r^2 - 1)}$$

$$p_{10} = \frac{1}{2} \left(3 - \frac{\lambda}{\varepsilon} \right)$$

The SOH Estimation Problem

Problem Statement

Estimate physical parameters from measurements I(t), V(t) and SPM

The SOH Estimation Problem

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Estimate physical parameters from measurements I(t), V(t) and SPM

Relate uncertain parameters to SOH-related concepts

- Capacity fade
- Power fade

The SOH Estimation Problem

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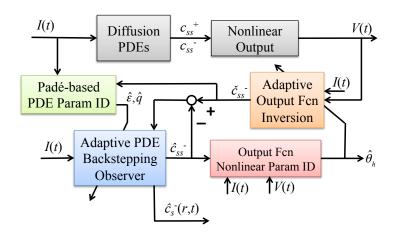
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Technical Challenges

- PDE models
- Nonlinear in parameters

Adaptive Observer

Combined State & Parameter Estimation



Output Function Nonlinear Parameter ID

Nonlinearly Parameterized Output

$$V(t) = h(c_{ss}^{-}(t), I(t); \theta)$$

- \bullet θ contains many parameters
- Linear dependence between parameters?

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Identifiability Analysis Result

- Linearly independent parameter subset : $\theta_h = [n_{Li}, R_f]^T$
 - n_{Li} : Total amount of cyclable Li (Capacity Fade)
 - \bullet R_f : Resistance of current collectors, electrolyte, etc. (Power Fade)

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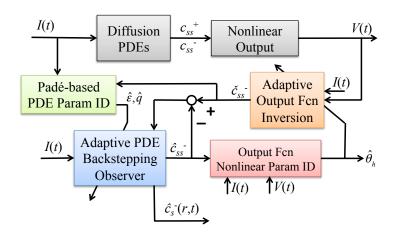
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Enables the application of nonlinear least squares parameter identification tools applied to vector θ_h



Adaptive Observer

Combined State & Parameter Estimation



Adaptive Output Function Inversion

Recall state observer requires boundary value $c_{ss}^-(t)$ for output error injection

Adaptive Output Function Inversion

Recall state observer requires boundary value $c_{ss}^-(t)$ for output error injection

Nonlinear Function Inversion

Solve $g(c_{ss}^-,t)=0$ for c_{ss}^- , where

$$g(c_{ss}^-, t) = h(c_{ss}^-(t), I(t); \hat{\theta}_h) - V(t)$$

Adaptive Output Function Inversion

Recall state observer requires boundary value $c_{ss}^-(t)$ for output error injection

Nonlinear Function Inversion

Solve $g(c_{ss}^-,t)=0$ for c_{ss}^- , where

$$g(c_{ss}^-, t) = h(c_{ss}^-(t), I(t); \hat{\theta}_h) - V(t)$$

Newton's Method

Main Idea: Construct ODE with exp. stable equilibrium $g(c_{ss}^-,t)=0$

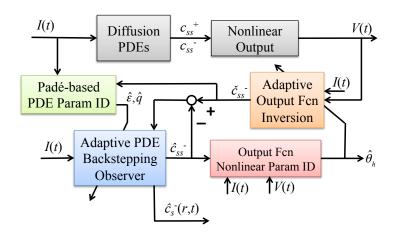
$$\frac{d}{dt}\left[g(\check{c}_{ss}^{-},t)\right] = -\gamma g(\check{c}_{ss}^{-},t)$$

which expands to a Newton's method update law:

$$\frac{d}{dt} \check{\mathbf{c}}_{ss}^{-} = -\frac{\gamma g(\check{\mathbf{c}}_{ss}^{-}, t) + \frac{\partial g}{\partial t}(\check{\mathbf{c}}_{ss}^{-}, t)}{\frac{\partial g}{\partial c_{ss}^{-}}(\check{\mathbf{c}}_{ss}^{-}, t)}$$

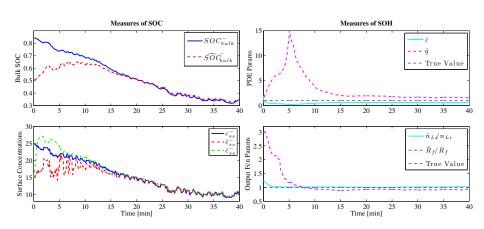
Adaptive Observer

Combined State & Parameter Estimation



Results

UDDS Drive Cycle Input



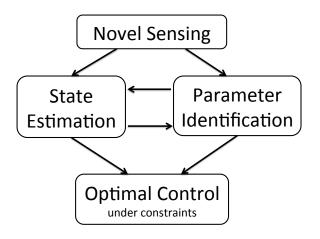
Work in Progress: Validation on Full Electrochemical Model



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Vision for Electrochemical-model based BMS



Future Research Tasks

Adaptive SOC/SOH Observer for Single Particle Model

- Simulator for full model
- Validate adaptive observer
- Publish

Target completion: May 15

Parameter Estimation for Full Model (i.e. retain x-dimension)

- Analyze parameter identifiability
- Develop parameter estimation algorithm
- Validation
- Publish

Target completion: Aug 1

ARPA-E AMPED Project



ARPA-E AMPED Project

Advanced Management and Protection of Energy-storage Devices

A Coupled Mechanical/Electrochemical Approach

- Stress/strain sensor in case
- Analyze observability and parameter identifiability
- Estimate SOC, stress, and params

Optimal-Safe Fast Charging - A Model Predictive Control Approach

- Output feedback
- Temp, side-rxn, and stress constraints

Thanks for your attention! Questions?

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UC Presidential Postdoctoral Fellow
UC San Diego
http://flyingv.ucsd.edu/smoura/

Parameterized Output

$$V(t) = h(t, c_{ss}^{-}(t); \theta)$$

$$\theta = \left[n_{Li}, \frac{1}{a^{+}AL^{+}k^{+}\sqrt{c_{e}^{0}}}, \frac{1}{a^{-}AL^{-}k^{-}\sqrt{c_{e}^{0}}}, R_{f} \right]^{T}$$

Linear dependence between parameters?

Parameter Sensitivity

$$S_i = \frac{\partial h}{\partial \theta_i}$$

$$S = [S_1, S_2, S_3, S_4]^T$$

$$S \in R^{n_T \times 4}$$

A particular decomposition of S^TS reveals linear dependence between parameters!



Decomposition of $S^TS = D^TCD$

$$C = \begin{bmatrix} 1 & \frac{\langle S_1, S_2 \rangle}{\|S_1\| \|S_2\|} & \frac{\langle S_1, S_3 \rangle}{\|S_1\| \|S_2\|} & \frac{\langle S_1, S_3 \rangle}{\|S_1\| \|S_3\|} & \frac{\langle S_1, S_4 \rangle}{\|S_1\| \|S_4\|} \\ \frac{\langle S_2, S_1 \rangle}{\|S_2\| \|S_1\|} & 1 & \frac{\langle S_2, S_3 \rangle}{\|S_2\| \|S_3\|} & \frac{\langle S_2, S_4 \rangle}{\|S_2\| \|S_4\|} \\ \frac{\langle S_3, S_1 \rangle}{\|S_3\| \|S_1\|} & \frac{\langle S_3, S_2 \rangle}{\|S_4\| \|S_2\|} & 1 & \frac{\langle S_3, S_4 \rangle}{\|S_4\| \|S_4\|} \\ \frac{\langle S_4, S_1 \rangle}{\|S_4\| \|S_1\|} & \frac{\langle S_4, S_2 \rangle}{\|S_4\| \|S_2\|} & \frac{\langle S_4, S_3 \rangle}{\|S_4\| \|S_3\|} & 1 \end{bmatrix}$$

$$\frac{|\langle S_i, S_j \rangle|}{\|S_i\| \|S_j\|} pprox 1 \Rightarrow \text{linear dependence} \qquad \qquad \frac{|\langle S_i, S_j \rangle|}{\|S_i\| \|S_j\|} pprox 0 \Rightarrow \text{linear independence}$$

Decomposition of $S^TS = D^TCD$

$$\frac{|\langle S_i, S_j \rangle|}{||S_i|| ||S_i||} \approx 1 \Rightarrow \text{linear dependence}$$

$$\frac{|\langle S_i, S_j \rangle|}{||S_i|| ||S_j||} pprox 0 \Rightarrow$$
 linear independence

Example: UDDS Drive Cycle Applied to Battery Model

$$C = \begin{bmatrix} 1 & -0.3000 & 0.2908 & 0.2956 \\ -0.3000 & 1 & -0.9801 & -0.9805 \\ 0.2908 & -0.9801 & 1 & 0.9322 \\ 0.2956 & -0.9805 & 0.9322 & 1 \end{bmatrix}$$

 $\theta_2, \theta_3, \theta_4$ are linearly dependent Identify the subset $\theta_h = [\theta_1, \theta_4]^T$ via nonlinear least squares

- ullet $heta_1 = n_{Li}$: Capacity Fade
- $\theta_4 = R_f$: Power Fade

Decomposition of $S^TS = D^TCD$

$$\frac{|\langle S_i, S_j \rangle|}{\|S_i\| \|S_j\|} pprox 1 \Rightarrow \text{linear dependence}$$

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 linear independence

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Remarks on extensions to high-dimensional parameter spaces

- Orthogonalization and permutation of S^TS to rank sensitivity
- Min parameter variance via Cramer-Rao inequality to rank certainty