

AC/DC power flow aimed at large scale systems

Josep Fanals i Batllori

## **Large Scale Systems Week**

eRoots Analytics

02/12/2024  
Hamburg, Germany

AC/DC power flow  
aimed at large scale  
systems

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Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

## 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

## 3. Installation

## 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

## 5. Conclusions

## Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

## Installation

## Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

## Conclusions

# 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

# 3. Installation

# 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

# 5. Conclusions

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

## Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

## Installation

## Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

## Conclusions

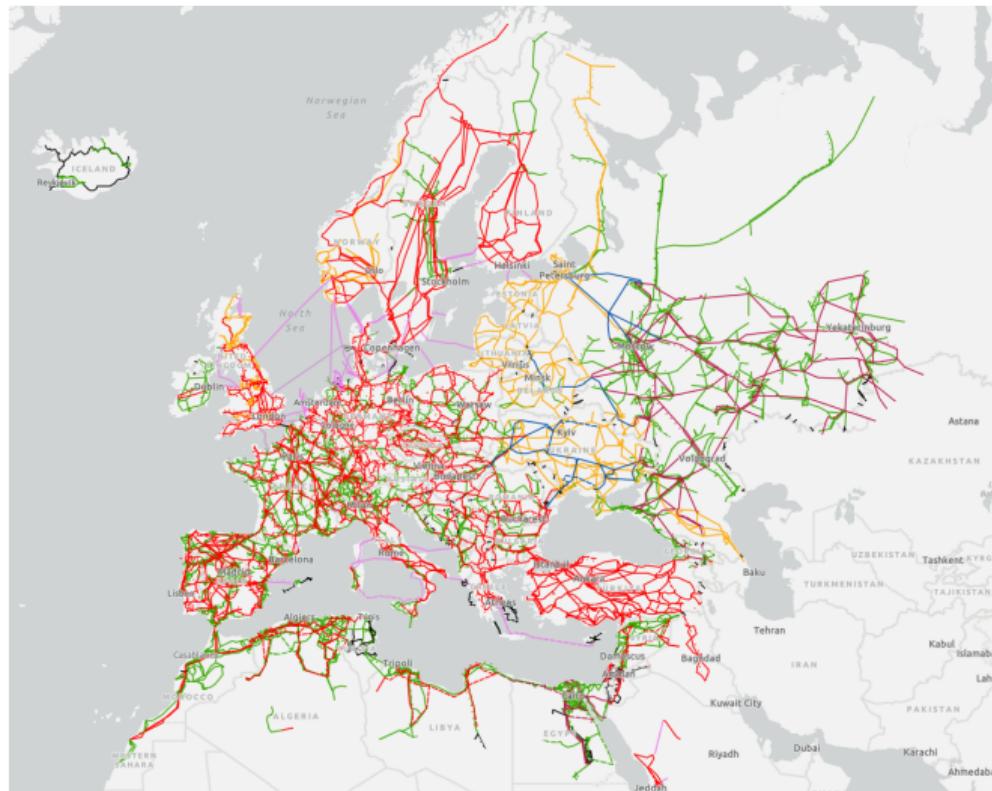


Figure 1: Grid map of Europe, with HVDC links in purple.

# Objectives

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

## Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

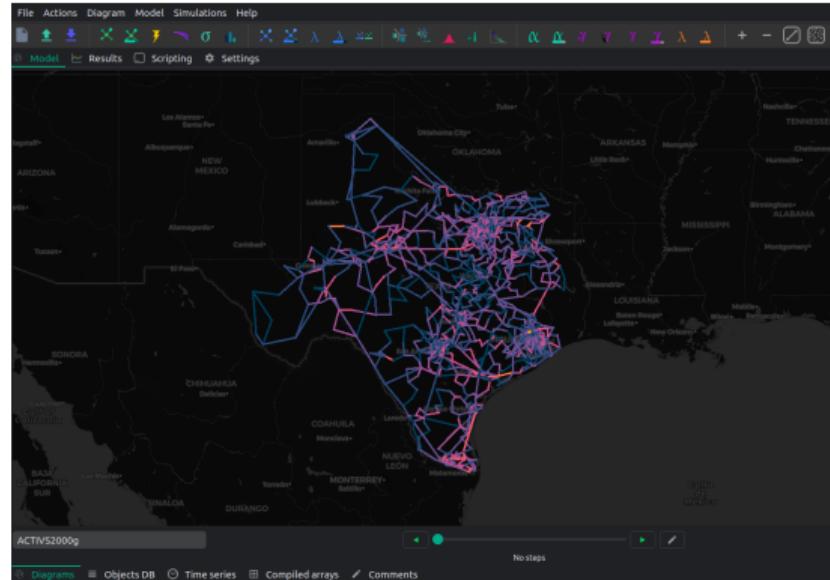


Figure 2: GridCal interface used for power flow analysis in Spain.

- ▶ Integrate both AC and DC systems into a unified framework.
- ▶ Address the convergence issues found in current methods.
- ▶ Model complex components like converters and controllable transformers.
- ▶ Implement the method and test its scalability.

We present a generalised approach to the power flow problem, much more flexible than conventional methods.

Feature	Traditional	Classical	Generalised
Handles AC systems	✓	✓	✓
Remote controls	✗	✗	✓
Control more than two magnitudes at a bus	✗	✓	✓
Controlled branch magnitudes	✗	✓	✓
Interconnected AC/DC grids	✗	✓	✓
Flexible bus type definition	✗	✗	✓

Table 1: Comparison between traditional, classical, and generalised power flow.

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

## 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

## 3. Installation

## 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

## 5. Conclusions

# What is a power grid?

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

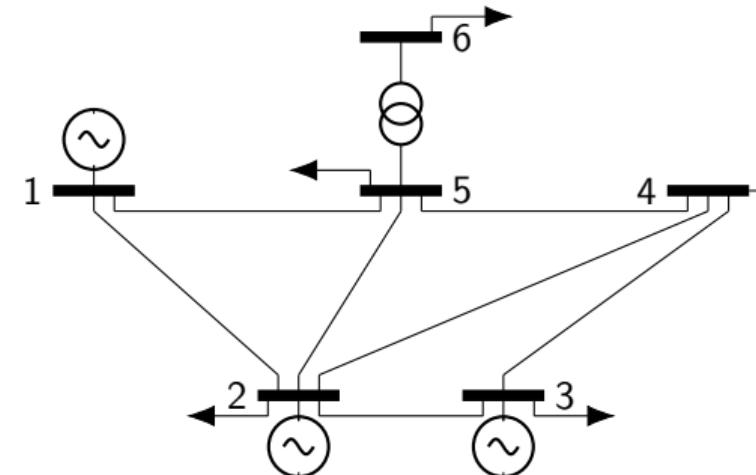


Figure 3: Example grid showing buses linked through branches.

A grid is modeled as an undirected graph the set of buses (nodes) are connected to each other by the set of branches (edges):

- ▶ **Buses:** Represent the points in the network where generation, load, or interconnections occur.
- ▶ **Branches:** Power lines, transformers and converters, which can be passive or controllable.

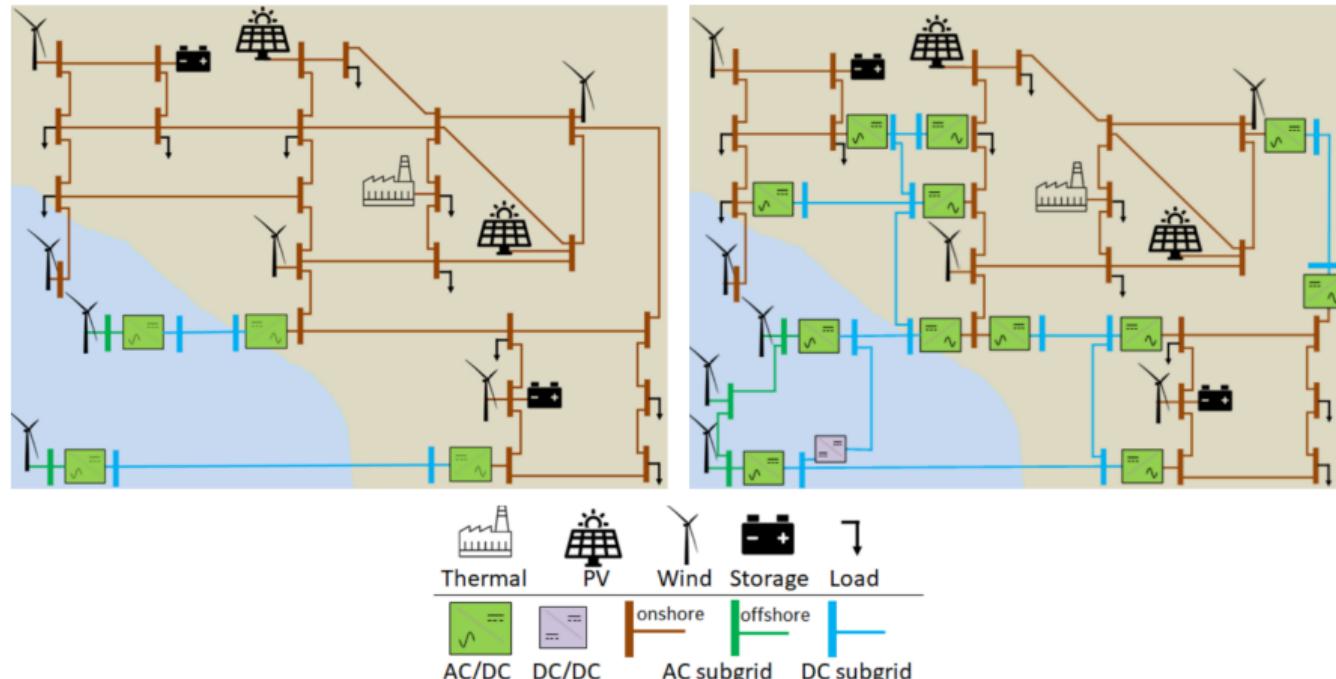


Figure 4: From present grids to future systems.

Voltage source converters (VSCs) interlink AC subsystems with DC subsystems, allowing for controlling two magnitudes. This controllability, while providing more flexibility, also introduces more complexity.

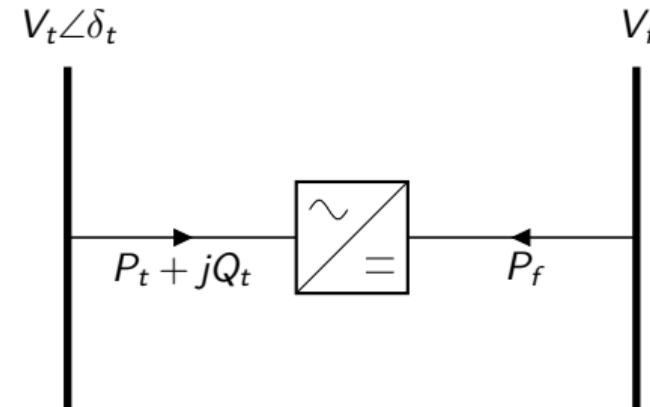


Figure 5: Representation of a VSC.

Converters interconnect DC and AC buses. Hence, there are two approaches to the problem:

- ▶ **Sequential:** we first solve the AC networks, then the DC networks, merge them, and repeat the calculation → non-scalable
- ▶ **Unified:** we solve all AC and DC grids at the same time → much more scalable

The active powers on the  $f$  and  $t$  sides are related through the power loss equation:

$$P_f + P_t = P_{\text{loss}},$$

$$P_f + P_t = a + b \frac{\sqrt{(P_t)^2 + (Q_t)^2}}{V_t} + c \frac{(P_t)^2 + (Q_t)^2}{V_t^2}. \quad (1)$$

- ▶ Grid operators are interested in knowing the operating state of the network.
- ▶ That is, voltages, currents and powers have to be found everywhere in the grid.
- ▶ The underlying equations, which come from the physics, are non-linear in nature.
- ▶ Among many solvers, we opt for the Newton-Raphson given its quadratic convergence and scalability properties.

$$\mathbf{x} = [\delta, V, \tau, m, P^{\text{zip}}, Q^{\text{zip}}, P_f, P_t, Q_f, Q_t]^T \quad (2)$$

$$\mathbf{g} = [g_{p,ac}, g_{q,ac}, g_{p,dc}, g_{I,acdc}, g_{I,hvdc}, g_{p,hvdc}, g_{p_f,tr}, g_{p_t,tr}, g_{q_f,tr}, g_{q_t,tr}]^T \quad (3)$$

- ▶ To solve the system using the Newton-Raphson method, we need a Jacobian matrix.
- ▶ This matrix contains the partial derivatives of the form  $\frac{\partial \mathbf{g}}{\partial \mathbf{x}}$ . Two ways to calculate:
  1. Partial differences such as  $\frac{g(x+h) - g(x-h)}{h}$  → easier but slower
  2. With previously derived closed-form expressions → harder but faster
- ▶ The typical Newton-Raphson system is represented as:

$$-\mathbf{J}\Delta\mathbf{x} = \mathbf{g} \quad (4)$$

where:

- ▶  $\mathbf{J}$  is the Jacobian matrix.
- ▶  $\Delta\mathbf{x}$  is the vector of unknown variations.
- ▶  $\mathbf{g}$  is the residual vector of equations.

To ensure solvability in generalized power flow, the following rules are defined:

- ▶ Each subgrid must have at least one reference for voltage magnitude and angle.
- ▶ Control of a remote bus is allowed.
- ▶ No two devices can control the same nodal voltage.
- ▶ Buses can have up to 4 controlled magnitudes in AC subsystems and 2 in DC subsystems.

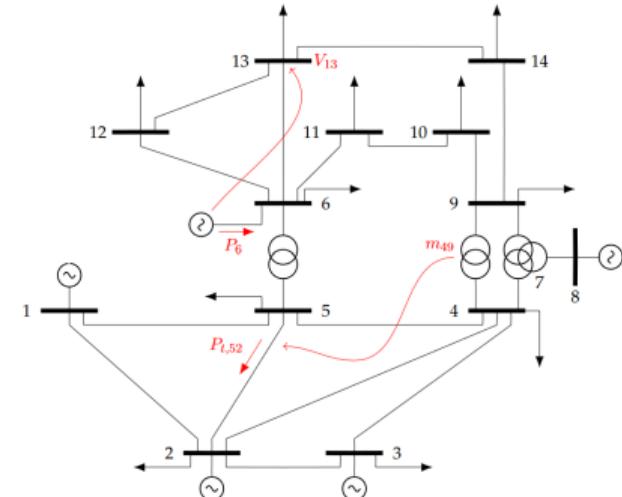


Figure 6: Scheme of the IEEE 14-bus grid with remote controls.

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

## 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

## 3. Installation

## 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

## 5. Conclusions

[Introduction](#)[AC/DC theory](#)[Grid basics](#)[AC/DC converters](#)[The power flow](#)[Solving approach](#)[Installation](#)[Practical cases](#)[Fundamental 6-bus case](#)[Interconnected 17-bus case](#)[IEEE 118-bus case](#)[Conclusions](#)

The three requisites are:

1. Python 3.10 or 3.11.
2. VSCode.
3. GridCal wheels.

- ▶ For instance, download Python 3.10.9 from <https://www.python.org/downloads/release/python-3109/>.
- ▶ Make sure to add Python to the PATH.

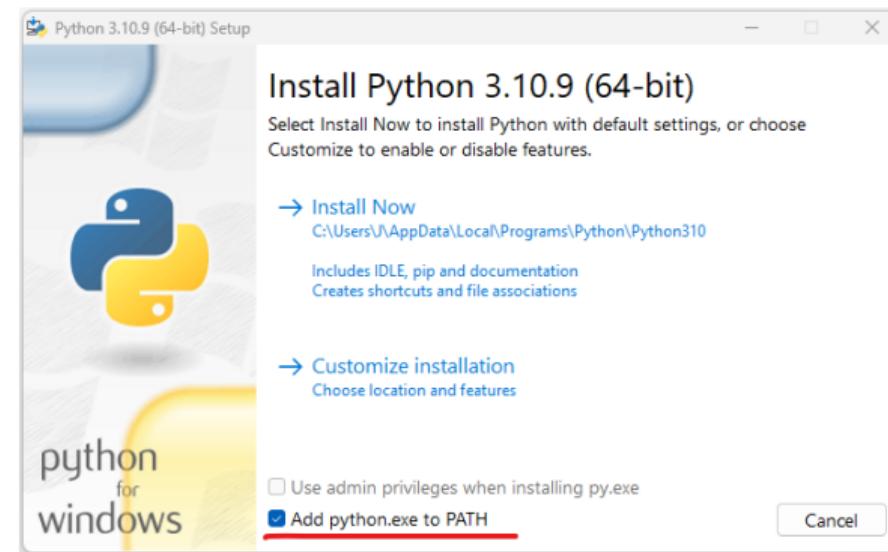


Figure 7: Python installation.

- ▶ Download VSCode from <https://code.visualstudio.com/>.
- ▶ Install the Python extension.



Figure 8: Python VSCode extension.

- ▶ Create a virtual environment in VSCode: Ctrl+Shift+P, then Python: Create Environment.
- ▶ Activate with `./.venv/Scripts/Activate`.
- ▶ Install the latest alpha GridCal release: `pip install GridCal==5.3.0a3`.
- ▶ Verify the installation with `pip list`.

Open the interface:

- ▶ Windows:

```
python -c "from GridCal.ExecuteGridCal import runGridCal; runGridCal()"
```

- ▶ Unix:

```
python3 -c "from GridCal.ExecuteGridCal import runGridCal; runGridCal()"
```

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

## 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

## 3. Installation

## 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

## 5. Conclusions

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

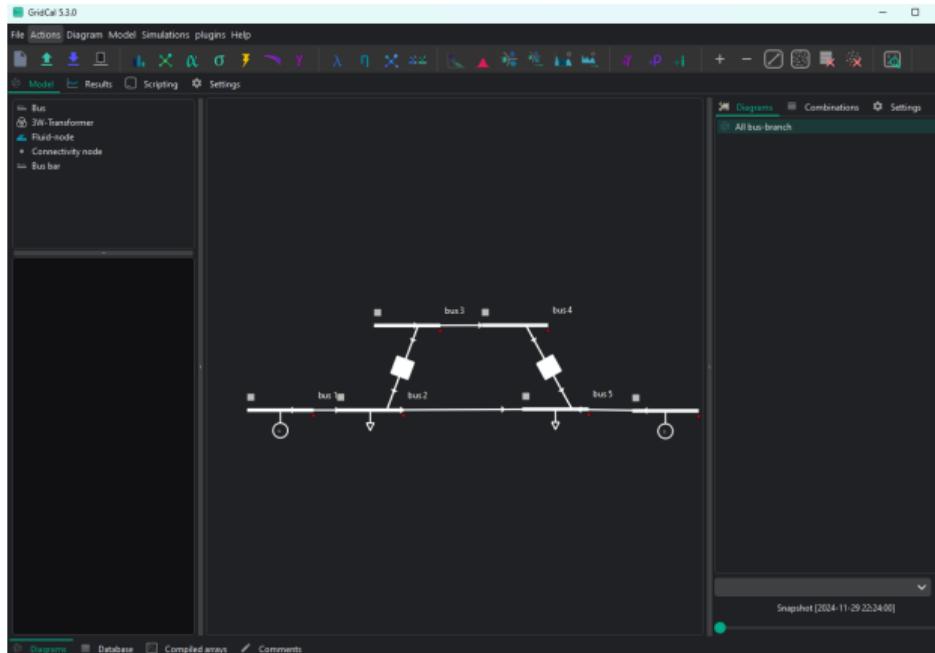


Figure 9: Visualization of the 6-bus grid through the GUI.

- ▶ Go over the complete database.
- ▶ Check the controls of the generators.
- ▶ Check the controls of the VSCs. What to expect?

# GUI usage: solving

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

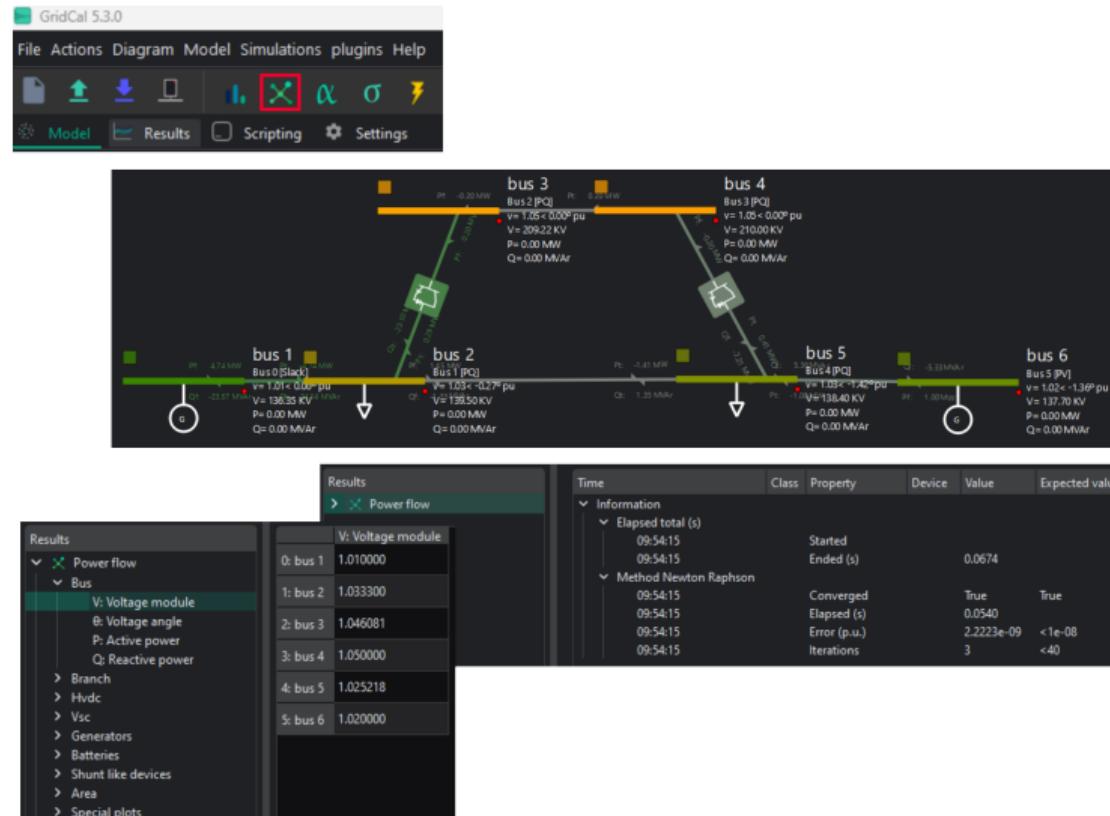


Figure 10: GUI simulation execution, solver selection and results visualization on the 6-bus grid.

### Solver selection:

- ▶ Run the power flow with both the Newton-Raphson and the Gauss-Seidel.
- ▶ How many iterations do we need in both?
- ▶ What is the computational time?

### Control setting:

- ▶ What if the two converters control active power?
- ▶ What if the two converters control voltage on the DC side?

► Let's move into our code editor.

```
1 import numpy as np
2 import GridCalEngine as gce
3 from GridCalEngine.enumerations import ConverterControlType
4
5 # Grid instantiation
6 grid = gce.MultiCircuit()
7
8 # Define buses
9 bus1 = gce.Bus(name='B1', Vnom=135, is_slack=True)
10 ...
11
```

[Introduction](#)[AC/DC theory](#)[Grid basics](#)[AC/DC converters](#)[The power flow](#)[Solving approach](#)[Installation](#)[Practical cases](#)[Fundamental 6-bus case](#)[Interconnected 17-bus case](#)[IEEE 118-bus case](#)[Conclusions](#)

- ▶ Let's move into our code editor.

```
1 pf_driver = gce.PowerFlowDriver(grid=grid)
2 pf_driver.run()
3 Vm = pf_driver.results.voltage
4 Va = np.angle(pf_driver.results.voltage, deg=True)
5
```

- ▶ The 6-bus case had 1 AC and 1 DC subsystem.
- ▶ Transnational grids are composed of many AC and DC grids.
- ▶ Real grids may also have controllable transformers.

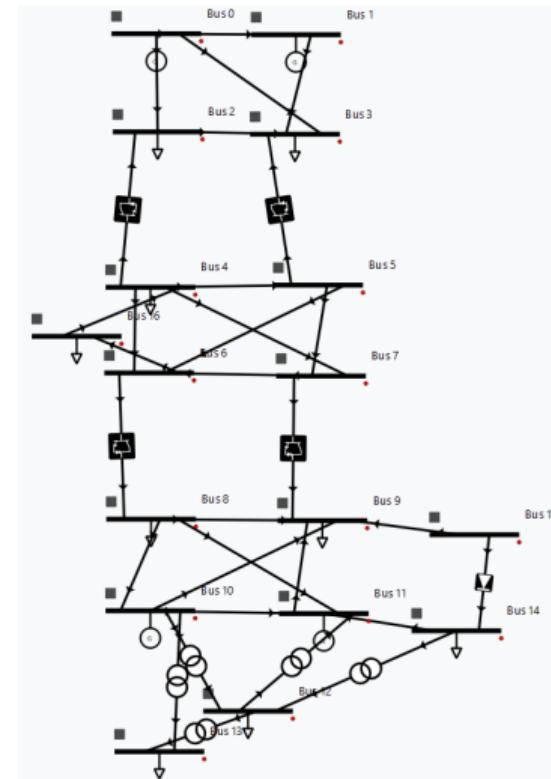


Figure 11: Interconnected AC systems overview.

# Issues in the 17-bus cases

What issues are we facing?

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

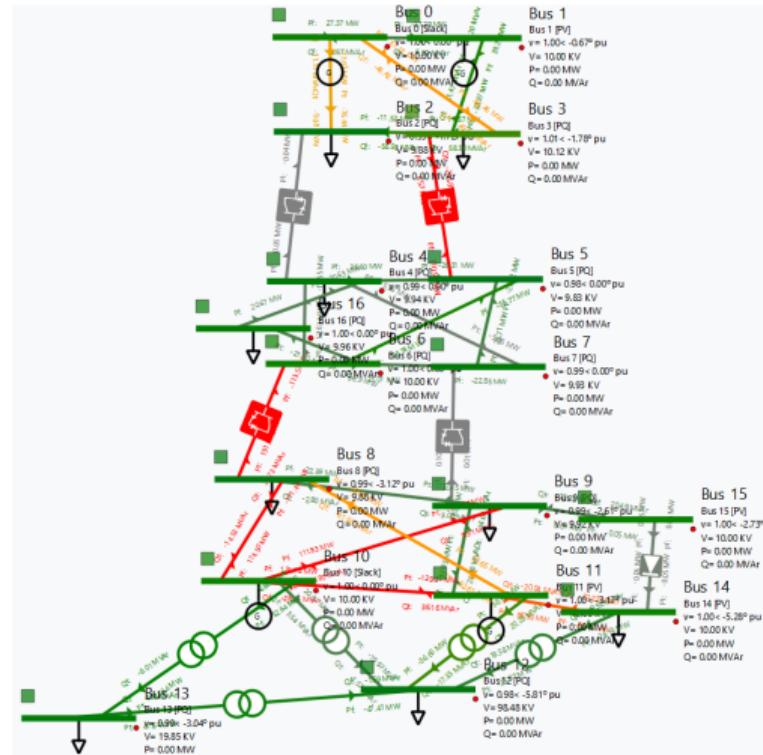


Figure 12: Default interconnected AC system results.

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

Some potential fixes include:

- ▶ Adjust the transformer control setpoints.
- ▶ Change the VSCs control modes.
- ▶ Modify the VSCs control setpoints.
- ▶ Regulate the generators voltage reference.

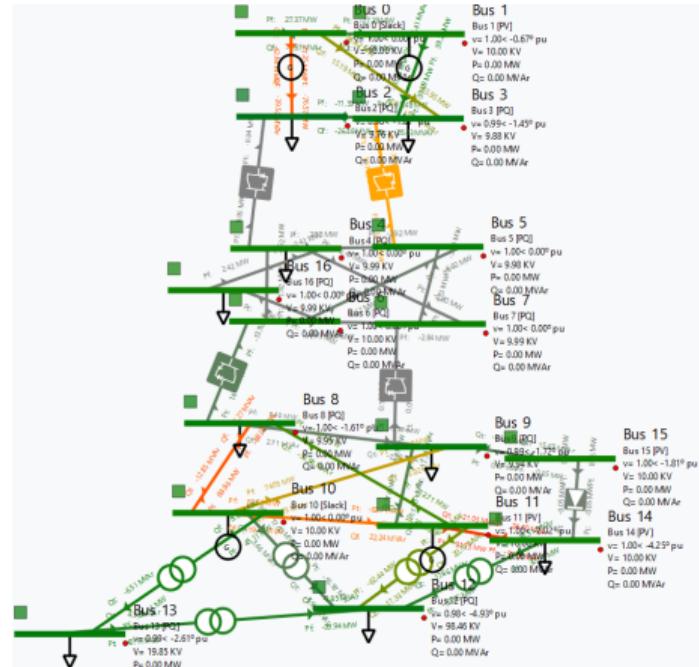


Figure 13: Interconnected AC systems with a feasible solution.

Despite being less flexible than VSCs, some transformers are also controllable:

- ▶  $m$ : the tap module can regulate  $V_m$  and  $Q$
- ▶  $\tau$ : the tap angle can adjust  $P$

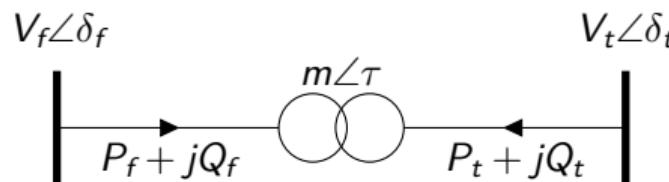


Figure 14: Representation of a controllable transformer.

- ▶ Let's increase  $V_{m,13}$  to 1.019876 p.u..
- ▶ Is it reasonable to have  $0.9 \leq m \leq 1.0$ ?

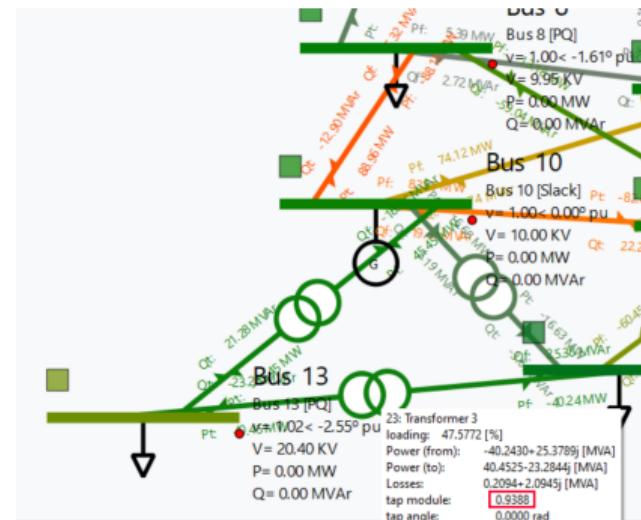


Figure 15: Transformer controlling  $V_m$  with  $m$ .

# What is a large system?

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

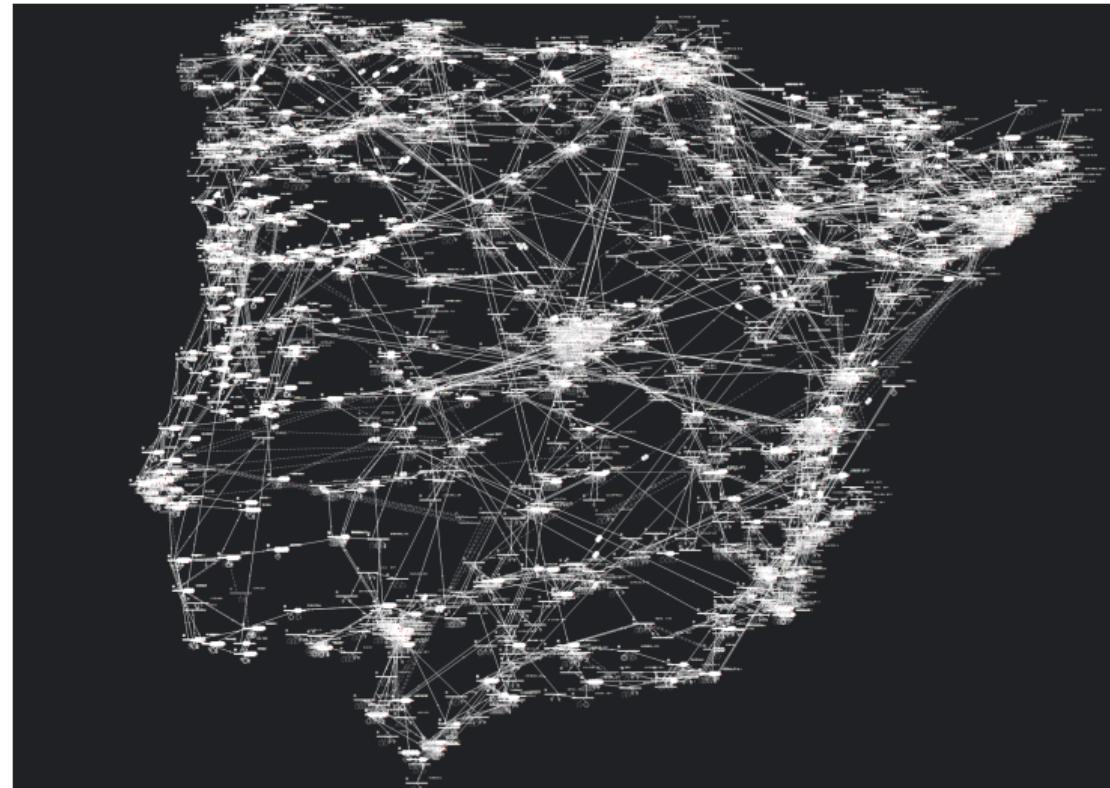


Figure 16: Grid topology of the Iberian system.

# What is a large system?

- ▶ Note: open the grid of Las Palmas to exemplify.

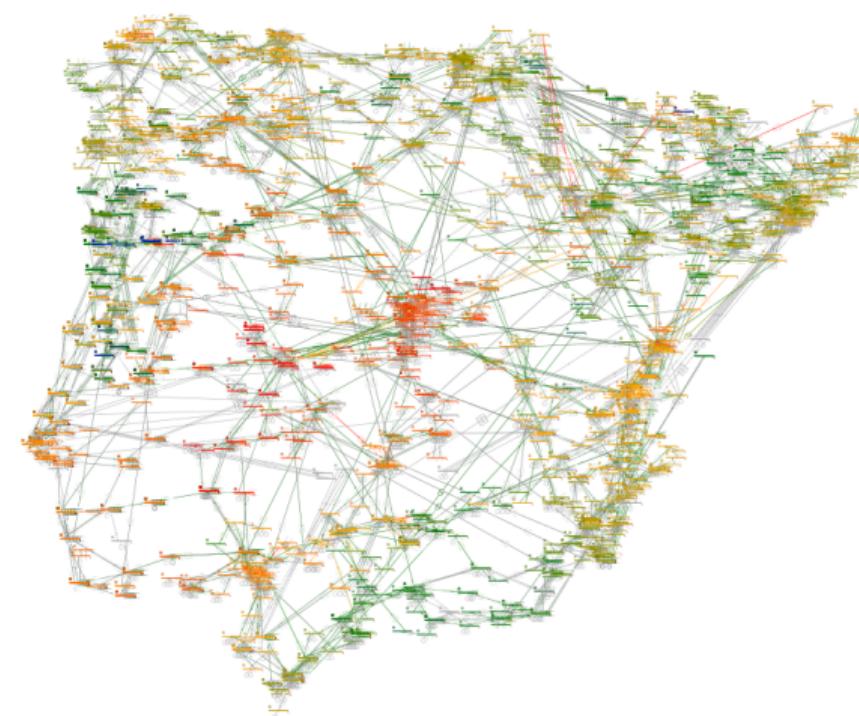


Figure 17: Solved power flow for the Iberian system.

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

- ▶ Are voltage magnitudes correct?
- ▶ Are branch loadings within limits?
- ▶ How could an AC/DC link help?



Figure 18: Original operation of the IEEE 118-bus grid.

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Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

	$\sigma_{\text{real}}$	$\sigma_{\text{imaginary}}$	Distances
0: RIVERSIDE	0.044743	-0.330696	-0.067843
1: POKAGON	0.057569	-0.328277	-0.062932
2: HICKRYCK	0.052871	-0.321406	-0.069194
3: NWCARLSL	0.066760	-0.271208	-0.092044
4: OLIVE	0.069208	-0.264941	-0.094672
5: KANKAKEE	0.068362	-0.305969	-0.070524
6: JACKSNRD	0.069418	-0.313037	-0.065848
7: OLIVE	0.080985	-0.180272	-0.143201
8: BEQUINE	0.096747	-0.060591	-0.222048
9: BRED	0.105512	0.071149	-0.211999
10: SOUTHBND	0.063735	-0.309297	-0.070870
11: TWINBRCH	0.071057	-0.319265	-0.061382
12: CONCORD	0.051331	-0.326355	-0.067108
13: GOSHENUT	0.065444	-0.329608	-0.058224
14: FTWAYNE	0.045229	-0.332796	-0.066415
15: N. E.	0.062711	-0.322913	-0.063462
16: SORENSEN	0.056832	-0.299198	-0.080163
17: MCKINLEY	0.045738	-0.328629	-0.068535
18: LINCOLN	0.036807	-0.333075	-0.070316
19: ADAMS	0.025516	-0.316174	-0.085138

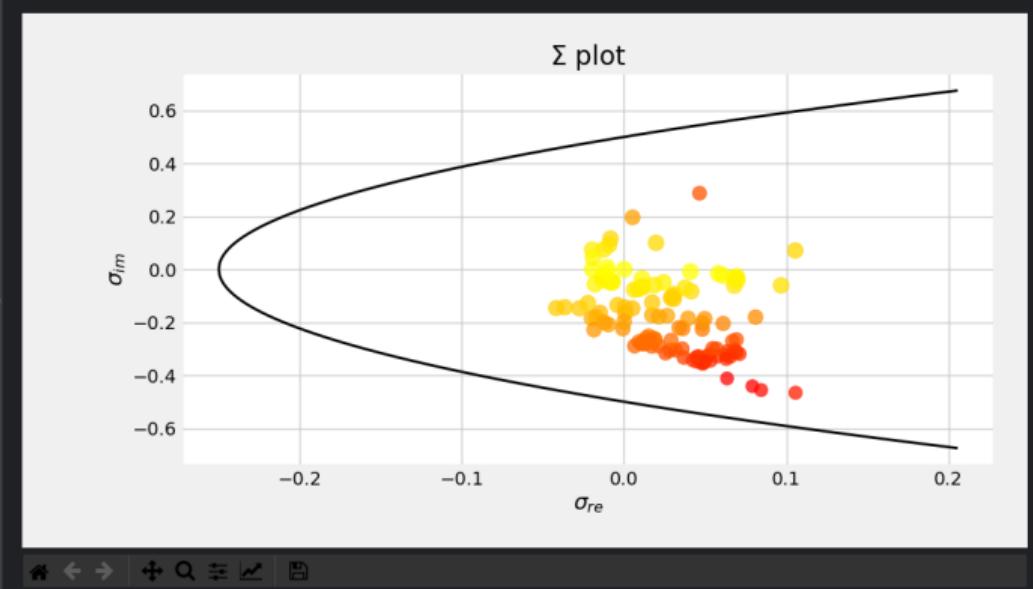


Figure 19: HELM's Sigma plot showing the complicated feasibility of the systems.

### AC/DC theory

IEEE 118-bus case

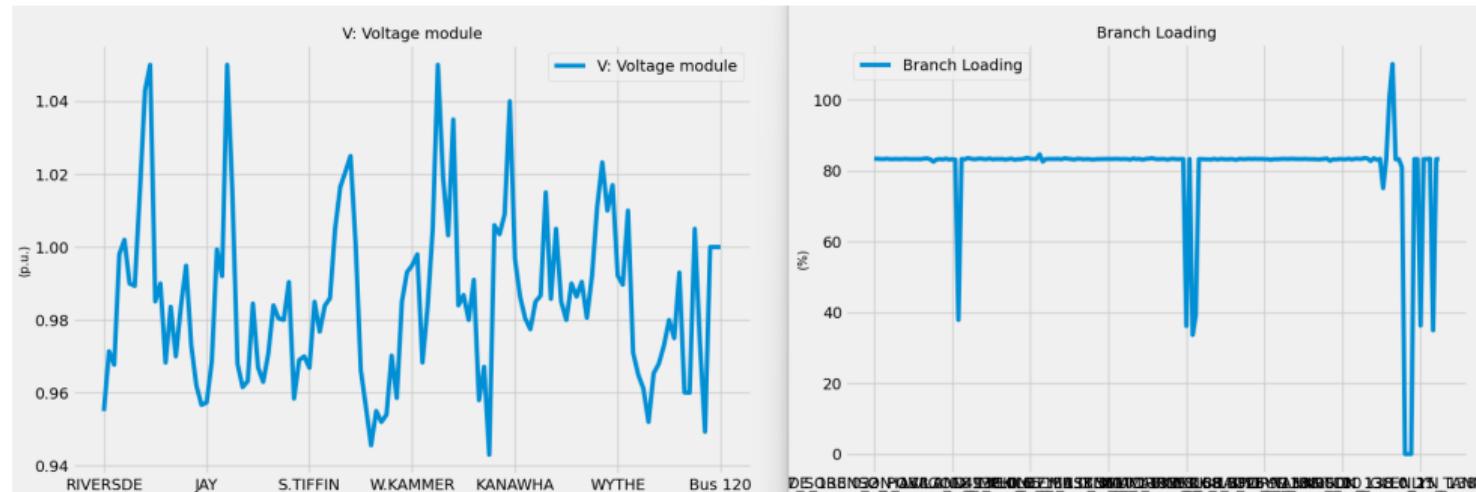


Figure 20: Voltage and branch loadings for the whole IEEE 118-bus system.

AC/DC power flow  
aimed at large scale  
systems

Josep Fanals

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

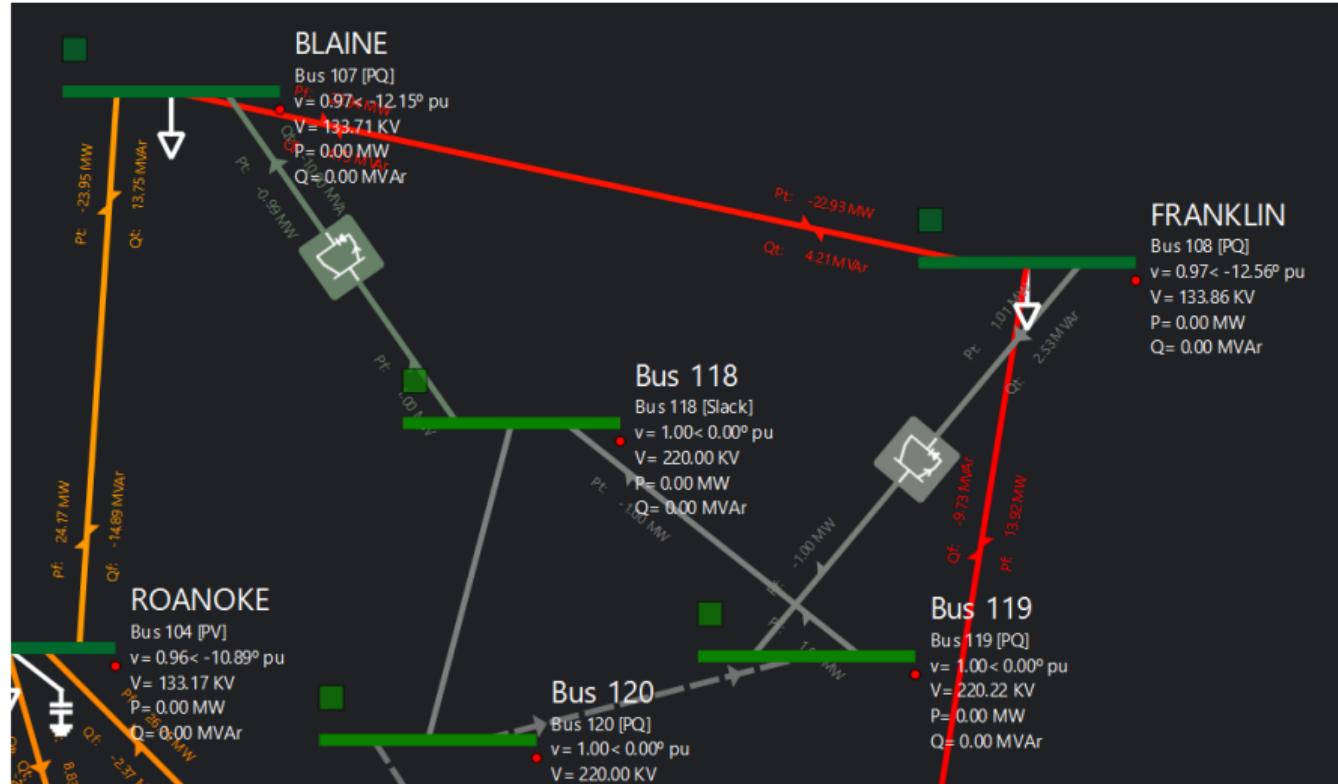


Figure 21: Potential AC/DC link configuration.

Introduction

AC/DC theory

Grid basics

AC/DC converters

The power flow

Solving approach

Installation

Practical cases

Fundamental 6-bus case

Interconnected 17-bus case

IEEE 118-bus case

Conclusions

## 1. Introduction

## 2. AC/DC theory

### 2.1 Grid basics

### 2.2 AC/DC converters

### 2.3 The power flow

### 2.4 Solving approach

## 3. Installation

## 4. Practical cases

### 4.1 Fundamental 6-bus case

### 4.2 Interconnected 17-bus case

### 4.3 IEEE 118-bus case

## 5. Conclusions

- ▶ AC/DC converters require a new approach to their modelling.
- ▶ The Newton-Raphson method is the go-to algorithm due to its convergence properties.
- ▶ Setting the right AC/DC controls is key towards achieving a convergent case.
- ▶ Importance of relying on a GUI.

For more information:

- ▶ [info@eroots.tech](mailto:info@eroots.tech)
- ▶ <https://gridcal.readthedocs.io/en/latest/>

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