

## Problem 12-7

```

• # physical data
• begin
•     Tin = 300. # K
•     Tmax = 400. # K
•     Ea = 1e4 # cal/mol
•     R = 1.987 # cal/mol/K
•     k0 = 0.01 # L/mol/s
•     v0 = 2. # L/s
•     Cp = 30 # cal/mol
•     ΔH = -6e3 # cal/mol
•     Ua = 20 # cal/L/s/K
•     ṁ0 = 50 # g/s
• end;

```

(a)

From mass balance of  $A + B \rightarrow C$  in a CSTR,

$$\frac{X_A}{(1 - X_A)^2} = \frac{VC_{A0}}{v_0} k^0 \exp \left[ \frac{-E_a}{R} \left( \frac{1}{T^0} - \frac{1}{T} \right) \right]$$

and from energy balance on an adiabatic system,

$$X_{eb} = \frac{C_p(T - T^0)}{-\Delta H}$$

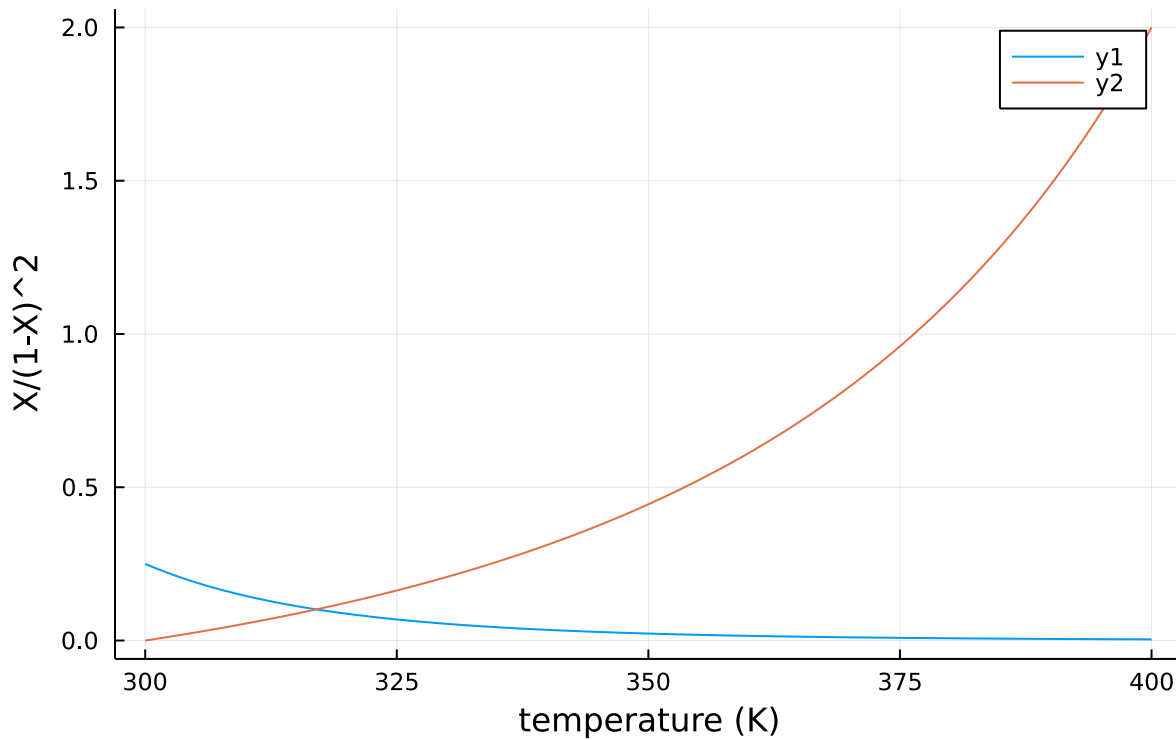
Letting  $y_1 = \frac{X_A}{(1 - X_A)^2}$  and  $y_2 = \frac{X_{eb}}{(1 - X_{eb})^2}$ , we can solve for  $T$  consistent with both:

```

• begin
•     # conversion from energy balance
•     Xeb(T; T0) = Cp * (T - T0) / -ΔH
•
•     # conversion expressions
•     y1(T; V, T0, Ca0) = V * Ca0 * k0 * exp(-Ea * (1/T0 - 1/T) / R) / v0
•     y2(T; T0) = Xeb(T; T0=T0) / (1 - Xeb(T; T0=T0))^2
•
•     # temperature range
•     T = [Tin:0.1:Tmax...]
• end;

```

## 500.0 L CSTR, 300.0 K inlet



```

• # plot curves
• begin
•   local V = 500. # L
•   local T0 = 300. # K
•   local Ca0 = 0.1 # mol/L
•
•   plot(T, y1.(T; V=V, T0=T0, Ca0=Ca0),
•     ylabel="X/(1-X)^2",
•     xlabel="temperature (K)",
•     title="$V$ L CSTR, $T^0$ K inlet"
•   )
•
•   plot!(T, y2.(T; T0=T0))
• end

```

The intercept is at 317.0 K and 8.5 % conversion.

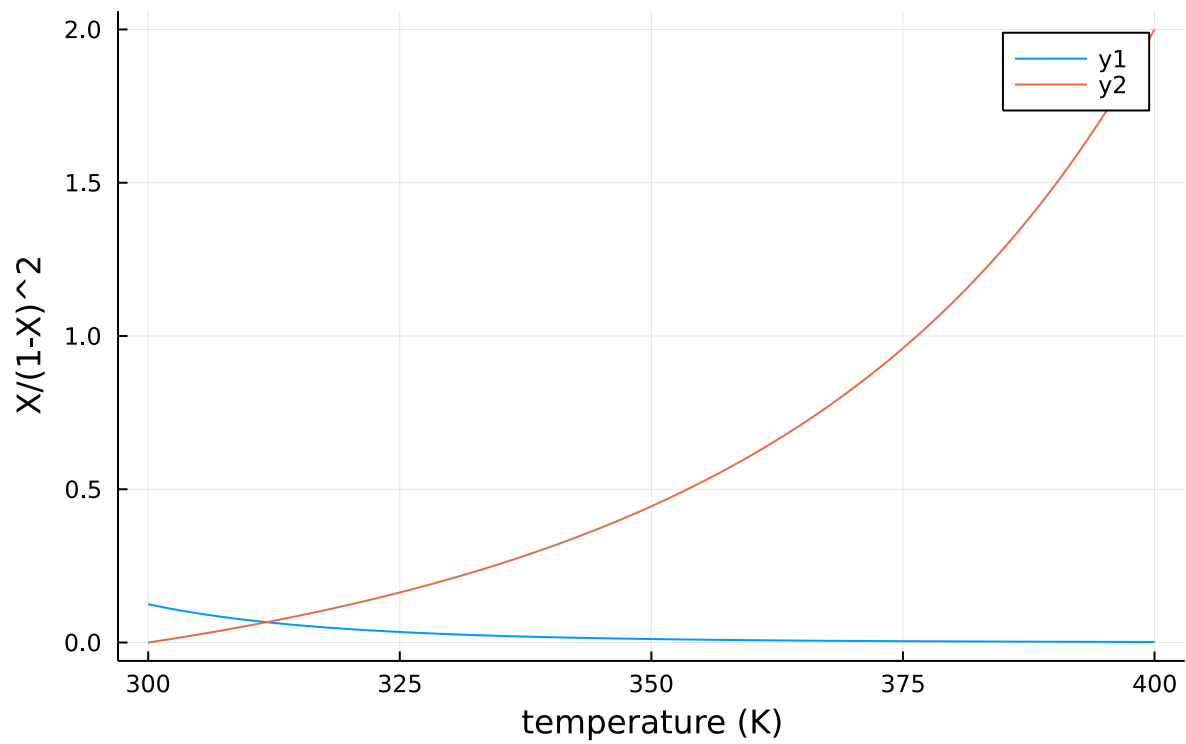
```

• # find the intercept
• begin
•   local Ca0 = 0.1
•   local i = argmin(abs.(y1.(T; V=500, T0=300, Ca0=Ca0) .- y2.(T; T0=300)))
•   local t = T[i]
•   local x = Xeb(t; T0=300) * 100
•   md"The intercept is at $t$ K and $x$ % conversion."
• end

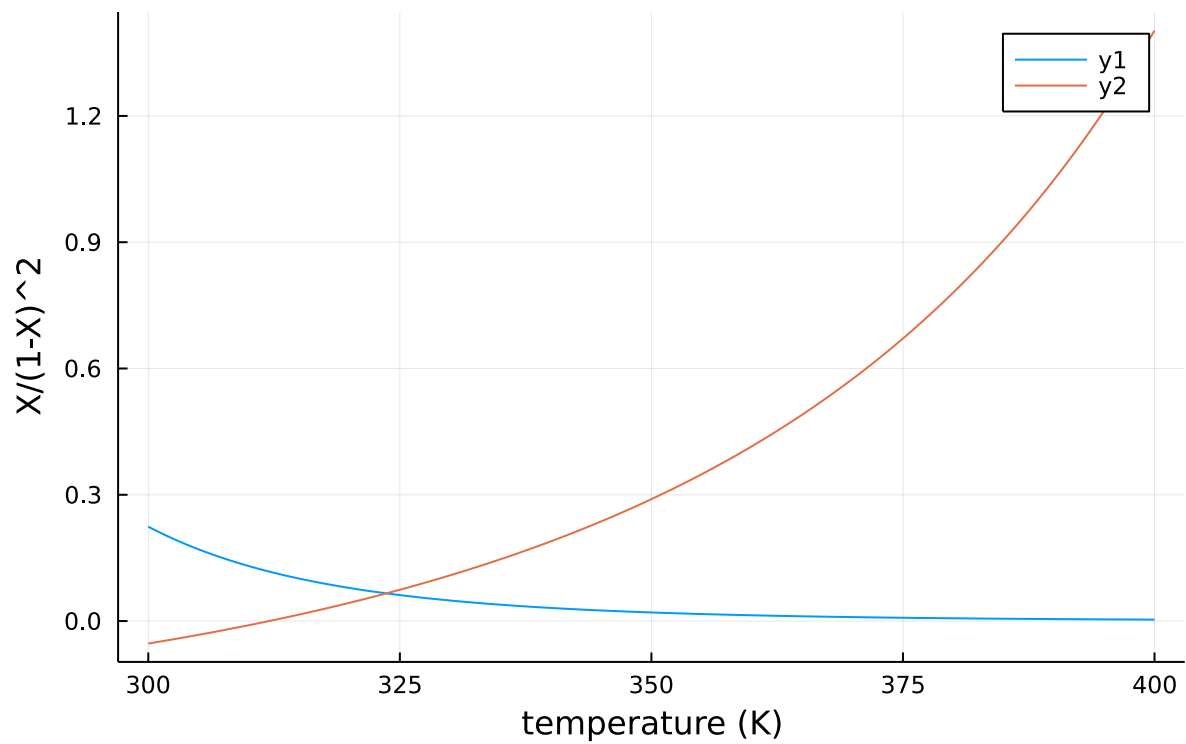
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Repeating for two 250-L reactors in series:

reactor 1: 250.0 L CSTR, 300.0 K inlet



reactor 2: 250.0 L CSTR, 312.0 K inlet



The outlet of the first reactor is at 311.8 and 6.0 % conversion, and the second reactor is at 323.5 K and 11.0 % conversion.

```

• begin
•     local T0 = 300.
•     local V = 250.
•     local Ca0 = 0.1
•
•     # get outlet conditions of first reactor by using above inputs
•     local i = argmin(abs.(y1.(T; V=V, T0=T0, Ca0=Ca0) .- y2.(T; T0=T0)))
•     local t1 = T[i]
•     local x1 = Xeb(t1; T0=T0)
•     local c1 = round(x1, digits=2) * 100
•
•     # get outlet conditions of second reactor by using rxr#1 output as inputs
•     local j = argmin(abs.(y1.(T; V=V, T0=t1, Ca0=(1-x1)*Ca0) .- y2.(T; T0=t1)))
•     local t2 = T[j]
•     local x2 = (1 - Xeb(t2; T0=t1)) * x1 + x1
•     local c2 = round(x2, digits=2) * 100
•
•     md"The outlet of the first reactor is at $t1 and $c1 % conversion, and the second
      reactor is at $t2 K and $c2 % conversion."
• end

```

**(b)**

For the same reaction in a PFR with constant-temperature heat exchanger:

$$\frac{dT}{dV} = \frac{U_a * (T_a - T) + r_A \Delta H}{2C_{A0}(1 - X_A)v_0 C_{p,A}}$$

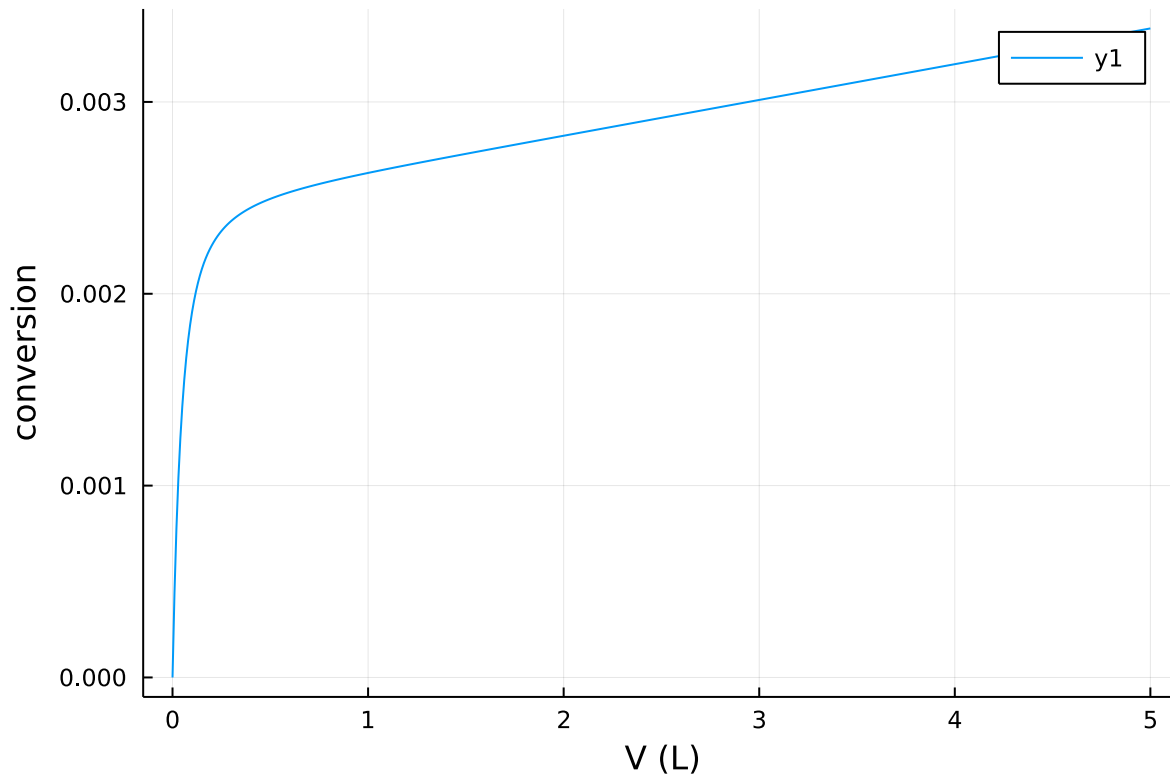
$$\frac{dX}{dV} = \frac{-r_A}{C_{A0}v_0}$$

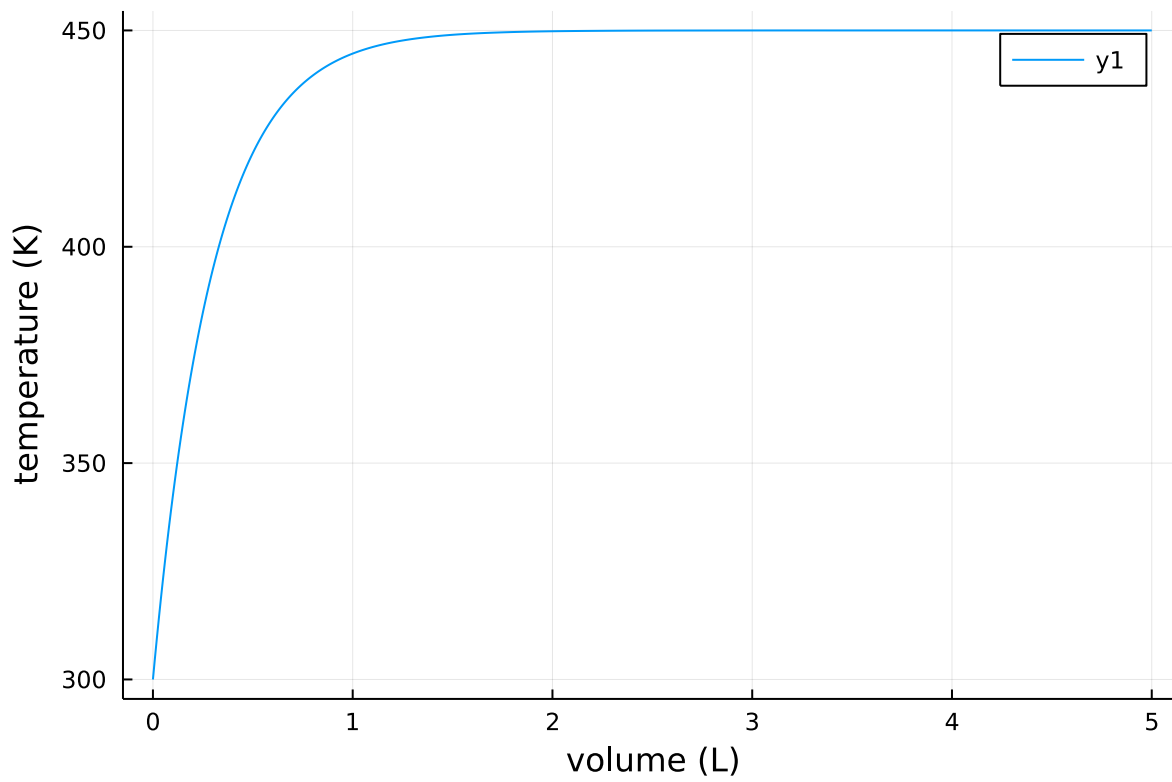
$$r_A = -k^0 \exp \left[ \frac{-E_a}{R} \left( \frac{1}{T^0} - \frac{1}{T} \right) \right] C_{A0}^2 (1 - X_A)^2$$

```

• begin
•     function update_f!(f, u, _, t)
•         X, T = u
•
•         # dX/dV
•         f[1] = -r_a(T, X) / C_a0 / v_0
•
•         # dT/dV
•         f[2] = (U_a * (T_a - T) + r_a(T, X) * ΔH) / (C_a0 * (1 - X) * v_0 * C_p)
•     end
•
•     local X_0 = 0.
•     local T_0 = T^0 = 300.
•     local C_a0 = 0.1
•     local u_0 = [X_0, T_0]
•     local T_a = 450.
•
•     r_a(T, X) = -k^0 * exp(-E_a * (1/T^0 - 1/T) / R) * C_a0^2 * (1 - X)^2
•
•     local prob = ODEProblem(update_f!, u_0, (0., 5.),
•                             saveat=0.01)
•
•     sol_12_7_b = solve(prob)
• end;

```





**(c)**

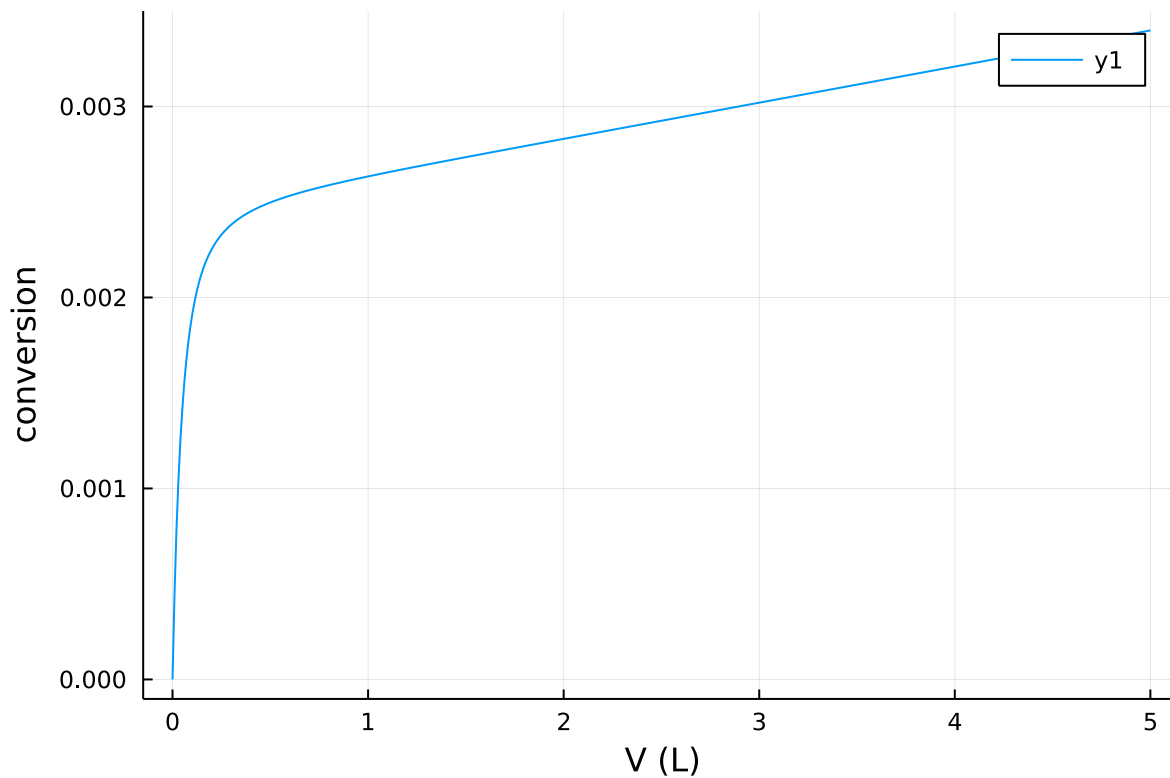
Add the heat exchanger expression:

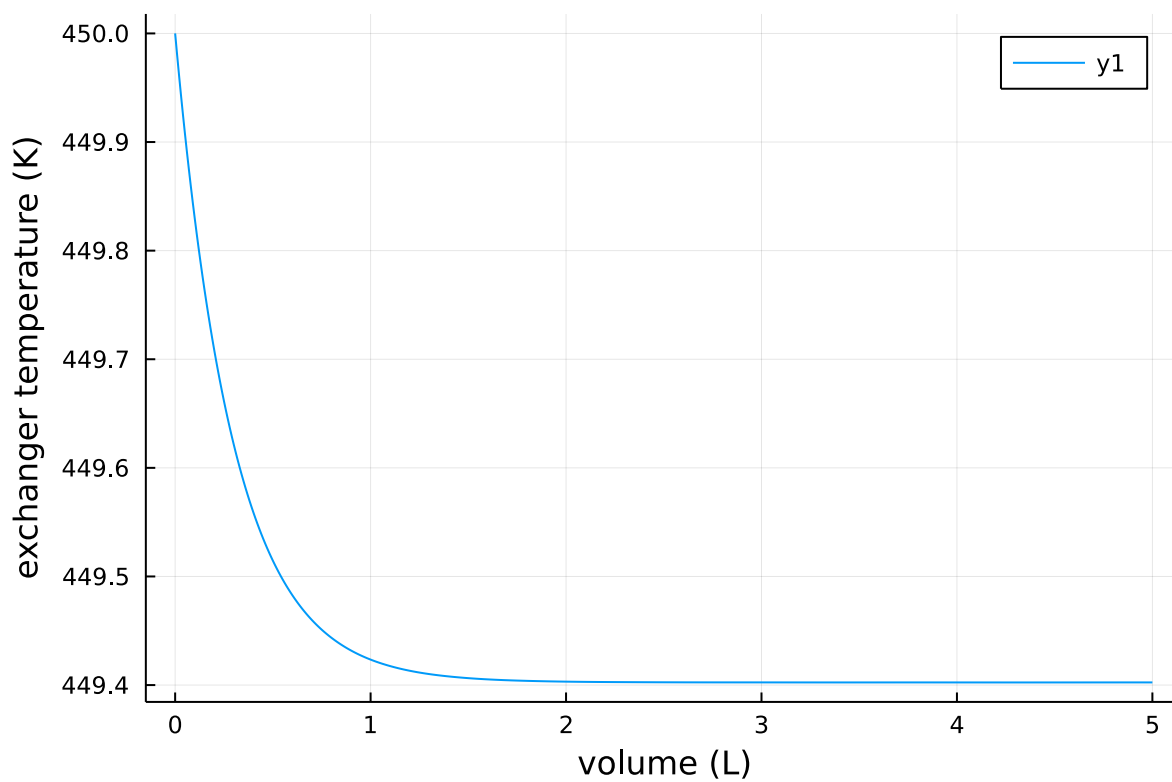
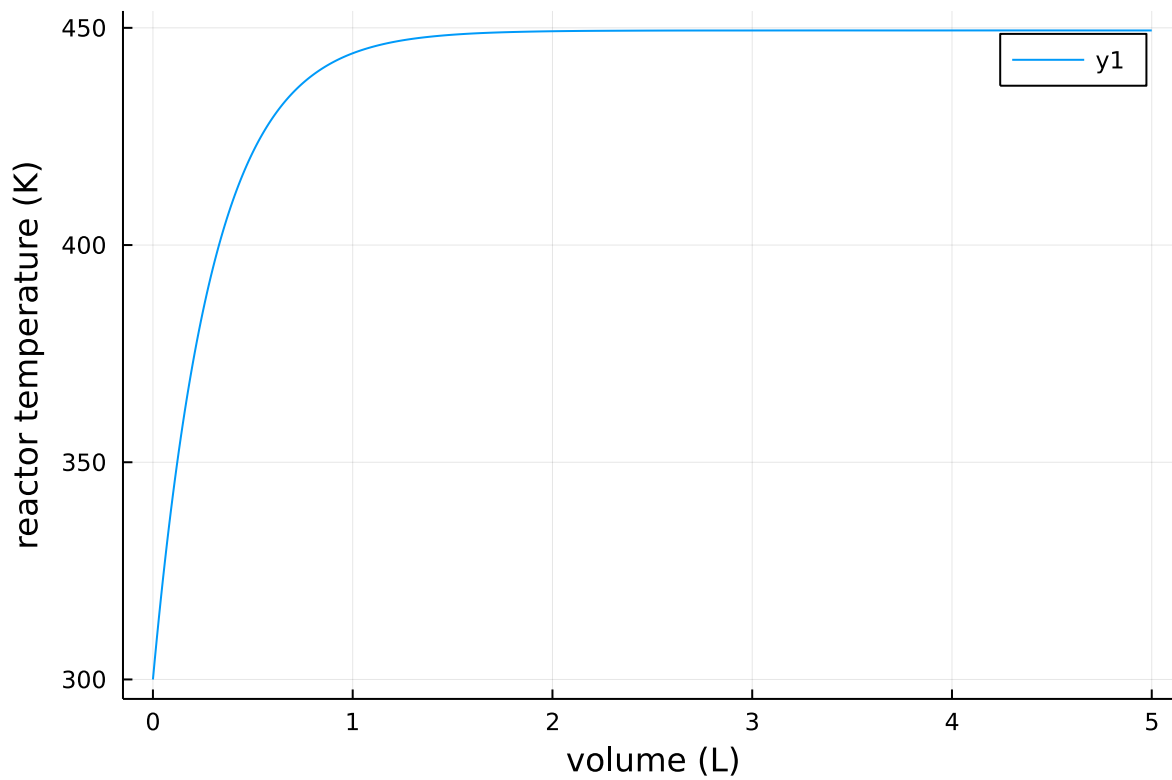
$$\dot{m}_0 c_{p,0} \frac{dT_a}{dV} = U_A (T - T_0)$$

```

• begin
•     function update_f2!(f, u, _, t)
•         X, T, Ta = u
•
•         # dX/dV
•         f[1] = -ra(T, X) / Ca0 / v0
•
•         # dT/dV
•         f[2] = (Ua * (Ta - T) + ra(T, X) * ΔH) / (Ca0 * (1 - X) * v0 * Cp)
•
•         # dTa/dV
•         f[3] = Ua * (T - Ta) / (ṁ0 * Cp)
•     end
•
•     local X0 = 0.
•     local T0 = local T0 = 300.
•     local Ca0 = 0.1
•     local Ta0 = 450.
•     local u0 = [X0, T0, Ta0]
•
•     sol_12_7_c = solve(ODEProblem(update_f2!, u0, (0., 5.),
•                                     saveat=0.01))
• end;

```







(e)

Change the energy balance expression:

$$\frac{dT}{dV} = \frac{r_A \Delta H}{2C_{A0}(1 - X_A)v_0 C_{p,A}}$$

```
• begin
•   function update_f3!(f, u, _, t)
•       X, T = u
•
•       # dX/dV
•       f[1] = -r_a(T, X) / C_a0 / v0
•
•       # dT/dV
•       f[2] = r_a(T, X) * ΔH / (C_a0 * (1 - X) * v0 * C_p)
•   end
•
•   local X0 = 0.
•   local T0 = local T° = 300.
•   local C_a0 = 0.1
•   local T_a0 = 450.
•   local u0 = [X0, T0]
•
•   sol_12_7_e = solve(ODEProblem(update_f3!, u0, (0., 5.),
•                                   saveat=0.01))
• end;
```

