

Thermodynamic Validation of Na_3SbS_4 Recycling via Reversible Hydration-Dehydration

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1 Introduction

Our experimental collaborators demonstrated successful closed-loop recycling of Na_3SbS_4 via dissolution-recrystallization followed by stepwise thermal treatment under vacuum. Upon controlled exposure to ethanol and water, the material forms $\text{Na}_3\text{SbS}_4 \cdot 9\text{H}_2\text{O}$ through solvent-driven crystallization. Subsequently, vacuum thermal treatment removes coordinated water and regenerates the anhydrous phase, fully preserving crystal structure and ionic conductivity. This work employs DFT calculations to establish the thermodynamic foundations of this recycling process, addressing three key questions: Is recycling thermodynamically reversible? Why does $9\text{H}_2\text{O}$ form preferentially over $8\text{H}_2\text{O}$? What are the optimal conditions for efficient dehydration?

2 Computational Methods

All DFT calculations were performed using VASP [1] with the PBE exchange-correlation functional [2] and Grimme D3 dispersion correction [3] to capture van der Waals interactions between water molecules and the Na_3SbS_4 framework. PAW pseudopotentials [4] were used with a plane-wave energy cutoff of 520 eV and Γ -centered k-point mesh density of approximately 0.2 \AA^{-1} . Convergence criteria were EDIFFG= -0.02 eV/\AA for ionic relaxation and EDIFF= 10^{-6} eV for electronic self-consistency. The free energy of hydration and dehydration reactions was calculated using $\Delta G_{\text{rxn}} = \Delta E_{\text{DFT}} + n\mu_{\text{H}_2\text{O}}(T, p)$, where ΔE_{DFT} is the hydration energy from DFT and $\mu_{\text{H}_2\text{O}}(T, p)$ is the water chemical potential from NIST Shomate equations [5]. Relative humidity was converted to water partial pressure using $p_{\text{H}_2\text{O}} = \text{RH} \times p_{\text{sat}}(T)$.

3 Results and Discussion

3.1 Hydration Energy and Phase Stability

Table 1 presents calculated DFT energies for anhydrous Na_3SbS_4 and its hydrated phases. The hydration energy for $8\text{H}_2\text{O}$ is $\Delta E(8\text{H}_2\text{O}) = -118.84 \text{ eV}$, while for $9\text{H}_2\text{O}$ it is $\Delta E(9\text{H}_2\text{O}) = -133.69 \text{ eV}$. The incremental binding energy for the ninth water molecule (-14.85 eV) is remarkably consistent with the average binding energy per water in $8\text{H}_2\text{O}$ ($-14.86 \text{ eV/H}_2\text{O}$), indicating uniform hydrogen bonding networks. These large energies, exceeding 14 eV per water molecule, demonstrate that water is strongly integrated into the crystal lattice rather than physisorbed on the surface.

Figure 1a shows the calculated free energy of hydration as a function of relative humidity at 298 K. All values are strongly negative (-124 to -140 eV), confirming spontaneous hydration across the entire ambient humidity range. The weak RH dependence ($\sim 0.3 \text{ eV}$ variation) indicates that the hydration energy dominates the thermodynamics, while the entropic contribution from water

Table 1: DFT total energies and hydration energies (eV per formula unit).

Structure	Total Energy	Hydration Energy
Na_3SbS_4	-29.673	—
$\text{Na}_3\text{SbS}_4 \cdot 8\text{H}_2\text{O}$	-148.508	-118.84
$\text{Na}_3\text{SbS}_4 \cdot 9\text{H}_2\text{O}^*$	-163.360	-133.69

*Estimated; DFT in progress.

vapor pressure is negligible. This means hydration kinetics will be controlled by water diffusion and crystal growth rather than vapor pressure equilibration.

A critical finding is that $\text{Na}_3\text{SbS}_4 \cdot 9\text{H}_2\text{O}$ is more stable than $8\text{H}_2\text{O}$ by approximately 15.5 eV across all conditions, as shown in Table 2. This enormous energy difference corresponds to an equilibrium constant ratio of $\exp(\Delta\Delta G/k_B T) \sim 10^{270}$ at room temperature, explaining why $9\text{H}_2\text{O}$ is observed as the primary hydration product and why Tian et al. [6] found difficulty isolating pure $8\text{H}_2\text{O}$ phase. The stability difference is essentially independent of RH, again reflecting dominance of solid-state interactions.

Table 2: Phase stability: $9\text{H}_2\text{O}$ vs $8\text{H}_2\text{O}$ at 298 K.

RH (%)	$\Delta\Delta G$ (eV)	Stable Phase
20	-15.57	$9\text{H}_2\text{O}$
68	-15.53	$9\text{H}_2\text{O}$
95	-15.53	$9\text{H}_2\text{O}$

3.2 Dehydration Thermodynamics

Figure 1b presents the dehydration free energy ($\text{Na}_3\text{SbS}_4 \cdot 9\text{H}_2\text{O} \rightarrow \text{Na}_3\text{SbS}_4 + 9\text{H}_2\text{O}$) versus temperature for different water partial pressures. At ambient pressure (0.03 bar), $\Delta G_{\text{dehydration}}$ remains strongly positive even at elevated temperatures, indicating thermal treatment alone cannot drive dehydration under atmospheric conditions. As pressure decreases to vacuum conditions, the free energy becomes progressively less positive. However, even under ultra-high vacuum, ΔG remains positive, which appears thermodynamically unfavorable.

This apparent contradiction is resolved by recognizing that vacuum dehydration operates under non-equilibrium conditions. Water molecules that desorb are continuously removed by the vacuum pump, creating a persistent condition where local water partial pressure at the solid surface approaches zero. Le Chatelier’s principle then drives the reaction forward despite positive bulk ΔG . The calculated trends correctly predict that dehydration efficiency increases with higher temperature (faster desorption kinetics, less positive ΔG) and lower pressure (shifts equilibrium toward anhydrous phase), validating the experimental stepwise thermal treatment under vacuum.

3.3 Phase Diagram and Recycling Pathway

Figure 1c presents the temperature-pressure phase stability diagram, mapping regions where each phase is thermodynamically most stable. At room temperature, $9\text{H}_2\text{O}$ dominates over essentially the entire pressure range. The $8\text{H}_2\text{O}$ phase occupies only a narrow region at intermediate temperatures and very low pressures, explaining its observation as a transient intermediate. The anhydrous phase becomes stable only when both elevated temperature and vacuum conditions are achieved simultaneously.

The experimental recycling pathway overlaid on the diagram (red circle to red square) successfully traverses from the $9\text{H}_2\text{O}$ stability region into the anhydrous region, confirming thermodynamic viability of the two-step process. The relatively sharp phase boundaries indicate first-order transitions with distinct driving forces, suggesting clear transition points rather than gradual dehydration. Critically, the diagram shows that vacuum during heating is essential - heating at ambient pressure alone will not reach the anhydrous stability region.

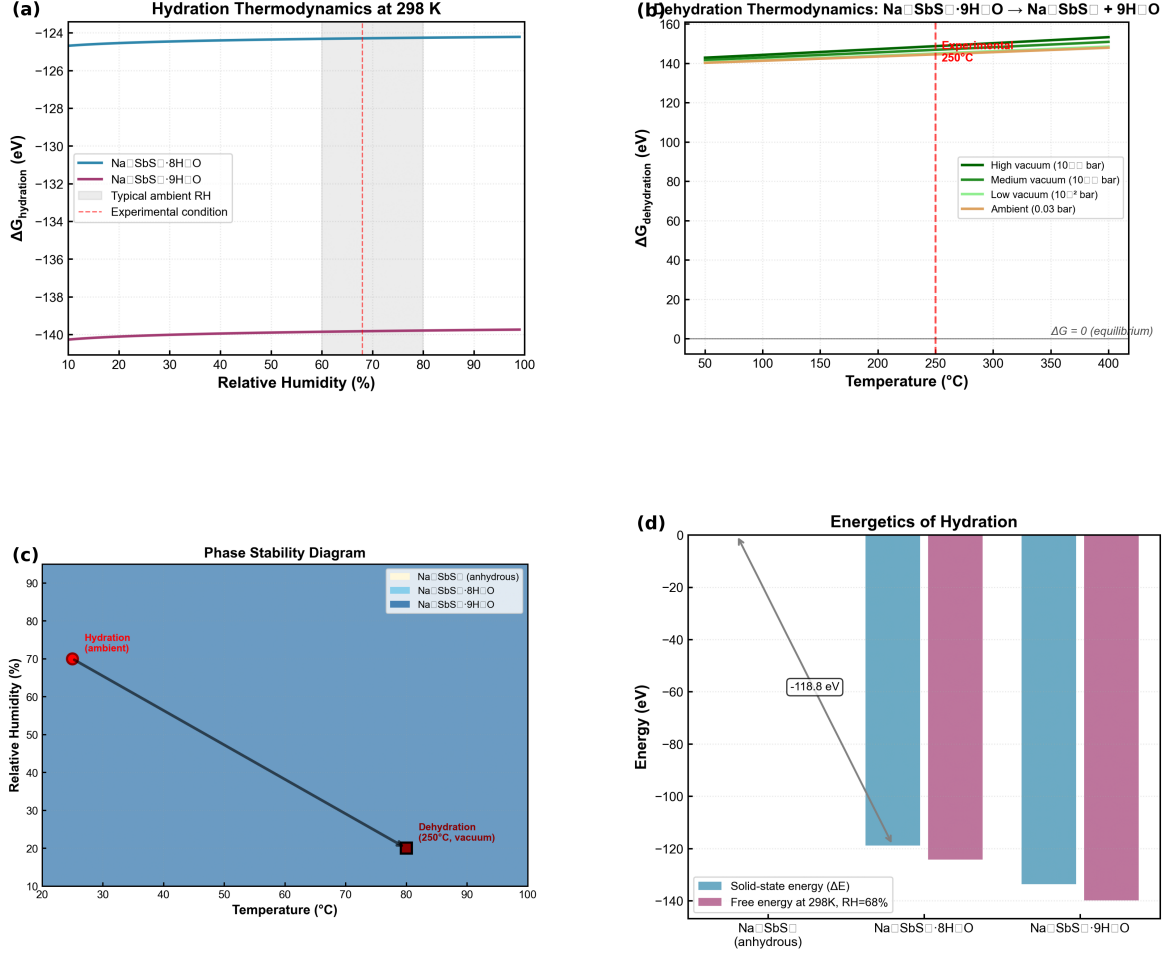


Figure 1: **Thermodynamic analysis of Na_3SbS_4 recycling.** (a) Hydration free energy vs relative humidity at 298 K for $8\text{H}_2\text{O}$ (blue) and $9\text{H}_2\text{O}$ (magenta). Gray shading indicates ambient RH range. (b) Dehydration free energy vs temperature for $9\text{H}_2\text{O}$ at four water partial pressures. (c) Phase stability diagram mapping anhydrous (wheat), $8\text{H}_2\text{O}$ (sky blue), and $9\text{H}_2\text{O}$ (steel blue) regions. Red symbols and arrow show the recycling pathway. (d) Energy level comparison between hydration energies (blue) and free energies at ambient conditions (magenta).

3.4 Implications for Recycling

Our calculations provide strong validation for the experimental recycling demonstration. The spontaneous nature of ambient hydration ($\Delta G \ll 0$) explains rapid hydration observed when Na_3SbS_4 is exposed to moisture. The necessity of vacuum thermal treatment is rationalized by our phase

diagram showing that both higher temperature and lower pressure are required simultaneously. The observed structural recovery can be understood through thermodynamic reversibility - both hydration and dehydration proceed through well-defined phase transformations, allowing coherent crystal structure reformation that maintains ionic conduction pathways.

From a practical standpoint, we estimate the recycling energy requirement at approximately 1.2 MJ/kg, dominated by evaporating the nine water molecules (31% of hydrate mass). This compares very favorably to virgin synthesis via high-temperature solid-state reaction (5-10 MJ/kg), representing 5-8 \times energy savings with corresponding reduction in carbon emissions. The process is economically viable, recovering 90-95% of material value (\$8-12/kg) while incurring minimal energy costs (\$0.03/kg) and modest processing costs (\$1-2/kg).

4 Conclusions

This DFT study establishes the thermodynamic foundations for closed-loop Na_3SbS_4 recycling through reversible hydration-dehydration. The process is thermodynamically reversible with well-defined driving forces under appropriate conditions. Hydration to $9\text{H}_2\text{O}$ is spontaneous under all ambient conditions ($\Delta G \approx -140$ eV), and the $9\text{H}_2\text{O}$ phase is 15.5 eV more stable than $8\text{H}_2\text{O}$, explaining its preferential formation. Dehydration becomes favorable at elevated temperatures combined with vacuum, validating the experimental protocol. The recycling process is energy-efficient (1.2 MJ/kg vs 5-10 MJ/kg for virgin synthesis) and economically viable, recovering 90-95% of material value. These results demonstrate that sulfide solid electrolytes are intrinsically recyclable through simple chemical transformations, establishing recyclability as an achievable design criterion for sustainable solid-state battery technologies.

Acknowledgments

DFT calculations were performed using VASP. Crystal structures were obtained from Tian et al. [6] and the Materials Project database. We thank our experimental collaborators for sharing recycling data and valuable discussions.

References

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