

Figure 1: An example of exact evaluation when m=2

## 1 Proof of Theorem 4.1

*Proof.* Suppose the  $k^{th}$  largest sum is  $S_r = d_{s_1 l_1} + d_{s_2 l_1} + \ldots + d_{s_m l_m}$ .

- For any pair in the combination or queue Q that has already been output, the combinations with indices less than or equal to k must have been popped or exist in Q.
- Construct a chain S, then we have the following chain, denoted as  $S_0 \leq S_1 \leq \ldots \leq S_l$ .

$$d_{s_{1}0} + d_{s_{2}0} + \dots + d_{s_{m}0},$$

$$\geq d_{s_{1}1} + d_{s_{2}0} + \dots + d_{s_{m}0},$$

$$\geq \dots,$$

$$\geq d_{s_{1}l_{1}} + d_{s_{2}0} + \dots + d_{s_{m}0}$$

$$\geq \dots,$$

$$\geq d_{s_{1}l_{1}} + d_{s_{2}l_{2}} + \dots + d_{s_{m}0}$$

$$\geq \dots,$$

$$\geq d_{s_{1}l_{1}} + d_{s_{2}l_{2}} + \dots + d_{s_{m}l_{m}}$$

- Let  $S_j$  be the first sum in chain S which has not been popped from queue Q before the  $j^{th}$  iteration. During the  $j^{th}$  iteration, when  $S_{j-1}$  is popped,  $S_j$  is added to Q.
- For the  $k^{th}$  iteration, the popped sum  $S_k$  satisfies  $S_k \leq S_j \leq S_l = d_{s_1l_1} + d_{s_2l_1} + \ldots + d_{s_ml_m}$ .
- By induction, since the  $(k-1)^{th}$  largest sum has been popped before the  $k^{th}$  iteration, the sum popped in the  $k^{th}$  iteration is exactly the  $k^{th}$  largest sum  $S_l = d_{s_1l_1} + d_{s_2l_1} + \ldots + d_{s_ml_m}$ .

The proof ends. An example is shown when m=2 in Fig.1.

# 2 A Theoretical Quantitative Analysis between Estimation Error and Sample Size

To theoretically quantify the relationship between estimation error and sample size of data, we construct a new random variable S that is the sum of the random variables that make up the

1

Table 1: Relationship between EE and sample size

Estimation error $(\%)$	5	0.5	0.05	0.005
Hoeffding's bound	139	13863	1386295	138629437
Chernoff's bound [1]	278	27726	2772589	277258873
Alamo's bound [2]	1573	15723	157227	1572269

solution of CCMCKP. We also define a Bernoulli variable  $Z \in \{0,1\}$  as below:

$$Z = \begin{cases} 1, & S \le W \\ 0, & S > W \end{cases} \tag{1}$$

Since Z is a Bernoulli variable, the expectation  $\mathbb{E}[Z]$  is also the true confidence level p defined in the original chance constraint. Hoeffding's inequality shows that for independent identically distributed random variables  $Z_1, Z_2, \ldots, Z_L$  taking values [a, b], for any  $\epsilon > 0$ , the following inequality holds,

$$\mathcal{P}(|\mathbb{E}[Z] - \frac{1}{L} \sum_{l=1}^{L} Z_l| \ge \epsilon) \le 2exp(-\frac{2L\epsilon^2}{(b-a)^2})$$
 (2)

We only care about whether the difference between the sample mean and the true confidence is greater than the estimation error  $\epsilon$ . Let  $\mathbb{E}Z = p$  and a = 0, b = 1, the inequality becomes

$$\mathcal{P}(p - f(Z_1, Z_2, \dots, Z_L) \le -\epsilon) \le \exp(-2L\epsilon^2)$$
(3)

where  $f(Z_1, Z_2, ..., Z_L)$  denotes the confidence evaluation algorithm on some combination of items and p is the true confidence level. Assuming that at least 5 of the 10 solutions in the output solution set are true feasible solutions, and  $f(Z_1, Z_2, ..., Z_L)$  is accurate, we have  $1 - exp(-2L\epsilon^2) \ge 5/10$ , leading to

$$L \ge \frac{\ln 2}{2\epsilon^2} \tag{4}$$

The inequality indicates that a large amount of samples is necessary if we do not have other information about the random variables. Practically, it is verified that the amount of data required to meet the corresponding error requirement for the true confidence is much smaller than the theoretical value obtained through Monte Carlo simulation.

## 3 Detailed Adaptation of GDSO and DRO for CCMCKP

#### 3.1 GDSO

Yang and Chakraborty [3] assumed known Gaussian distributions of the random variables in their work. They transformed the chance-constrained knapsack problem into several iterative risk-averse knapsack problems, which could be solved by dynamic programming method. We adapt their method, referred to as the Gaussian-distribution stochastic optimization (GDSO), to address CCMCKP. A statistical fitting approach is first applied to sample data to obtain the means and standard deviations of the Gaussian distributions, i.e.,  $\mu_{ij} = \mathbb{E}(w_{ij}), \sigma_{ij}^2 = Var(w_{ij}), i \in \{1, ..., m\}, j \in N_i$ . The CCMCKP is formulated as below:

$$\min \quad \sum_{i=1}^{m} \sum_{j \in N_i} c_{ij} x_{ij} \tag{5a}$$

s.t. 
$$\sum_{i=1}^{m} \sum_{j \in N_i} \mu_{ij} x_{ij} + \Phi^{-1}(P_0) \sqrt{\sum_{i=1}^{m} \sum_{j \in N_i} \sigma_{ij}^2 x_{ij}} \le W$$
 (5b)

$$\sum_{j \in N_i} x_{ij} = 1, \forall i \in \mathcal{M} \tag{5c}$$

$$x_{ij} \in \{0, 1\}, \forall i \in \mathcal{M}, j \in N_i$$
 (5d)

where  $\Phi$  represents the CDF of a standard normal distribution with zero mean and unit variance. The above optimization problem can be transformed into risk-averse multiple-choice knapsack problem as below:

$$\min \quad \sum_{i=1}^{m} \sum_{j \in N_i} c_{ij} x_{ij} \tag{6a}$$

s.t. 
$$\sum_{i=1}^{m} \sum_{j \in N_i} (\mu_{ij} + \lambda \sigma_{ij}^2) x_{ij} \le W'$$
 (6b)

$$\sum_{j \in N_i} x_{ij} = 1, \forall i \in \mathcal{M}$$
 (6c)

$$x_{ij} \in \{0,1\}, \forall i \in \mathcal{M}, j \in N_i \tag{6d}$$

where  $\lambda$  is risk-averse parameter and W' is the adapted W in the original CCMCKP.

#### 3.2 DRO

Ji and Lejeune [4] studied distributionally robust multidimensional knapsack problem with Wasserstein ambiguity sets. To fit the chance constraint into Ji's framework, we reformulate the chance constraint as:

$$\mathcal{P}(\sum_{i=1}^{m} \sum_{j \in N_i} w_{ij} x_{ij} > W) \le 1 - P_0 \tag{7}$$

Then we define  $b = -W, \epsilon = 1 - P_0, \tilde{w}_{ij} = -w_{ij}, \forall i \in \mathcal{M}, j \in N_i. \ \bar{x} \in \{0, 1\}^{NM}$  is the vectorization of  $x \in \{0, 1\}^{N \times M}$ , and  $\xi \in \mathbb{R}^{NM}$  is the vectorization of  $\hat{w} \in \mathbb{R}^{N \times M}$ . Finally, we have the standard form as [4]:

$$\mathcal{P}(\xi^T \bar{x} < b) \le \epsilon \tag{8}$$

We utilize Theorem 10 in [4] to reformulate the inequation (7), and get the MILP formulation of

CCMCKP:

P:
$$(\bar{x}, \lambda, \eta, s, \phi) \in \mathcal{Z}_{LP}^{MCKP} = \begin{cases} \lambda \theta + \frac{1}{L} \sum_{l=1}^{L} s_{l} \leq \epsilon, \\ \lambda \geq 0, \\ s_{l} \geq 0, \eta_{l} \geq 0, \end{cases} & \forall l \in \mathcal{L} \\ 1 + \eta_{l}b' - \sum_{q \in \mathcal{Q}} \xi_{ql}^{0} \phi_{ql} \leq s_{l}, & \forall l \in \mathcal{L} \\ \phi_{ql} \leq \lambda, & \forall q \in \mathcal{Q}, l \in \mathcal{L} \\ \phi_{ql} \leq \eta_{l}, & \forall q \in \mathcal{Q}, l \in \mathcal{L} \\ \phi_{ql} \leq U_{\eta_{l}} \bar{x}_{q}, & \forall q \in \mathcal{Q}, l \in \mathcal{L} \\ \phi_{ql} \geq 0, & \forall q \in \mathcal{Q}, l \in \mathcal{L} \\ \phi_{ql} \geq \eta_{l} + U_{\eta_{l}} \bar{x}_{q} - U_{\eta_{l}}, & \forall q \in \mathcal{Q}, l \in \mathcal{L} \\ \sum_{i=Nm-N+1}^{Nm} \bar{x}_{i} = 1, & \forall m \in \mathcal{M} \\ \bar{x}_{q} \in \{0,1\}, & \forall q \in \mathcal{Q} \end{cases}$$

where  $b' = b - \delta$ ,  $\delta$  is a user-defined infinite small positive number.  $\mathcal{Q}$  is the set of all  $N \times M$  items, and  $\mathcal{M}$  is the set of M classes. Note that  $\sum_{i=N}^{Nm} \bar{x}_i = 1, \forall m \in \mathcal{M}$  is the multiple-choice constraint in the CCMCKP.  $U_{\eta}$  is the upper bound of  $\eta$  and can be determined by:

$$U_{\eta_l} = \begin{cases} \mathcal{K}'^*, & if \quad \exists \bar{x} : \bar{x}^T \xi_l^0 - b > 0 \\ 0, & otherwise \end{cases}$$
 (10)

where  $\mathcal{K}^{\prime *}$  is the optimal objective value of the linear programming problem:

$$\mathcal{K}'^{*} = \min \bar{x}^{T} \xi_{l}^{0} - b$$
s.t.  $b - \bar{x}^{T} \xi_{l}^{0} \leq 0 - \tau'$ 

$$\bar{x} \in \bar{\mathcal{X}}$$
(11)

where  $\tau'$  is a user-defined small non-negative number. Based on the reformulation of CCMCKP, we first solve (11) and obtain  $U_{\eta_l}, \forall l \in \mathcal{L}$ . The the MILP  $\mathcal{Z}_{LP}^{MCKP}$  is solved with Gurobi solver. The optimal solution of MILP is also the optimal solution of CCMCKP.

# 4 Full experimental results

Full results on the problem instances of LAB and APP in Section VI-C are presented in Table 2 and Table 3, respectively.

### References

- [1] R. Tempo, E.-W. Bai, and F. Dabbene, "Probabilistic robustness analysis: Explicit bounds for the minimum number of samples," in *Proceedings of 35th IEEE Conference on Decision and Control*, vol. 3. IEEE, 1996, pp. 3424–3428.
- [2] T. Alamo, R. Tempo, and A. Luque, "On the sample complexity of randomized approaches to the analysis and design under uncertainty," in *Proceedings of the 2010 American Control Conference*. IEEE, 2010, pp. 4671–4676.
- [3] F. Yang and N. Chakraborty, "Algorithm for optimal chance constrained knapsack problem with applications to multi-robot teaming," in 2018 IEEE International Conference on Robotics and Automation (ICRA). IEEE, 2018, pp. 1043–1049.
- [4] R. Ji and M. A. Lejeune, "Data-driven distributionally robust chance-constrained optimization with wasserstein metric," *Journal of Global Optimization*, vol. 79, no. 4, pp. 779–811, 2021.

Table 2: Full results of performance on the problem instances of LAB.

Table 2: Full results of performance on the problem instances of LAB.													
Benchmark	small $T_{ m max}$						large $T_{ m max}$						
	C	ET	ECL	RCL	FSR	Time	$\mathbf{C}$	ET	ECL	RCL	FSR	Time	
ss1-Greedy	$22.2{\pm}0.0$	$2.0\pm0.0$	0±0.0	$99.6 {\pm} 0.0$	1	$\underline{0.1{\pm}0.0}$	$\underline{10.8{\pm}0.0}$	$4.0 \pm 0.0$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$\underline{0.1{\pm}0.0}$	
ss1-GA	18.7±0.1	356.2±4.9	99.8±0.3	99.7±0.7	0.87	7.1±0.5	10.8±0.1	233.7±3.8	99.9±0.1	99.5±0.9	0.87	3.1±0.3	
ss1-EDA ss1-DDALS(O)	21.2±1.6 18.6±0.0	$354.3\pm2.8$ $349.5\pm7.6$	29.9±45.7 99.9±0.0	$99.5\pm0.5$ $99.9\pm0.0$	0.93 <u>1</u>	$8.8\pm3.6$ $2.2\pm0.1$	$12.8\pm2.4$ $10.8\pm0.0$	$234.6\pm2.8$ $234.6\pm17.2$	$99.8\pm0.3$ $99.9\pm0.0$	$99.7\pm0.6$ $99.9\pm0.0$	0.9 <u>1</u>	$2.4\pm1.2$ $1.7\pm0.3$	
ss1-DDALS(V1)	$\frac{18.6\pm0.0}{18.6\pm0.0}$	349.5±7.6	99.9±0.0	99.9±0.0	1	2.2±0.1	$\frac{10.8\pm0.0}{10.8\pm0.0}$	$234.6\pm17.2$	99.9±0.0	99.9±0.0	1	1.7±0.3	
ss1-DDALS(V2)	$18.6{\pm}0.0$	$349.5{\pm}7.6$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$2.2 {\pm} 0.1$	$\overline{10.8{\pm}0.0}$	$234.6 {\pm} 17.2$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$1.7 \pm 0.3$	
ss1-DDALS(V3)	$20.7{\pm}2.0$	345	$74.7 \pm 0.4$	$99.3 \pm 0.8$	0.75	2.3	$13.0 \pm 1.7$	228	$99.8 \pm 0.3$	$99.1 \pm 1.0$	0.7	1.7	
ss2-Greedy	$\underline{19.4{\pm}0.0}$	$2.0 \pm 0.0$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	<u>1</u>	$\underline{3.9{\pm}0.1}$	$13.8 {\pm} 0.0$	$4.0 {\pm} 0.0$	$99.5 {\pm} 0.0$	$99.0 {\pm} 0.0$	1	$\underline{7.3{\pm}0.2}$	
ss2-GA	$\frac{19.4\pm0.0}{10.0\pm0.4}$	385.6±3.9	99.9±0.0	99.9±0.0	1	555.9±133.9	11.4±1.6	308.5±6.0	99.8±0.1	99.8±0.3	1	1311.7±217.9	
ss2-EDA ss2-DDALS(O)	$19.8\pm0.4$ $19.4\pm0.0$	$384.7\pm2.8$ $387.2\pm5.2$	99.9±0.0 99.9±0.0	$99.9\pm0.0$ $99.9\pm0.0$	<u>1</u> <u>1</u>	$144.3\pm29.2$ $1241.9\pm73.9$	$15.5\pm2.3$ $10.4\pm0.0$	$305.0\pm3.1$ $302.0\pm10.7$	$99.7\pm0.2$ $99.8\pm0.0$	$99.7\pm0.3$ $99.9\pm0.0$	$\frac{1}{1}$	$582.4\pm476.3$ $555.1\pm80.6$	
ss2-DDALS(V1)	$\frac{19.4\pm0.0}{19.4\pm0.0}$	387.2±5.2	99.9±0.0	99.9±0.0	1	$1241.9\pm73.9$ $1241.9\pm73.9$	$\frac{10.4\pm0.0}{10.4\pm0.0}$	302.0±10.7	99.8±0.0	$99.9\pm0.0$	1	555.1±80.6	
ss2-DDALS(V2)	$19.4{\pm}0.0$	$387.2 \pm 5.2$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$1241.9 \pm 73.9$	12.1±2.0	$302.0{\pm}10.7$	$99.9 {\pm} 0.1$	$99.9 {\pm} 0.0$	1	$555.1 \pm 80.6$	
ss2-DDALS(V3)	$21.8 \pm 2.4$	392	$99.9 \pm 0.0$	$99.9\pm0$	1	1228.1	$14.3 \pm 2.2$	296	$99.8 \pm 0.2$	$99.8 \pm 0.3$	1	432.5	
ss3-Greedy	$\underline{21.4{\pm}0.0}$	$3.0 \pm 0.0$	$99.9 {\pm} 0.0$	$99.5 {\pm} 0.0$	<u>1</u>	$\underline{0.2{\pm}0.0}$	$17.4 {\pm} 0.0$	$4.0 {\pm} 0.0$	$100.0 {\pm} 0.0$	$100.0 {\pm} 0.0$	1	$\underline{0.4\pm0.0}$	
ss3-GA	22.4±1.4	306.0±3.7	99.9±0.0	99.7±0.2	1	31.7±1.9	14.2±2.4	263.5±2.9	99.7±0.4	99.2±1.3	0.73	37.9±1.1	
ss3-EDA ss3-DDALS(O)	$24.8\pm1.9$ $21.4\pm0.0$	$305.3\pm3.0$ $288.5\pm9.3$	$99.9\pm0.1$ $99.9\pm0.0$	$99.8\pm0.5$ $99.5\pm0.0$	0.93 <u>1</u>	$44.1\pm3.0$ $9.6\pm0.5$	$13.7\pm1.3$ $12.6\pm0.0$	$264.5\pm2.8$ $254.4\pm4.7$	$99.9\pm0.0$ $100.0\pm0.0$	$99.9\pm0.1$ $99.9\pm0.0$	$\frac{1}{1}$	$42.8\pm3.4$ $14.7\pm0.9$	
ss3-DDALS(V1)	$\frac{21.1\pm0.0}{21.4\pm0.0}$	288.5±9.3	99.9±0.0	99.5±0.0	1	9.6±0.5	$\frac{12.6\pm0.0}{12.6\pm0.0}$	254.4±4.7	100.0±0.0	99.9±0.0	1	14.7±0.9	
ss3-DDALS(V2)	$21.4{\pm}0.0$	$288.5 \pm 9.3$	$99.9 {\pm} 0.0$	$99.5 {\pm} 0.0$	1	$9.6 {\pm} 0.5$	$12.6{\pm}0.0$	$254.4 \pm 4.7$	$100.0 \pm 0.0$	$99.9 {\pm} 0.0$	1	$14.7 {\pm} 0.9$	
ss3-DDALS(V3)	$23.9 {\pm} 1.7$	284	$99.8 {\pm} 0.2$	$99.1 {\pm} 0.8$	0.75	9.1	$15.5 {\pm} 1.7$	264	$99.9 {\pm} 0.3$	$99.5 {\pm} 0.9$	0.9	14.9	
ss4-Greedy	30.1±0.0	2.0±0.0	$99.9 \pm 0.0$	$99.9 \pm 0.0$	1	$0.1 \pm 0.0$	$14.9 \pm 0.0$	$5.0\pm0.0$	$99.9 \pm 0.0$	$99.9 \pm 0.0$	1	$0.3 \pm 0.0$	
ss4-GA	23.1±4.4	$773.5\pm8.0$ $764.5\pm3.0$	99.9±0.2	99.7±0.4	1	65.6±2.5	$16.4\pm3.0$	559.3±8.8	99.8±0.3	99.4±0.6	$0.9 \\ 0.93$	60.9±3.1	
ss4-EDA ss4-DDALS(O)	$\frac{17.4 \pm 0.0}{17.4 \pm 0.0}$	757.9±31.9	99.9±0.0 99.9±0.0	$99.9\pm0.0$ $99.9\pm0.0$	<u>1</u> <u>1</u>	$98.8\pm1.7$ $21.4\pm1.0$	$13.4\pm1.0$ $11.2\pm0.0$	$554.3\pm2.6$ $538.8\pm31.9$	$99.8\pm0.2$ $99.2\pm0.0$	$99.1\pm0.41$ $99.0\pm0.0$	0.93 <u>1</u>	$83.5\pm3.3$ $23.6\pm1.1$	
ss4-DDALS(V1)	$\frac{17.4\pm0.0}{17.4\pm0.0}$	757.9±31.9	99.9±0.0	99.9±0.0	1	21.4±1.0	12.3±0.7	538.8±31.9	99.6±0.1	$98.9\pm0.2$	1	23.6±1.1	
ss4-DDALS(V2)	$\overline{17.4{\pm}0.0}$	$757.9 \pm 31.9$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$21.4 \pm 1.0$	$14.1 {\pm} 0.9$	$538.8 \pm 31.9$	$99.9 {\pm} 0.2$	$99.0 {\pm} 0.1$	1	$23.6 {\pm} 1.1$	
ss4-DDALS(V3)	$25.3 \pm 4.1$	822	$99.8 \pm 0.2$	$99.6 \pm 0.5$	1	22.9	$14.3 \pm 1.5$	514	$99.6 \pm 0.3$	$99.2 \pm 0.7$	0.9	24.1	
ls1-Greedy	$58.5 \pm 0.0$	$2.0\pm0.0$	$99.8 \pm 0.0$	99.8±0.0	1	$0.3 \pm 0.0$	$45.2\pm0.0$	$4.0\pm0.0$	$99.7\pm0.0$	$99.4 \pm 0.0$	1	$0.6 \pm 0.1$	
ls1-GA ls1-EDA	$50.8\pm1.0$ $54.3\pm1.7$	$3009.2\pm8.5$ $3004.9\pm2.5$	$99.2\pm0.2$ $99.2\pm0.1$	$99.2\pm0.2$ $99.3\pm0.1$	1	$776.1\pm30.2$ $678.1\pm7.6$	$40.7\pm4.2$ $36.9\pm1.9$	$1411.0\pm9.0$ $1403.6\pm2.7$	$99.5\pm0.3$ $99.3\pm0.1$	$99.3\pm0.4$ $99.3\pm0.0$	0.9	$458.3\pm9.4$ $417.2\pm8.1$	
ls1-DDALS(O)	$49.7\pm0.1$	2924.1±50.1	99.2±0.1 99.3±0.1	99.3±0.1 99.2±0.0	1 1	476.7±14.6	$30.9\pm1.9$ $32.0\pm0.0$	1387.8±24.5	99.2±0.0	$99.3\pm0.0$ $99.1\pm0.0$	$\frac{1}{1}$	$240.0\pm6.2$	
ls1-DDALS(V1)	52.2±0.4	$2924.1 \pm 50.1$	99.6±0.1	99.5±0.1	1	$476.7 \pm 14.6$	34.4±0.7	$1387.8\pm24.5$	99.6±0.0	99.5±0.1	1	240.0±6.2	
ls1-DDALS(V2)	$50.0 {\pm} 0.4$	$2924.1 \pm 50.1$	$99.3 \pm 0.0$	$99.3 {\pm} 0.1$	<u>1</u>	$476.7 \pm 14.6$	$34.1 \pm 1.7$	$1387.8 \pm 24.5$	$99.5 {\pm} 0.2$	$99.5 {\pm} 0.2$	1	$240.0{\pm}6.2$	
ls1-DDALS(V3)	51.9±1.1	2889	99.3±0.2	99.3±0.2	1	475.2	34.7±1.3	1357	99.4±0.2	99.3±0.2	1	233.2	
ls2-Greedy	66.6±0.0	2.0±0.0	99.7±0.0	99.7±0.0	1	0.3±0.0	66.6±0.0	2.0±0.0	100.0±0.0	100.0±0.0	1	0.3±0.0	
ls2-GA ls2-EDA	$53.0\pm3.2$ $50.9\pm3.1$	$9626.6\pm20.4$ $9604.7\pm2.9$	99.1±0.1 99.0±0.0	99.1±0.2 99.2±0.0	1 1	$2106.4\pm68.7$ $1955.5\pm17.2$	$44.4\pm6.8$ $38.9\pm2.8$	$3315.4\pm14.1$ $3304.4\pm2.9$	$99.4\pm0.3$ $99.5\pm0.2$	$99.4\pm0.3$ $99.6\pm0.2$	1 1	$806.4\pm32.0$ $902.6\pm23.7$	
ls2-DDALS(O)	$47.9\pm0.0$	9628.4±89.2	99.0±0.0	99.0±0.0	1	815.0±16.3	$27.2\pm0.0$	3191.7±71.5	99.3±0.0	99.3±0.0	1	373.4±11.6	
ls2-DDALS(V1)	53.3±2.3	$9628.4 \pm 89.2$	$99.4 {\pm} 0.0$	$99.5 {\pm} 0.0$	1	$815.0 {\pm} 16.3$	$28.0 \pm 0.7$	$3191.7 \pm 71.5$	$99.6 {\pm} 0.0$	$99.6 {\pm} 0.1$	1	$373.4 {\pm} 11.6$	
ls2-DDALS(V2)	49.7±0.9	9628.4±89.2	99.3±0.1	99.3±0.1	1	815.0±16.3	28.4±0.9	3191.7±71.5	99.6±0.2	99.7±0.2	1	373.4±11.6	
ls2-DDALS(V3)	50.8±1.7	9682	99.2±0.2	99.2±0.2	1	816.1	29.2±1	3072	99.4±0.2	99.4±0.3	1	356.9	
$ m ls3\text{-}Greedy \\  m ls3\text{-}GA$	$100.9\pm0.0$ $83.4\pm4.6$	$3.0\pm0.0$ $7209.0\pm7.3$	$99.9\pm0.0$ $99.1\pm0.1$	99.8±0.0 98.8±0.2	1	$\underline{1.0\pm0.0}$ 52257.1 $\pm$ 127.9	$101.2\pm0.0$ $73.9\pm5.8$	$5.0\pm0.0$ $5210.3\pm8.4$	$99.83\pm0.0$ $99.2\pm0.3$	$98.5\pm0.0$ $99.2\pm0.3$	0	$\frac{1.7\pm0.0}{3499.6\pm73.8}$	
ls3-EDA	82.2±1.3	$7209.0\pm7.3$ $7204.9\pm2.4$	99.1±0.1 99.1±0.2	98.9±0.2	1 1	3924.2±137.9	$73.9\pm3.6$ $74.8\pm3.4$	$5210.3\pm 8.4$ $5204.5\pm 2.4$	$99.2\pm0.3$ $99.7\pm0.2$	$99.2\pm0.3$ $99.6\pm0.3$	$\frac{1}{1}$	3132.0±82.4	
ls3-DDALS(O)	$\textbf{74.9} {\pm} \textbf{0.2}$	$7276.1\pm68.6$	99.1±0.0	98.7±0.0	1	$2534.7\pm29.4$	$63.4{\pm}0.9$	$5182.9 \pm 197.4$	99.4±0.2	99.3±0.2	1	$1785.0\pm73.6$	
ls3-DDALS(V1)	$79.6 \pm 1.5$	$7276.1 \pm 68.6$	$99.6 {\pm} 0.1$	$99.4 {\pm} 0.1$	1	$2534.7 \pm 29.4$	$64.4{\pm}1.9$	$5182.9{\pm}197.4$	$99.6 {\pm} 0.1$	$99.5 {\pm} 0.2$	1	$1785.0 \pm 73.6$	
ls3-DDALS(V2)	$76.6\pm1.2$	7276.1±68.6	99.4±0.1	99.2±0.1	1	2534.7±29.4	64.8±1.7	5182.9±197.4	99.7±0.2	99.7±0.2	1	1785.0±73.6	
ls3-DDALS(V3)	77.1±1.3	7290	99.3±0.1	99.0±0.2	1	2520.8	63.8±0.5	5114	99.3±0.2	99.1±0.3	1	1750.2	
ls4-Greedy ls4-GA	$167.5\pm0.0$ $124.1\pm8.7$	$7.0\pm0.0$ $11309.8\pm7.4$	99.2±0.0 99.1±0.2	99.1±0.0 99.1±0.3	1 0.97	$\frac{3.5\pm0.0}{12310.4\pm282.8}$	$167.6\pm0.0$ $107.5\pm6.8$	$8.0\pm0.0$ $8411.4\pm9.8$	$99.9\pm0.0$ $99.1\pm0.1$	$99.9\pm0.0$ $99.0\pm0.3$	1 0.93	$\frac{3.7\pm0.2}{8437.8\pm157.5}$	
ls4-EDA	$123.6\pm3.6$	11305.1±3.4	99.3±0.2	99.4±0.2	1	9498.8±243.3	116.6±3.2	8403.9±3.1	99.6±0.2	$99.7\pm0.2$	1	7970.2±162.7	
ls4-DDALS(O)	$\underline{107.1{\pm}1.0}$	$11360.9{\pm}206.6$	$99.1 \pm 0.1$	$99.2 {\pm} 0.1$	1	$5537.5 \pm 95.9$	$\underline{92.6{\pm}1.1}$	$8483.8 \pm 335.8$	$99.1 \pm 0.1$	$99.0 {\pm} 0.3$	0.93	$4113.9{\pm}147.9$	
ls4-DDALS(V1)	$109.5\pm0.5$ $108.9\pm1.1$	$11360.9\pm206.6$ $11360.9\pm206.6$	$99.7\pm0.1$	99.7±0.1	1	5537.5±95.9	98.8±2.1	8483.8±335.8	99.6±0.1	$99.6\pm0.1$	1	4113.9±147.9	
ls4-DDALS(V2) ls4-DDALS(V3)	$108.9\pm1.1$ $110.8\pm3.5$	11360.9±206.6 11576	$99.6\pm0.2$ $99.3\pm0.2$	$99.6\pm0.2$ $99.4\pm0.2$	1 1	$5537.5\pm95.9$ 5651.3	$94.4\pm2.0$ $95.1\pm2.5$	8483.8±335.8 7964	$99.4\pm0.2$ $99.1\pm0.1$	$99.3\pm0.3$ $99.3\pm0.1$	$\frac{1}{1}$	$4113.9\pm147.9$ 3883.5	
ls5-Greedy	226.7±0.0	2.0±0.0	99.9±0.0	99.9±0.0	1	1.0±0.1	216.5±0.0	5.0±0.0	99.8±0.0	99.8±0.0	1	2.9±0.2	
ls5-GA	$191.6 \pm 6.3$	$29012.8 \pm 9.4$	$99.0 {\pm} 0.0$	$98.9 {\pm} 0.1$	1	$441\overline{67.0\pm53}6.9$	$165.6 \pm 9.6$	18311.6±8.5	99.1±0.1	$98.9 {\pm} 0.2$	0.97	$24188.0\pm369.9$	
ls5-EDA	195.8±3.1	29004.5±2.8	99.2±0.1	99.0±0.2	1	30259.7±544.7	$168.5 \pm 4.0$	18303.9±3.3	99.4±0.2	99.4±0.2	1	22596.0±330.0	
ls5-DDALS(O)	$\frac{178.2\pm0.9}{184.5\pm2.2}$	28935.6±446.0	99.0±0.0	98.9±0.0	1	18837.0±279.3	$\frac{145.3\pm1.5}{155.0\pm3.6}$	18509.9±825.5	99.0±0.0	99.0±0.0	1	11986.4±506.2	
ls5-DDALS(V1) ls5-DDALS(V2)	$184.5\pm2.2$ $180.9\pm2.0$	$28935.6\pm446.0$ $28935.6\pm446.0$	$99.3\pm0.0$ $99.2\pm0.1$	99.2±0.0 99.1±0.1	1 1	$18837.0\pm279.3$ $18837.0\pm279.3$	$155.9\pm3.6$ $148.4\pm3.2$	$18509.9\pm825.5$ $18509.9\pm825.5$	$99.5\pm0.1$ $99.3\pm0.2$	$99.5\pm0.1$ $99.3\pm0.2$	<u>1</u> <u>1</u>	$11986.4\pm506.2$ $11986.4\pm506.2$	
ls5-DDALS(V3)	180.0±1.8	28519	99.0±0.0	98.9±0.0	1	18654.3	$145.4\pm3.2$ $145.6\pm1.0$	17804	99.1±0.1	$99.1\pm0.1$	1	11506.5	
ls6-Greedy	266.2±0.0	2.0±0.0	99.9±0.0	99.9±0.0	1	1.7±0.0	260.9±0.0	4.0±0.0	99.8±0.0	99.8±0.0	1	3.2±0.0	
ls6-GA	$226.1 \pm 10.9$	$34609.0 \pm 8.2$	$99.0 \pm 0.1$	$98.9 {\pm} 0.1$	<u>1</u>	$62450.7 \pm 680.7$	$192.7{\pm}13.8$	$20213.2{\pm}10.3$	$99.0 {\pm} 0.1$	$99.0 {\pm} 0.1$	<u>1</u>	$38172.5 \pm 307.5$	
ls6-EDA	215.5±1.1	34604.7±2.7	99.3±0.1	99.2±0.2	1	43323.9±115.5	181.9±3.3	20204.8±2.9	99.4±0.2	99.4±0.2	1	31784.8±192.8	
ls6-DDALS(O) ls6-DDALS(V1)	$\frac{198.9 \pm 0.8}{205.3 \pm 1.7}$	$34546.2\pm496.2$ $34546.2\pm496.2$	$99.0\pm0.0$ $99.5\pm0.1$	$98.9\pm0.1$ $99.4\pm0.1$	1 1	28114.3±402.1 28114.3±402.1	$\frac{161.7\pm1.3}{169.3\pm2.3}$	$20060.4\pm974.6$ $20060.4\pm974.6$	$99.1\pm0.1$ $99.5\pm0.1$	$99.0\pm0.1$ $99.5\pm0.1$	1	$15872.1\pm537.1$ $15872.1\pm537.1$	
ls6-DDALS(V1)	205.5±1.7 201.5±1.7	$34546.2\pm496.2$ $34546.2\pm496.2$	99.3±0.1 99.3±0.1	99.4±0.1 99.2±0.1	<u>1</u>	28114.3±402.1 28114.3±402.1	$169.3\pm2.3$ $163.4\pm2.3$	20060.4±974.6 20060.4±974.6	$99.3\pm0.1$ $99.4\pm0.1$	$99.3\pm0.1$ $99.3\pm0.1$	$\frac{1}{1}$	15872.1±537.1 15872.1±537.1	
ls6-DDALS(V3)	$203.1 \pm 2.1$	34251	$99.1 \pm 0.1$	99.1±0.2	1	27936.2	$164.0 \pm 1.6$	18641	99.2±0.2	$99.1 \pm 0.2$	1	15077.8	

	Table 3: Full results of performance on the problem instances of APP.											
Benchmark	small $T_{ m max}$					large $T_{ m max}$						
	C	ET	ECL	RCL	FSR	Time	C	ET	ECL	RCL	FSR	Time
ss1-Greedy	$14.0 {\pm} 0.0$	$4.0 \pm 0.0$	$99.9 {\pm} 0.0$	$97.2 \pm 0.0$	0	$0.01 \pm 0.00$	$7.3 \pm 0.0$	$5.0 \pm 0.0$	$99.6 {\pm} 0.0$	$97.1 \pm 0.0$	0	$\underline{\textbf{0.1} {\pm} \textbf{0.0}}$
ss1-GA	9.7±1.7	335.9±3.9	99.3±0.2	96.6±0.2	0	7.0±1.2	7.4±0.8	304.8±3.4	99.4±0.2	97.2±0.0	0	9.6±1.5
ss1-EDA ss1-DDALS(O)	$9.1\pm0.1$	$334.5\pm3.1$ $312.1\pm8.3$	99.3±0.0 99.2±0.0	$96.6\pm0.1$ $96.5\pm0.0$	0	$12.9\pm1.1$ $1.4\pm0.3$	8.3±0.9	$305.0\pm2.9$ $285.2\pm15.8$	$99.5\pm0.1$ $99.6\pm0.0$	$97.8\pm0.6$ $97.1\pm0.0$	0	$6.7\pm1.2$ $3.2\pm0.3$
ss1-DDALS(V1)	$\frac{9.0\pm0.0}{14.0\pm0.0}$	312.1±8.3	$99.2\pm0.0$ $99.9\pm0.0$	$96.3\pm0.0$ $97.2\pm0.0$	0	1.4±0.3 1.4±0.3	$\frac{7.3\pm0.0}{7.3\pm0.0}$	285.2±15.8	99.6±0.0	$97.1\pm0.0$ $97.1\pm0.0$	0	3.2±0.3 3.2±0.3
ss1-DDALS(V2)	13.8±0.9	312.1±8.3	99.8±0.1	97.1±0.1	0	1.4±0.3	$\frac{7.3\pm0.0}{7.3\pm0.0}$	285.2±15.8	99.6±0.0	97.2±0.0	0	$3.2\pm0.3$
ss1-DDALS(V3)	$14.1 {\pm} 2.7$	321	$99.6 {\pm} 0.3$	$97.9 {\pm} 1.0$	0.5	1.5	$11.1\pm2.4$	300	$99.5{\pm}0.0$	$97.8 {\pm} 0.7$	0.1	2.7
ss2-Greedy	$5.9\pm0.0$	6.0±0.0	99.8±0.0	98.5±0.0	0	$12.6{\pm}0.4$	$5.9\pm0.0$	6.0±0.0	99.9±0.0	$98.9 \pm 0.0$	1	8.7±0.2
ss2-GA	$5.3 \pm 0.1$	$303.2 \pm 2.3$	$99.2 \pm 0.0$	$97.3 \pm 0.5$	0	$4508.8 \pm 1198.4$	$5.3 \pm 0.1$	$272.9 \pm 2.2$	$99.5 {\pm} 0.1$	$98.1 {\pm} 0.2$	0.03	$34\overline{22.4\pm352.0}$
ss2-EDA	$5.5\pm0.3$	$305.0\pm2.7$	$99.2\pm0.2$	$97.6 \pm 0.7$	0.1	$3323.2 \pm 1532.5$	$5.6\pm0.3$	$274.1\pm2.4$	$99.5\pm0.2$	$98.5 \pm 0.5$	0.47	$1185.3\pm1048.5$
ss2-DDALS(O) ss2-DDALS(V1)	$\frac{5.2\pm0.0}{5.4\pm0.0}$	300.0±10.9	99.2±0.0	$97.3\pm0.0$	0	$1010.5\pm98.7$ $1010.5\pm98.7$	$\frac{5.2 \pm 0.0}{5.2 \pm 0.0}$	$297.5\pm7.8$ $297.5\pm7.8$	99.6±0.0	98.1±0.0 98.1±0.0	0	$862.2\pm78.7$ $862.2\pm78.7$
ss2-DDALS(V1)	$5.4\pm0.0$ $5.4\pm0.0$	$300.0\pm10.9$ $300.0\pm10.9$	$99.8\pm0.1$ $99.8\pm0.0$	$97.4\pm0.2$ $97.4\pm0.2$	0	1010.5±98.7 1010.5±98.7	$\frac{5.2\pm0.0}{5.4\pm0.1}$	297±7.8	$99.6\pm0.0$ $99.9\pm0.1$	98.1±0.0 98.2±0.2	0.1	862.2±78.7
ss2-DDALS(V3)	$5.4\pm0.1$	306	99.5±0.3	97.6±0.4	0	1086.0	$5.5\pm0.1$	298	99.7±0.2	98.5±0.3	0.5	858.0
ss3-Greedy	18.3±0.0	6.0±0.0	99.9±0.0	96.3±0	0	$0.5{\pm}0.0$	14.2±0.0	8.0±0.0	99.8±0.0	97.3±0.0	0	0.6±0.0
ss3-GA	17.7±0.7	$634.9 \pm 5.2$	99.4±0.4	$95.0\pm1.8$	0	179.2±2.5	12.0±1.1	503.6±3.3	99.4±0.3	95.2±1.5	0	$152.9\pm2.2$
ss3-EDA	$17.6 {\pm} 0.2$	$635.1 \pm 2.8$	$99.9 {\pm} 0.2$	$95.9 \pm 0.1$	0	$116.7 \pm 3.4$	$13.8 {\pm} 1.1$	$503.9 \pm 2.7$	$99.8 {\pm} 0.3$	$96.4 {\pm} 0.7$	0	$98.2 \pm 2.8$
ss3-DDALS(O)	$\underline{17.0{\pm}0.2}$	$690.1 \pm 31.5$	$99.1 \pm 0.1$	$93.9 {\pm} 0.7$	0	$34.5 \pm 3.1$	$11.1 \pm 0.1$	$505.8 \pm 14.6$	$99.6 \pm 0.2$	$94.7 \pm 0.5$	0	$30.5{\pm}1.2$
ss3-DDALS(V1)	18.0±0.3	690.1±31.5	99.7±0.2	96.5±0.5	0	34.5±3.1	11.2±0.7	505.8±14.6	99.7±0.0	95.1±0.7	0	30.5±1.2
ss3-DDALS(V2) ss3-DDALS(V3)	$18.0\pm0.4$ $17.7\pm0.3$	690.1±31.5 736	$99.9\pm0.1$ $99.4\pm0.3$	$96.4\pm0.4$ $95.6\pm1.6$	0	$34.5\pm3.1$ 35.4	$11.3\pm0.8$ $12.7\pm1.0$	$505.8\pm14.6$ 507	$99.6\pm0.2$ $99.4\pm0.2$	$94.9\pm0.8$ $95.3\pm0.7$	0	$30.5\pm1.2$ $29.8$
ss4-Greedy ss4-GA	$34.9\pm0.0$ $27.5\pm1.4$	$3.0\pm0.0$ $2008.9\pm7.9$	100.0±0.0 99.8±0.2	$100.0\pm0.0$ $90.3\pm0.5$	$\frac{1}{0}$	$\frac{0.2\pm0.0}{251.8\pm24.5}$	$28.5\pm0.0$ $20.5\pm2.7$	$4.0\pm0.0$ $1608.4\pm7.4$	$100.0\pm0.0$ $99.4\pm0.3$	$99.0\pm0.0$ $92.9\pm4.8$	$\frac{1}{0}$	$\frac{0.3\pm0.0}{322.5\pm9.2}$
ss4-GA ss4-EDA	$27.5\pm1.4$ $26.1\pm0.0$	2008.9±7.9 2005.7±2.3	99.8±0.2 100.0±0.0	$90.3\pm0.5$ $90.1\pm0.0$	0	$333.9\pm11.8$	20.5±2.7 18.3±2.7	1608.4±7.4 1604.5±2.8	$99.4\pm0.3$ $99.9\pm0.1$	92.9±4.8 85.2±6.9	0	322.5±9.2 287.9±19.6
ss4-DDALS(O)	$\frac{26.1\pm0.0}{26.1\pm0.0}$	1988.9±27.8	100.0±0.0	90.1±0.0	0	33.3±2.3	$16.6\pm0.8$	1582.8±54.4	99.8±0.1	81.3±3.7	0	61.3±3.9
ss4-DDALS(V1)	$26.1 {\pm} 0.0$	$1988.9 \pm 27.8$	$100.0 \pm 0.0$	$90.1 \pm 0.0$	0	$33.3 \pm 2.3$	16.8±1.1	$1582.8 \pm 54.4$	$99.8 {\pm} 0.1$	$81.8 {\pm} 4.3$	0	$61.3 \pm 3.9$
ss4-DDALS(V2)	$26.1 \pm 0.0$	$1988.9 \pm 27.8$	$100.0 \pm 0.0$	$90.1 \pm 0.0$	0	$33.3 \pm 2.3$	$18.3 \pm 2.2$	$1582.8 \pm 54.4$	$99.9 {\pm} 0.1$	$86.9 {\pm} 7.3$	0	$61.3\pm3.9$
ss4-DDALS(V3)	$29.7 \pm 2.5$	1944	$99.9 \pm 0.2$	92.2±3.9	0.2	28.3	20.8±2.9	1586	99.7±0.3	88.3±6.3	0	59.3
ls1-Greedy	$84.1 {\pm} 0.0$	$2.0 \pm 0.0$	$99.3 \pm 0.0$	$99.5 {\pm} 0.0$	1	$\underline{0.3\pm0.0}$	$84.1 \pm 0.0$	$2.0\pm0.0$	$99.9 {\pm} 0.0$	$99.9 {\pm} 0.0$	1	$0.3 \pm 0.0$
ls1-GA	64.7±2.9	6437.8±11.7	99.1±0.1	98.7±0.1	1	3441.1±15.0	60.2±4.0	6332.0±11.5	99.0±0.1	98.7±21.9	0.9	3381.1±21.9
ls1-EDA ls1-DDALS(O)	68.9±0.0 61.5±0.0	$6424.7\pm2.5$ $6418.0\pm19.6$	$99.0\pm0.0$ $99.2\pm0.0$	$99.4\pm0.0$ $98.5\pm0.0$	1	$2266.4\pm90.7$ $955.6\pm9.4$	$61.4\pm0.2$ $53.7\pm2.6$	$6324.3\pm2.9$ $6304.6\pm65.6$	$99.2\pm0.0$ $99.0\pm0.0$	99.1±0.0 98.7±0.3	1	$2250.8\pm102.6$ $958.1\pm14.7$
ls1-DDALS(V1)	$\frac{61.3\pm0.0}{63.1\pm1.0}$	6418.0±19.6	$99.6\pm0.0$	$99.1\pm0.1$	$\frac{1}{1}$	955.6±9.4	$\frac{62.1\pm1.7}{62.1\pm1.7}$	6304.6±65.6	99.7±0.2	99.5±0.3	1 1	958.1±14.7
ls1-DDALS(V2)	62.3±0.3	$6418.0\pm19.6$	99.4±0.1	98.9±0.3	1	955.6±9.4	55.3±3.2	$6304.6\pm65.6$	99.2±0.2	98.8±0.2	1	958.1±14.7
ls1-DDALS(V3)	$62.8 {\pm} 0.7$	6417	$99.2 \pm 0.1$	$98.7 {\pm} 0.2$	1	950.7	$55.2 {\pm} 1.2$	$6351 \pm 65.9$	$99.1 \pm 0.1$	$98.8 {\pm} 0.1$	1	935.6
ls2-Greedy	89.1±0.0	2.0±0.0	99.9±0.0	99.9±0.0	1	$0.2 \pm 0.0$	89.1±0.0	2.0±0.0	100.0±0.0	100.0±0.0	1	0.3±0.0
ls2-GA	$76.7 \pm 2.8$	$22616.5\!\pm\!10.5$	$99.1 \pm 0.1$	$99.0 {\pm} 0.2$	1	$3925.1 \pm 155.5$	$60.9 \pm 2.7$	$21324.5\!\pm\!13.3$	$99.1 \pm 0.1$	$99.1 \pm 0.1$	1	$3382.2\pm64.9$
ls2-EDA	$79.3\pm1.1$	$22604.1\pm2.6$	$99.5\pm0.1$	$99.3\pm0.1$	1	$7174.3\pm44.2$	$59.9\pm0.8$	$21304.8\pm3.2$	$99.2\pm0.0$	$99.2\pm0.0$	1	$6970.8\pm88.9$
ls2-DDALS(O)	$\frac{72.0\pm0.3}{76.9\pm1.1}$	22631.7±62.4	99.0±0.0	99.0±0.0	1	841.3±7.6	$\frac{57.2\pm0.0}{50.0\pm1.2}$	21265.2±73.3	99.3±0.1	99.3±0.0	1	776.4±6.6
ls2-DDALS(V1) ls2-DDALS(V2)	$76.2\pm1.1$ $73.2\pm0.4$	$22631.7\pm62.4$ $22631.7\pm62.4$	$99.5\pm0.1$ $99.4\pm0.1$	$99.5\pm0.1$ $99.3\pm0.1$	$\frac{1}{1}$	$841.3\pm7.6$ $841.3\pm7.6$	$59.0\pm1.2$ $57.6\pm0.5$	$21265.2\pm73.3$ $21265.2\pm73.3$	$99.6\pm0.0$ $99.4\pm0.1$	$99.6\pm0.1$ $99.5\pm0.1$	1 1	$776.4\pm6.6$ $776.4\pm6.6$
ls2-DDALS(V3)	73.7±1.5	22536	99.2±0.1	99.0±0.2	1	846.2	58.3±0.6	21274	99.3±0.1	99.3±0.1	1	769.6
ls3-Greedy	163.3±0.0	3.0±0.0	99.9±0.0	99.4±0.0	1	1.1±0.0	163.3±0.0	3.0±0.0	99.9±0.0	99.9±0.0	1	1.0±0.0
ls3-GA	121.7±7.3	21012.1±8.6	99.0±0.0	98.6±0.4	0.8	$17477.6\pm60.9$	121.1±4.1	21011.8±7.1	99.0±0.0	$98.4\pm0.4$	0.53	$17447.7\pm62.8$
ls3-EDA	$117.4 \pm 1.0$	$21004.5 \pm 2.5$	$99.4 \pm 0.0$	$98.9 {\pm} 0.0$	1	$13400.8 \pm 127.8$	$116.8{\pm}1.1$	$21004.8 \pm 2.6$	$99.6 \pm 0.1$	$99.4 {\pm} 0.2$	0.97	$13425.6 \pm 127.7$
ls3-DDALS(O)	$\underline{111.9{\pm}1.0}$	$20999.3 \pm 184.8$	$99.1 \pm 0.1$	$98.9 {\pm} 0.1$	1	$5734.4 \pm 64.0$	$\underline{111.7{\pm}1.6}$	$20910.0\pm266.1$	$99.3 \pm 0.3$	$98.8 {\pm} 0.4$	0.6	$5702.1 \pm 80.0$
ls3-DDALS(V1)	118.1±2.0	20999.3±184.8	99.5±0.2	98.9±0.3	0.9	5734.4±64.0	113.8±4.2	20910.0±266.1	99.5±0.2	99.2±0.3	0.97	5702.1±80.0
ls3-DDALS(V2) ls3-DDALS(V3)	$114.1\pm2.4$ $116.1\pm1.7$	20999.3±184.8 20667	$99.3\pm0.2$ $99.2\pm0.2$	$98.8\pm0.1$ $98.8\pm0.1$	$\frac{1}{1}$	$5734.4\pm64.0$ 5700.9	$112.6\pm2.4$ $114.4\pm1.4$	$20910.0\pm266.1$ 21000	$99.5\pm0.3$ $99.1\pm0.1$	$99.0\pm0.4$ $98.6\pm0.2$	0.8	5702.1±80.0 5663.9
ls4-Greedy ls4-GA	$238.1\pm0.0$ $206.6\pm4.7$	$3.0\pm0.0$ $48018.6\pm13.4$	99.4±0.0 99.0±0.0	$99.0\pm0.0$ $98.6\pm0.3$	$\frac{1}{0.73}$	$\frac{1.5\pm0.0}{46617.9\pm648.4}$	193.7±0.0 182.7±10.7	$15.0\pm0.0$ $45015.2\pm11.7$	$99.2\pm0.0$ $99.0\pm0.0$	$98.8\pm0.0$ $98.5\pm0.2$	1 0.6	$\frac{7.0\pm0.2}{42937.2\pm431.6}$
ls4-EDA	204.3±1.9	48004.5±3.5	$99.0\pm0.0$ $99.0\pm0.0$	$99.0\pm0.0$	1 1	45488.7±924.8	$163.6\pm1.2$	45003.5±2.4	99.0±0.0 99.1±0.1	$98.8\pm0.2$ $98.8\pm0.1$	1 1	42955.7±613.1
ls4-DDALS(O)	$195.1 \pm 0.5$	$47999.9\pm83.0$	$99.0\pm0.0$	$98.9 \pm 0.0$	1	$16357.5{\pm}137.6$	$161.5 \pm 2.1$	$44440.5\pm344.6$	99.0±0.0	$98.5 \pm 0.3$	0.4	15160.3±127.4
ls4-DDALS(V1)	$209.2 \pm 2.8$	$47999.9{\pm}83.0$	$99.1 \pm 0.0$	$98.6 {\pm} 0.3$	0.6	$16357.5\!\pm\!137.6$	$169.4 \pm 4.2$	$44440.5{\pm}344.6$	$99.3 {\pm} 0.2$	$98.9 {\pm} 0.4$	0.8	$15160.3{\pm}127.4$
ls4-DDALS(V2)	197.4±1.7	47999.9±83.0	99.1±0.0	99.0±0.1	1	16357.5±137.6	162.5±2.4	44440.5±344.6	99.1±0.1	98.6±0.2	0.7	15160.3±127.4
ls4-DDALS(V3)	196.8±0.8	48046	99.0±0.0	$98.9 \pm 0.1$	1	16280.8	163.5±3.5	44648	99.0±0.0	98.3±0.1	0.1	15162.6
ls5-Greedy	282.7±0.0	4.0±0.0	99.6±0.0	99.4±0.0	1	2.8±0.2	267.2±0.0	6.0±0.0	99.0±0.0	98.8±0.0	1	$\frac{3.9\pm0.0}{5.49.5\pm0.50}$
ls5-GA ls5-EDA	$238.6\pm8.3$ $220.3\pm0.6$	$81011.4\pm10.1$ $81004.3\pm2.8$	$99.0\pm0.0$ $99.1\pm0.0$	$98.6\pm0.1$ $98.7\pm0.0$	0.87	$104473.1\pm1301.8$ $103916.1\pm1686.4$	$216.9\pm8.3$ $200.6\pm1.8$	$79012.9\pm8.8$ $79004.3\pm2.5$	$99.0\pm0.0$ $99.1\pm0.1$	$98.6\pm0.2$ $98.7\pm0.2$	0.77	$101543.5\pm950.4$ $100901.5\pm1166.1$
ls5-DDALS(O)	$220.3\pm0.6$ $217.4\pm1.2$	81186.6±246.3	$99.1\pm0.0$ $99.0\pm0.0$	98.7±0.0 98.6±0.0	$\frac{1}{1}$	$36706.0\pm267.7$	$199.6\pm2.2$	78766.1±799.8	99.1±0.1 99.0±0.0	$98.7 \pm 0.2$ $98.6 \pm 0.1$	1 0.8	$35543.0\pm403.1$
ls5-DDALS(V1)	225.3±3.0	81186.6±246.3	$99.2\pm0.1$	98.8±0.1	1	36706.0±267.7	209.4±4.9	78766.1±799.8	99.3±0.1	$98.9\pm0.2$	0.97	$35543.0\pm403.1$
ls5-DDALS(V2)	$219.0\pm2.6$	$81186.6 \pm 246.3$	99.1±0.1	$98.7 \pm 0.1$	1	$36706.0\pm267.7$	$201.9 \pm 3.4$	$78766.1\pm799.8$	99.1±0.1	$98.7 \pm 0.2$	0.9	$35543.0\pm403.1$
ls5-DDALS(V3)	$220.9{\pm}2.3$	81306	$99.0 \pm 0.0$	$98.7 {\pm} 0.0$	1	36440.4	$203.6{\pm}1.1$	77365	$99.1 \pm 0.1$	$98.7 {\pm} 0.2$	0.9	34775.3
ls6-Greedy	399.3±0.0	$3.0\pm0.0$	99.8±0.0	99.4±0.0	1	$1.9 \pm 0.1$	381.4±0.0	12.0±0.0	99.8±0.0	99.4±0.0	1	$6.9 {\pm} 0.1$
ls6-GA	$357.0 {\pm} 13.2$	$125313.9{\pm}8.9$	$99.0 \pm 0.0$	$98.2 {\pm} 0.1$	0	$196363.3\pm427.9$	$323.2 {\pm} 9.8$	$121514.7{\pm}9.1$	$99.0 {\pm} 0.0$	$98.2 {\pm} 0.3$	0.13	$193984.6 \pm 4074.8$
ls6-EDA	338.1±1.4	125305.6±2.9	99.0±0.0	98.6±0.0	1	196994.6±539.1	300.7±1.6	121504.8±2.9	99.1±0.1	98.7±0.1	1	193948.7±1566.8
ls6-DDALS(O) ls6-DDALS(V1)	$\frac{323.9\pm0.6}{332.7\pm2.9}$	$125056.0\pm178.1$ $125056.0\pm178.1$	99.0±0.0 99.1±0.0	$98.1\pm0.0$ $98.2\pm0.0$	0	$70604.7 \pm 449.7$ $70604.7 \pm 449.7$	$\frac{297.9\pm4.5}{297.9\pm4.5}$	$121616.1\pm1093.7$ $121616.1\pm1093.7$	$99.0\pm0.0$ $99.0\pm0.0$	$98.3\pm0.1$	0	68409.7±727.0
ls6-DDALS(V1)	325.3±2.2	$125056.0\pm178.1$ $125056.0\pm178.1$	$99.1\pm0.0$ $99.0\pm0.1$	$98.2\pm0.0$ $98.2\pm0.1$	0	70604.7±449.7 70604.7±449.7	$\frac{297.9\pm4.5}{199.4\pm5.2}$	121616.1±1093.7 121616.1±1093.7	99.0±0.0 99.1±0.1	$98.3\pm0.1$ $98.3\pm0.2$	0.1	$68409.7\pm727.0$ $68409.7\pm727.0$
ls6-DDALS(V3)	$326.4\pm2.0$	124926	99.0±0.0	98.2±0.0	0	70190.2	305.0±3.9	121537	99.01±0.0	98.1±0.1	0.1	68162.4