

UNIVERSITY OF LEEDS

DOCTORAL THESIS

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# Simulating the thermal conductivity of lower mantle minerals

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*A thesis submitted in fulfillment of the requirements*

*for the degree of Doctor of Philosophy*

*in the*

Institute of Geophysics and Tectonics

School of Earth and Environment

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## Declaration of Authorship

I, Ben TODD, declare that this thesis titled, “Simulating the thermal conductivity of lower mantle minerals” and the work presented in it are my own. I confirm that:

- This work was done wholly or mainly while in candidature for a research degree at this University.
- Where any part of this thesis has previously been submitted for a degree or any other qualification at this University or any other institution, this has been clearly stated.
- Where I have consulted the published work of others, this is always clearly attributed.
- Where I have quoted from the work of others, the source is always given. With the exception of such quotations, this thesis is entirely my own work.
- I have acknowledged all main sources of help.
- Where the thesis is based on work done by myself jointly with others, I have made clear exactly what was done by others and what I have contributed myself.

Signed:

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Date:

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*Do it!*  
*Just do it!*

*Don't let your dreams be dreams.*  
*Yesterday you said tomorrow, so just do it!*  
*Make your dreams come true!*  
*Just do it!*

*Some people dream of success,*  
*while you're gonna wake up,*  
*and work hard at it!*  
*Nothing is impossible!*

*You should get to the point,*  
*where anyone else would quit,*  
*and you're not going to stop there.*  
*No, what are you waiting for?*

*Do it!*  
*Just do it!*  
*Yes you can!*  
*Just do it!*

*If you're tired of starting over,*  
*stop giving up.*

Shia LeBeouf



UNIVERSITY OF LEEDS

# *Abstract*

Faculty of Environment

School of Earth and Environment

Doctor of Philosophy

**Simulating the thermal conductivity of lower mantle minerals**

by Ben TODD

The Thesis Abstract is written here (and usually kept to just this page). The page is kept centered vertically so can expand into the blank space above the title too...





## *Acknowledgements*

The acknowledgments and the people to thank go here, don't forget to include your project advisor...

Everyone is smart, set yourself apart by being kind.



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# List of Abbreviations

<b>CMB</b>	<b>C</b> ore- <b>m</b> antle <b>b</b> oundary
<b>LLSVP</b>	<b>L</b> arge, <b>l</b> ow-shear- <b>v</b> elocity <b>p</b> rovince
<b>ULVZ</b>	<b>U</b> ltra <b>l</b> ow <b>v</b> elocity <b>z</b> one
<b>DAC</b>	<b>D</b> iamond <b>a</b> nvil <b>c</b> ell
<b>MgSiO<sub>3</sub></b>	<b>M</b> agnesium <b>S</b> ilicate
<b>FeSiO<sub>3</sub></b>	<b>I</b> ron <b>S</b> ilicate
<b>bdg</b>	<b>b</b> ridgmanite
<b>pv</b>	<b>p</b> erovskite
<b>ppv</b>	<b>p</b> ost- <b>p</b> erovskite
<b>LAMMPS</b>	<b>L</b> arge-scale <b>A</b> tomic/ <b>M</b> olecular <b>M</b> assively <b>P</b> arallel <b>S</b> imulator
<b>DFT</b>	<b>D</b> ensity <b>F</b> unctional <b>T</b> heory
<b>MD</b>	<b>M</b> olecular <b>D</b> ynamics
<b>EMD</b>	<b>E</b> quilibrium <b>M</b> olecular <b>D</b> ynamics
<b>NEMD</b>	<b>N</b> on-equilibrium <b>M</b> olecular <b>D</b> ynamics
<b>DM</b>	<b>D</b> irect <b>M</b> ethod
<b>GK</b>	<b>G</b> reen- <b>K</b> ubo
<b>ACF</b>	<b>A</b> uto-correlation <b>f</b> unction
<b>MFP</b>	<b>M</b> ean free <b>p</b> ath
<b>FSE</b>	<b>F</b> inite-size <b>e</b> ffects
<b>BPT</b>	<b>B</b> allistic <b>p</b> honon <b>t</b> ransport



# Physical Constants

Boltzmann constant  $k_B = 1.380\,648\,528 \times 10^{-23} \text{ J K}^{-1}$

Boltzmann constant  $k_B = 8.617\,330\,350 \times 10^{-5} \text{ eV/K}$



# List of Symbols

$a$	distance	m
$P$	power	W (J s <sup>-1</sup> )
$\omega$	angular frequency	rad





*For/Dedicated to/To my...*



## Chapter 1

# Introduction

### 1.1 Why is thermal conductivity important?

Knowledge of the thermal conductivity of solids is key in a wide range of technological applications and for our understanding of natural systems.

#### 1.1.1 Man-made applications

Low thermal conductivities are required in thermoelectric materials, to maximise the efficiency of heat-electricity conversion (Snyder and Toberer, 2008).

#### 1.1.2 In the context of the Earth

For example, in the Earth's lower mantle thermal conductivity controls the nature of planetary convection (Tosi et al., 2013), and the heat flux out of the core which powers the geotherm.

The lower mantle encompasses the region between the mantle transition zone (660 km deep,  $\sim 1900$  K,  $\sim 25$  GPa) and the CMB (2891 km deep,  $\sim 4000$  K,  $\sim 136$  GPa). The composition of this region can be approximated as 80%  $\text{MgSiO}_3$ /magnesium silicate perovskite (bridgmanite) and 20%  $\text{MgO}$ /magnesium oxide (periclase), both of which are insulators and past their Debye temperatures at lower mantle conditions.

### 1.2 What is thermal conductivity?

Thermal conductivity determines whether a material is a conductor or insulator of heat, both of which have many technological applications.

### 1.2.1 What affects it?

pressure, temperature, and composition

### 1.2.2 Mechanisms of heat transport

RADIATIVE AND ELECTRONIC TOO

Heat is transported as lattice vibrations, or phonons. The further phonons travel before scattering (mean free path, MFP) the more efficient the heat transport and thus higher the thermal conductivity. A number of effects (MENTION MATTHIESSEN'S RULE) cause phonons to scatter: (1) collisions with other phonons in the lattice, (2) boundaries or defects in the material, and (3) impurities in the atomic structure.

## 1.3 Previous work - geophysics

INSERT GEOPHYSICS INTRO HERE ASWELL

A range of atomic scale simulation methods are available to determine the lattice thermal conductivity of materials. These are invaluable for calculating thermal conductivity at conditions of which experiments are difficult, e.g. the extreme conditions found in the Earth's lower mantle (pressures and temperatures up to 136 GPa and 4000 K at the core-mantle boundary).

### 1.3.1 Mantle/core dynamics

Thermal conductivity in the deep Earth influences dynamic processes such as mantle convection and heat loss from the core (Lay et al., 2008).

### 1.3.2 Thermal conductivity of the lower mantle

Many studies assume lowermost mantle thermal conductivity to be  $10 \text{ Wm}^{-1}\text{K}^{-1}$  (e.g. Lay et al., 2008), but uncertainty in the extrapolation of results made at low pressures

and temperatures gives a range of 4 - 16  $\text{Wm}^{-1}\text{K}^{-1}$  (Brown and McQueen, 1986; Osako and Ito, 1991; Hofmeister, 1999; Goncharov et al., 2009; Manthilake et al., 2011; Ohta et al., 2012).

There have been several computational studies to calculate the lattice thermal conductivity of bridgmanite at CMB conditions. Osako and Ito (1991) measured the lattice thermal conductivity of  $\text{MgSiO}_3$  perovskite, using a modified Ångström method. They investigated a temperature range of 160 - 340 K at ambient pressure. At 300 K, a conductivity of  $5.1 \text{ Wm}^{-1}\text{K}^{-1}$  was obtained. This value is similar to that reported for chemical and structural analogues,  $\text{MgSiO}_3$  enstatite ( $5.0 \text{ Wm}^{-1}\text{K}^{-1}$  REF) and  $\text{CaTiO}_3$  perovskite ( $4 \text{ Wm}^{-1}\text{K}^{-1}$  REF). The authors extrapolated the value to mantle conditions, neglecting radiative thermal conductivity. They predicted a value of  $3.0 \text{ Wm}^{-1}\text{K}^{-1}$  just beneath the mantle transition zone at 1900 K, and  $12.0 \text{ Wm}^{-1}\text{K}^{-1}$  at the top of the  $D''$  layer at 2500 K, a four-fold increase. Thermal conductivity is highlighted as an important indicator of lowermost mantle structure, whether or not the  $D''$  layer can behave as a thermal boundary between core and mantle.

Manthilake et al. (2011) measured  $\text{MgSiO}_3$  perovskite at 26 GPa and 473 - 1073 K, and periclase at 8 and 14 GPa between 373 - 1273 K. In order to estimate values of thermal conductivity at the top and bottom of  $D''$  for a lower mantle compositional model of 4 perovskite : 1 periclase, the authors extrapolated their measurements to high temperature and pressure. For an iron-free mantle, thermal conductivities of  $18.9 \pm 1.6 \text{ Wm}^{-1}\text{K}^{-1}$  and  $15.4 \pm 1.4 \text{ Wm}^{-1}\text{K}^{-1}$  are estimated for the top of  $D''$  and CMB respectively. Similarly, for a mantle composition with Fe, thermal conductivities of  $9.1 \pm 1.2 \text{ Wm}^{-1}\text{K}^{-1}$  and  $8.4 \pm 1.2 \text{ Wm}^{-1}\text{K}^{-1}$  are calculated. This highlights the importance of impurities in controlling thermal conductivity in the lower mantle.

Ohta et al. (2012) measured the lattice thermal diffusivity of  $\text{MgSiO}_3$  perovskite and post-perovskite at room temperature and pressures up to 144 GPa (using a diamond-anvil cell (DAC) and light heating thermoreflectance). These results suggest a perovskite-dominant lowermost mantle would have conductivity of around  $11 \text{ Wm}^{-1}\text{K}^{-1}$ , and that parts of the lowermost mantle where post-perovskite is stable will have a conductivity approximately 60% higher. The authors suggest that these differences in conductivity between phases will not have a large effect on CMB heat flux, assuming the double-crossing perovskite phase model. The lattice conductivity

of  $\text{MgSiO}_3$  perovskite is shown to increase with pressure and decrease with temperature as expected. The inclusion of impurities is expected to decrease lattice thermal conductivity.

MANTHILAKE'S HIGH T RESULTS? CAN'T FIND REFERENCE?

My approach is similar to that of Ammann et al. (2014), who use the direct method and interatomic potentials reporting a value of  $\sim 8.5 \text{ Wm}^{-1}\text{K}^{-1}$ . Stackhouse et al. (2015) again use the direct method but with density functional theory, yielding conductivity of  $6.8 \pm 0.9 \text{ Wm}^{-1}\text{K}^{-1}$ . Using Green-Kubo, Haigis (2013) report a value of  $12.4 \pm 2.0 \text{ Wm}^{-1}\text{K}^{-1}$  for conditions of 3000 K, 139 GPa. Tang et al. (2014) and Dekura et al. (2013) employed first principles, anharmonic lattice dynamics techniques, obtaining values of  $\sim 1 \text{ Wm}^{-1}\text{K}^{-1}$  (CMB conditions) and  $2.3 \text{ Wm}^{-1}\text{K}^{-1}$  (for 4000 K and 100 GPa) respectively. These results are much lower than other studies, and could be because of LD TRUNCATION OF CONDUCTIVITY [CRITICAL ANALYSIS].

## 1.4 Thesis outline

In Chapter 2 we provide an overview of the methods and expand on issues. I outline my computational approaches, for the non-equilibrium molecular dynamics direct method and equilibrium molecular dynamics Green-Kubo method. I show convergence of computed conductivity with respect to simulation cell size and shape

In Chapter 3, PRESSURE/TEMPERATURE EFFECTS. DISCUSS [P/T] SCALING LAW / THEORETICAL MODEL

In Chapter 4, ADAPTING SYSTEM TO INCLUDE IRON, DETERMINING EFFECT OF IMPURITY CONTENT, PRODUCING A MODEL OF THE LOWER MANTLE CONDUCTIVITY WITH VARIABLE TEMPERATURE AND BRIDGMANITE COMPOSITION

### 1.4.1 Aims

### 1.4.2 Objectives

## Chapter 2

# Intro/Background/Theory 2

### 2.1 Atomic-scale modelling

Knowledge of thermal conductivity is important for modelling the deep earth, but can not be measured experimentally at core mantle boundary conditions. Atomic scale simulations sidestep experimental limitations, but system size must be chosen carefully in order to determine accurate conductivity values. Classical molecular dynamics approaches are utilised, with the intention of constraining appropriate system parameters.

A range of atomic scale simulation methods are available to determine the lattice thermal conductivity of materials. These are invaluable for calculating thermal conductivity at conditions of which experiments are difficult, e.g. the extreme conditions found in the Earth's lower mantle (pressures and temperatures up to 136 GPa and 4000 K at the core-mantle boundary).

#### 2.1.1 Molecular dynamics

##### Parameter drift/convergence

We ensure all calculations are run for a sufficient length of time for the conductivity value to converge. When conductivity fails to converge it means either the simulations needs to be run for longer (unlikely with our nanosecond-scale classical calculations), or the system temperature has drifted. When NVE simulations are run for a long time there is noticable drift in the average system temperature (due to numerical approximations in the equation of motion), which in turn causes drift in the computed conductivity.

## NPT-NVT-NVE PROCESS

### 2.1.2 Interatomic potentials / Atomic interactions?

With the interatomic potential of Oganov et al. (2000) we simulate bridgmanite, a magnesium silicate otherwise referred to as  $\text{MgSiO}_3$  or perovskite (the name of its crystal structure family). To assess finite-size effects we use larger simulation cells than those employed in previous studies. The atom counts associated with these cells (the largest cell considered having over 100,000 atoms) means an ab initio study would be impractical, necessitating the use of interatomic potentials. We expect the potentials to represent the finite size effects well, even if computed conductivities may inaccurate compared to first-principles calculations.

WHY OGANOV?

WHAT CUTOFFS?

### 2.1.3 LAMMPS

LAMMPS (Large-scale Atomic/Molecular Massively Parallel Simulator) is a classical molecular dynamics code (Plimpton, 1995).

### 2.1.4 DFT/other

Required? Subsubsection somewhere?

## 2.2 Computing thermal conductivity

Stackhouse and Stixrude (2010) review different methods to compute thermal conductivity, in the present work we focus on two of these: (1) Equilibrium molecular dynamics based on the Green-Kubo relations to determine the thermal conductivity from heat flux fluctuations and their time-dependence (Green, 1954; Kubo, 1957; Kubo, 1966; Schelling et al., 2002). (2) The non-equilibrium molecular dynamics-based “direct method”, where thermal conductivity is calculated from an imposed heat flux and corresponding temperature gradient via Fourier’s Law (Müller-Plathe, 1997; Nieto-Draghi and Avalos, 2013).



### 2.2.1 Finite-size effects

[[[Give its own section, or as subsection in each method?]]]

Computational techniques are not limited by the reproduction of physical conditions like experiments, however they are affected by the size and shape of the simulation cell. The effects of the finite system size available for computation must be checked, as systems with too few atoms are sometimes unable to reproduce the behaviour of the bulk material. If the wavelength of a phonon is too long to fit into a cell, it is not able to transport heat like it should. In the case of the direct method, the length to cross sectional area (CSA) aspect ratio can also matter.

Considering systems of varying size, length-dependent conductivities are obtained from the direct method and extrapolated to the bulk material (Schelling et al. (2002)). The validity of this extrapolation procedure have been called into question (e.g. Sellan et al. (2010)), when a linear trend cannot be fit through the length-dependent conductivities. We describe finite-size effects (FSE) which cause the conductivity result of a simulation to diverge from the value expected by a linear trend, and offer a comparison with results obtained from the Green-Kubo method. The two methods have previously been compared (e.g. Schelling et al. (2002) [[[REFERENCED EARLIER IN THIS PARAGRAPH, THIS OKAY?]]] ), and have been found to give results in good agreement.

The finite-size effects (FSE) I describe are associated with phonon-phonon scattering, or the lack thereof, and boundary-scattering or truncation of phonon mean free path due to limited system sizes. These phenomena combine to misrepresent the phonon behaviour of the bulk material.

The FSE observed for a material change with thermal conductivity/phonon MFP, and thus are pressure, temperature, and composition sensitive. Higher conductivity(or is it MFP?) materials/conditions require larger systems to eliminate FSE (and vice versa) [[[BUT IS THIS TRUE?]]].

### 2.2.2 Direct method

The direct method is the computational implementation of a typical experiment to measure thermal conductivity, using Fourier's law to relate heat flux ( $q$ ) and temperature gradient ( $\nabla T$ ) to thermal conductivity ( $k$ ),

$$q = -k\nabla T. \quad (2.1)$$

#### System setup

In the direct method energy is transferred from one group of atoms to another, creating hot and cold regions between which heat flows. The resultant temperature gradient is measured by calculating the temperature of individual groups of atoms along the direction of the heat flux. Simulation cells tend to be long relative to their cross-sectional area, defined as height by width (see Figure 2.1). Cell boundaries are periodic and the hot and cold sections are half the cell length apart, meaning heat flows in both directions from hot to cold (one of which is across the length-end periodic boundary). This results in two similar temperature gradients which can be averaged.

From kinetic theory [[[REF?]]], conductivities computed by the direct method ( $k_L$ ) are dependent on length of simulation cell,

$$k_L = \frac{1}{3}C_V v l_L, \quad (2.2)$$

where  $C_v$  is the volumetric heat capacity,  $v$  is the average phonon drift velocity, and  $l_L$  is the phonon mean free path.

#### Data processing

The finite size of the simulation cell truncates the mean free path, underestimating conductivity compared to that of the bulk material ( $k_\infty$ ). Using results from simulations of varying cell length ( $L$ ), conductivity is extrapolated to a length-independent value (where  $b$  is a material dependent parameter),

$$k_L^{-1} = bL^{-1} + k_\infty^{-1}. \quad (2.3)$$

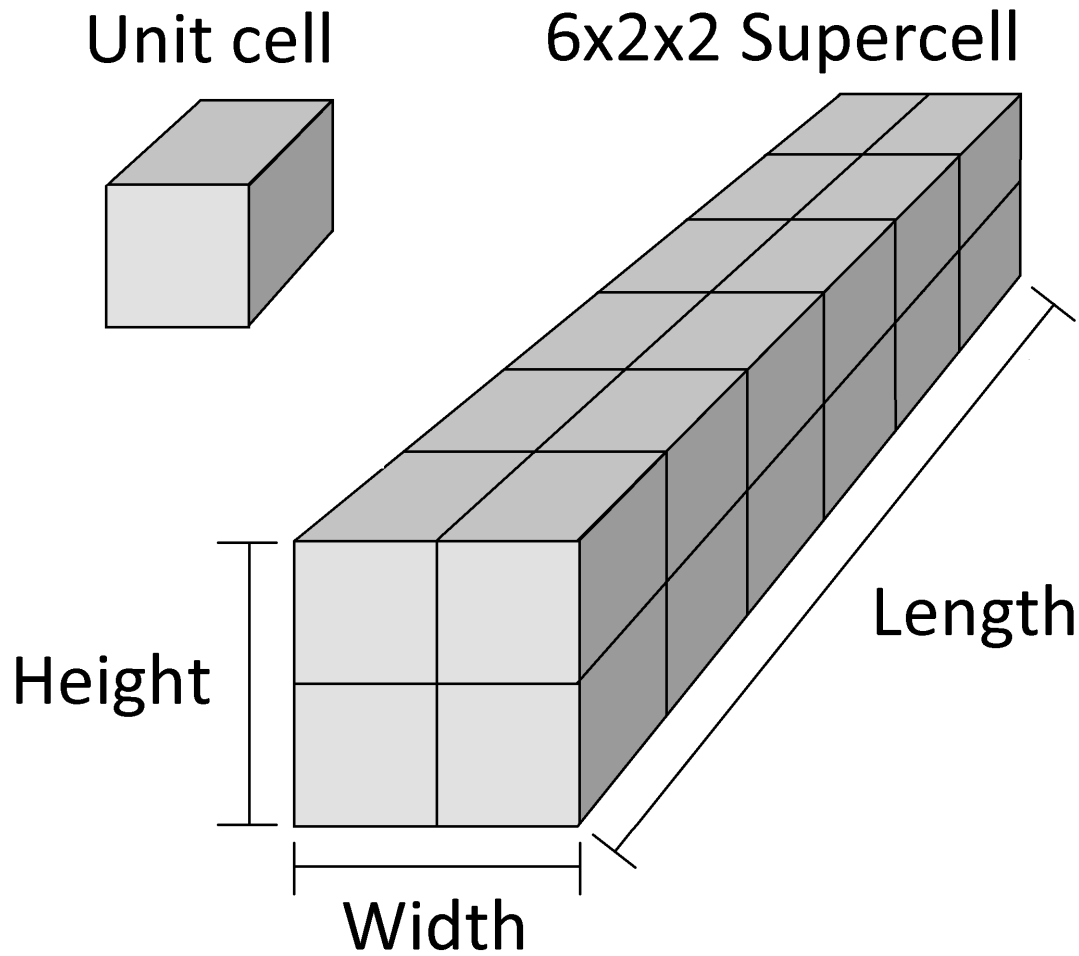


FIGURE 2.1: The unit cell represents the smallest box of atoms that can be replicated to produce a crystal structure. A supercell is an arrangement of unit cells.

Inverse conductivities from direct method simulations are plotted against corresponding inverse cell lengths. A straight line is fit to the data and extrapolated to the y-axis (at which the inverse cell length equals zero and real length equals infinity), where the intercept gives the inverse of the bulk material conductivity (Schelling et al., 2002).

### Finite-size effects

Problems arise when the data do not support a linear trend. There are two effects of finite system size that can cause an individual direct method simulation to diverge away from an inferred/expected linear trend, both of which result in overestimation of the length-dependent conductivity data point. First, when the distance between hot and cold sections (controlled by cell length) is shorter than the MFP, phonons



FIGURE 2.2: Movement and distribution of heat in the direct method. Orange to white scale represents temperature (modified from Stackhouse et al., 2015).

travel ballistically (i.e. without any scattering events) from heat source to sink (Sellan et al., 2010). Conductivities in shorter length cells are overestimated when this occurs, reducing the gradient of the linear fit and thus underestimating the extrapolated conductivity.

For a given length, conductivity is dependent on the CSA, or aspect ratio of the simulation cell. Conductivity is overestimated due to an underestimation of phonon-phonon scattering, from sparse phonon phase sampling in cells where cross-section is small compared to length. Phonons that aren't resolved cannot contribute to phonon-phonon scattering effects. Reduced scattering means heat transport is artificially more efficient than expected from the bulk material.

[[[SPECIFIC ALERT, REFERENCING THINGS I FOUND]]] However, the required CSA to abate this FSE is length-dependent. When the CSA is smaller than required for all cell lengths (e.g. 1x1 [FIGURE]), all conductivities are overestimated (Thomas et al., 2010, albeit for nanotube diameter?). As the CSA is increased, the data points (and thus also the extrapolated result) shift to lower conductivities (higher inverse conductivities). It is at this point that the short cells with lengths of similar order, will report conductivities converged with respect to CSA. Assuming these cells are sufficiently long to avoid the ballistic phonon transport (BPT), a linear fit can be extrapolated to obtain conductivity (for CSA around 2x2, the case at

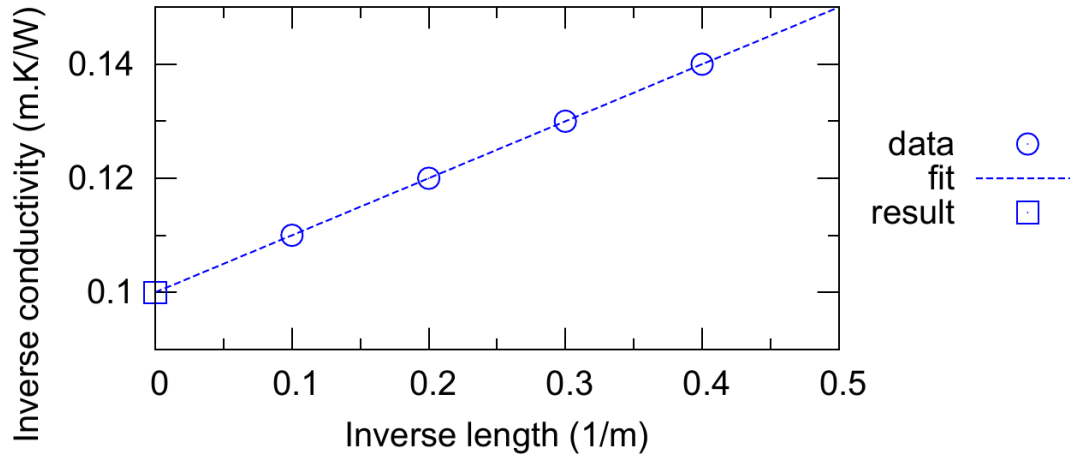


FIGURE 2.3: Idealised example of linear extrapolation procedure. Inverse computed conductivities are plotted against inverse simulation lengths. Extrapolation to y-axis gives conductivity of an infinite system length, i.e. the bulk material.

4000 K).

The convergence is not necessarily observed concurrently for longer cells however, where they may show overestimated conductivities compared to the fit through short cells (Hu et al., 2011). This would cause the fit to all data to be steeper than it should, increasing the extrapolated result. [[[HOPEFULLY THIS IS TRUE]]] I can show that increasing CSA does not change the computed conductivity at short lengths, but does reduce values from longer cells and bring them into alignment with the expected fit.

### Other NEMD

Fixed ends?

Sinusoidal temperature perturbation.

### 2.2.3 Green-Kubo

The Green-Kubo method uses auto-correlation functions (ACFs) to quantify time-dependence of heat fluxes (shown in Figure 2.4, and Equation 2.4), in a simulation cell of roughly cubic dimensions (WHY??) and spatially-consistent average temperature. Instantaneous heat fluxes can be used to determine how energy is dissipated within a system, where brief flux events mean heat is transferred quickly indicating high thermal conductivity [[[and vice versa, BUT IS THIS TRUE?]]].



FIGURE 2.4: Normalised ACF. Correlation is taken over a longer length than shown on this plot (100 ps), however the function decays to less than 1% of its initial value at 2 ps. It continues to oscillate about zero, with a positive average value.

The auto-correlation is obtained over the net heat flux series in each crystallographic direction, for a timescale up to a chosen correlation length.

$$ACF_i = \langle J_i(0) \cdot J_i(t) \rangle, \quad (2.4)$$

where  $i$  specifies direction,  $J$  is heat flux, and  $t$  is the correlation length. The integral of heat flux ACF is proportional to thermal conductivity via the Green-Kubo equation (see Figure 2.5 and Equation 2.5),

$$\kappa_i = \frac{V}{k_B T^2} \int_0^\infty \langle J_i(0) \cdot J_i(t) \rangle dt, \quad (2.5)$$

[[[I am using “k”s and “kappa”s to represent thermal conductivity, kappa here and k earlier?]]] where  $V$  is the simulation cell volume,  $k_B$  is the Boltzmann constant, and  $T$  is the average temperature of the system. In this study we use Green-Kubo results as an independent check on the direct method, as they do not have the same finite size-effects. Obtaining a converged conductivity result simply depends on using a large enough cell volume / number of atoms.

The individual integrals obtained from the Green-Kubo show variation from the average combined integral on the order of the mean. Many simulations from different initial temperature conditions are required in order to ensure good sampling of conductivity, as well as ensuring the computation time for each is long enough for



FIGURE 2.5: Integrated ACF, multiplied by constants to get thermal conductivity. Large variation in the first 1 ps corresponds to the correlation time where the ACF is unconverged (still decaying / large oscillations). Thermal conductivity is averaged from correlation time of 5 ps - 10 ps (region in red box).

convergence. This makes Green-Kubo a computationally expensive method, especially for large systems.

The ACF should decay to zero as correlation time tends to infinity, however noise in the ACF prevents this. This will ultimately cause the integral to diverge/drift on long timescales. Howell (2012) fits a series of exponential decays to their ACF, forcing the expected decay to zero and subsequent (constant) integral convergence. This represents a significant improvement on the conductivity estimate at long correlation lengths, but is mostly similar with the un-fit integrals early in the correlation. (INTEGRAL DRIFT FIGURE, JUST THE ONE INTEGRAL FOR 100PS)

(STACKHOUSE 2010 REFERENCES Volz and Chen 2000; Sun and Murthy 2006)

#### 2.2.4 Other

- (3) Anharmonic lattice dynamics (Tang and Dong, 2009).
- (4) Combined quasiharmonic lattice dynamics and molecular dynamics method (Koker, 2009).

## **2.3 Previous work**

### **2.3.1 Method comparison**

### **2.3.2 Finite-size effects**

Should this section be interspersed into when FSE are mentioned in methods?

**STUFF THAT MIGHT BE WRONG BECAUSE FSE?**



## Chapter 3

# Constraining the finite-size effects of molecular dynamics methods to compute thermal conductivity

### 3.1 Introduction

Knowledge of the thermal conductivity of solids is key in a wide range of technological applications and for our understanding of natural systems. For example, in the Earth's lower mantle thermal conductivity controls the nature of planetary convection (Tosi et al., 2013), and the heat flux out of the core which powers the geotherm. Low thermal conductivities are required in thermoelectric materials, to maximise the efficiency of heat-electricity conversion (Snyder and Toberer, 2008).

A range of atomic scale simulation methods are available to determine the lattice thermal conductivity of materials. These are invaluable for calculating thermal conductivity at conditions of which experiments are difficult, e.g. the extreme conditions found in the Earth's lower mantle (pressures and temperatures up to 136 GPa and 4000 K at the core-mantle boundary).

(MOVE - to where though?) Many studies assume lowermost mantle thermal conductivity to be  $10 \text{ Wm}^{-1}\text{K}^{-1}$  (e.g. Lay et al., 2008), but uncertainty in the extrapolation of results made at low pressures and temperatures gives a range of 4 - 16  $\text{Wm}^{-1}\text{K}^{-1}$  (Brown and McQueen, 1986; Osako and Ito, 1991; Hofmeister, 1999; Goncharov et al., 2009; Manthilake et al., 2011; Ohta et al., 2012).

### 3.1.1 Finite-size effects

#### THE PROBLEM OF FSE IN COMPUTATIONAL TECHNIQUES

##### EXACERBATED BY RANGE OF LOWER MANTLE CONDITIONS

The effect of FSE on conductivity results depends on the magnitude of conductivity/phonon MFP/physical conditions. At low kappa/low MFP/high T/ (my 4000 K), no BPT is observed, and short cells (>16 unit cells) can be used for extrapolation. In fact, short cells must be used to extrapolate, unless CSA considerations are made to ensure convergence of long cell results.

At high kappa/high MFP/low T (my 1000 K), BPT must be considered at the shorter cells (just 6?). Effectively there is a "sweet-spot", a window of cell lengths for a given CSA that produce consistently-converged results. Long cells outside of the window require a larger CSA, short cells outside show BPT. At 4000 K the lower limit of the window is smaller than the minimum cell length considered, and the upper limit is between 16-24 unit cells. For 1000 K the lower limit of the window moves inside the simulated cell length range around 6-8 unit cells (OR MORE?). The upper limit of the window appears to be larger than 96 unit cells, including all long cells up to this value produces an extrapolation in agreement with GK.

## 3.2 Computational approaches

In this section I talk about my specific approaches to applying the methods discussed in Chapter 2

### 3.2.1 Direct method

The simulation supercell is split into sections along its length, each half a unit cell wide. Two of these sections, half the supercell length apart, are designated as the heat source and heat sink. We measure (HOW?) the temperature in all sections to obtain the temperature gradient. Heat flows in both directions from the hot section because of cell periodicity [NEED DIRECT METHOD DIAGRAM BY THIS PARA], meaning there are two temperature gradients to average. Where  $L$  is supercell length in unit cells and  $S (= 2L)$  gives the number of sections, we obtain  $S/2 + 1$  temperature points to fit the gradient. Because the temperature gradient is non-linear around the

heat source and sink, we ignore  $S/12$  sections (rounded to nearest integer) from both ends of the temperature gradient. For a given simulation cell we fit  $S/3 + 1$  points to obtain the temperature gradient. We use a minimum supercell length of 6 unit cells (12 sections, 5 data points), in order for sufficient fitting of the temperature gradient. [HOW NECESSARY IS THIS PARA, VERY JARGONY]

(MOVE TO RESULTS?) Changing the width of the heated sections has no effect on the conductivity result. Furthermore, changing the width (and thus number) of temperature bins has no effect on the sampled gradient, assuming resolution is large enough to capture the non-linear region around the heat source/sink.

An important factor for utilising the direct method is maintaining a sensible temperature gradient where Fourier's law remains valid, i.e. conductivity is constant along the length of the cell. Thermal conductivity is strongly temperature-dependent at upper lower-mantle conditions (1000 K), it is therefore undesirable to have substantially different conductivities as a function of temperature across the cell. The opposite case is also true, the difference in temperature between hot and cold sections must be larger than the uncertainty in the average system temperature.

We typically observe fluctuations in temperature of around  $\pm 50$  K during temperature equilibration, and look for temperature increases/decreases on the order of 10% the mean temperature. We control the magnitude of the gradient by altering the interval at which heat is exchanged. To produce the desired gradients we find shorter intervals are required as cell length decreases, cross-sectional area increases, and system equilibrium temperature decreases.

### 3.2.2 Green-Kubo

The bridgmanite unit cell does not have cell dimensions resembling a cube ( $a:b:c = 1:1:1.4$ ), so we use supercell structures of  $3 \times 3 \times 2$ ,  $4 \times 4 \times 3$ ,  $5 \times 5 \times 4$ ,  $6 \times 6 \times 4$  etc. to make an approximately cubic simulation cell. Temperature initialisation (NVT) of 1 ns is run to ensure convergence of system pressure and temperature. To obtain heat flux auto-correlation functions, a simulation for each initial temperature condition is run for  $X$  ns, with 9 successive repeats for a total of 10 jobs. This gives 10 ACFs from

each initial condition. Simulation runs are split in this manner to be feasible computationally, and also to provide enough samples for ensemble averaging statistics (??).

3x3x2 - X = 10 ns, for 20 initial conditions - 2  $\mu$ s total time

4x4x3 - X = 10 ns, for 30 initial conditions - 3  $\mu$ s total time

5x5x4 - X = 5 ns, for 20 initial conditions - 1  $\mu$ s, X = 1 ns, for 70 initial conditions - 0.7  $\mu$ s, 1.7  $\mu$ s total time

6x6x4 - X = 1 ns, for 80 initial conditions - 0.8  $\mu$ s total time

THIS INFO IN A TABLE, OR JUST GIVE FOR THE RELEVANT VOLUME?

I DON'T LIKE THE INCLUSION OF ALL THE ABOVE INFORMATION

In this study we compute ACFs up to correlation lengths of 100 ps, with (100,000) 1 fs timesteps. This length is longer than required but selected as a proof of concept to show convergence in the conductivity result, additionally to display the extent and behaviour of drift in the integrals for long correlation times. We show in Figure ?? that the magnitude of the ACF decays to much less than 1% of its initial value around a correlation time of 1 ps, inferring the start of convergence for the integral and thus conductivity. (ACF FIGURE FOR CORREL < 10PS?, RUNNING AVERAGE SHOWS CONVERGENCE)

ACFs produced by each simulation are integrated separately, and averaged into a single series. This process is performed for heat fluxes in each crystallographic direction, to allow analysis of anisotropy and finite system size effects. From this combined integral we pick a window of correlation lengths to capture a flat, converged region (or the section just after the 'bottleneck' if convergence is not obvious). This correlation length window is then applied to all N integrals constituent to the combined series, giving N integral averages and corresponding standard deviations. A weighted average is then taken of these data points, to give a single value with uncertainty. This value is directly proportional to thermal conductivity, as given by EQUATION XXX.

Considering bridgemanite at lower mantle conditions, we find correlation time windows in the range of 2-30 ps to be suitable. At the low-end, this allows the initial high-variability in integral value to be ignored. At the high-end, the time is long enough for good sampling of the integral, but short enough to ignore the

drift-effects. The magnitude and range of the window typically increases with conductivity (or with decreasing temperature etc.), e.g. 2-10 ps at 4000 K, and 10-30 ps at 1000 K.

### 3.3 Results

#### 3.3.1 Green-Kubo

A supercell volume of  $3 \times 3 \times 2$  (((REFER TO GRAPH, WILL NEED 1000K TOO))) fails to reproduce conductivities on the same order as the larger cells for all directions. We identify  $4 \times 4 \times 3$  and larger cells as being converged with respect to cell volume (((PROBLEMATIC STATEMENT, NOT CONVINCING, BY WHAT METRIC?))). This a useful result in terms of computation efficiency, as  $6 \times 6 \times 4$  supercells are 3 times as large (VOLUMOUS? REFERENCE ATOM COUNT?) as  $4 \times 4 \times 3$ .

#### 3.3.2 Direct method

When determining finite-size effects, it is important to consider the scenario with largest phonon mean-free paths. Phonon MFPs are largest at low temperatures (beyond the Debye temperature) and high pressures. In light of this we consider pressure of 136 GPa and temperatures of 1000 K and 4000 K. 136 GPa / 4000 K represents the expected conditions of the core-mantle boundary, whereas 136 GPa / 1000 K is unphysical in the context of the Earth but maximises MFP. UPDATE - GK RUINS EVERYTHING

By computing conductivities across a range of cell lengths we show that direct method simulations with small cross-sectional areas fail to produce converged results with respect to larger CSAs. Without considering any extrapolation, it is clear that small CSA cells overestimate conductivity (Figures ?? & ??) at conditions of both 1000 K and 4000 K. On both figures the results for cells with CSA  $2 \times 2$  and larger plot close to on top of each other. Producing the same results as  $8 \times 8$  cells, we conclude that cells with CSA of  $2 \times 2$  are suitable for direct method simulations of bridgmanite.

Now considering CSAs of  $2 \times 2$ , we examine the divergence of conductivity result with cell length from an expected linear trend (Figure ??). As mentioned in Section ??, cells that are too long or short cause a conductivity result to be overestimated. At

4000 K we find that cells up to 24 unit cells length ( $<0.06$  in inverse length) produce a reasonably linear trend. At this condition, there is no reasonable overestimation due to short cells and ballistic phonon transport. However at 1000 K where the MFP is longer, a cell of length 6 unit cells (inverse length 0.167) produces conductivity larger than expected. The same long-cell divergence is found  $>24$  unit cells length, the onset of insufficient phonon sampling. For all direct method simulations of bridgmanite at lower mantle conditions, we recommend employing cell lengths of 8 -  $<24$  unit cells. Due to the increasing computational cost associated with cell length (especially for ab initio methods), we recommend the longest cells be 16 unit cells. FINITE SIZE EFFECTS INCREASE WITH MFP/KAPPA

Now we consider CSA of 2x2 and supercell lengths of 8, 10, 12, and 16 unit cells for comparison with the results from Green-Kubo. After performing a weight least squares regression (extrapolation) on the direct method results, we obtain a conductivity with uncertainty. Figure ?? shows the extrapolation and Green-Kubo result (at  $x = 0$ ). They agree within error, meaning we have chosen a suitable set of criteria for working with direct method results. DO I NEED TO PROVE THAT OTHER LENGTHS/EXTRAPOLATIONS DON'T MATCH GK? FINE AT HIGH T / SHORT MFP, LOW T / HIGH MFP NEEDS LONGER CELLS TO EXTRAPOLATE, OR MORE SHORTER CELLS IGNORED.

### 3.4 Summary

For bridgmanite (at conditions representing the lower mantle), we show that use of the direct method for calculation of thermal conductivity will lead to an overestimate if the simulation cell is too long ( $>16$  unit cells, 4000 ONLY!!!). Small cross-sectional areas ( $<2 \times 2$  unit cells) also overestimate the thermal conductivity. This informs future work using Density Functional Theory, and will allow a model of lower mantle conductivity considering composition to be established [[[OOPS]]].

(ASSUMING THE RESULTS ARE CORRECT AND AGREE WITH GK) We see the non-linear region as described by Sellan et al. (2010) for the cell length of 6 unit cells at 1000 K, which has individually higher conductivity than expected from the

linear fit through data points corresponding to lengths of 8-16 unit cells. When included in the extrapolation, this reduces the gradient of the fit, raising the intercept and thus causing conductivity to be underestimated. At temperature of 4000 K, the 6 length cell is inline with the fit through other cells with length less than 16 unit cells. As the ratio of cell length to phonon MFP increases with temperature, we believe the onset of divergence as described by Sellan et al. moves to the right (??? - MENTION ACTUAL EFFECT - QUANTIFY RATHER THAN REFERENCING GRAPH). A shorter MFP needs shorter cell lengths to display divergent conductivity, of which we have not sampled (at high temperature). DOING THE DIRECT METHOD WITH CELLS OF LENGTH LESS THAN 6 UNIT CELLS AT ANY TEMPERATURE IS A BAD IDEA BECAUSE ...

We find conductivity is definitely dependent on CSA, but we were not able to increase CSA enough to eliminate aspect ratio-dependent divergence as reported by Hu et al. (2011). This does support our conclusion ignoring long cell lengths however, in order to keep the aspect ratio within a reasonable limit and ensure a linear fit is extrapolated. (EVEN THOUGH 48x8x8 HAS A SMALLER RATIO than 8x2x2?)

(WAFFLE ALERT) Ignoring the specifics of this study, we stress the importance of performing finite-size analysis when performing direct method calculations. Direct method cells spanning a range of lengths must be considered to find the linear regime for extrapolation. Cross-sectional area must be increased until the conductivity result converges. The same can be said about the Green–Kubo method, where the result converges with increasing volume. These effects vary with phonon mean-free path, sensitive to pressure, temperature, and compositional variations such as impurities. Completing finite-size effect analysis at conditions with the largest phonon mean-free path / thermal conductivity ensure all other conditions represent converged results. We believe classical molecular dynamics with interatomic potentials to be an excellent way of quantifying these effects quickly, performing ab initio methods (SHOULD I TAKE THIS SENTENCE OUT, NO PROOF OF THIS CLAIM).





## Chapter 4

# Modelling the thermal conductivity of Fe-bearing bridgmanite at the CMB

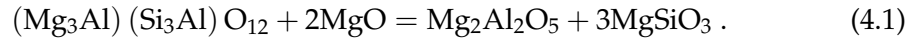
As stated earlier (REF), there are no experiments that can reach the high pressures and temperatures necessary to replicate the conditions of the lower mantle. The addition of impurities into minerals further complicates the matter. In addition to pressure and temperature-dependence, composition must be considered for full evaluation.

DISCUSS/RE-ITERATE EARLIER-DISCUSSED SEMI-RELEVANT EXPERIMENTS HERE, MANTHILAKE

### 4.1 Simulating the effect of atomic impurities

The bulk of the lower mantle comprises bridgmanite (~70%, and its high-pressure polymorph post-perovskite), ferropericlase (~20%), along with others (~10%) such as calcium silicate perovskite  $\text{CaSiO}_3$  (Trønnes, 2009). The composition can vary within these mineral archetypes, significantly the concentration of iron impurities. Magnesium is replaced with iron in  $\text{MgSiO}_3$  and  $\text{MgO}$  compositions, leading to  $\text{FeSiO}_3$  and  $\text{FeO}$  endmembers. Aluminium can similarly be substituted for Magnesium and Silicon (as in Brodholt, 2000) where, ((DOES THIS NEED TO BE IN, WITH

EQ NUMBER?))



Impurities reduce thermal conductivity by providing more opportunities for phonon scattering events. An impurity is an irregularity to a propagating phonon, much like a speedbump to a car. They have different properties to the atoms the phonon expects to meet from crystal regularity, namely mass and their bonds with neighbouring atoms. For this reason that the thermal conductivity of a solid solution is lower at intermediate compositions than at the endmembers. Even if one endmember has lower conductivity than the other, an irregular mix of the two can produce even lower values.

### 4.1.1 How do impurities affect conductivity?

The effect of impurities on lattice thermal conductivity is approximated by Klemens (1960) and Padture and Klemens (1997), a review of which can be found in the Supplementary Material of Stackhouse et al. (2015). The lattice thermal conductivity of a binary solid solution is given (Stackhouse et al., 2015, Eq. S6) as

$$\kappa_{SS} = \kappa_V \left( \frac{\omega_0}{\omega_D} \right) \arctan \left( \frac{\omega_D}{\omega_0} \right), \quad (4.2)$$

where  $\omega_0$  is the phonon frequency at which the mean free path is equal to that of the solute atoms, and  $\omega_D$  is the phonon frequency corresponding to the maximum of the acoustic branch in the phonon spectrum (the Debye frequency).  $\kappa_V$  is the compositionally-weighted (Voigt) average of endmember conductivities,

$$\kappa_V = (1 - C) \kappa_1 + C \kappa_2, \quad (4.3)$$

where  $\kappa_1$  and  $\kappa_2$  are the solid solution endmember conductivities, and  $C$  is the fractional concentration of the second endmember (Stackhouse et al., 2015, Eq. S7).

#### $\omega_0/\omega_D$ overview

When  $\omega_0 \gg \omega_D$ ,  $\arctan(\omega_D/\omega_0) \rightarrow (\omega_D/\omega_0)$ , so  $\kappa_{SS} \rightarrow \kappa_V$ , the conductivity including the effect of impurities tends toward the endmember linear average. This is the scenario when other factors, such as Umklapp processes at high temperatures, have caused conductivity to decrease significantly. Adding impurities at this point has little additional effect, conductivity is already close to its saturated minimum.

On the other hand, when  $\omega_D \gg \omega_0$ ,  $\arctan(\omega_D/\omega_0) \rightarrow \pi/2$ , but  $(\omega_0/\omega_D) \ll 2/\pi$ , so  $\kappa_{SS} < \kappa_V$ , and impurity scattering has a noticeable effect on the resultant conductivity. Adding impurities affects conductivity in this fashion when phonon-phonon collisions are not the dominant conductivity reducing process, like at low temperatures compared to the conditions mentioned in the above case.

### What effects the magnitude of impurity scattering?

That factors that affect the severity of impurity scattering are temperature, the mass difference between the impurity and what it replaced, and the concentration of said replacements. The ratio of the phonon frequencies in Eq. 4.2 can be expressed (Stackhouse et al., 2015, Eq. S11) as

$$\left(\frac{\omega_0}{\omega_D}\right)^2 = \frac{1}{(6\pi^2)^{1/3}} \frac{T}{3\varepsilon T_0}, \quad (4.4)$$

where  $T$  is temperature,  $T_0$  is the temperature associated with  $\omega_0$ , and  $\varepsilon$  is related to the mass difference and proportion of endmembers by

$$\varepsilon = \frac{(M_2 - M_1)^2}{\bar{M}^2} C(1 - C), \quad (4.5)$$

where  $M_i$  is the atomic mass of the  $i$ -th endmember,  $\bar{M}$  is the mean atomic mass of the solid solution, and  $C$  is the proportion of endmembers (Stackhouse et al., 2015, Eq. S9).

As the temperature increases, so too does the left-hand side of Equation 4.4. As discussed earlier, this reduces the effect of scattering caused by impurities, which will be relevant at CMB conditions where temperature is large ( $\sim 4000$  K).

$\varepsilon$  increases with the mass difference of the endmembers, and the impurity concentration. Increasing  $\varepsilon$  tends to reduce the phonon frequency ratio, meaning impurity scattering will affect the resultant conductivity more. The atomic masses of Mg and Fe are 24 and 56, so FeSiO<sub>3</sub> is 1.32 times heavier than MgSiO<sub>3</sub>.

As an aside, Equation 4.5 predicts that isotopic variations will have little effect on conductivity, where the mass changes are typically small (e.g. <sup>24</sup>Mg to <sup>25/26</sup>Mg) and abundances are low (Mg standard atomic weight is 24.3, the ratio of <sup>24</sup>Mg to heavier isotopes is roughly 4:1). Mass difference is an additional reason why Fe impurities are more interesting theoretically than Al. The mass of Al is 27, compared to Mg with 24 and Si at 28.

The composition control term in Equation 4.5,  $C(1 - C)$ , increases from 0 to 0.25, when  $x = 0.5$ .  $\varepsilon$  increases with composition up to 50%, the furthest point away from both endmembers, therefore the condition of most disorder in the atomic structure.

---

While I investigate the full range of C, most of the lower mantle (Mg,Fe)SiO<sub>3</sub> is going to have compositions up to 20% Fe ((REF)). Knowledge of conductivity up to FeSiO<sub>3</sub> composition is interesting if ultra low velocity zones are thermochemical features of high Fe content ((REF)).

#### 4.1.2 $\omega$ and $\tau$ in depth

$\omega_0$  is defined (by Klemens, 1960, Eq. 11) as the frequency at which

$$\tau'(\omega_0) = \tau_u(\omega_0), \quad (4.6)$$

where  $\tau'$  and  $\tau_u$  are the contributions of point defect scattering and Umklapp processes respectively to the effective phonon relaxation time (Klemens, 1960, Eq. 2 & 3), where

$$1/\tau' = A\omega^4, \quad (4.7)$$

and

$$1/\tau_u = B\omega^2. \quad (4.8)$$

The effective phonon relaxation time of the system, using the Matthiesen Rule (modified from Klemens, 1960, Eq. 7), is

$$\frac{1}{\tau(\omega)} = \frac{1}{\tau_u} + \frac{1}{\tau'}. \quad (4.9)$$

When Equation 4.6 is satisfied, the effective relaxation time will equal to half of either its constituents,

$$\frac{1}{\tau(\omega_0)} = \frac{1}{\tau_u} + \frac{1}{\tau'} = \frac{1}{\tau_{\omega_0}} + \frac{1}{\tau_{\omega_0}} = \frac{2}{\tau_{\omega_0}}. \quad (4.10)$$

When  $\tau' \neq \tau_u$ , the effective relaxation time will tend toward the smaller of the two as the difference increases. [[INCLUDE ARCTAN GRAPH TO ILLUSTRATE THIS POINT ???]]

For a CMB-like condition of high temperature, Umklapp process relaxation time is short. Adding impurities doesn't contribute much to the already large scattering effect. Where the Umklapp process relaxation time is long, even adding a small amount of atomic impurity can influence the effective system behaviour. Considering the average phonon velocity, a longer relaxation time means a greater distance travelled, or phonon mean free path.

Calling back to Equation 4.7 & 4.8,  $A$  and  $B$  are constants, where only the latter is temperature-dependent ( $T$ ). The contribution of point defect scattering to the effective phonon relaxation time is constant with temperature (varying with impurity

concentration and composition). It is the relative magnitude of  $\tau_u$ , which decreases with temperature ( $\propto 1/T$ , via  $B$ ), to  $\tau'$  that influences the effect of impurities on thermal conductivity (see Equation 4.9).

The two relaxation time terms above can be equated via Equation 4.6, showing  $\omega_0$  is similarly temperature-dependent

$$\begin{aligned} A\omega_0^4 &= B(T)\omega_0^2, \\ \omega_0^2 &= B(T)/A, \\ \omega_0 &\propto T. \end{aligned} \tag{4.11}$$

The Debye frequency is a constant, so

$$\left(\frac{\omega_0}{\omega_D}\right) \propto T. \tag{4.12}$$

As temperature increases (above the Debye temperature), conductivity decreases because of Umklapp processes. The significance (SHOWN IN A LATER FIGURE) of point defect scattering decreases as phonon-phonon scattering becomes more prominent. Therefore the relative conductivity decrease due to impurities is inversely proportional with temperature.

IS DEBYE FREQUENCY A CONSTANT? DEPENDENT ON SOUND VELOCITY, THEREFORE SMALLER WITH TEMPERATURE, A FUNCTION OF TEMPERATURE? DEBYE TEMPERATURE DEPENDS ON DEBYE FREQUENCY, WHICH DEPENDS ON SOUND VELOCITY IN MATERIAL, WHICH DEPENDS ON TEMPERATURE, SO DEBYE TEMPERATURE DEPENDS ON TEMPERATURE???

## 4.2 Methodology

In this section I outline the process of taking Fe from chemistry to computer, by fitting my own coefficients to a Buckingham potential. I also go over how the Fe is incorporated into the  $\text{MgSiO}_3$ , considering its placement and concentration.

### 4.2.1 How does iron behave?

I use two methods to introduce iron impurities to my bridgmanite models. The first approach is to simply create a magnesium atom with the mass of an iron atom, without changing any coefficients of the interatomic potentials from Oganov et al. (2000). Despite being an obviously "quick and dirty" method, (I will show) this is a reasonable first-order approximation(((PROVE IT!))). As the variation in mass number from Mg to Fe is large (24 to 56, a 133% increase), it is likely to change the behaviour of the system more than a subtle change in the atomic interactions.

MENTION AMMANN IRON STUFF HERE

The second approach to add Fe into the  $\text{MgSiO}_3$  system is to fit interatomic potentials, as well as using the aforementioned mass change for a more realistic model. I adapted the Oganov et al. (2000)  $\text{MgSiO}_3$  Buckingham interatomic potential ( $U$ ) to include the Fe-O interaction. I determined two short-range potential parameters,  $b$  and  $\rho$ , shown in Eq. 11 from Oganov et al. (2000),

$$U_{ij}(R_{ij}) = \frac{z_i z_j}{R_{ij}} + b_{ij} \exp\left(-\frac{R_{ij}}{\rho_{ij}}\right) - \frac{c_{ij}}{R_{ij}^6}, \quad (4.13)$$

where  $ij$  refers to an atom pair,  $R$  is interatomic distance,  $z$  is atomic charge, and  $c$  relates to the Van der Waals force (zero for non O-O interactions). We determine  $\rho$  in the same fashion as Oganov et al. (2000), calculated from the atomic first ionisation potentials,

$$\rho_{ij} = \frac{1.85}{\sqrt{I_i} + \sqrt{I_j}}. \quad (4.14)$$

$b$  is constrained using the GULP code (Gale, 1997), using the calculated  $\rho$  value for Fe-O. We fit to the elasticity results of Parise and Wang (1990), an experimental study



of  $(\text{Mg}_{0.9}\text{Fe}_{0.1})\text{SiO}_3$  bridgmanite up to 433 K. Despite potential fitting being an improvement on solely changing mass (((PROVE IT!))), it is still not perfect as the charge of our fitted Fe is not varied from the original Mg.

!!! Validate potentials

!!! Validate Fe vs. heavy Mg, isotope mass

!!! Include Oganov table (earlier?), with the fitted Fe info

#### 4.2.2 Where do the impurities go?

Iron is substituted with magnesium into the bridgmanite atomic structure. The unit cell contains 4 Mg atoms, and the smallest direct method cell I employ is a 6x2x2 supercell. Therefore the smallest amount of iron that can be added is 1/96 atoms, a concentration just over 1%. A simple MATLAB script (((REF, APPENDIX))) is used to modify LAMMPS input files, randomly selecting a specified proportion of Mg atoms to be replaced with Fe. When a Mg atom changes to Fe, its mass and interatomic potential properties change.

Due to the microscopic nature of the system, we do not want all of the added iron to be concentrated together in the simulation cell, especially in a heat source/sink region (((ELABORATE WITH FIGURE?))). To avoid this we order Mg atoms by length along supercell, and change a single atom every so many. For example, changing 1/4 atoms is different to changing 24/96. The latter has a higher variance in Fe per unit length, and the former chooses one atom to swap for every four along the system. After iron is added, the standard direct method or Green-Kubo workflow is followed.

!!! NICE PICTURE/DIAGRAM HERE?

!!! Comparison of random and homogeneous distribution, don't make reader engage their imagination, show obvious picture

### 4.3 Results

Lattice thermal conductivities obtained from Green-Kubo calculations are plotted against temperature in Figure 4.1, for Mg and Fe-endmembers and the 50/50 solid solution mix.

Conductivity decreases with temperature, approximately following  $\kappa \propto 1/T^{0.9}$  at the pressure of 136 GPa considered here. This is in contrast to the typically expected  $\kappa \propto 1/T$  relation, indicating some kind of saturation in conductivity decrease with temperature.

FeSiO<sub>3</sub> has a consistently lower conductivity than MgSiO<sub>3</sub>, which is to be expected due to the atomic mass increase [WRONG, SHEAR MOD DECREASE, DENSITY INCREASE, WAVESPEED EQUATION]. The two trends appear to be converging, indicating the conductivity of both species may be equal given a high enough (though unphysical for the lower mantle) temperature. This suggests there is a minimum conductivity associated with the crystal structure, reached first by FeSiO<sub>3</sub> with its inherently lower conductivity.

The 50% solid solution has a consistently lower conductivity than MgSiO<sub>3</sub>, and a lower than or equal to relation to FeSiO<sub>3</sub>. This is again to be expected, conductivity decreases from endmember to intermediate compositions as impurity concentration increases. It can be seen that conductivity differences are very small at high temperatures for FeSiO<sub>3</sub> and the solid solution. If FeSiO<sub>3</sub> has already reached its theoretical minimum, adding impurities will do little to decrease it further.

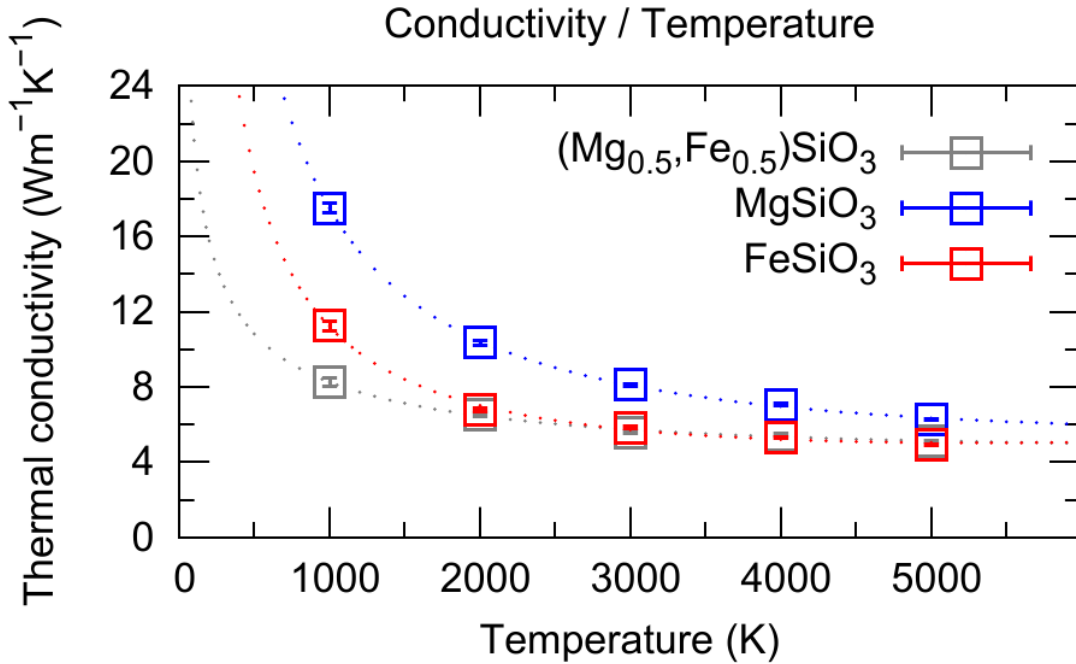


FIGURE 4.1: Data points are GK conductivity results, dotted line is the fit from Equation 4.25.

An alternative perspective to Figure 4.1 is presented in Figure 4.2, where Green-Kubo conductivity results are plotted as a function of Fe impurity content for several temperature series.

Conductivity generally decreases with increasing temperature at all compositions, though the change becomes minimal at temperatures above 3000 K.

The  $\text{MgSiO}_3$  endmember has a consistently higher conductivity than the  $\text{FeSiO}_3$ . This can be explained by the general reduction in shear modulus and increase in density associated with adding Fe, which decreases seismic velocity and thus conductivity [TRUTH ALERT, REF???].

The amount of Mg atoms replaced with Fe has a variable effect on conductivity. A better way to label the effect is impurities added to an endmember, i.e. Fe is added to  $\text{MgSiO}_3$  and Mg to  $\text{FeSiO}_3$ , which always serves increase phonon scattering and decrease conductivity. The decrease from this effect saturates towards a 50% compositional mix. At high temperatures, this effect is minimal when adding Mg to  $\text{FeSiO}_3$ . The conductivity could already be close to its theoretical minimum due to temperature effects, little reduction is observed from adding impurities.

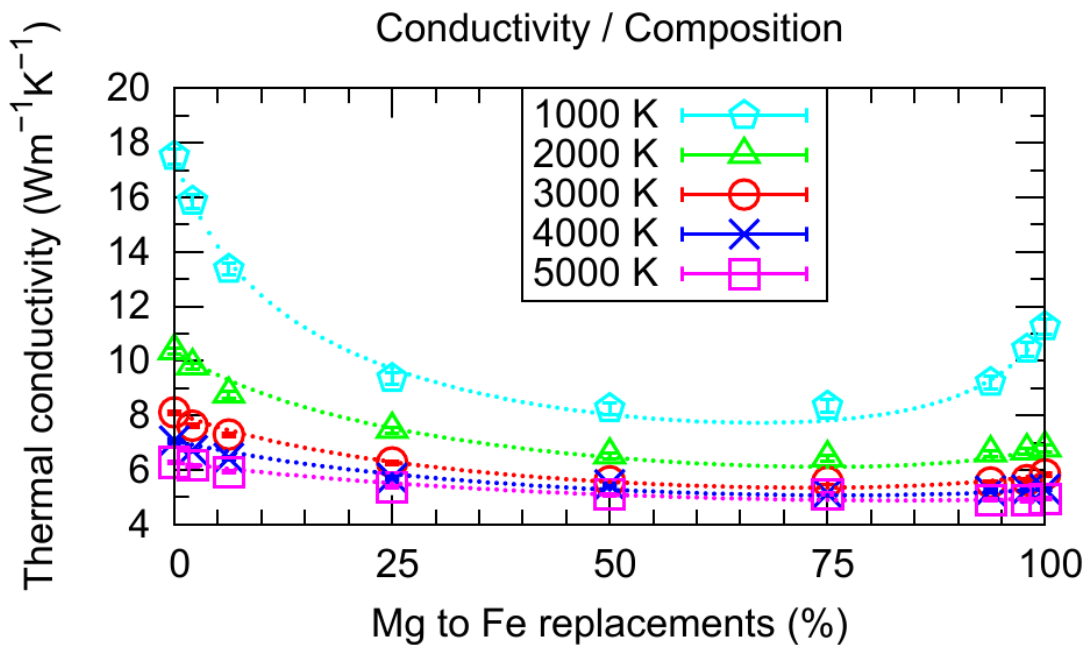


FIGURE 4.2: CAPTION

A simple interpolation between endmember conductivities is insufficient, the

presence of a compositional mix has an effect. This effect is itself temperature-dependent, the trough-like trend flattens with increasing temperature. These temperature and compositional dependences can be combined, allowing conductivity to be determined for a range of possible CMB conditions (Figure 4.3).

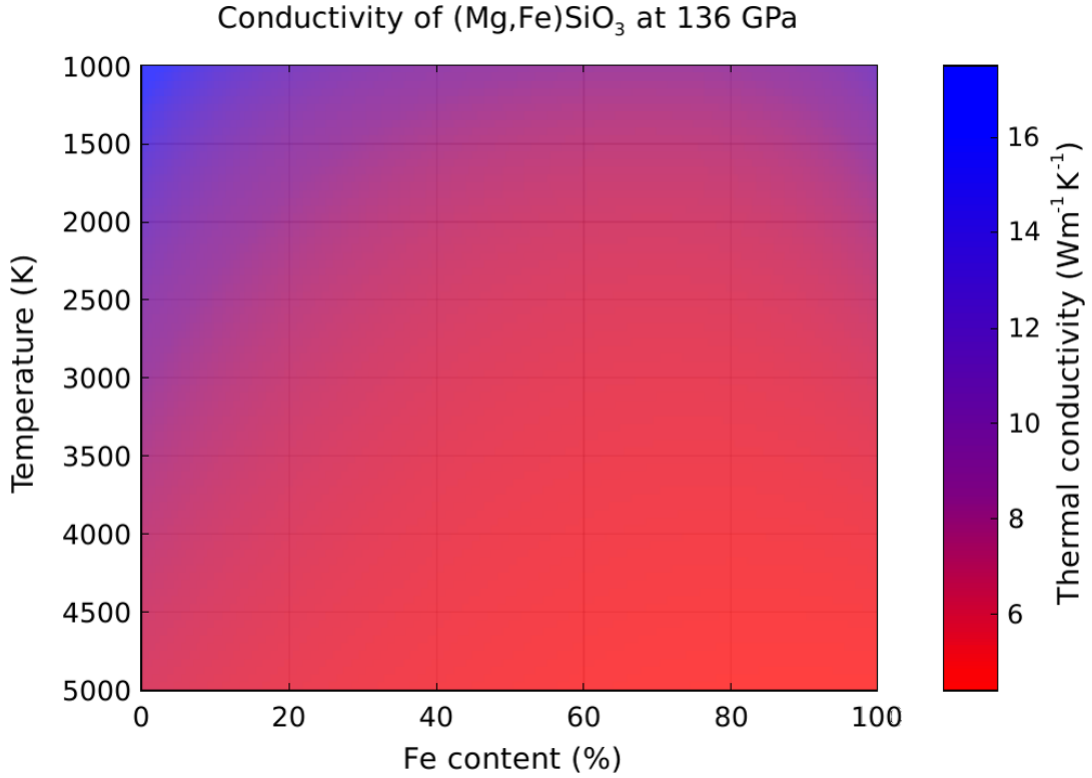


FIGURE 4.3: Modelled conductivity, shown plotted against temperature and composition. Note the sensitivity of the colour scale, showing low conductivities as dominant at high temperatures and intermediate compositions. High values are found only at low temperatures, and even then they rapidly decay and saturate to  $<8\text{Wm}^{-1}\text{K}^{-1}$ . Such conditions are unphysical at 136 GPa within the lower mantle.

#### 4.4 Parameterising the effect of composition and temperature on CMB conductivity

In this section I develop a model for the lattice thermal conductivity of  $(\text{Mg,Fe})\text{SiO}_3$  perovskite at CMB conditions. Whilst the CMB is a small section of the lower mantle, it marks the heat flow boundary from core to mantle. Mantle-side thermal conductivity controls the nature of this heat flow, making it an important parameter in studies on both sides of an important interface. The CMB is isobaric at 136 GPa, and isothermal at an uncertain temperature. Fe-content can vary with position. In

terms of making a model I can collect data at one pressure condition, and investigate how an array of temperatures and compositions affect thermal conductivity.

Due to uncertainty in the lower mantle's composition, properties like thermal conductivity are often averaged considering the abundance of each mineral component. There are also solid solutions to consider though, particularly the concentration of Fe in  $\text{MgSiO}_3$ , as well as the phase boundary between bridgmanite and  $\text{MgSiO}_3$  post-perovskite.

The conductivity of an intermediate composition is not a simple weighted average of the endmember values, you cannot interpolate linearly. This can be seen in Figure 4.1, where the  $(\text{Mg}_{0.5}\text{Fe}_{0.5})\text{SiO}_3$  results do not plot between those of  $\text{MgSiO}_3$  and  $\text{FeSiO}_3$ .

#### 4.4.1 Parameterising the data fit

[Equations from Ohta et al., 2017 (eq. 7,8,9), and Okuda et al., 2017 (eq. 5)]

Equations and functional forms exist for the temperature and compositional dependence of thermal conductivity, and it is possible to combine the two. The basic idea is to determine the conductivity of  $\text{MgSiO}_3$  and  $\text{FeSiO}_3$  endmembers at the temperature of interest, and then apply the (temperature-dependent) effect of composition.

Padtare and Klemens (1997) propose a model for how impurities affect lattice thermal conductivity of a solid solution, which Ohta et al. (2017) use to fit experimental ferropericlase data. Following a similar methodology, I fit the functional form to my  $(\text{Mg,Fe})\text{SiO}_3$  perovskite results at various temperatures (1000 K, 2000 K, 3000 K, 4000 K, and 5000 K). In an additional step, I establish how the functional forms change with temperature, the temperature-dependence of the compositional-dependence if you will.

Okuda et al. (2017) present a temperature scaling relation for lattice conductivity (originally from Manthilake et al., 2011), fit to their experimental results of bridgmanite. I apply this temperature scaling to computational results of  $\text{MgSiO}_3$  and  $\text{FeSiO}_3$  at 136 GPa. With the temperature dependence of these endmembers and of

the compositional effect, I am able to determine the conductivity of any composition, interpolating to temperatures in the range 1000 K to 5000 K, at 136 GPa pressure representative of the CMB.

The aforementioned temperature dependence from Manthilake et al. (2011) considers density, allowing conductivity to be determined as a function of temperature and pressure. In the examples I will present, I am only concerned with systems at 136 GPa. All density changes will result from thermal expansion, and the equations will be altered to accomodate this.

Some of the equations in the following section have already been presented as analogous forms in Section 4.1.1. The equations are kept similar to their published form, which was Stackhouse et al. (2015) in the former, and Ohta et al. (2017) and Okuda et al. (2017) in the following.

### Compositional dependence

REFERENCE BACK TO METHODOLOGY FOR FIRST TWO EQUATIONS AND DEFINITIONS ETC.

The lattice thermal conductivity of a solid-solution as a function of temperature and composition can be approximated by the following equation, WHY DOES THIS EQUATION EVEN WORK?

$$\kappa_{SS} = \kappa_V \left( \frac{\omega_0}{\omega_D} \right) \arctan \left( \frac{\omega_D}{\omega_0} \right), \quad (4.15)$$

where  $\omega_0$  is the phonon frequency at which the Umklapp/regular processes and impurity scattering effects' contributions to the mean free path (average distance travelled by a phonon) are equal. In terms of generating thermal resistance, neither effect dominates the other at this frequency.  $\omega_D$  is the phonon frequency corresponding to the maximum of the acoustic branch in the phonon spectrum (the Debye frequency).  $\kappa_V$  is the conductivity of the solid solution in the absence of impurity scattering

$$\kappa_V = (1 - C) \kappa_{\text{MgSiO}_3} + C \kappa_{\text{FeSiO}_3}, \quad (4.16)$$

where  $C$  is the fractional concentration of Fe, and  $\kappa_{\text{MgSiO}_3}$  and  $\kappa_{\text{FeSiO}_3}$  the temperature

dependent conductivities of the endmembers. The ratio of the phonon frequencies can be expressed as

WHAT IS THE THEORY BEHIND THIS?

$$\left(\frac{\omega_0}{\omega_D}\right)^2 = \frac{\chi^T}{C(1-C)}, \quad (4.17)$$

where  $\chi$  is a temperature-dependent constant, and  $T$  is the temperature of interest.  $\chi$  can be thought of as a measure of resistance to the effects of impurity scattering. The  $\kappa$  against  $C$  relationship (Figure 4.2) shows a larger effect of impurity scattering in the form of greater curvature when  $T$  and  $\chi$  are lower (TABLE XX - CHI VALUES NEXT TO T). For a given  $T$  and  $C$ , increasing  $\chi$  increases the phonon frequency ratio  $\left(\frac{\omega_0}{\omega_M}\right)$  which, as discussed in Section 4.1.1, means  $\kappa_{\text{latt}}$  tends towards  $\kappa_i$ .  $\chi$  is fit to the data at each temperature, but for the model we need it as a function of temperature. Figure 4.4 shows a plot of  $\chi$  against  $T$  with a power law (LEFT/B.) and 4th-order polynomial (RIGHT/B.), the former of which is a poor fit and the latter an egregious overfitting.

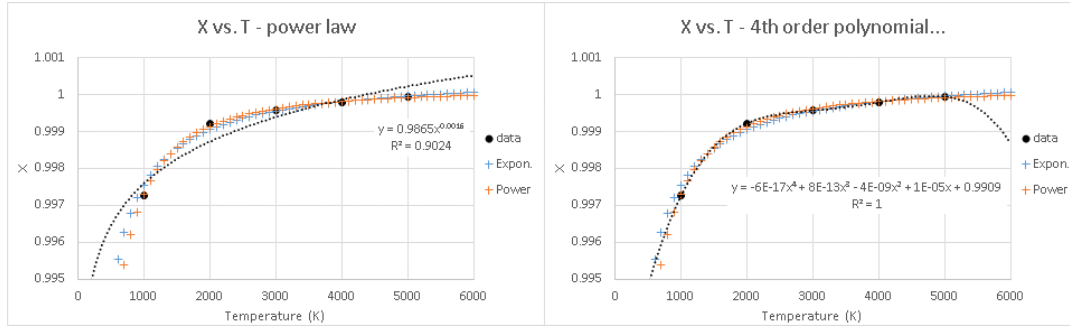


FIGURE 4.4: The fit  $\chi$  values plotted against  $T$ , with power law (LEFT/A.) and 4th order polynomial (RIGHT/B.) trendlines (both black). Blue and orange series are the exponential and power law fits obtained from plotting  $\chi^T/T$  (see Figure 4.5).

The lack of an obvious trend in  $\chi$  against  $T$  can be mitigated by plotting  $\chi^T$  over  $T$ , and fitting either a exponential or power law relationship (Figure 4.5). I use the following power law-relationship,

$$\chi^T = AT^B, \quad (4.18)$$

where  $A$  is the coefficient and  $B$  is the exponent to be determined. The magnitudes

of these fit parameters are  $3.468 \times 10^{-6}$  and 1.426 respectively. This fit represents the temperature-dependence better, both statistically and sensitivity-wise compared to an exponential relationship ( $\chi^T = Ae^{BT}$ ). The value of  $\chi^T$  at high  $T$  has a lesser effect on the conductivity-composition relationship than at low  $T$ , where the power law fit matches the data closer. In Figure 4.4, we can see that both the power law and exponential  $\chi^T$  over  $T$  relationships fit the data better than the  $\chi$  over  $T$  power law or polynomial relations.

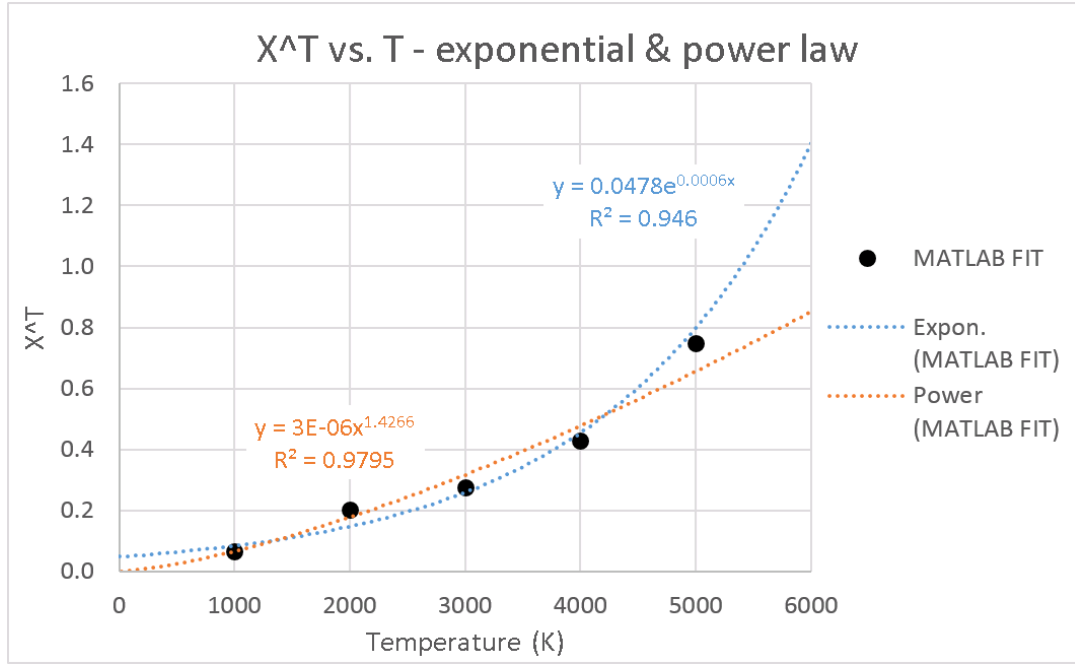


FIGURE 4.5: Exponential fit in blue (more curved), power law in orange (flatter)

The conductivities of  $\kappa_{\text{MgSiO}_3}$  and  $\kappa_{\text{FeSiO}_3}$  from Equation 4.16 can be scaled with temperature, giving an adjusted value

$$\kappa_{\text{adj}} = \kappa_{\text{ref}} \left( \frac{\rho}{\rho_{\text{ref}}} \right)^g \left( \frac{T_{\text{ref}}}{T} \right)^a. \quad (4.19)$$

$\rho$  is density,  $g$  and  $a$  are exponents which control the nature of the density and temperature-dependence, and “ref” denotes a reference value. This equation is fit to the data, anchored around the values of the reference data point (the fit is shown in Figure 4.1). I fit to the data point at 1000 K, as the conductivities at higher temperatures become more similar, converging towards a minimum point. Anchoring to 1000 K reduces the error in the fit, on account of the relatively larger conductivity



at this temperature. BIGGER VALUE, IS THE ERROR RELATIVE TO THE VALUE SMALLER?

For a given composition, the mass of the simulated system does not change with temperature. The number and type of atoms remains constant, while thermal effects cause density variations. The density relation in Equation 4.19 can be reformulated as

$$\frac{\rho}{\rho_{\text{ref}}} \equiv \frac{V_{\text{ref}}}{V}, \quad (4.20)$$

because  $\rho \propto V^{-1}$ , where  $V$  is the volume of the system in question. This leads to a modified version of Equation 4.19

$$\kappa_{\text{adj}} = \kappa_{\text{ref}} \left( \frac{V_{\text{ref}}}{V} \right)^g \left( \frac{T_{\text{ref}}}{T} \right)^a. \quad (4.21)$$

The exponent  $g$  represents the rate of change of lattice thermal conductivity with density, at a constant temperature,

$$g = (\partial \ln \kappa_{\text{latt}} / \partial \ln \rho)_T. \quad (4.22)$$

The density/volume changes that I observe result from thermal effects, i.e. not at a constant temperature and not pressure-driven. The rate of change in conductivity with density in my data are better represented as something like

$$h \sim (\partial \ln \kappa_{\text{latt}} / \partial \ln \rho)_P, \quad (4.23)$$

where pressure ( $P$ ) is the condition kept constant. The significance here is that pressure-driven and temperature-driven density changes affect the conductivity differently. At constant temperature, conductivity and density increase with pressure. The opposite is true at constant pressure for the material and temperatures considered here, conductivity and density decrease with increasing temperature. The result is  $g$  and  $h$  having opposite polarities based on the scenarios they describe.

Volume does not need to be input ((INDEPENDENT?)) variable for the model, as all the data are obtained from constant pressure (136 GPa) calculations and any volume variations relate to thermal expansion. I express the volume ratio shown in

Equation 4.21 as

$$\frac{V_{\text{ref}}}{V(T)} \approx mT + c, \quad (4.24)$$

a simple linear function of temperature (see Figure 4.6), where  $m$  is the gradient and  $c$  the intercept (as you might expect).

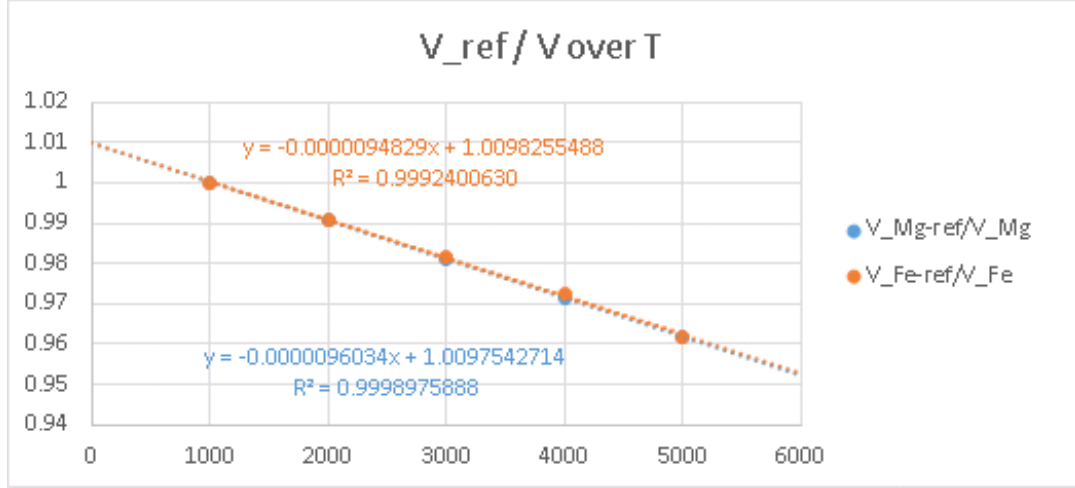


FIGURE 4.6:  $V_{\text{ref}}/V$  can be expressed as a simple linear function of  $T$ .

With Equation 4.24, we rewrite Equation 4.19 one more time,

$$\kappa_{\text{adj}} = \kappa_{\text{ref}} (mT + c)^h \left( \frac{T_{\text{ref}}}{T} \right)^a. \quad (4.25)$$

This equation allows me to obtain a conductivity value at any temperature within the fit range, comprising a reference conductivity and temperature for the material in question, with constants ( $m$ ,  $c$ ,  $h$ , &  $a$ ) fit to data across a range of temperatures (1000 K, 2000 K, 3000 K, 4000 K, & 5000 K). This scaling process is necessary for  $\kappa_{\text{MgSiO}_3}$  and  $\kappa_{\text{FeSiO}_3}$ , which have their own reference values and fit constants.

ADD MORE REFEEERENCES DUH

TABLES OF CONSTANTS AND STUFF

conductivity

		Temperature (K)				
		1000	2000	3000	4000	5000
Conductivity (Wm <sup>-1</sup> K <sup>-1</sup> )	Mg	17.51	10.36	8.11	7.07	6.28
	Fe	11.26	6.79	5.84	5.30	4.95
Volume (Å <sup>3</sup> )	Mg	5960	6017	6075	6136	6199
	Fe	6253	6310	6369	6431	6500
$V_{\text{ref}}/V(T)$	Mg	1	0.9906	0.9811	0.9714	0.9616
	Fe	1	0.9909	0.9817	0.9723	0.9619
$\chi$		0.9973	0.9992	0.9996	0.9998	0.9999
$\chi^T$		0.0649	0.2035	0.2748	0.4277	0.7494

	Endmember	
	Mg	Fe
$\kappa_{ref}$	17.51	11.26
$h$	-10.93	-17.32
$a$	0.896	0.913
$m$	-9.60E-06	-9.48E-06
$c$	1.00975	1.00983



## Chapter 5

# Modelling the lower mantle with variable thermal conductivity

### 5.1 Main Section 1

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#### 5.1.1 Subsection 1

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## Chapter 6

# Summary/Discussion/Conclusion

### 6.1 Main Section 1

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#### 6.1.1 Subsection 1

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## Appendix A

# Frequently Asked Questions

### A.1 How do I change the colors of links?

The color of links can be changed to your liking using:

```
\hypersetup{urlcolor=red}, or  
\hypersetup{citecolor=green}, or  
\hypersetup{allcolor=blue}.
```

If you want to completely hide the links, you can use:

```
\hypersetup{allcolors=.}, or even better:  
\hypersetup{hidelinks}.
```

If you want to have obvious links in the PDF but not the printed text, use:

```
\hypersetup{colorlinks=false}.
```



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