# EECS 16A Designing Information Devices and Systems I Final Review

#### 1. Force Touch (Fall 2017 Midterm 2)

So far, our capacitive touchscreens have been able to measure the presence or absence of a touch, but with some modifications, we can actually measure how hard the finger is pressing (i.e., force) as well. Figure 1 shows this type of touch screen without any touch and with the finger pressing on it; the more force the finger applies to the screen, the more the distance between the two metal plates decreases.

Assume that the insulator in between the plates has some permittivity  $\varepsilon_1$  and that the top metal plate has an area A. With no force applied on the screen, the top and bottom plates are a distance d apart. When a force is applied, the distance becomes d' (< d). Suppose when a finger is touching the screen, it creates a capacitance  $C_{F,E_{\text{top}}}$  between itself and the lower plate.

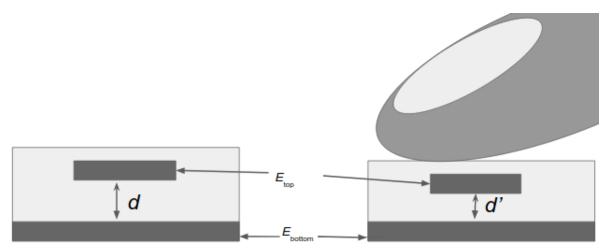


Figure 1: Sensor configurations.

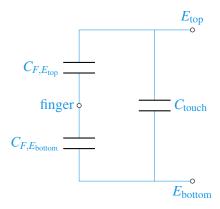
(a) With no finger touching or applying any force, find the capacitance  $C_{\text{no touch}}$  between the top metal plate and the bottom metal plate. Express your answer in terms of  $\varepsilon_1$ , d, and A.

Answer:

$$C_{\text{no touch}} = \frac{\varepsilon_1 A}{d}$$

(b) Now suppose that a finger that is touching the screen applies some force on our screen. **Draw a circuit model** including all of the capacitors connected to either  $E_{\text{top}}$  or  $E_{\text{bottom}}$ . **Label all elements** in your model.

**Answer:** 



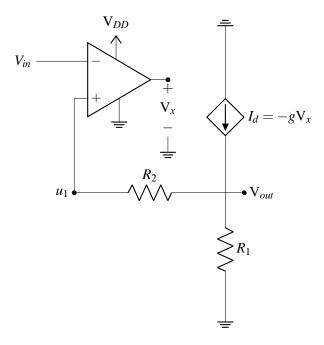
(c) Assuming that  $C_{F,E_{top}} = C_{F,E_{bottom}} = 0$  F, find the equivalent capacitance,  $C_{force}$ , between  $E_{top}$  and  $E_{bottom}$ . Express your answer in terms of  $\varepsilon_1$ , d', and A.

Answer:

$$C_{\text{force}} = C_{\text{touch}} = \frac{\varepsilon_1 A}{d'}$$

## 2. Can I Give You Some Feedback? (4 points)

The following circuit is a linear voltage regulator.



 $V_{DD}$  and  $V_{in}$  are both connected to ideal voltage sources. g is the gain factor of the dependent current source. The opamp has finite gain A.

Using the method for negative feedback analysis, if  $V_{out}$  increases, determine what happens to the following values. Circle one of the two options for each line below. Note that if a quantity is getting more negative, that means it is decreasing.

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Voltage at  $u_1$  will: Increase Decrease

 $V_x$  will: Increase Decrease

Dependent current  $I_d$  will: Increase Decrease

The circuit is in: Negative Feedback Positive Feedback

**Solution:** Increase, increase, decrease, and negative feedback.

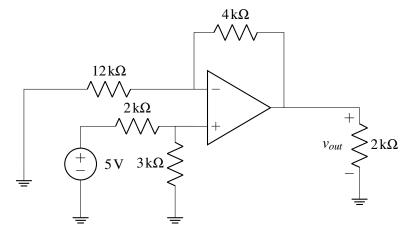
When  $V_{out}$  increases, because no current can go into the positive terminal of the op-amp, there cannot be voltage drop across  $R_2$ . As a result, voltage at  $u_1$  must follow  $V_{out}$  and increase.

By definition of op-amp output voltage,  $V_x = A(u_1 - V_{in})$ , as  $u_1$  increases,  $V_x$  increases.

Thus, because  $V_x$  increases,  $I_d = -gV_x$  must decrease. Finally, because  $I_d$  decreases, the current through  $R_1$  to decreases, therefore  $V_{out}$  ends decreases. This is the expected result of negative feedback.

## 3. Op-amps and Comparators (Spring 2022 Midterm 2 Question 10)

(a) You are given the following op-amp in negative feedback. Find  $v_{out}$ .



**Solution:** First, we can find V+ using a voltage divider.

$$V^{+} = 5V * \frac{3k\Omega}{2k\Omega + 3k\Omega}$$
$$V^{+} = 3V$$

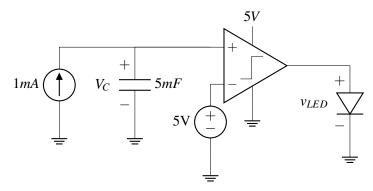
As op-amp is in negative feedback and it is an ideal opamp, by golden rules, V- = 3V too.

Next, using node voltage analysis at  $v^-$ , we can write:

$$\frac{V^- - 0}{12k\Omega} + \frac{V^- - v_{out}}{4k\Omega} = 0$$

Using  $V^- = 3V$ , we solve that  $v_{out} = 4V$ .

(b) You are given the circuit below. The capacitor is initially uncharged. At time t = 0, the current source is turned on. Find  $V_c(t)$ .



**Solution:** We know that the IV relationship of a capacitor is  $I = C \frac{dV}{dt}$ , By integrating both sides, we can derive that

$$V_C(t) = \frac{I * t}{C} + V(0)$$

In this case, we know V(0) = 0V because it is initially uncharged. Thus,  $V(t) = \frac{1mA}{5mF}t = 0.2t$ .

(c) The LED turns on when the voltage across it is greater than 3.3V. Using the same setup as part (b), at what time t does the LED turn on?

**Solution:** When V+ is greater than V- for the comparator, the op-amp will output Vdd (5V), which will turn on the LED. In order to have V+ > V-, V(t) > 5V. This happens when  $V_C = 5V$ , 0.2t = 5, so t = 25s.

### 4. An Easier Way To Do Math Homework (10 points)

You're working on your Math 1B homework and you don't know how to calculate an integral. Instead, you decide to put your circuit skills to use to solve this problem!

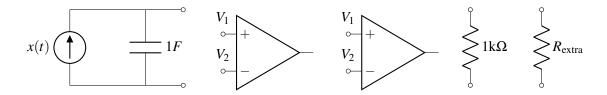
The integral that you're trying to solve is of the form

$$-\frac{1}{5}\int_0^{\tau} x(t) dt$$

Your helpful lab TA, Raghav, gives you several circuit elements that you can use.

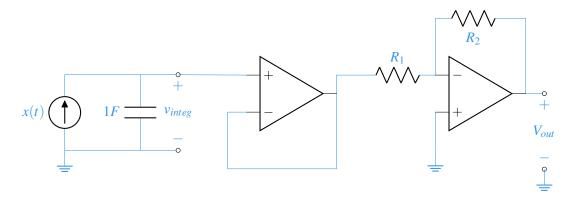
These elements are:

- A current source  $I_s = x(t)$  amps in parallel with a capacitance of 1F.
- Two op-amps (assume that the supply voltages to the op-amps are provided).
- A resistor  $R_{\text{fixed}} = 1 \text{k}\Omega$ .
- One additional resistor  $R_{\text{extra}}$  that can have **any value**. Be sure to specify the resistance you use.



Design a circuit to have the above output using the provided elements. Clearly specify the resistance of  $R_{extra}$  if used.

#### **Solution:**



The circuit consists of three main blocks: the current source and capacitor which integrate our signal, a buffer, and an inverting amplifier. The current source charges our capacitor resulting in:

$$v_{integ} = \frac{1}{1F} \int_0^{\tau} x(t) dt$$

Next, in order to scale and invert our signal we can chose  $R_1 = 5R_2$ . Since we have a fixed resistor of  $1\Omega$ , we pick  $R_2 = R_{fixed} = 1k\Omega$  and  $R_1 = R_{extra} = 5k\Omega$ .

Our overall result becomes:

$$v_{out} = \frac{-R_2}{R_1} v_{integ} = \frac{-1}{5} \int_0^{\tau} x(t) dt$$

## 5. Least Squares (Fall 2022 Final Question 3)

(a) Consider the system of equations  $\vec{a}x = \vec{b}$  where  $\vec{a}, \vec{b} \in \mathbb{R}^2$  and  $x \in \mathbb{R}$ . When applying least squares, we want to find the  $\vec{v} \in \text{span}(\vec{a})$  that is closest to  $\vec{b}$  in Euclidean distance.

Hint: It might be helpful to draw the vectors.

- i. When solving for vector  $\vec{v}$ , which of the following operations are required?
  - $\bigcirc$  Projecting  $\vec{b}$  onto  $\vec{a}$
  - $\bigcirc$  Projecting  $\vec{a}$  onto  $\vec{b}$
  - $\bigcirc$  Subtracting  $\vec{b}$  from  $\vec{a}$
  - $\bigcirc$  Subtracting  $\vec{a}$  from  $\vec{b}$
  - O None of the above

#### **Solution:**

Projecting  $\vec{b}$  onto  $\vec{a}$ .

When we are finding  $\vec{v}$ , or the best approximation of  $\vec{b}$  in the span of  $\vec{a}$ , we project  $\vec{b}$  onto  $\vec{a}$ .

ii. The vector  $\vec{v}$  can also be determined by minimizing the length of the error vector, represented as

$$\bigcirc \quad \vec{v} = \underset{\vec{v}}{\operatorname{argmin}} ||\vec{a} - \vec{v}|$$

$$\bigcirc \quad \vec{v} = \underset{\vec{b}}{\operatorname{argmin}} \|\vec{b} - \vec{v}\|$$

$$\bigcirc \quad \vec{v} = \underset{\vec{v}}{\operatorname{argmin}} ||\vec{b} - \vec{v}||$$

## **Solution:**

$$\vec{v} = \mathop{\rm argmin}_{\vec{v}} \|\vec{b} - \vec{v}\|$$

In the least squares problem, we minimize the length of the error vector,  $\vec{e}$ , defined as the difference between the known vector  $\vec{b}$  and the span of possible vectors  $\vec{a}x = \vec{v}$ . Thus the error vector is  $\vec{e} = \vec{b} - \vec{v}$ . And the vector  $\vec{v}$  is the minimization argument.

(b) For the following systems of  $A\vec{x} = \vec{b}$ , determine if they have a unique least squares solution.

i. 
$$A = \begin{bmatrix} 1 & 1 \\ 3 & 4 \\ 0 & 0 \end{bmatrix}, \quad \vec{b} = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$

- O Yes
- $\bigcirc$  No

#### **Solution:**

Yes. There is a unique least squares solution since A has linearly independent columns.

ii. 
$$A = \begin{bmatrix} 1 & 4 \\ 3 & 12 \\ 2 & 8 \end{bmatrix}, \quad \vec{b} = \begin{bmatrix} 2 \\ 5 \\ 6 \end{bmatrix}$$

- O Yes
- O No

## **Solution:**

No. There is not a unique least squares solution as *A* does not have linearly independent columns.

- (c) For the following three questions, consider the system of  $A\vec{x} = \vec{b}$  with  $A = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 0 \end{bmatrix}$  and  $\vec{b} = \begin{bmatrix} 3 \\ 5 \end{bmatrix}$ 
  - i. Can we apply the least squares formula?

O Yes

O No

## **Solution:**

No. The fat matrix A does not have linearly independent columns. Additionally,  $A^{T}A$  is not invertible since its determinant is zero.

ii. What is the determinant of  $A^TA$ ?

$$\det(A^T A) =$$

**Solution:** 

$$A^{T}A = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 0 \\ 1 & 0 & 1 \end{bmatrix}$$
$$\det(A^{T}A) = \det\begin{pmatrix} \begin{bmatrix} 1 & 0 & 1 \\ 0 & 1 & 0 \\ 1 & 0 & 1 \end{bmatrix} \end{pmatrix} = 0$$

The zero determinant can be inspected since  $A^TA$  is not invertible (i.e., not full column rank, not linearly independent columns).

iii. (1 point) Does  $A\vec{x} = \vec{b}$  have zero, one, or more than one solution for  $\vec{x}$ ?

No solutions

One unique solution

More than one solution

#### **Solution:**

More than one solution. There are less equations (rows) than unknowns (columns).

(d) Find the best approximation  $x = \hat{x}$  to this system of equations:

$$a_1x = b_1$$
$$a_2x = b_2$$

i. Write the problem into  $A\vec{x} \approx \vec{b}$  format and solve for  $\hat{x}$  using least squares. Choose the correct  $\hat{x}$ .

$$\bigcirc \hat{x} = \frac{a_1b_1 + a_2b_2}{a_1^2 + a_2^2}$$

$$\bigcirc \hat{x} = \frac{a_1b_1 - a_2b_2}{a_1^2 + a_2^2}$$

$$\bigcirc \hat{x} = \frac{a_1b_2 + a_2b_1}{a_1^2 + a_2^2}$$

$$\bigcirc \hat{x} = \frac{a_1b_2 - a_2b_1}{a_1^2 + a_2^2}$$

O None of the above

**Solution:** 

$$Ax = \vec{b} \rightarrow \begin{bmatrix} a_1 \\ a_2 \end{bmatrix} x = \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$$

$$\hat{x} = (A^T A)^{-1} A^T \vec{b} = (\begin{bmatrix} a_1 & a_2 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \end{bmatrix})^{-1} \begin{bmatrix} a_1 & a_2 \end{bmatrix} \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$$

$$= \frac{a_1 b_1 + a_2 b_2}{a_1^2 + a_2^2}$$

ii. Suppose the inner product is defined instead as a non-Euclidean  $\langle x, y \rangle = x^T \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix} y$ . Which of the following expressions must be true with respect to the minimized least squares error vector,  $\vec{e}$ ?

$$\bigcirc \quad \vec{\hat{e}}^T A = \vec{0}$$

$$\bigcirc A^T \vec{\hat{e}} = \vec{0}$$

$$\bigcirc A^T \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix} \vec{\hat{e}} = \vec{0}$$

$$\bigcirc \left( A^T \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix} A \right)^{-1} \vec{\hat{e}} = \vec{0}$$

O None of the above

#### **Solution:**

The least squares error,  $\vec{e}$ , is minimized when it is orthogonal to every column of A (i.e., colspace(A)). Orthogonality occurs when the inner product (in this case the non-Euclidean inner product) of two vectors is zero.

Mathematically,  $\langle \vec{a}_i, \vec{e} \rangle = 0$  for every column  $\vec{a}_i$  of A. Thus,  $A^T \begin{bmatrix} 2 & 0 \\ 0 & 1 \end{bmatrix} \vec{e} = \vec{0}$ .