

**NANYANG
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SINGAPORE
Xu Yan (NTU)

Temporal-Spatial Coordination of Distributed Energy Resources (DERs) in Microgrids

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Cham Tao Soon Professor in Engineering
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Nanyang Technological University

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

4. Hierarchy coordination

5. Trading

- 1) Centralized trading
- 2) P2P trading

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm

1

REIDS (Renewable Energy Integration Demonstrator – Singapore) Microgrid Demonstration Project

2

DER Control

- Islanded microgrid
- Grid-connected microgrid

Timescale

ms ~ seconds

3

DER Operation

- Energy dispatch
- Volt/Var regulation
- Volt/Var control
- Active power balancing

mins ~ hours

4

Hierarchy Coordination

- Centralized trading
- P2P trading

ms ~ hours

5

DER Energy Trading

- Distributed generation
- Energy storage systems

mins ~ hours

6

DER Planning

years ~ decades

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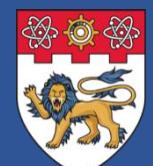
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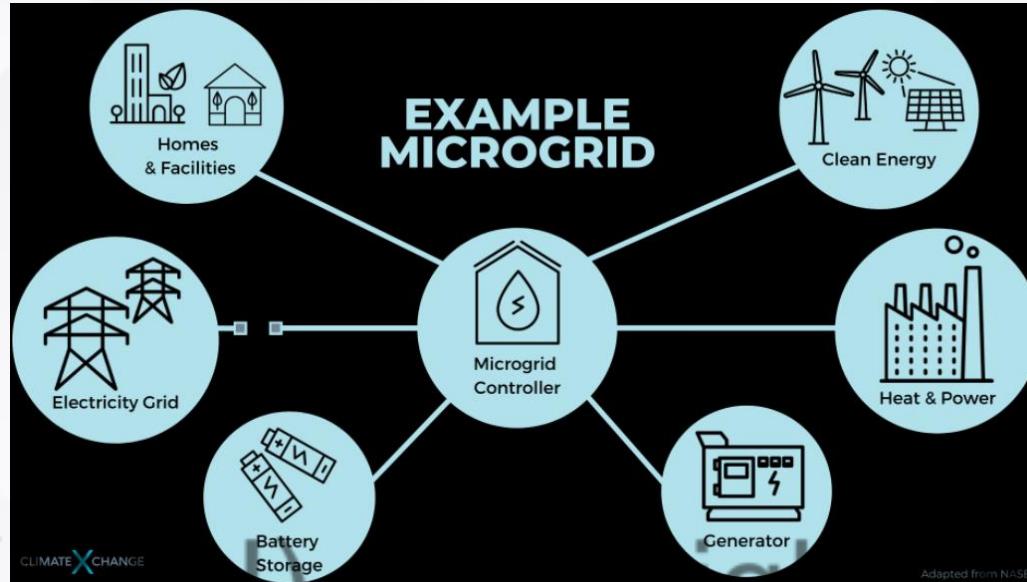
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■ Microgrid Definitions



Picture source: World Economic Forum

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1. The U.S. Department of Energy (DOE) defines a microgrid as '*a group of interconnected loads and DERs within clearly defined electrical boundaries that acts as a single controllable entity with respect to the main grid. A microgrid can connect and disconnect from the main grid to enable it to operate in both connected or island-mode*'.
2. The CIGRE C6.22 Working Group defines that '*Microgrids are electricity distribution systems containing loads and DERs, (such as distributed generators, storage devices, or controllable loads) that can be operated in a controlled, coordinated way either while connected to the main power network or while islanded*'.
3. N. Hatziargyriou, Microgrids: Architectures and Control, UK: Wiley-IEEE Press, 2014, ISBN: 978-1-118-72068-4. describes the microgrid as '*comprising low-voltage (LV) distribution systems with DERs. Such systems can operate either connected or disconnected from the main grid. The operation of DERs in the network can provide benefits to the overall system performance, if managed and coordinated efficiently*'.

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▪ *Renewable Energy Integration Demonstrator – Singapore (REIDS)*



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Energy Research Institute @ NTU

REIDS

Renewable Energy Integration Demonstrator - Singapore

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REIDS is a Singapore-based RD&D platform

dedicated to designing, demonstrating and testing solutions
for sustainable multi-activity off-grid communities in Southeast Asia

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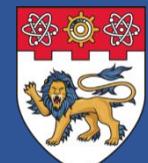
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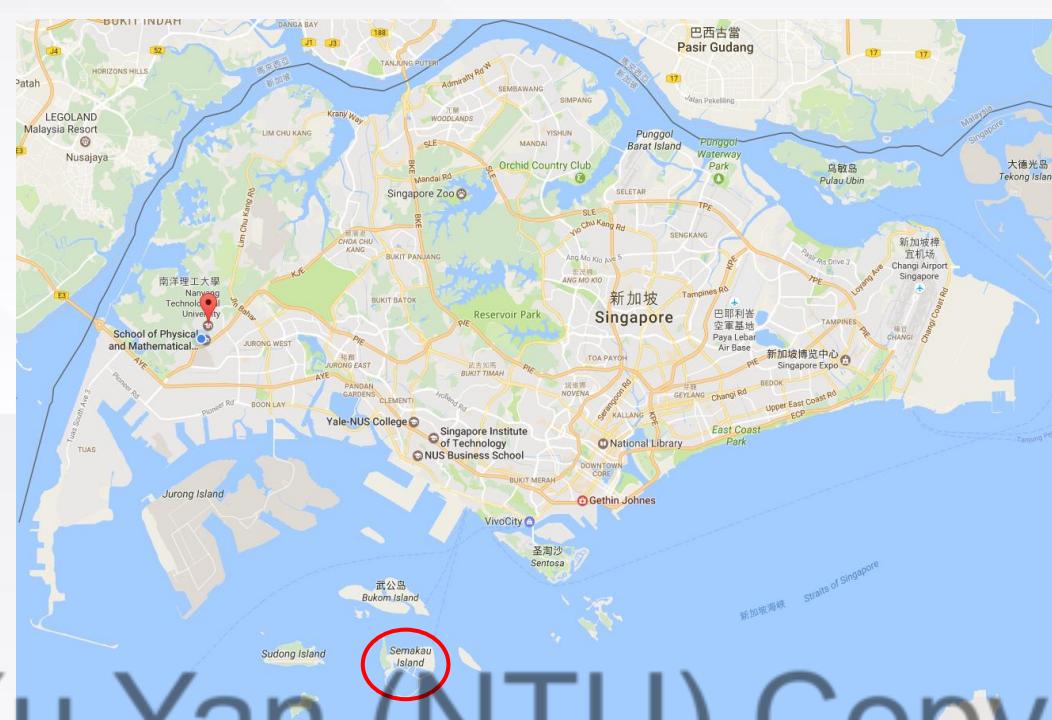
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REIDS Partners

accenture

adaro
POWER



ClassNK



edf



Research Leader



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engie

Evolution
Energie



IDSUD
ENERGIES

Keppel Offshore & Marine



Supporting Agencies

edb
singapore

National
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Agency
Safeguard • Nurture • Cherish

MERALCO

muRata
INNOVATOR IN ELECTRONICS

NORTIS ENERGY

REC

Rolls-Royce

Schneider
Electric

ENERGY
MARKET
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Smart Energy, Sustainable Future

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RESEARCH
FOUNDATION

SEAS
Sustainable Energy Association of Singapore

sembcorp

SPgroup

TrinaSolar

VDE
RENEWABLES

Vestas



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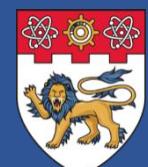
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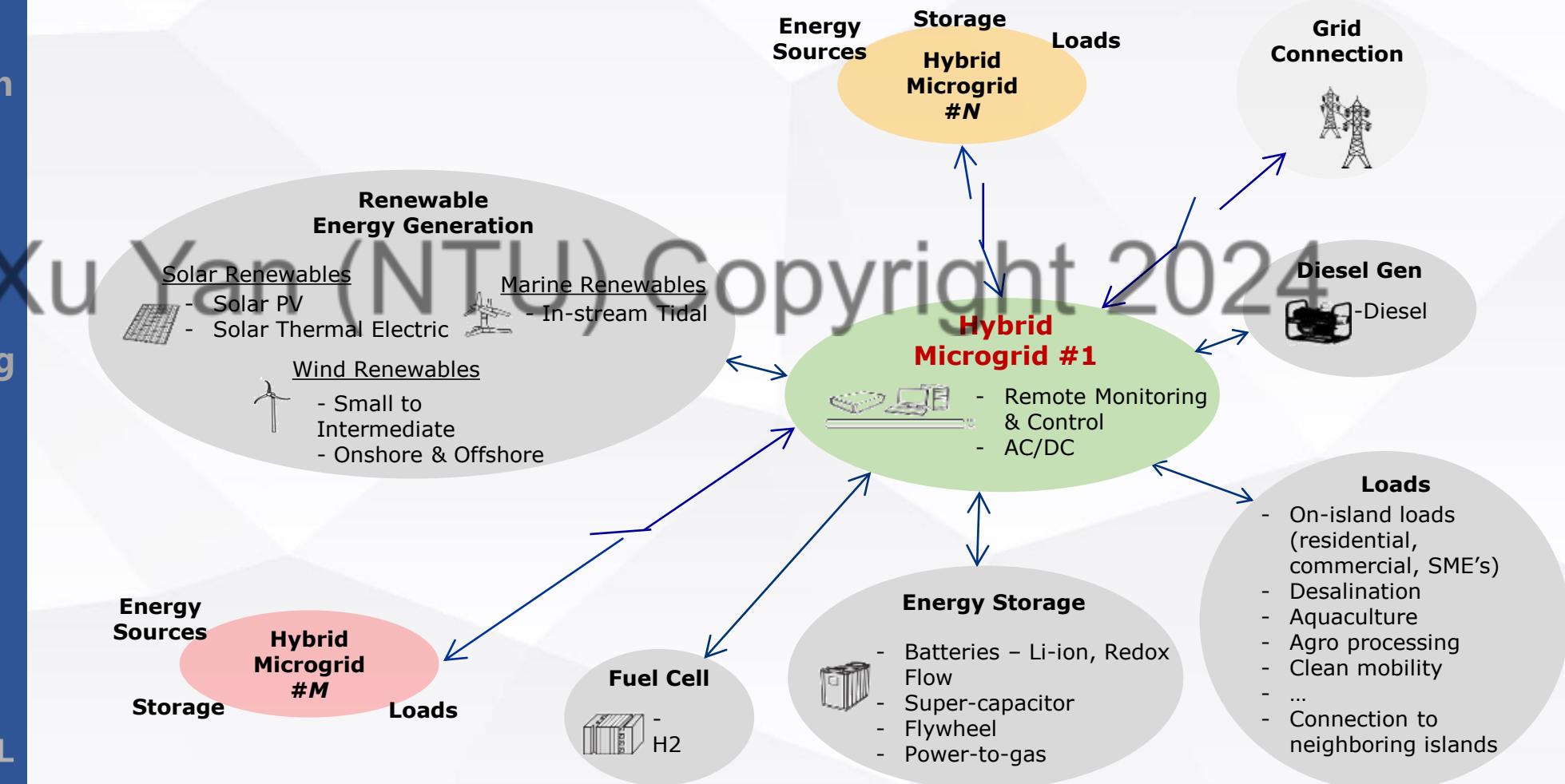
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■ REIDS Roadmap and Framework

Phase I – 4 independent MGs (500kW-1MW each)

Phase II – 4 MGs in a cluster configuration (100kW-250kW each)



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■ Onboard Industry Collaborators

1 Renewables:

Solar, Wind (onshore /offshore) & Tidal



2 Energy Storage/H₂

Batteries, Supercaps, CAES, Flywheels, Power-to-fuels and H₂



3 DERs:

Diesel, Bio-mass, Bio-fuels, Fuel Cells



4 Multi-microgrid Systems:

Interconnection, Urban Mesogrids, Blockchain Energy Trading, Resilience And Security



5 VOI:

Visualization, Optimization AI, Energy/Power Management Platforms



6 Microgrid Controller:

SW, HW, AC-DC Hybrid Grids, DERMS, SST & Power Electronics



7 DACS:

Data Analytics & Control Systems



8 Techno-enviro-socio Impact:

Techno-socio Economics, EIA, Certification



9 Rational End-use:

Utilities, Urban Residential, Industrial, Agri Loads, Desalination & EVs



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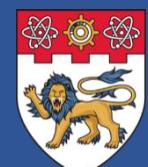
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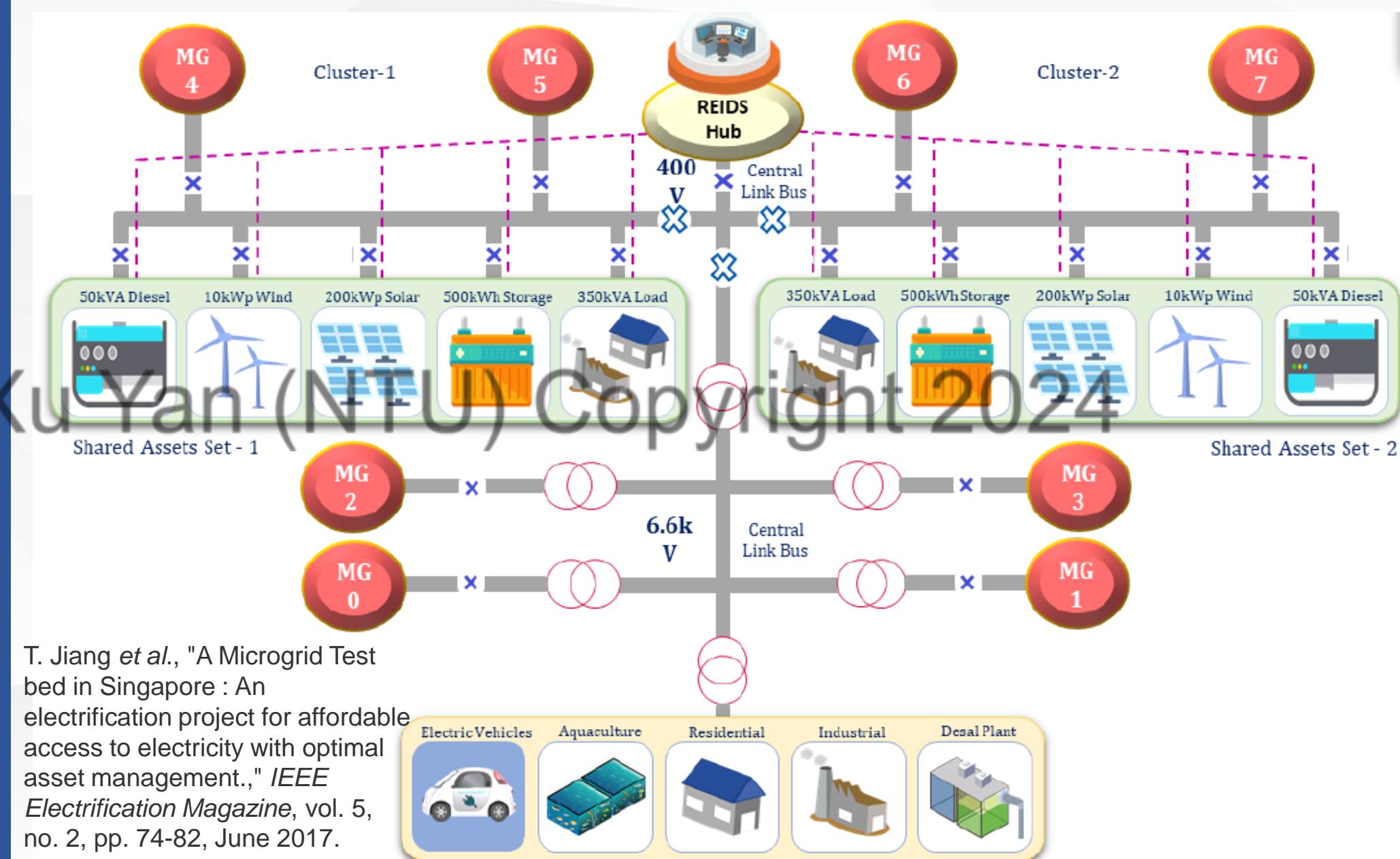
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REIDS Electrical Structure



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▪ Renewable Energy Integration Demonstrator – Singapore (REIDS)

REIDS

Renewable Energy Integration Demonstrator – Singapore

An ERI@N Flagship Project

X

Interoperable
Grid of Grids
Testbed

Prasanna I V, prasannaiv@ntu.edu.sg

Research Leader



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Supporting Agencies



National
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Smart Energy, Sustainable Future

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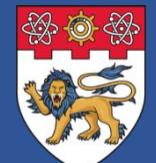
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Onsite pictures



REIDS
Renewable
Energy
Integration
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Singapore



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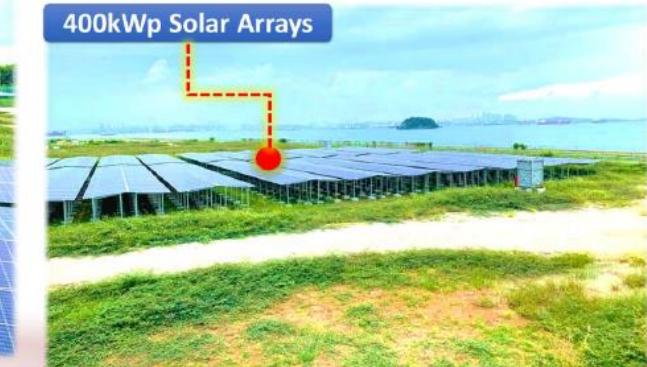
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Onsite pictures

70kW Hydrogen



200kWh Li-Ion LFP
Murata



250kWh Li-Ion LFP
Samsung



180kWh Li-Ion NMC
Durapower 2nd life EV



140kWh Lead Acid



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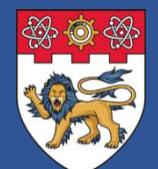
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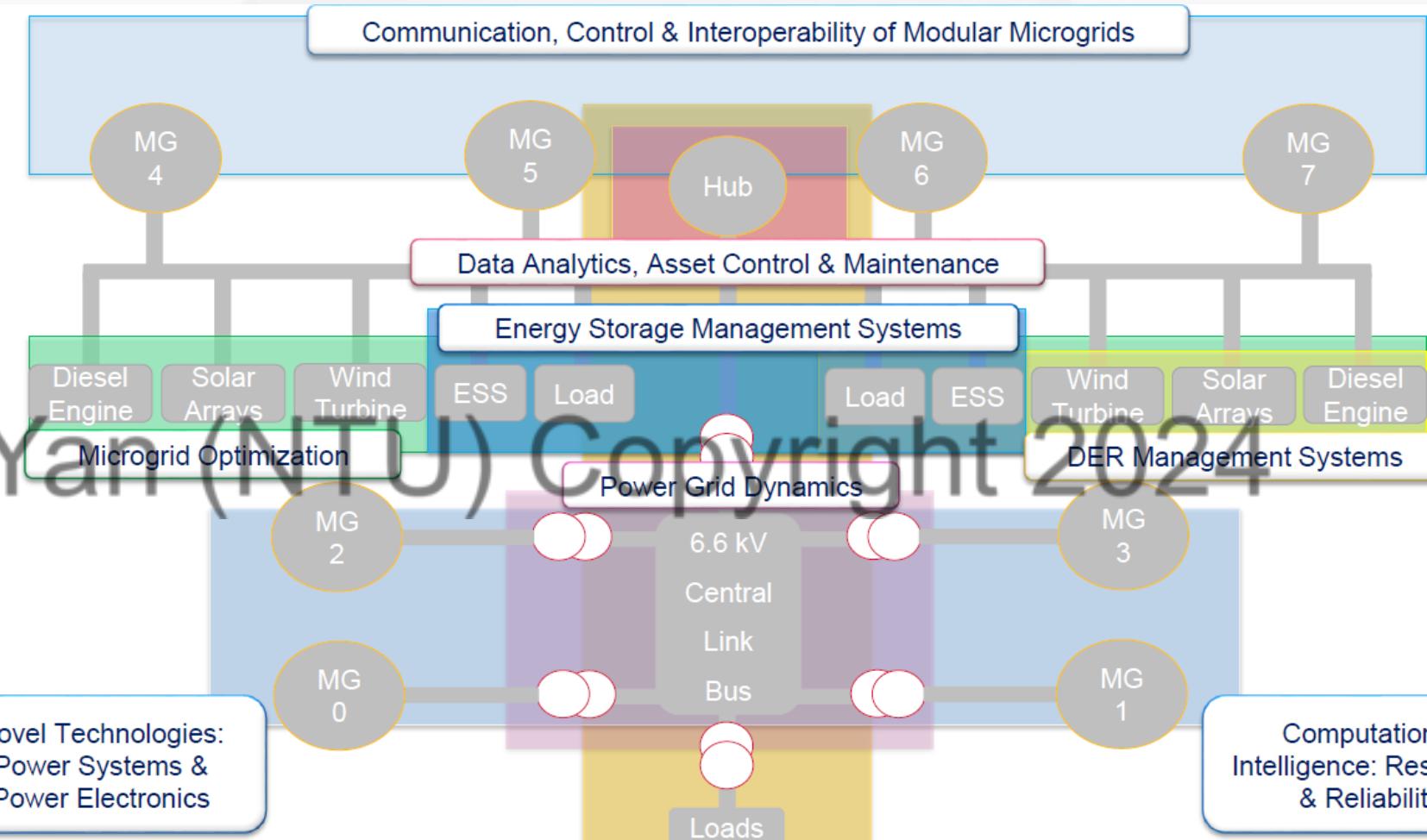
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REIDS Research Problems



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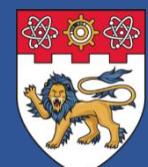
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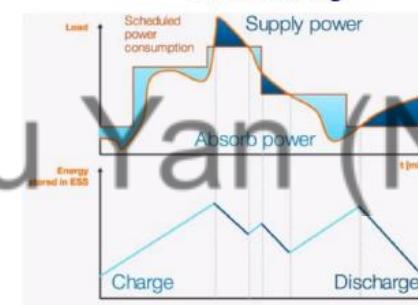
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REIDS Research Problems

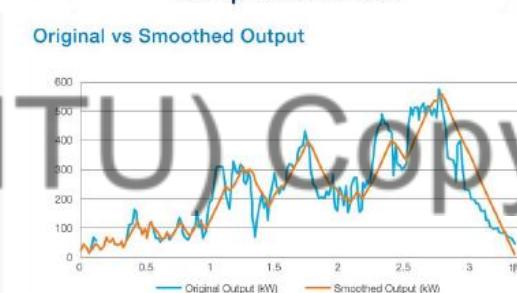
Grid Ancillary Services



Peak Shaving



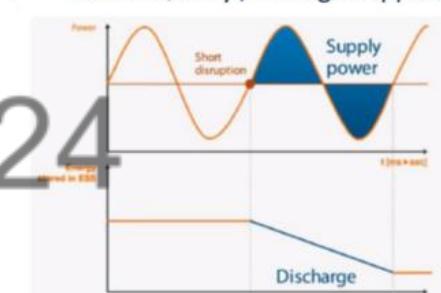
Ramp Rate Control



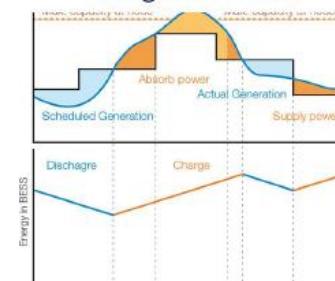
Load Levelling



Power Quality / Voltage Support



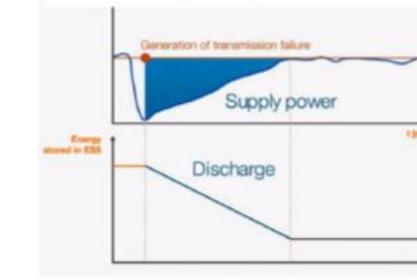
Congestion Relief



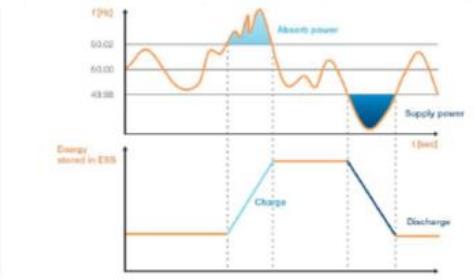
Capacity Firming



Spinning Reserve



Frequency Regulation



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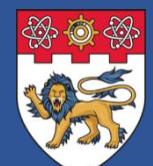
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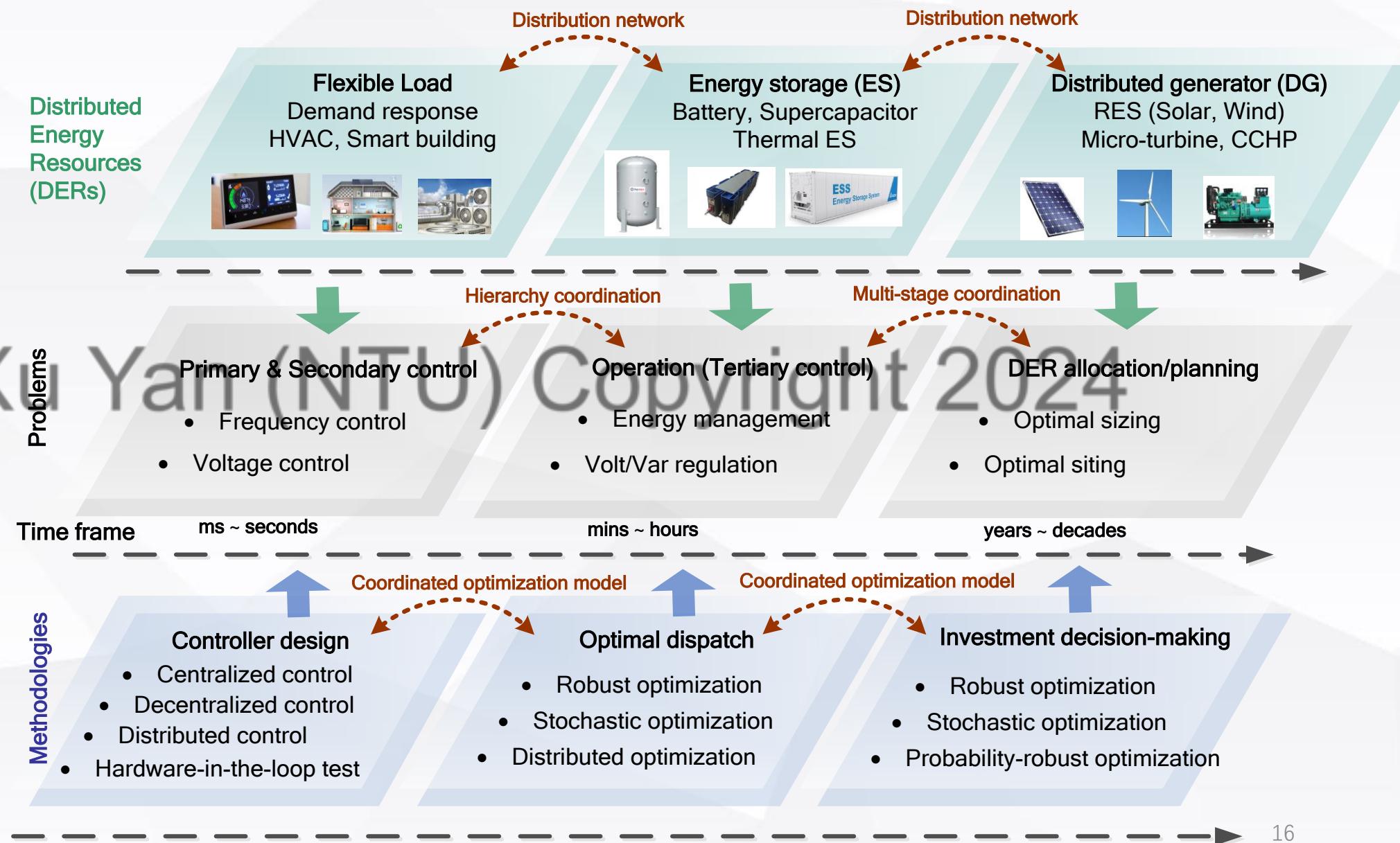
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Our research Framework: system-level coordination of DERs



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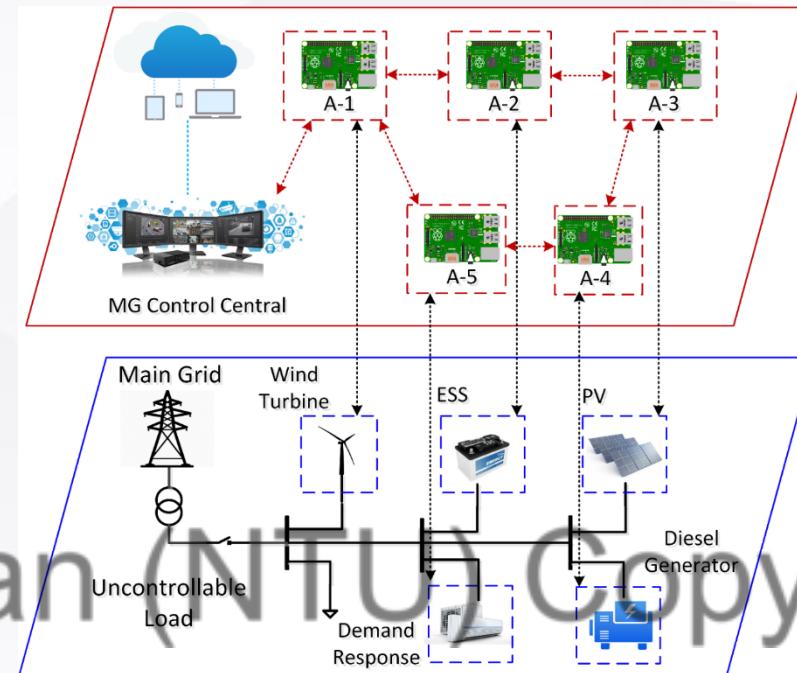
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Control of DERs in Microgrids

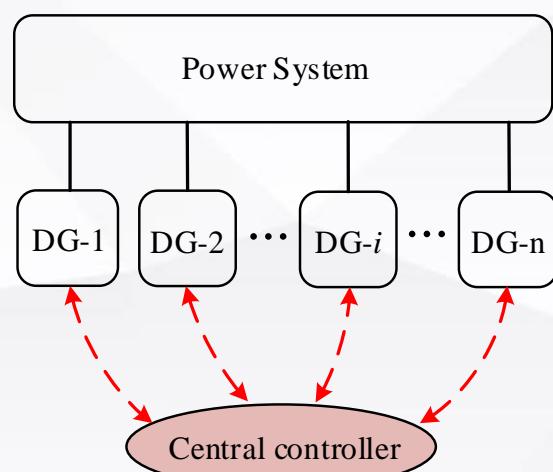


1. Islanded mode:

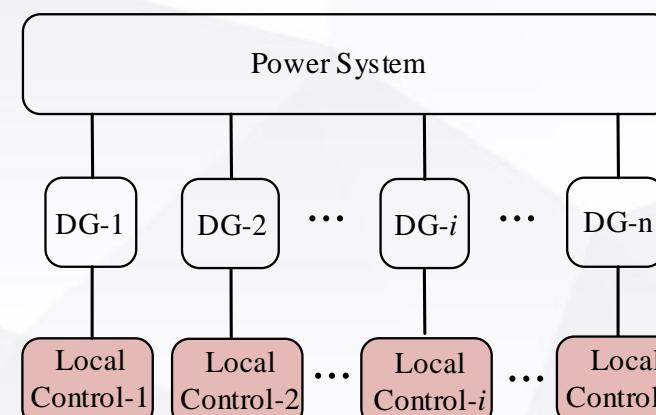
- Distributed control (event-triggered, finite-time)
- Hardware-in-the-Loop (Hil) validation

2. Grid-connected mode:

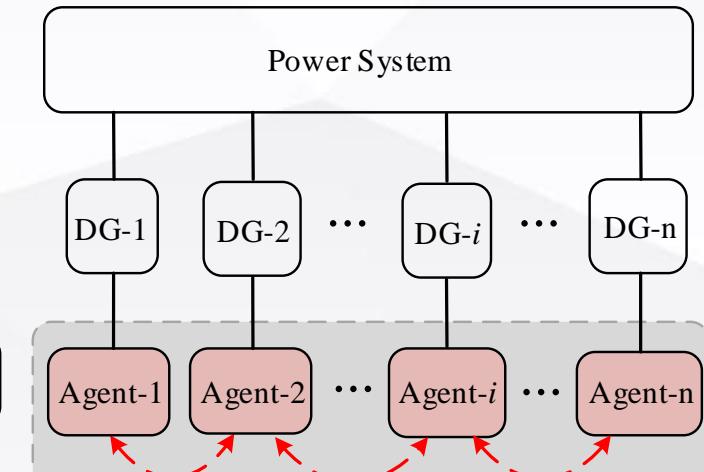
- DER for f support
- DER for V support



(a) Centralized control



(b) Decentralized control



(c) Distributed control

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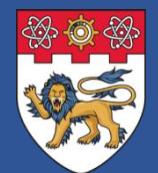
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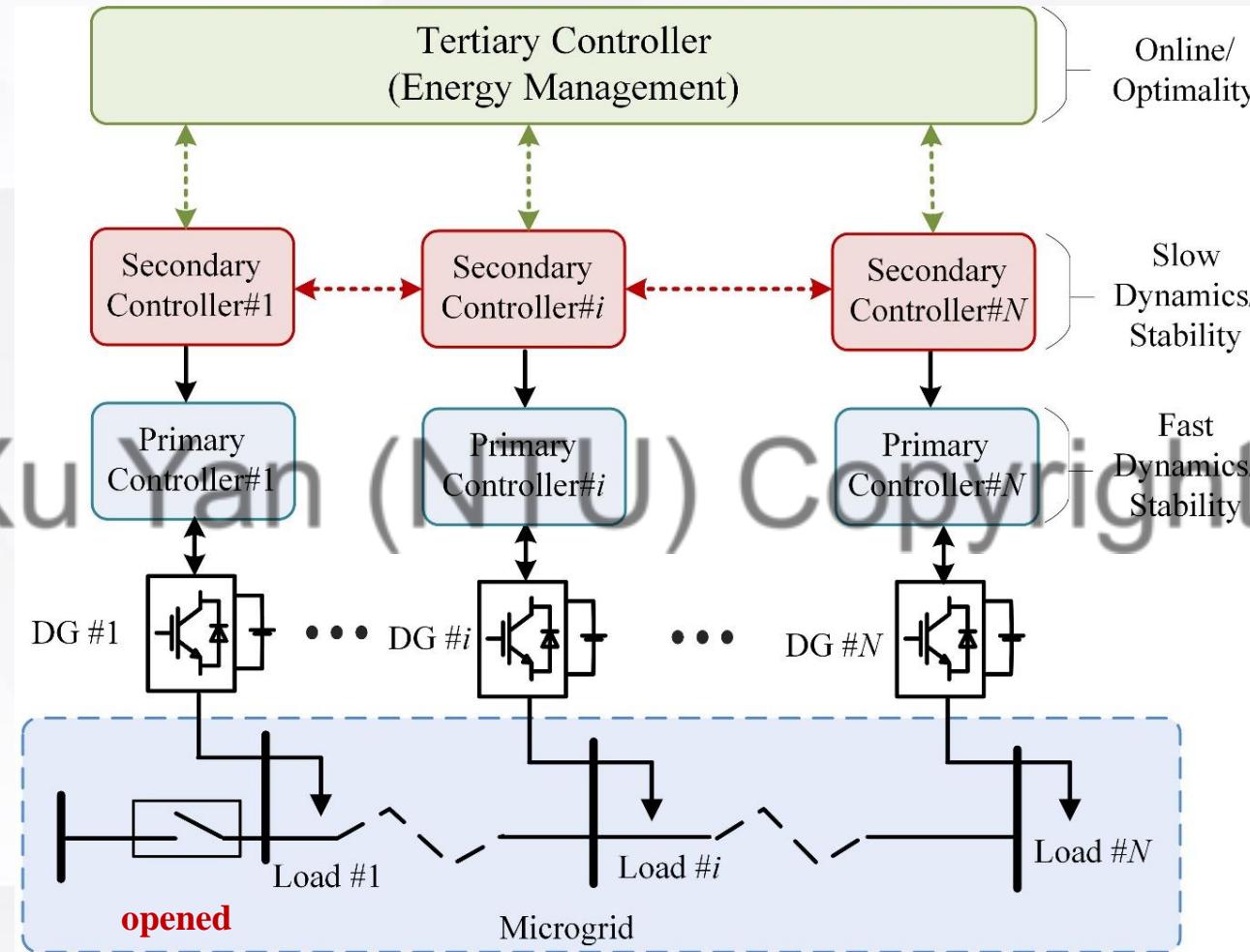
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Hierarchical control of an islanded microgrid



Hierarchical control framework of islanded microgrids

- **Tertiary control (centralized or distributed)**
- Economic dispatch, optimal power flow.
- **Secondary control (centralized or distributed)**
- V/f restoration and accurate power balancing
- **Primary control (decentralized)**
- Inner control loops and droop control
- Local V/f regulation and power sharing

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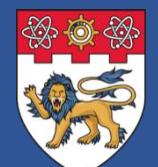
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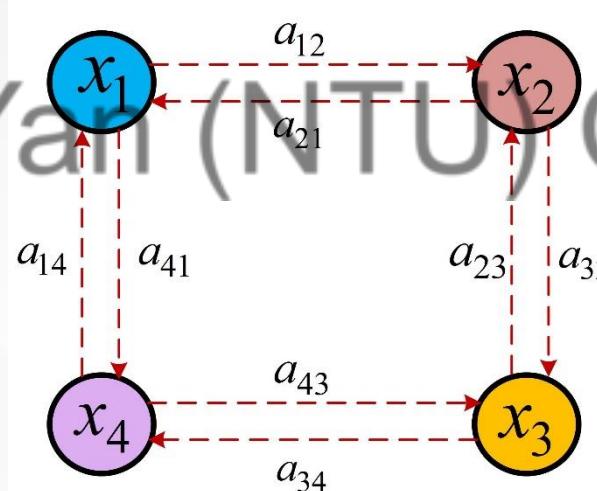
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- Distributed Control – Spatial Coordination of DERs
 - ✓ No need for a central controller
 - ✓ One node only communicates with neighbouring nodes
 - ✓ Share communication and computation burden among nodes
 - ✓ Higher resilience, plug-and-play, scalability, data privacy

Example of communication graph



Adjacent matrix of the graph

$$A = \begin{bmatrix} 0 & a_{12} & 0 & a_{14} \\ a_{21} & 0 & a_{23} & 0 \\ 0 & a_{32} & 0 & a_{34} \\ a_{41} & 0 & a_{43} & 0 \end{bmatrix}$$

a) Average consensus control

$$\dot{x}_i(t) = \sum_{j \in N_i} a_{ij}(x_j(t) - x_i(t))$$

$$\lim_{t \rightarrow \infty} \|x_i(t) - x_j(t)\| = 0$$

b) Leader-follower consensus control

$$\dot{x}_i(t) = \sum_{j=1}^n a_{ij}(x_j(t) - x_i(t)) + g_i(x_0(t) - x_i(t)).$$

$$\lim_{t \rightarrow \infty} \|x_i(t) - x_0(t)\| = 0$$

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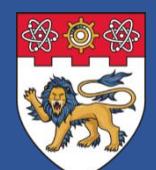
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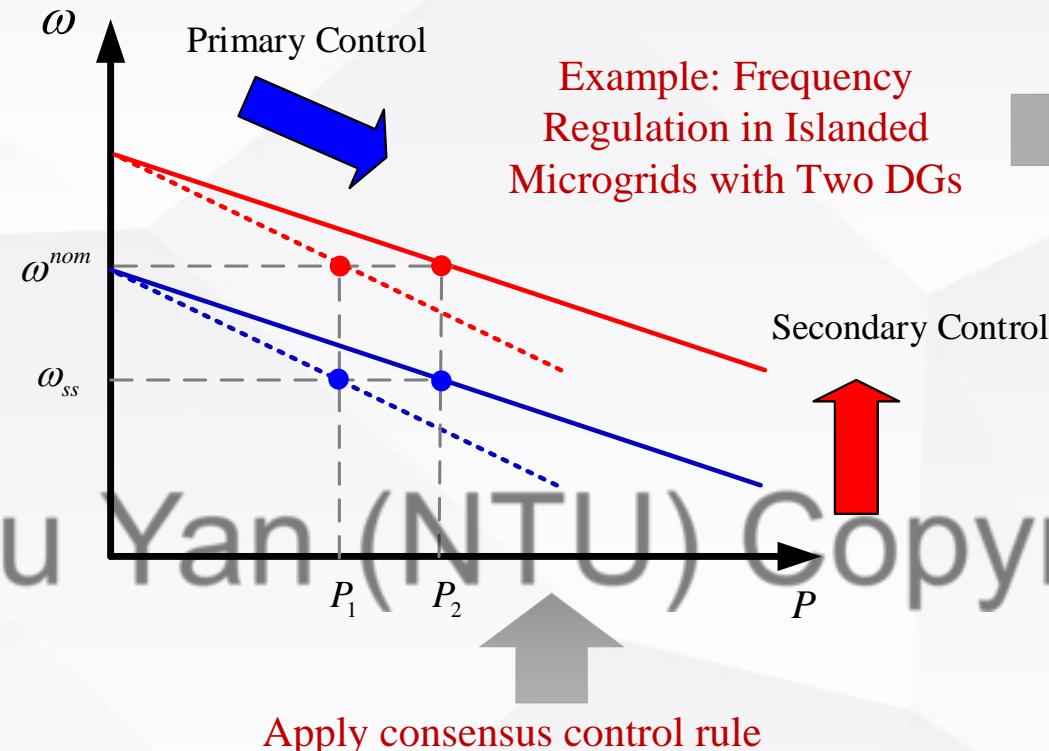
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Secondary Controller Design – Principle



Droop control

$$\omega_i = \omega_i^{\text{nom}} - m_i^P P_i$$

$$V_i = V_i^{\text{nom}} - m_i^Q Q_i$$

Taking Derivative

$$\dot{\omega}_i = \dot{\omega}_i^{\text{nom}} - m_i^P \dot{P}_i$$

$$\dot{V}_i = \dot{V}_i^{\text{nom}} - m_i^Q \dot{Q}_i$$

Problem formulation

$$\omega^{\text{nom}} = \int (\dot{\omega}_i + m_i^P \dot{P}_i) dt = \int (u_i^\omega + u_i^P) dt$$

$$V^{\text{nom}} = \int (\dot{V}_i + m_i^Q \dot{Q}_i) dt = \int (u_i^V + u_i^Q) dt$$

$$\begin{aligned}u_i^\omega &= \sum_{j=1}^N a_{ij}(\omega_j - \omega_i) + g_i(\omega^{\text{ref}} - \omega_i) \\u_i^P &= \sum_{j=1}^N a_{ij}(m_j^P P_j - m_i^P P_i) \\u_i^V &= \sum_{j=1}^N a_{ij}(V_j - V_i) + g_i(V^{\text{ref}} - V_i) \\u_i^Q &= \sum_{j=1}^N a_{ij}(m_j^Q Q_j - m_i^Q Q_i)\end{aligned}$$

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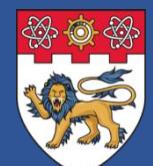
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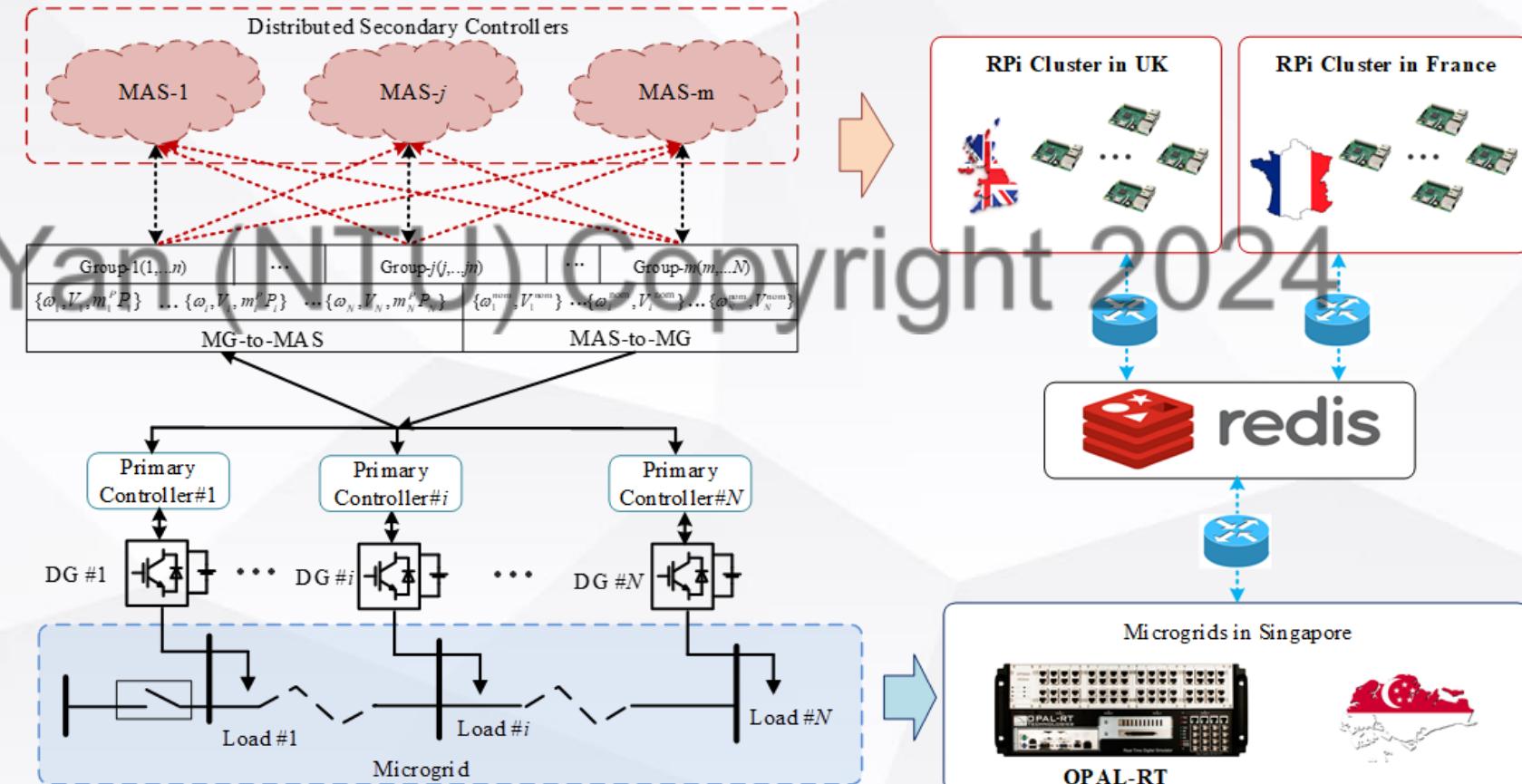


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■ Cross-national hardware-in-the-loop (HiL) testbed

Jointly developed by NTU (Singapore), University of Strathclyde (UK), and G2E Lab (France)

- Microgrids system with OPAL-RT in Singapore.
- Distributed controllers in Raspberry Pi in UK and France.
- Software environment based on gRPC and data exchange via Redis cloud server.



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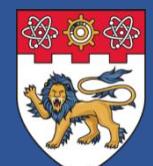
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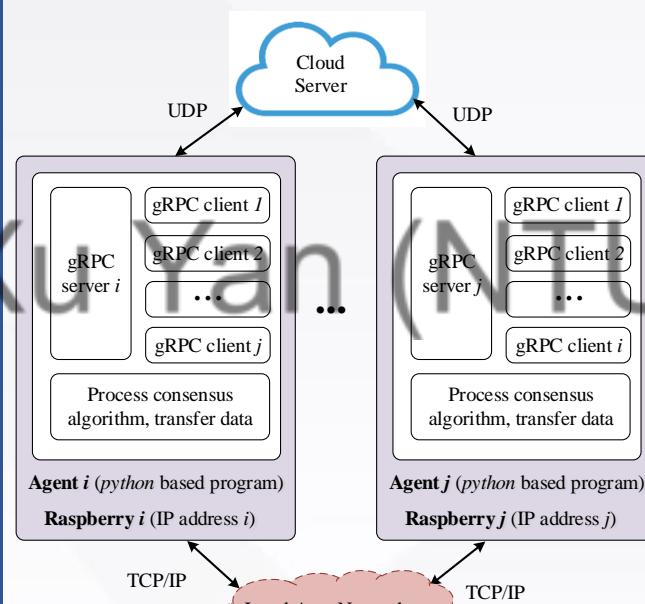
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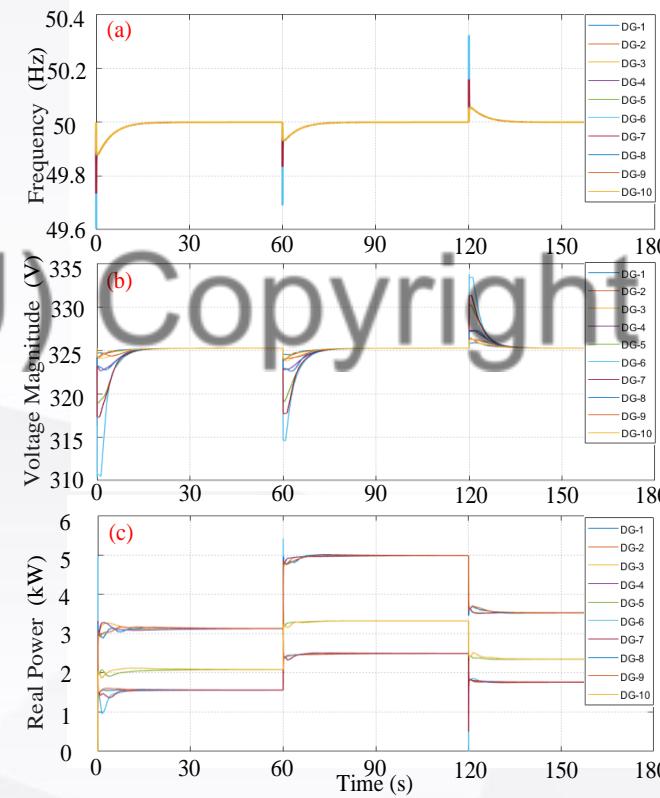
HiL Validation Results – Controller performance

Test system: 10-DG with two controller in UK and France
(Each controller for 5 DGs)

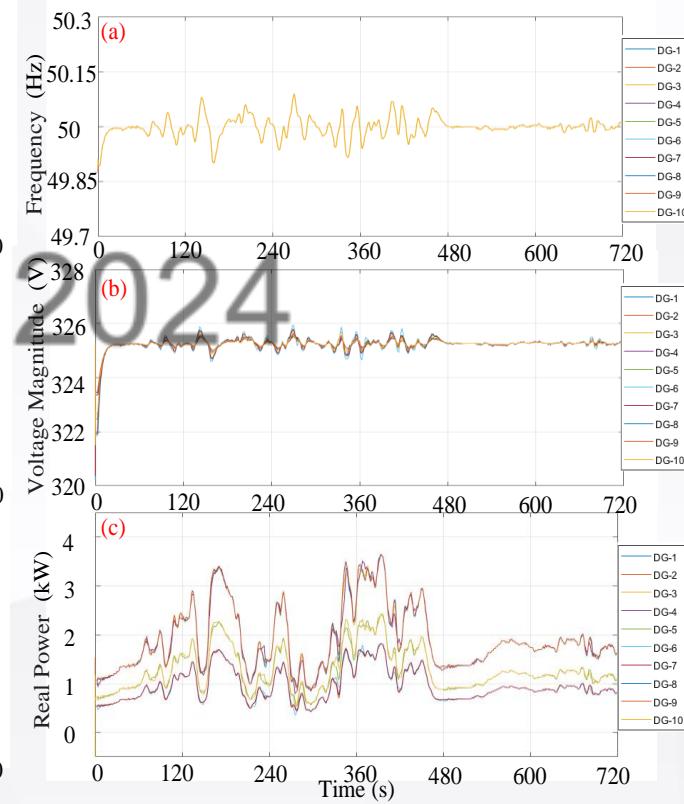
Structure of each agent based on gRPC



a) step load change case



b) Real PV and load profile case



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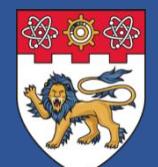
4. Hierarchy coordination

5. Trading

- 1) Centralized trading
- 2) P2P trading

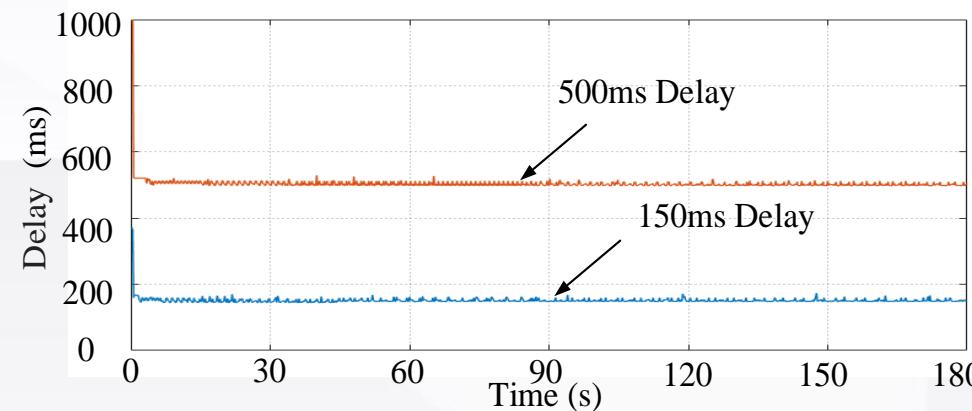
6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm

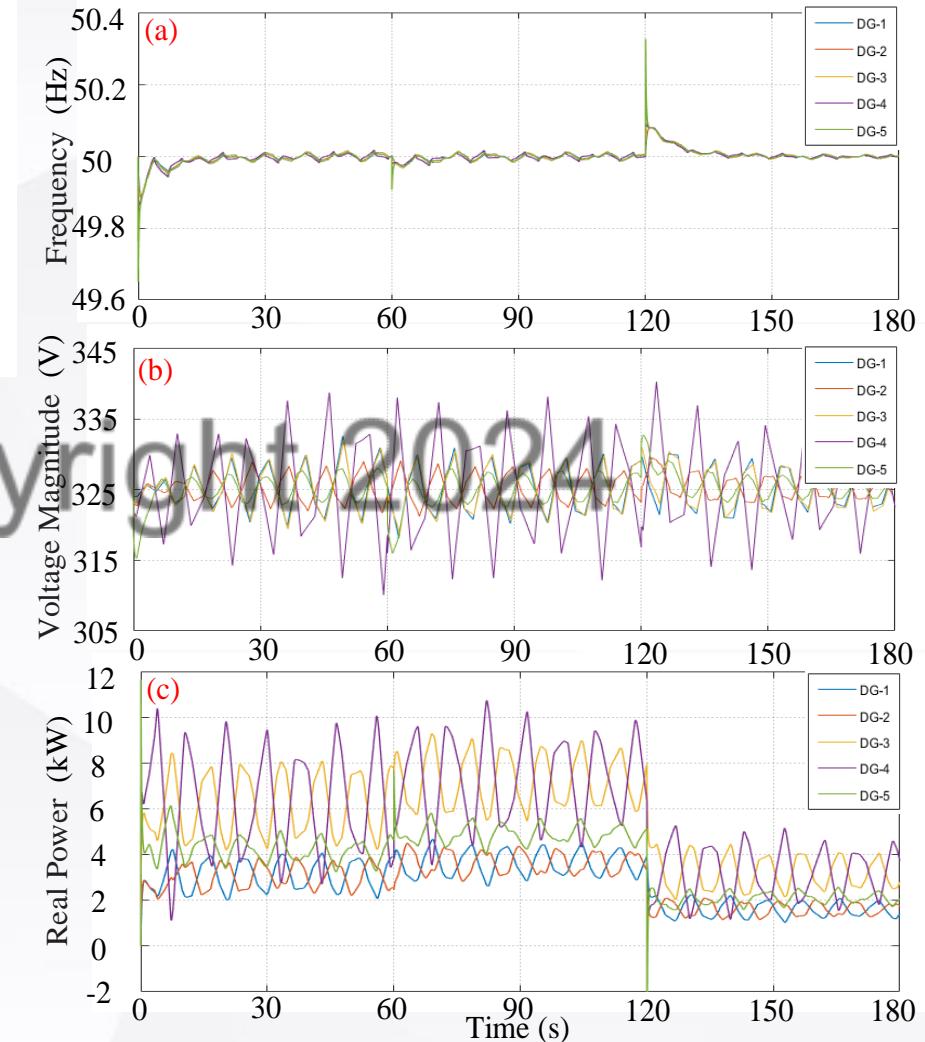


■ HiL Validation Results – Communication delay

Communication delay emulated by NS3 simulation tools.



Test system: 5-DG MG with one MAS in UK



System oscillation under large delay, which can be mitigated by tuning the control gain.

- ✓ Larger control gain -> converge faster
-> withstand smaller delay.
- ✓ Smaller control gain -> converge slower -> withstand larger delay

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- 2) Volt/Var regulation

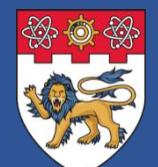
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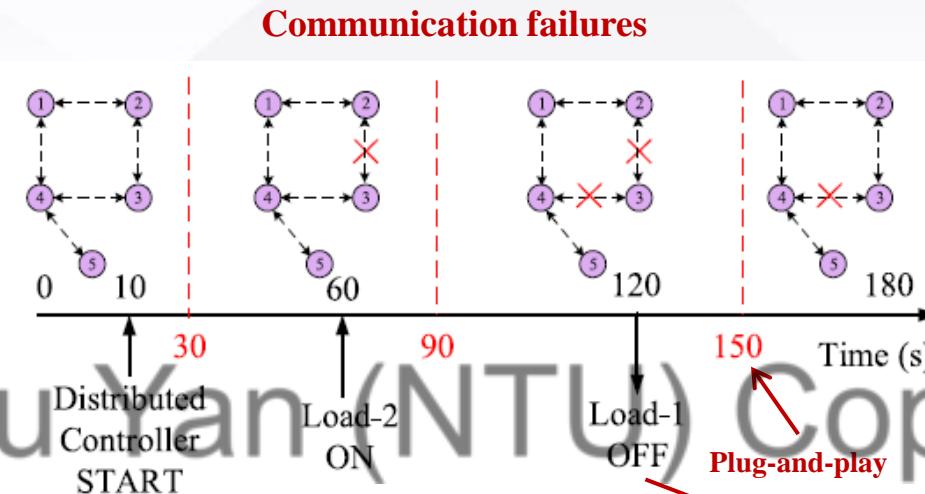
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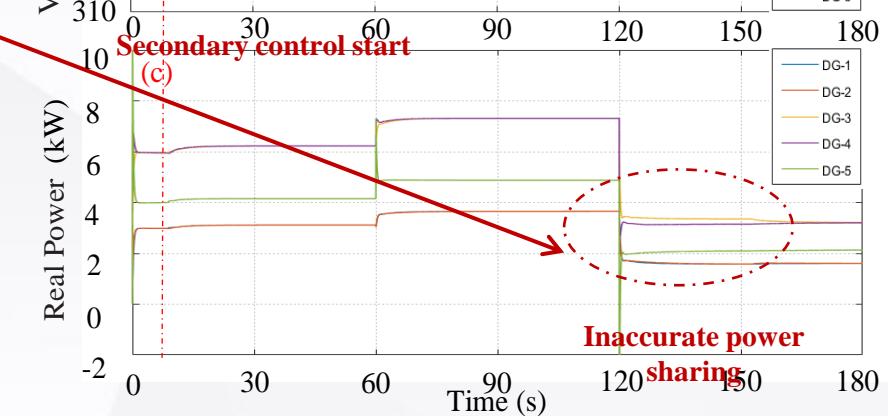
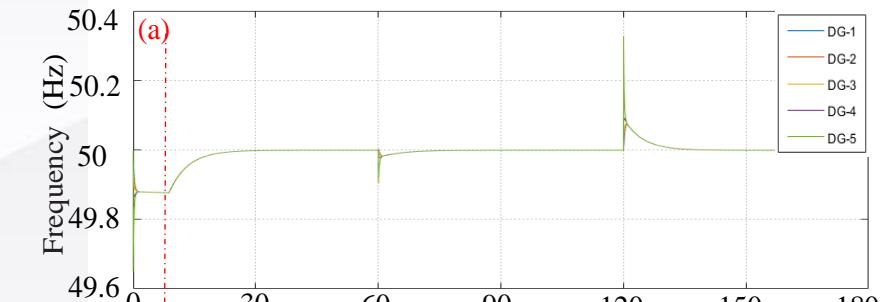
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HiL Validation Results – Communication failures



- ✓ Failure of communication will affect the convergence speed
- ✓ Loss of communication will lead to inaccurate power sharing

Test system: 5-DG MG with one controller in UK



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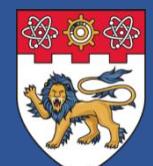
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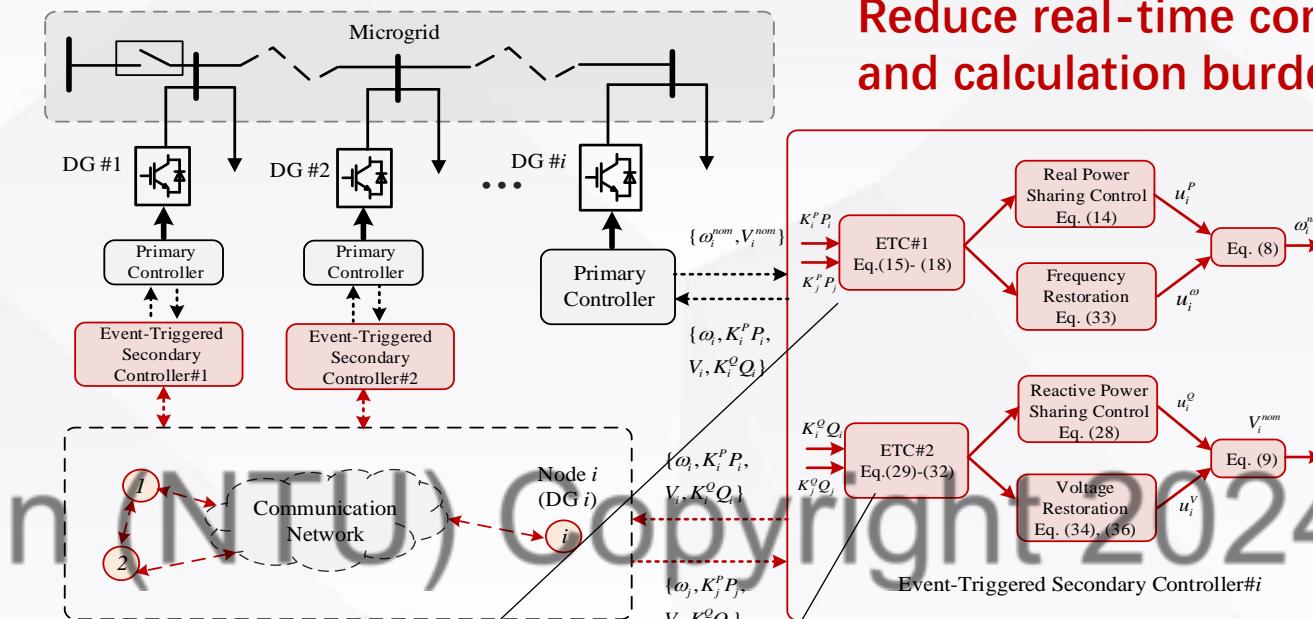
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Event-Triggered Distributed Control of Islanded Microgrids



Reduce real-time communication and calculation burden

Effects of ETC

Event-Trigger Condition for f and P:

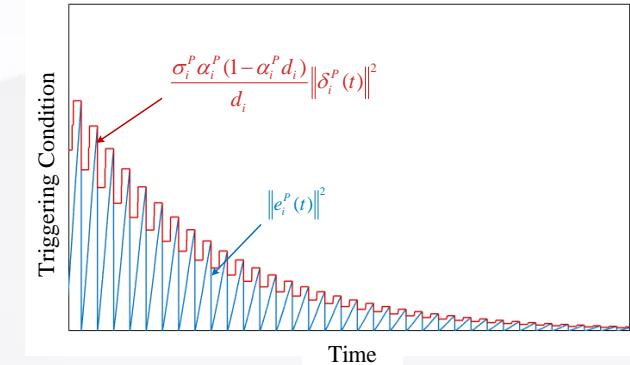
$$f_i^P(t) = \|e_i^P(t)\|^2 - \frac{\sigma_i^P \alpha^P (1 - \alpha^P d_i)}{d_i} \|\delta_i^P(t)\|^2$$

$$t_k^{P_i} = \inf\{t > t_{k-1}^{P_i} \mid f_i^P(t) = 0\}$$

Event-Trigger Condition for V and Q:

$$f_i^Q(t) = \|e_i^Q(t)\|^2 - \frac{\sigma_i^Q \alpha^Q (1 - \alpha^Q d_i)}{d_i} \|\delta_i^Q(t)\|^2$$

$$t_k^{Q_i} = \inf\{t > t_{k-1}^{Q_i} \mid f_i^Q(t) = 0\}$$



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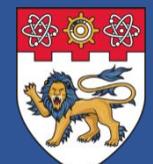
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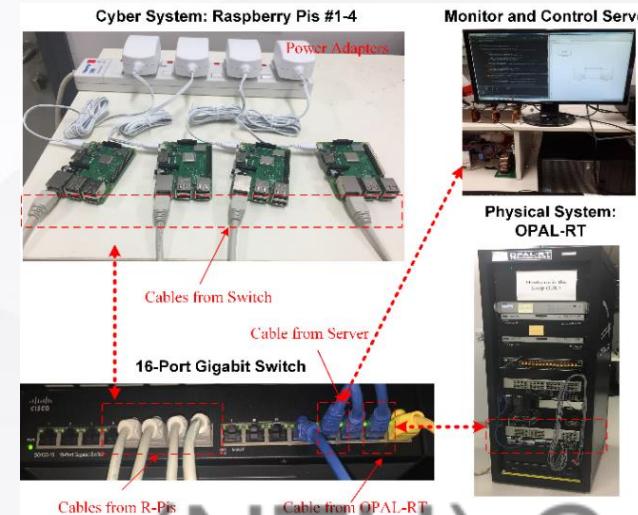
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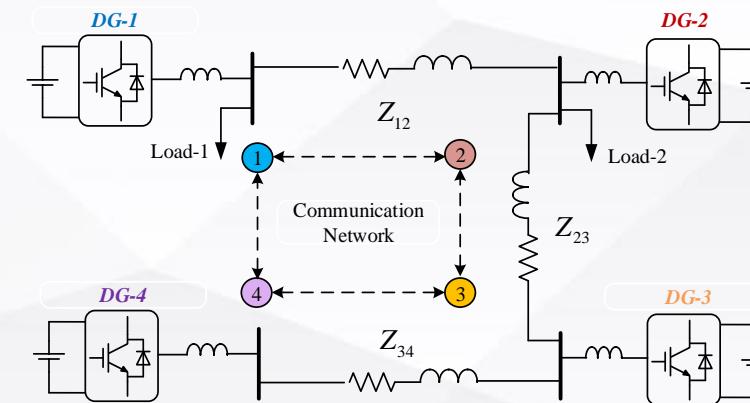
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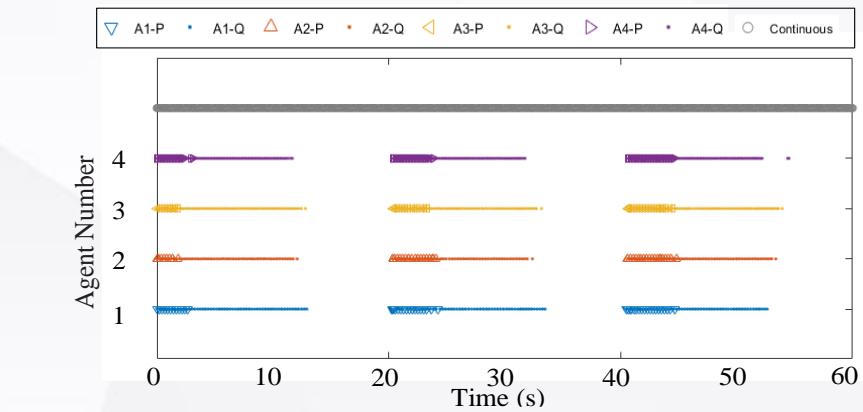
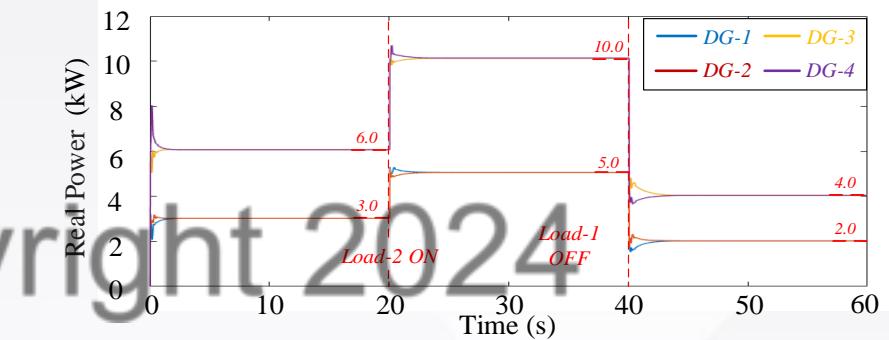
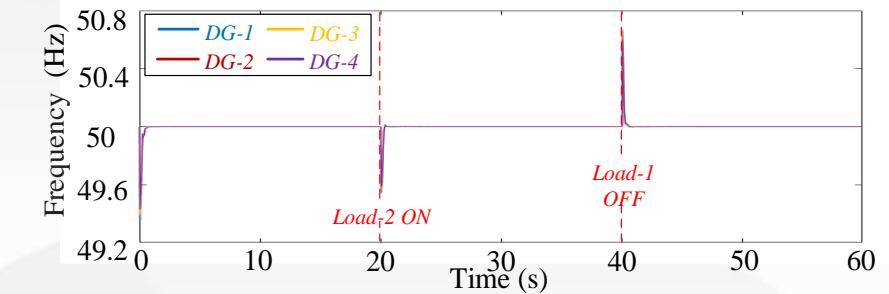
Controller Hardware-in-the-Loop (CHIL) Test



HiL testbed with Raspberry Pi and OPAL-RT



Microgrid topology with four DGs



Communication requirement

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

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- 2) Volt/Var regulation

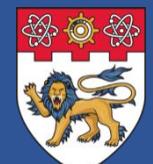
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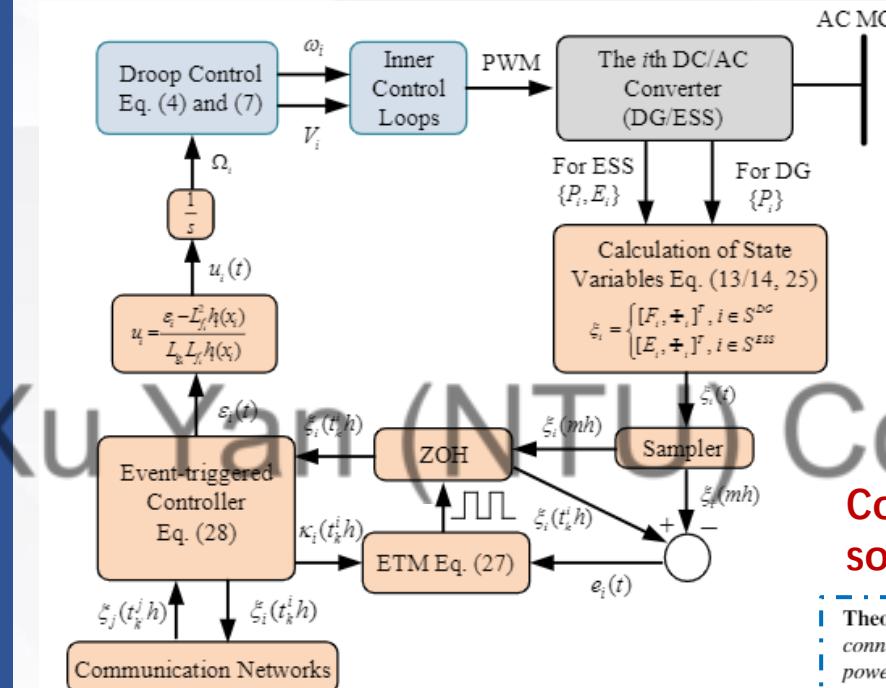
- 1) Centralized trading
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- 3) PRO algorithm



Dynamic Event-Triggered Control of Generators and Storages



Unified Control Framework for DGs and ESSs

System Model with DGs and ESSs

$$\dot{F}_i(t) = \Phi_i(t), i \in S^{DG}$$

$$\dot{\xi}_i(t) = \begin{cases} [F_i(t) \Phi_i(t) \Gamma_i(t)]^T, & i \in S^{DG}, \\ [E_i(t) \Phi_i(t) \Gamma_i(t)]^T, & i \in S^{ESS}. \end{cases}$$

$$\dot{\xi}_i(t) = A\xi_i(t) + B\varepsilon_i(t)$$

$$A = [0 \ 1 \ 0; 0 \ 0 \ 1; 0 \ 0 \ 0]$$

Event-Triggered Controller Design

$$\varepsilon_i(t) = K \sum_{j=1}^N a_{ij} [\xi_i(t_k^i h) - \xi_j(t_{k'}^j h)]$$

Control gain K design by solving LMI

Theorem 1. Assume that the communication graph \mathcal{G} is connected. For given γ , δ and h , the proportional active power sharing and energy balancing problems (20) and (21) are solved asymptotically by the distributed event-triggered controller (30) with event-triggered mechanism (28) if there exist matrices $Q > 0$, $P > 0$, $R > 0$, $\Sigma > 0$, K and S such that $\begin{bmatrix} R & S \\ S^T & R \end{bmatrix} > 0$ and $\Psi(\lambda_i) < 0$, where

$$\Psi(\lambda_i) = \begin{bmatrix} \Psi_{11} & * & * & * & * \\ \Psi_{21}(\lambda_i) & \Psi_{22}(\lambda_i) & * & * & * \\ S^T & \Psi_{32} & \Psi_{33} & * & * \\ \lambda_i K^T B^T P & \delta \lambda_i \Sigma & 0 & \Psi_{44}(\lambda_i) & * \\ \gamma PA & \gamma \lambda_i PBK & 0 & \gamma \lambda_i PBK & \Psi_{55} \end{bmatrix}$$

$$t_{k+1}^i h = \inf_{m \in \mathbb{N}} \{mh > t_k^i h | e_i^T(t) \Sigma e_i(t) \geq \delta \kappa_i^T(t_k^i h) \Sigma \kappa_i(t_k^i h) + \nu_i \beta_i(t)\} \quad (28)$$

where $t_0^i = 0$, $e_i(t) = \xi_i(t_k^i h) - \xi_i(mh)$ ($t \in [mh, mh + h)$) and $\kappa_i(t_k^i h) = \sum_{j=1}^N a_{ij} [\xi_i(t_k^i h) - \xi_j(t_{k'}^j h)]$ and $t_{k'}^j = \max_{k \in \mathbb{N}} \{t_k^j | t_k^j h \leq t\}$. The dynamic of $\beta_i(t)$ is given by

$$\dot{\beta}_i(t) = -\beta_i(t) + \kappa_i^T(t_k^i h) W \kappa_i(t_k^i h). \quad (29)$$

The scalar $\delta > 0$ and matrices $\Sigma > 0$ and $W > 0$ will be designed later.

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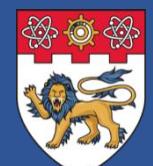
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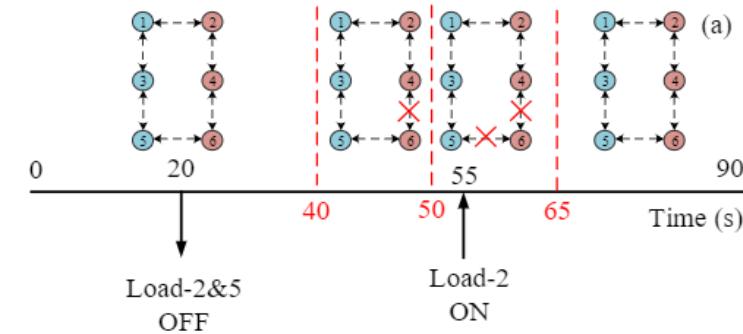
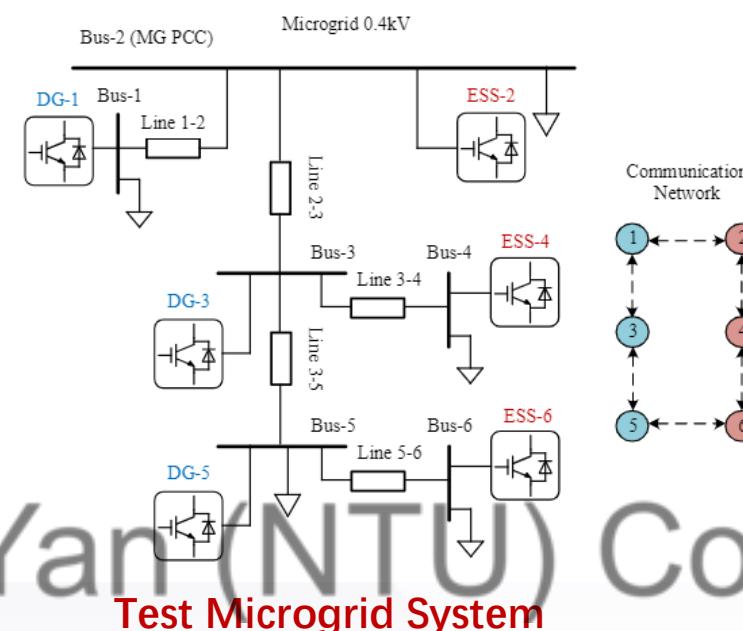
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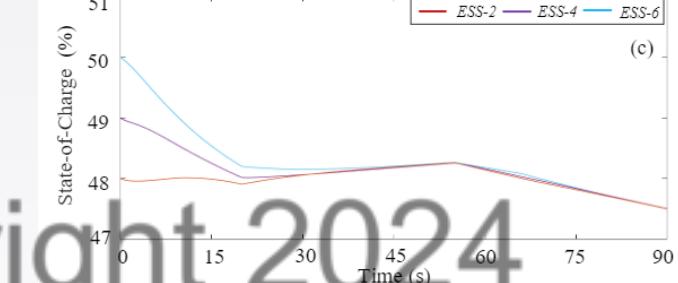
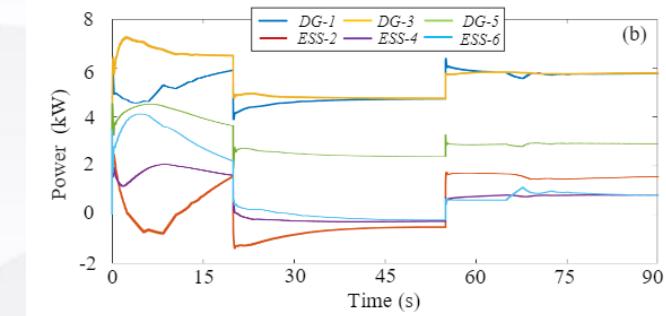


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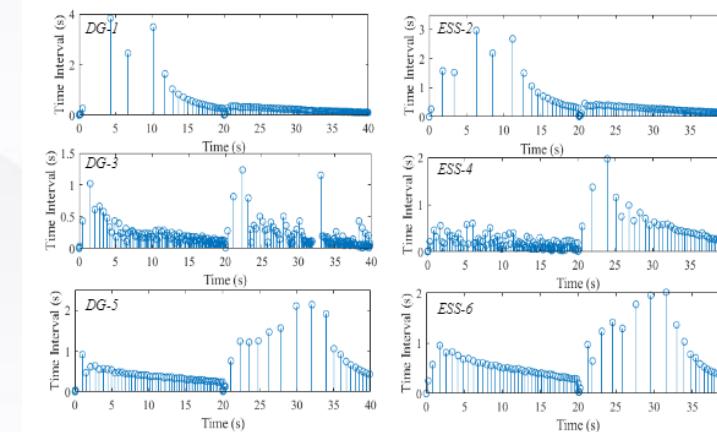
■ Real-time Simulation Test Results



Time sequence of simulation events



Real-Time Test Results



Event-triggered Time Instant

Y. Wang, C. Deng, D. Liu, **Y. Xu***, and J. Dai, "Unified Real Power Sharing of Generator and Storage in Islanded Microgrid via Distributed Dynamic Event-Triggered Control," *IEEE Trans. Power Syst.*, 2021.

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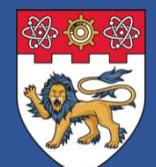
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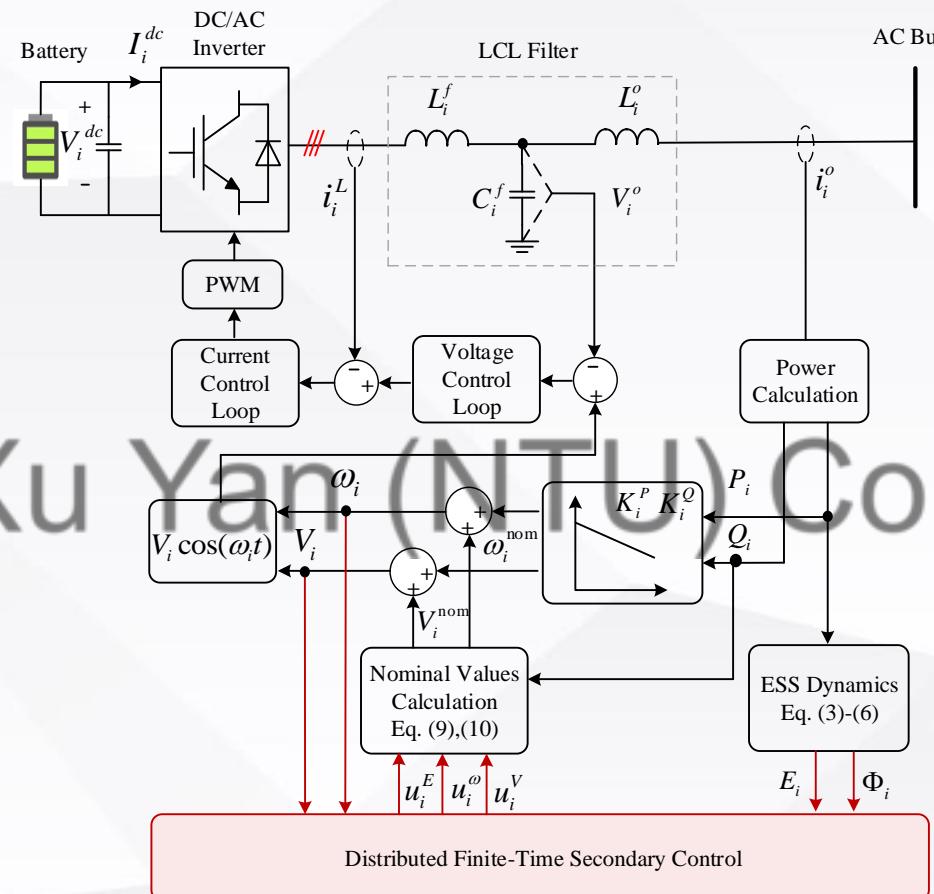
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Finite-Time Distributed Control of Energy Storage Systems



Control diagram of one ESS unit

Finite-time consensus control law

$$u_i^E = c_1 \text{sig} \left(\sum_{j=1}^N a_{ij} (E_j - E_i) \right)^{\alpha_1} + c_2 \text{sig} \left(\sum_{j=1}^N a_{ij} (\Phi_j - \Phi_i) \right)^{\alpha_2}$$

$$\begin{aligned} e_i^\omega &= \sum_{j=1}^N a_{ij} (\omega_j - \omega_i) + g_i (\omega^{ref} - \omega_i) \\ e_i^V &= \sum_{j=1}^N a_{ij} (V_j - V_i) + g_i (V^{ref} - V_i) \end{aligned}$$

Control objectives

$$\lim_{t \rightarrow T^E} |\Phi_i(t) - \Phi_j(t)| = 0, \quad \lim_{t \rightarrow T^E} |E_i(t) - E_j(t)| = 0$$

$$\Phi_i(t) = \Phi_j(t), E_i(t) = E_j(t) \forall t \geq T^E$$

$$\lim_{t \rightarrow T^\omega} |\omega_i(t) - \omega^{ref}| = 0, \quad \omega_i(t) = \omega^{ref}, \forall t \geq T^\omega$$

$$\lim_{t \rightarrow T^V} |V_i(t) - V^{ref}| = 0, \quad V_i(t) = V^{ref}, \forall t \geq T^V$$

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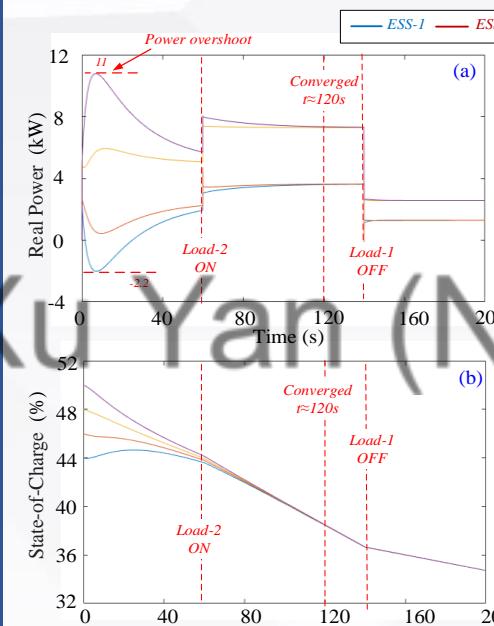
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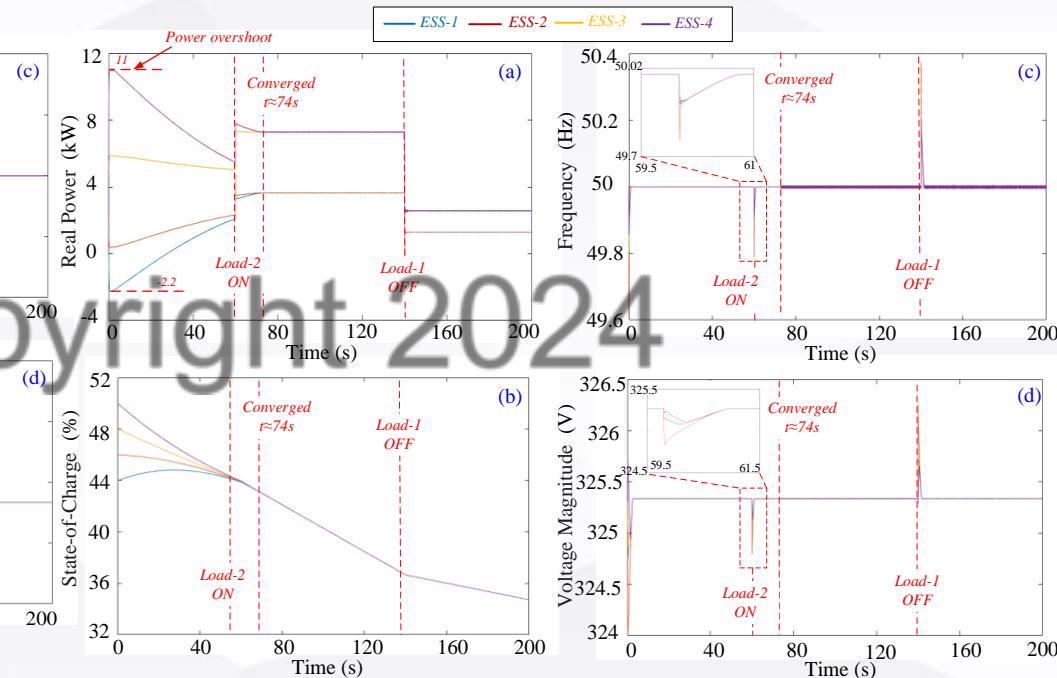
- 1) DG planning
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Finite-Time Distributed Control of Energy Storage Systems

Under the same power overshoot, the proposed controller converges much faster (74s vs 120s)



Linear consensus control



Finite-time consensus control

Y. Wang, T. L. Nguyen, Y. Xu*, D. Shi, "Distributed control of heterogeneous energy storage systems in islanded microgrids: Finite-time approach and cyber-physical implementation," *Int. J. Electrical Power & Energy Systems*, 2020.

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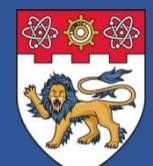
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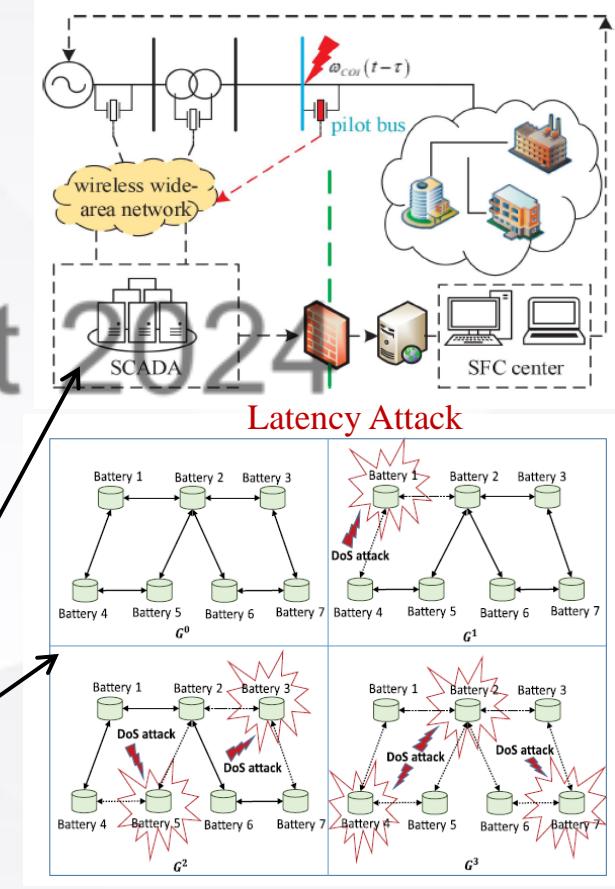
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■ Cyber-Security of Microgrids

A Microgrid might be prone to **suffer from cyber-attack** due to the huge utilization of information and communication technologies. Regarding the security of CPSs, there are three important aspects to be protected: **confidentiality, integrity, and availability.**

Security Elements	Definition	Targets	Typical Attack Forms
Confidentiality	Ensure information can only be obtained by authorized users.	Password; Encryption Algorithm	Password Cracking
		Communication Channel	Tapping
		Electric Quantity	FDIA
Integrity	Maintain the accuracy and consistency of data or information	Switching quantity; electrical quantity	Topology Tampering Attack
		Clock Signal; Timing Protocol	GPS Synchronous Clock Forgery Attack
Availability	Ensure information can be accessed by authorized parties	Computing; Communication; Storage resources; Communication channels	DoS; Command Delay/Latency Attack



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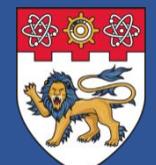
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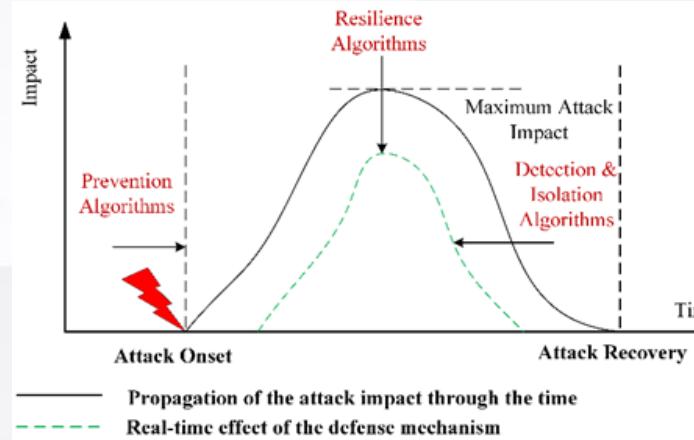
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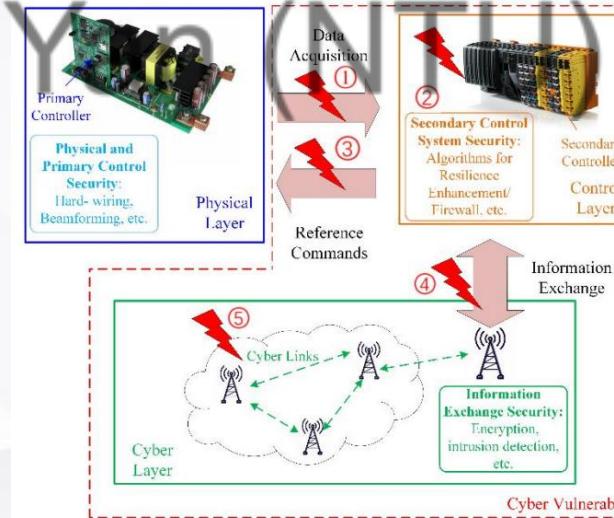
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Cyber-Resilient Control of Microgrids



Security of Cyber-Physical System

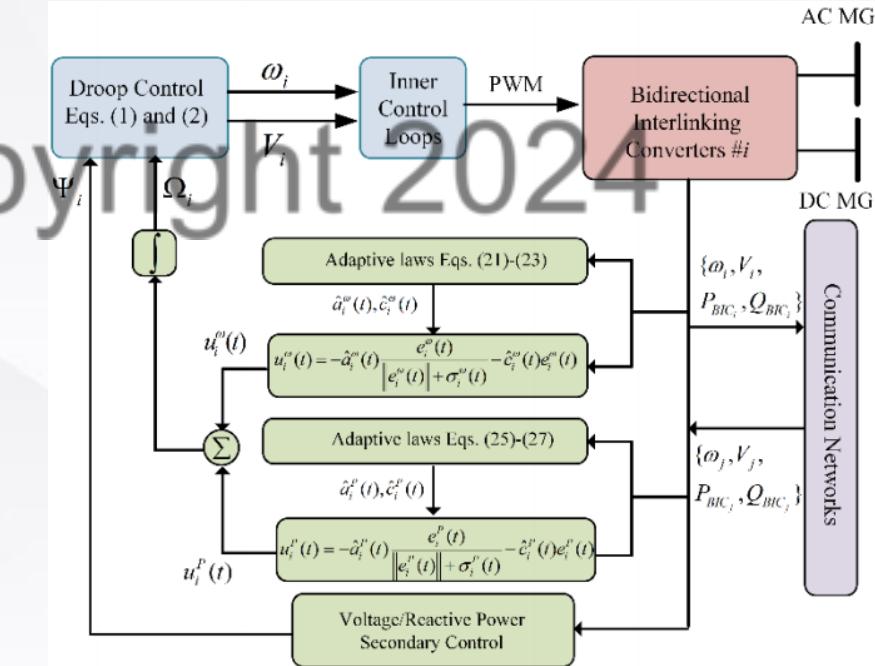


$$\text{Controller Attack: } u_i^f(t) = \varphi_i(t)u_i(t) + \delta_i(t)$$

Magnitude manipulation

False data injection

Framework of the Proposed Resilient Controller



Cyber Vulnerable Process in Microgrid Control

Y. Wang, S. Mondal, C. Deng, K. Satpathi, **Y. Xu*** and S. Dasgupta, "Cyber-Resilient Cooperative Control of Bidirectional Interlinking Converters in Networked AC/DC Microgrids," *IEEE Trans. Industrial Electronics*, 2021.

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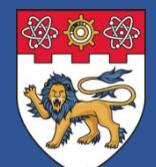
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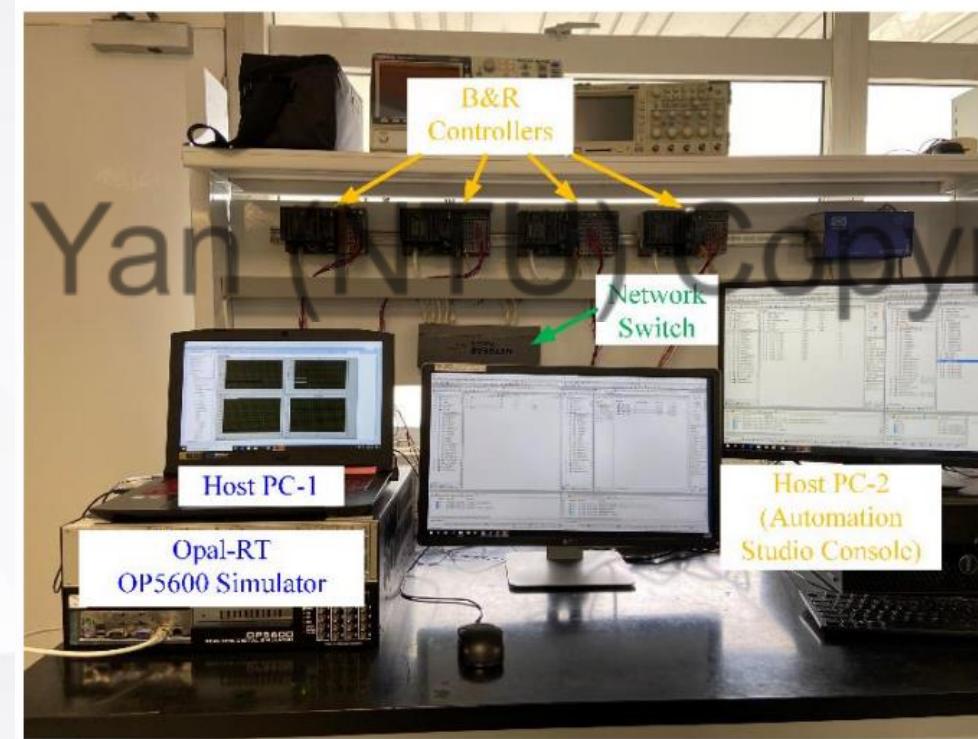
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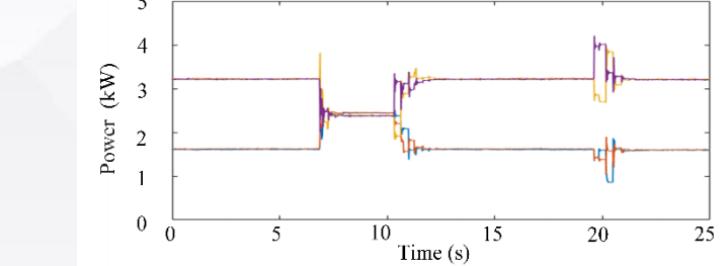
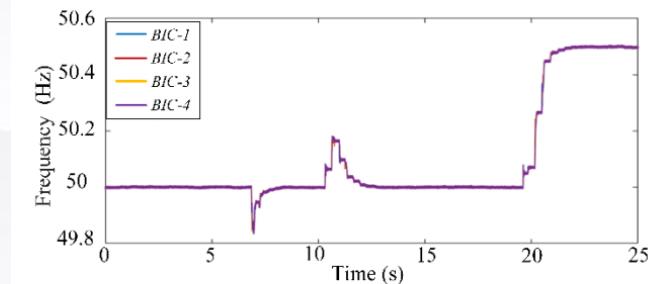
■ Experimental Test Results

□ MAS-MG Platform

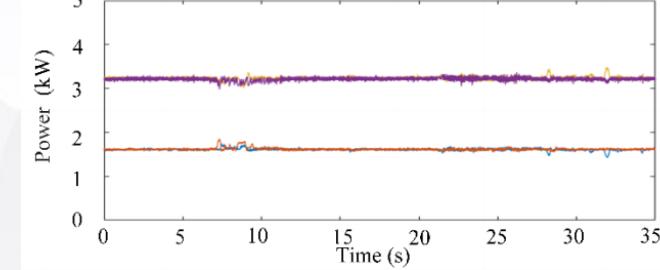
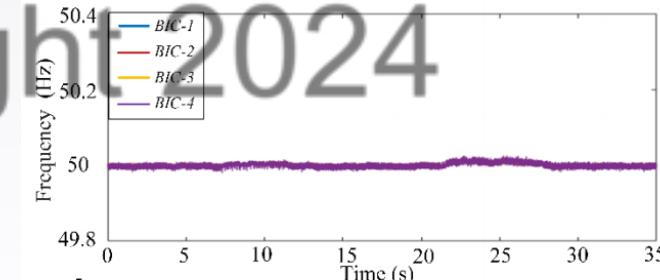
- Multi-agent system with B&R programmable logic controllers and network switch
- Enhance the cyber-resilience of the secondary controllers under false data injection attacks.



Experimental Platform of MAS-MG



Original Controllers subject to Cyber Attacks



Performance of Cyber-Resilient Control

1. REIDS Project

2. Control

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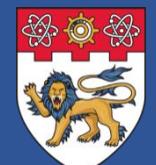
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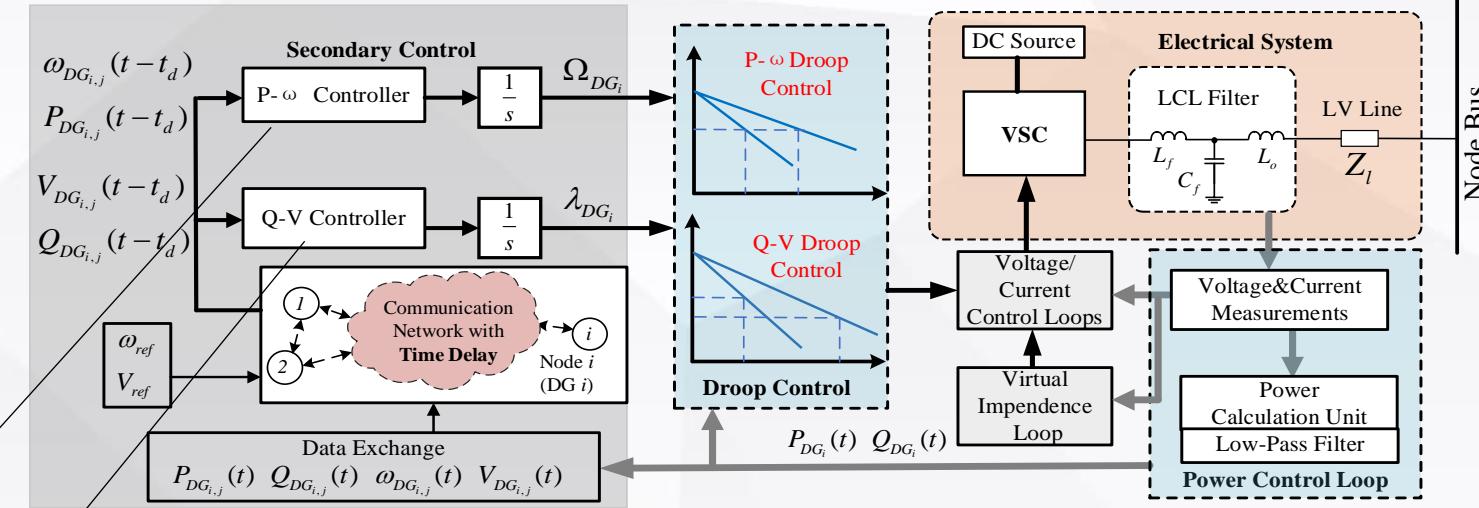
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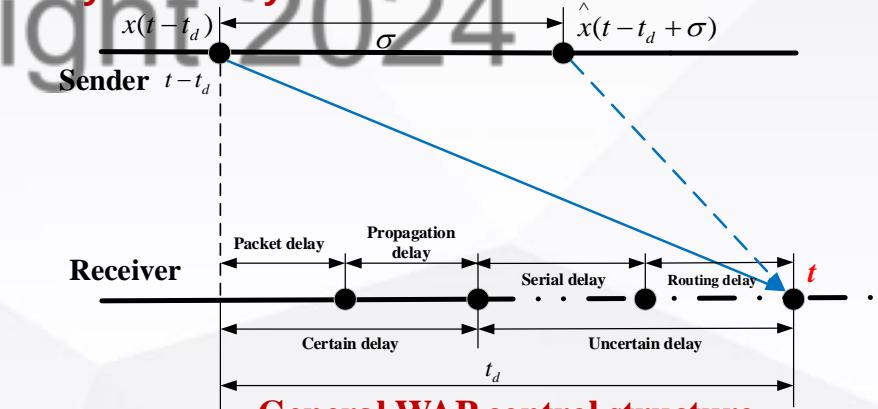
Weight-Average-Prediction Control and Stability Analysis



Control diagram of Time-delayed MG system

$$\begin{aligned}\dot{\Omega}(t) &= -c_\omega * L \left[\omega(t-t_d) + \sigma \dot{\omega}(t-t_d) \right] + c_\omega * G * (I * \omega_{ref} - \omega(t-t_d)) \\ &\quad - c_p * L * k_p \left[P(t-t_d) + \sigma \dot{P}(t-t_d) \right] \\ \dot{\lambda}(t) &= -c_v * L * \left[v_{od}(t-t_d) + \sigma v_{od}(t-t_d) \right] + c_v * G * (I * V_{ref} - v_{od}(t-t_d)) \\ &\quad - c_q * L * k_q \left[Q(t-t_d) + \sigma \dot{Q}(t-t_d) \right]\end{aligned}$$

Weight-average-prediction control law



$$\Delta X_{MG}(t) = A_{MG_1} \Delta X_{MG}(t) + A_{MG_2} \Delta X_{MG}(t-t_d) + A_{MG_3} \Delta X_{MG}(t-2t_d)$$

Time-delayed MG small-signal model under WAP control

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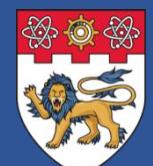
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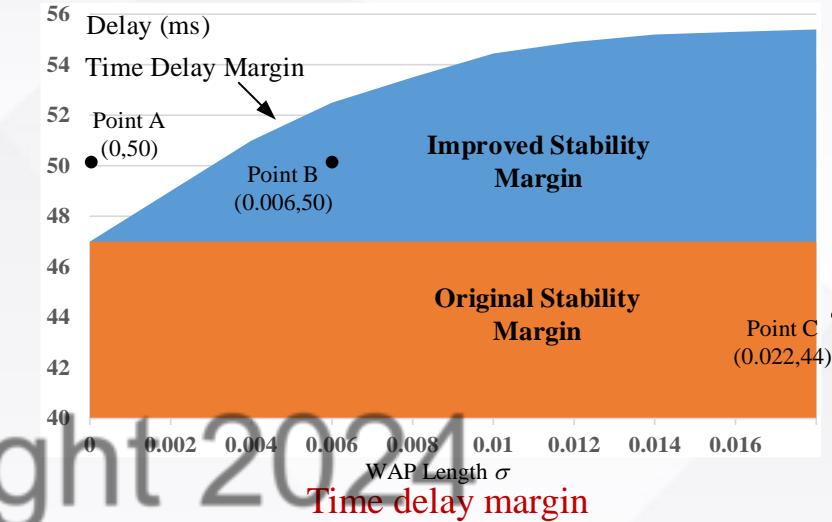
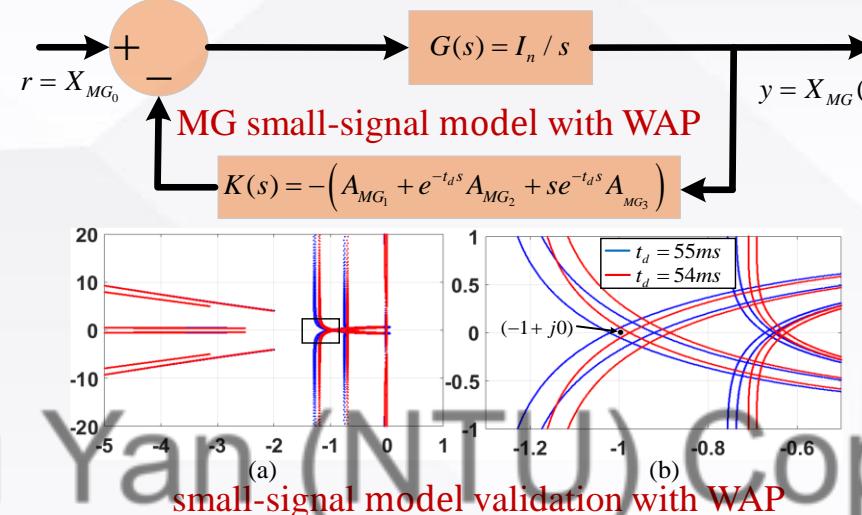
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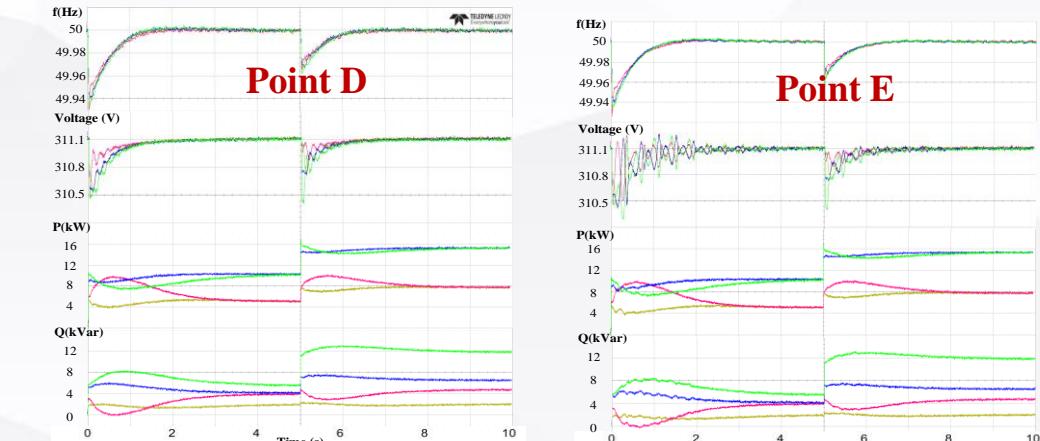
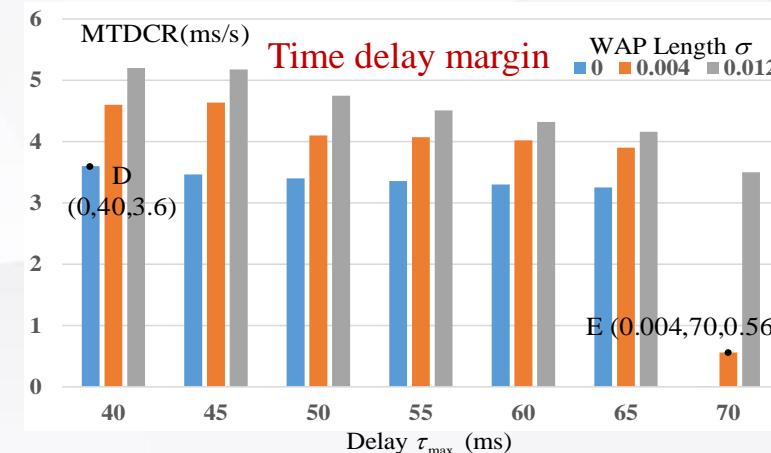


■ Weight-Average-Prediction Control and Stability Analysis

Analysis for fixed time delay (generalized Nyquist stability criterion)



Analysis for time-varying delay (Lyapunov-Krasovskii function and LMIs)



1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

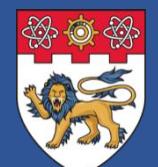
4. Hierarchy coordination

5. Trading

- 1) Centralized trading
- 2) P2P trading

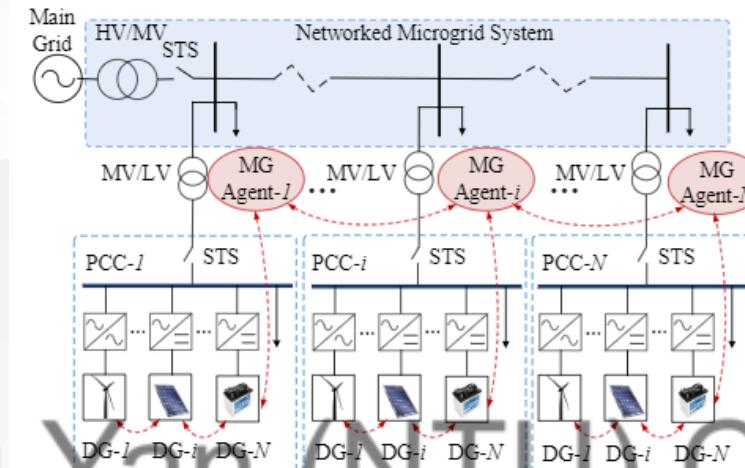
6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm

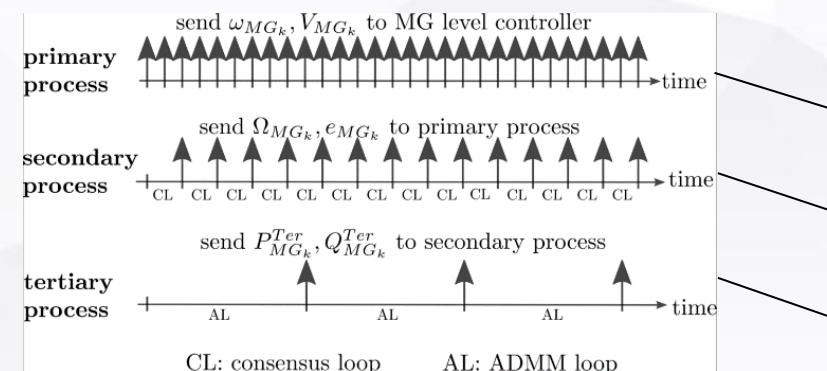


■ Multi-Layer Multi-Agent Control of Networked Microgrids

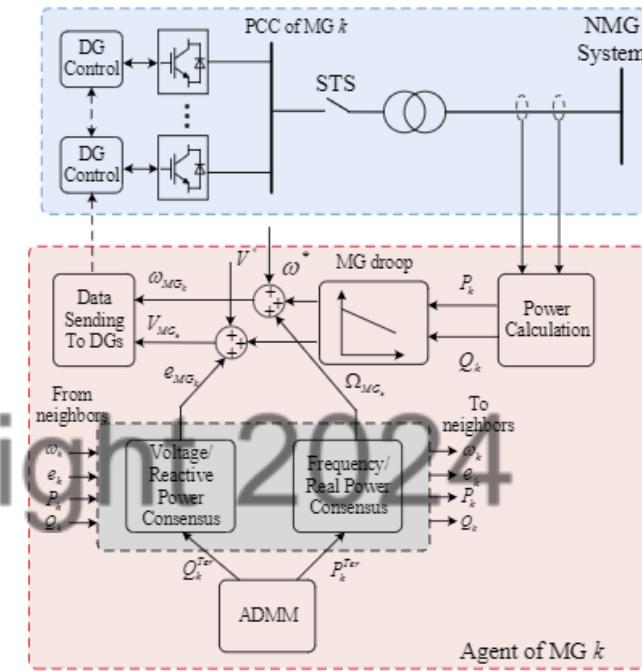
Structure of the Networked Microgrid System



Timescale Coordination of Control Layers



Control System of each Agent



Droop Control Loop: local measurement and signal from secondary control

Consensus Control Loop: local measurement, neighbouring signal, and signal from tertiary control

ADMM Loop: local measurement and neighbouring signal

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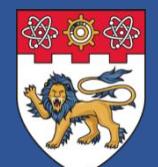
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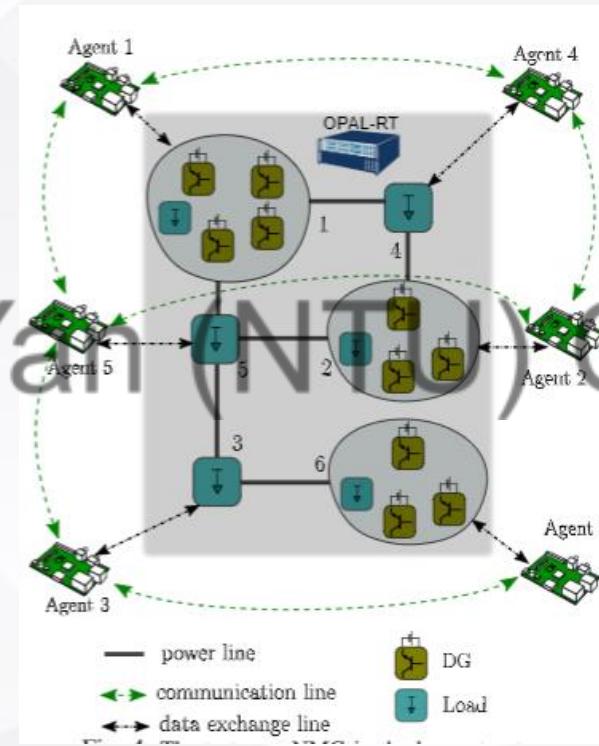
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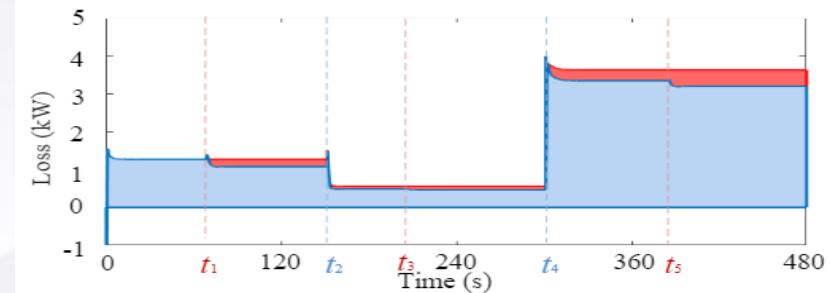
Controller HIL Test Results

- The proposed method realize frequency/voltage regulation, real power sharing and network loss minimization.

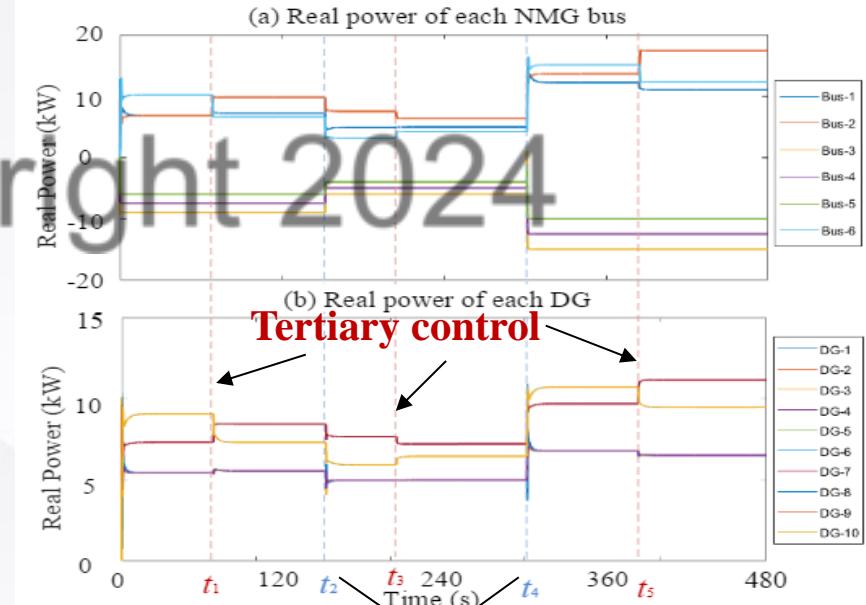


Structure of the controller HIL test system

System network loss minimization



Real power among buses and DGs



Load change

Performance of Cyber-Resilient Control

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

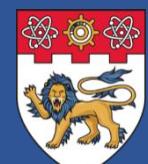
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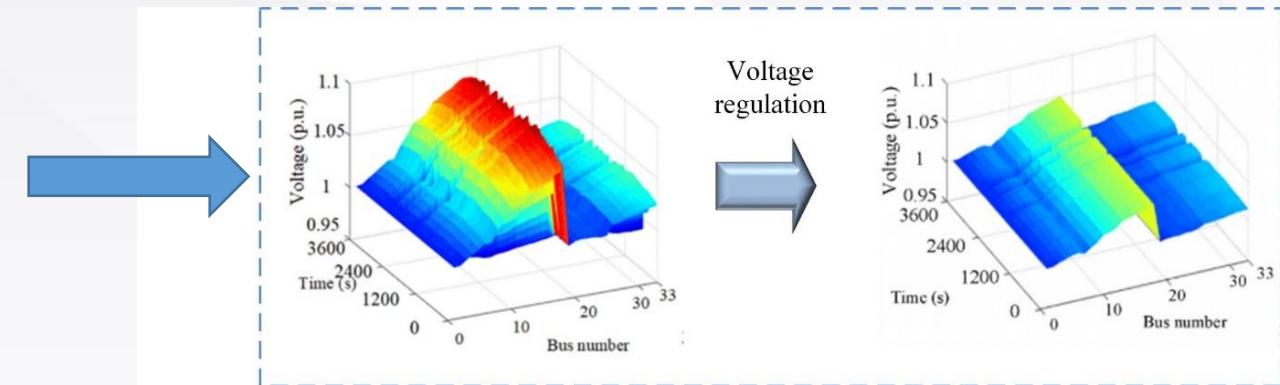
- 1) DG planning
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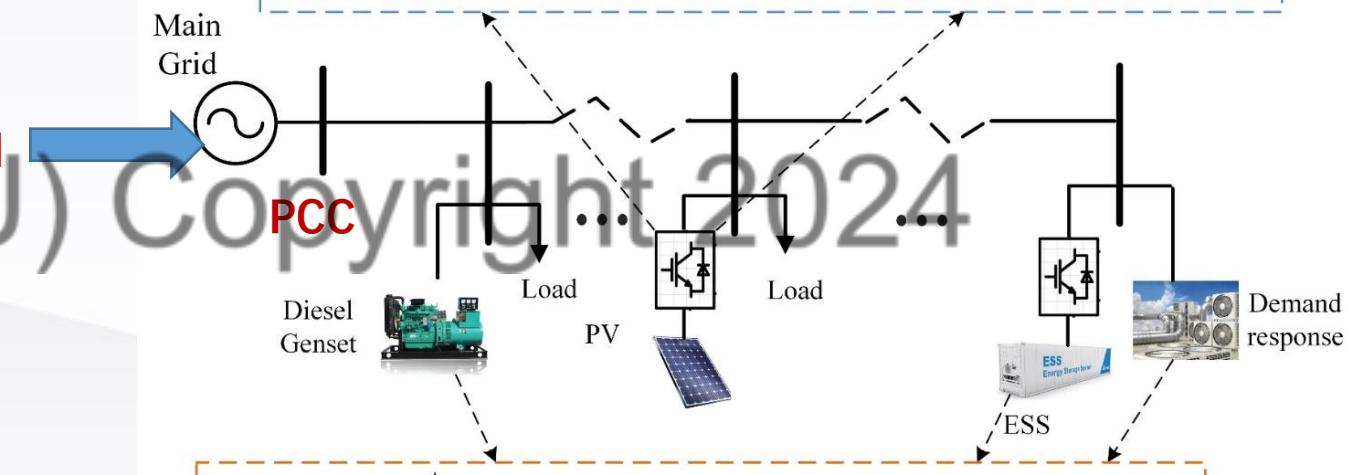
▪ Grid-connected mode of Microgrids (DER support)

Voltage control support:

mitigate voltage deviation
(seconds to minutes)

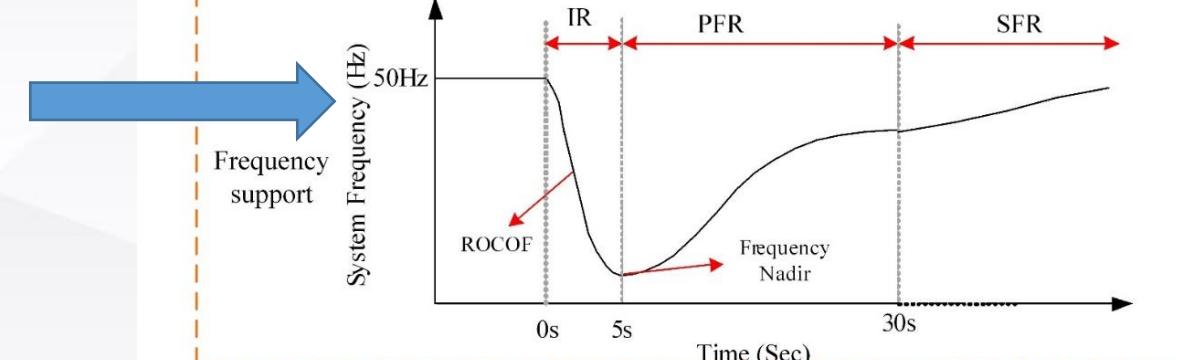


Frequency and voltage are dominated by the main grid through point of coupling connection (PCC).



Frequency control support:

mitigate frequency variation
(ms to seconds)



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3. Operation

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- 2) Volt/Var regulation

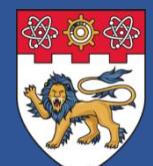
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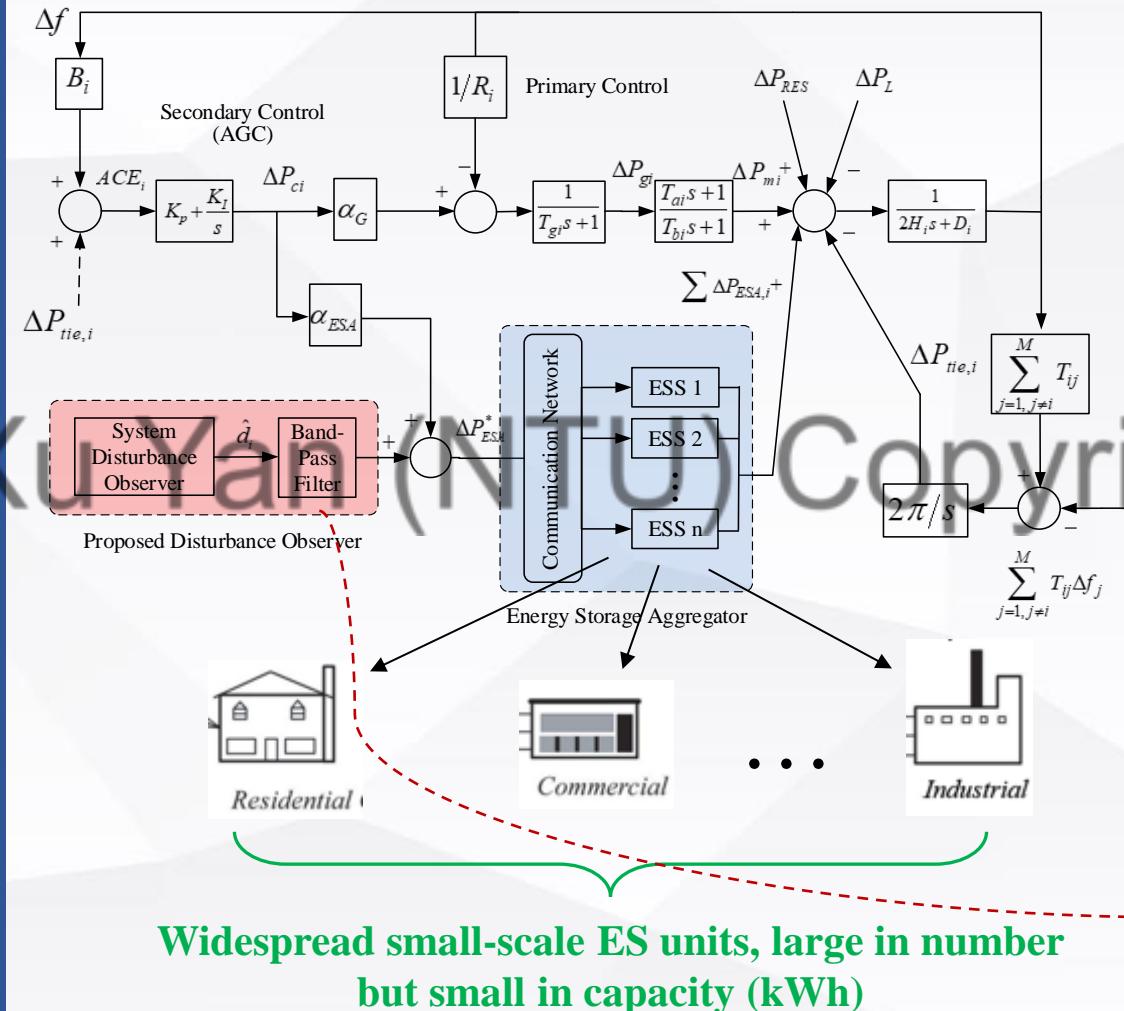
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Frequency Support from Aggregated Small-Scale Energy Storage Units

Proposed load frequency control (LFC) framework



Y. Wang, Y. Xu*, Y. Tang, et al “Aggregated Energy Storage for Power System Frequency Control: A Finite-Time Consensus Approach,” *IEEE Trans. Smart Grid*, May 2018.

$$\dot{\Delta f}_i(t) = -\frac{D_i}{2H_i} \Delta f_i(t) \quad \text{Frequency dynamic model}$$

$$+ \frac{1}{2H_i} (\Delta P_{mi}(t) - \Delta P_{L,i}(t) + \Delta P_{RES,i}(t) - \Delta P_{tie,i}(t) + \Delta P_{ESA,i}(t))$$

$$\dot{\Delta P}_{mi}(t) = -\frac{1}{T_{bi}} \Delta P_{mi}(t) + \frac{1}{T_{bi}} \Delta P_{gi}(t) + \frac{T_{ai}}{T_{bi}} \dot{\Delta P}_{gi}(t)$$

$$\dot{\Delta P}_{gi}(t) = -\frac{1}{T_{gi}} \Delta P_{gi}(t) + \frac{1}{T_{gi}} \Delta P_{ci}(t) - \frac{1}{R_i T_{gi}} \Delta f_i(t)$$

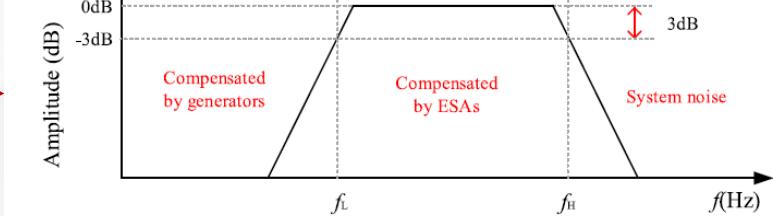
$$\dot{\Delta P}_{tie,i}(t) = 2\pi \cdot \left[\sum_{j=1, j \neq i}^M T_{ij} (\Delta f_i(t) - \Delta f_j(t)) \right]$$

Tie-line power flow

$$ACE_i(t) = B_i \Delta f_i(t) + \Delta P_{tie,i}(t)$$

$$\Delta P_{ci}(t) = -K_P ACE_i(t) - K_I \int ACE_i(t)$$

Secondary control



1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

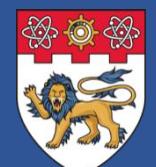
4. Hierarchy coordination

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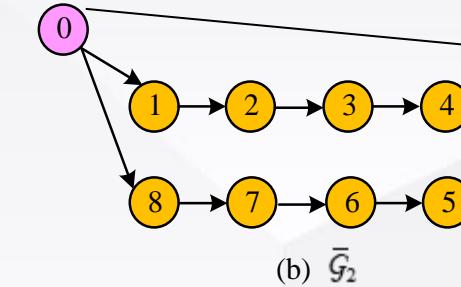
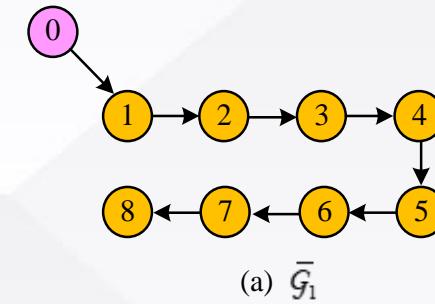
6. Planning

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- 3) PRO algorithm



Frequency Support from Aggregated Energy Storage

Communication topologies of ESSs



Leader model

$$\begin{cases} \dot{e}_0(t) = K_{ESS} p_0(t) \\ p_0(t) = \frac{P_{ESA}^*(t)}{P_{ESA}^{\max}} \end{cases}$$

LFC power reference

ESS model (follower)

$$\begin{cases} \dot{e}_i(t) = K_{ESS} p_i(t), \\ \dot{p}_i(t) = u_i(t) \end{cases}, \quad i = 1, 2, \dots, N.$$

Matrices to describe graph

Adjacent Matrix

$$A = [a_{ij}] \quad a_{ij} = \begin{cases} 1, & \text{if } (v_i, v_j) \in E \\ 0, & \text{otherwise.} \end{cases}$$

Pinning Matrix

$$G = \text{diag}\{g_i\} \quad g_i = \begin{cases} 1, & \text{if } \exists (v_i, v_0) \\ 0, & \text{otherwise.} \end{cases}$$

Proposed Control Protocol: achieve LFC power reference with consensus SOC in finite time

$$u_i(t) = \sum_{j=1}^N a_{ij} (\text{sig}(e_i(t) - e_j(t))^\alpha) - g_i (\text{sig}(e_i(t) - e_0(t))^\alpha)$$

Consensus SOC

$$-\gamma \sum_{j=1}^N a_{ij} (\text{sig}(p_i(t) - p_j(t))^\beta) - g_i (\text{sig}(p_i(t) - p_0(t))^\beta)$$

LFC power reference

$$\lim_{t \rightarrow T_0} \|e_i(t) - e_0(t)\| = 0, \quad \lim_{t \rightarrow T_0} \|p_i(t) - p_0(t)\| = 0$$

$$e_i(t) = e_0(t), \quad p_i(t) = p_0(t), \quad \forall t \geq T_0, \quad i = 1, 2, \dots, N.$$

1. REIDS Project

2. Control

- 1) Islanded mode
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3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

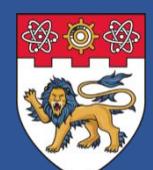
4. Hierarchy coordination

5. Trading

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- 2) P2P trading

6. Planning

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- 3) PRO algorithm



■ Simulation Results

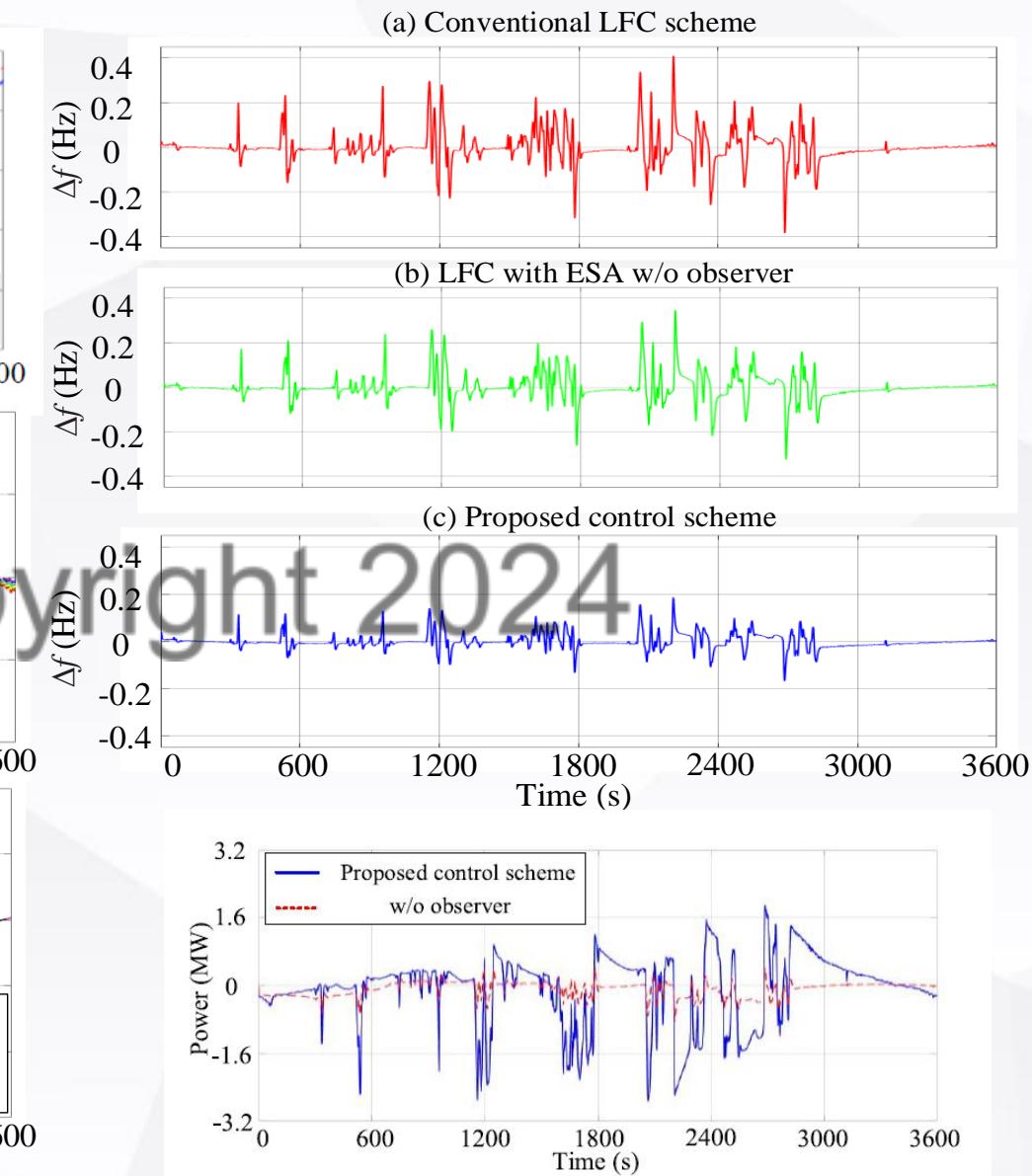
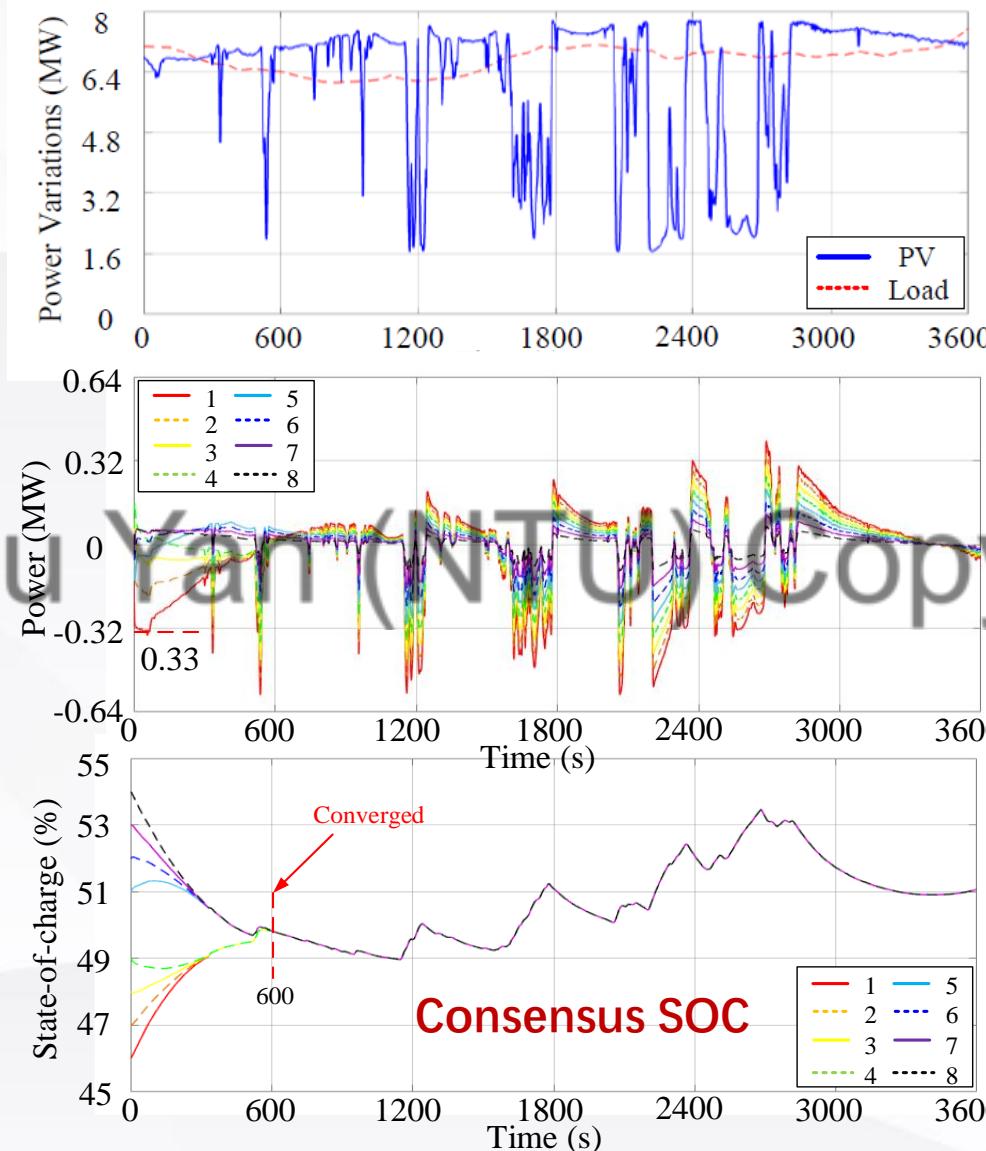


Fig. 11. Total power output of the ESA with and without the proposed disturbance observer.

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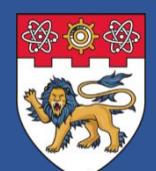
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Thermostatically Controlled Loads (TCLs) for frequency support

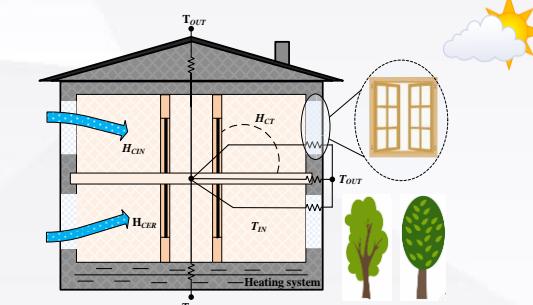
Temperature dynamics of TCL:

$$C_{th} \frac{dT_i(t)}{dt} = \frac{T_a(t) - T_i(t)}{R_{th}} - \eta \bar{P} \alpha_i(t), \quad i \in \mathcal{G}$$

Heat exchange with the ambient

Thermal energy from VFAC

Assume power state α_i is a continuous variable from 0 to 1.



Comfort zone of TCL:

$$\beta_i(t) = \frac{T_i(t) - T_s + \Delta T}{2\Delta T}, \quad i \in \mathcal{G}$$

Comfort state β_i is an index from 0 to 1.

State-space model of TCL:

$$\begin{bmatrix} \frac{d\alpha_i(t)}{dt} \\ \frac{d\beta_i(t)}{dt} \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 0 \\ -\frac{2\Delta T}{C_{th}R_{th}} & -\frac{\eta \bar{P}}{C_{th}} \end{bmatrix}}_A \begin{bmatrix} \alpha_i \\ \beta_i \end{bmatrix} + \underbrace{\begin{bmatrix} 1 \\ 0 \end{bmatrix}}_B u_i + \underbrace{\begin{bmatrix} 0 \\ \frac{T_a(t) - T_s + \Delta T}{C_{th}R_{th}} \end{bmatrix}}_W$$

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

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- 2) Volt/Var regulation

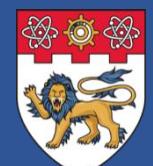
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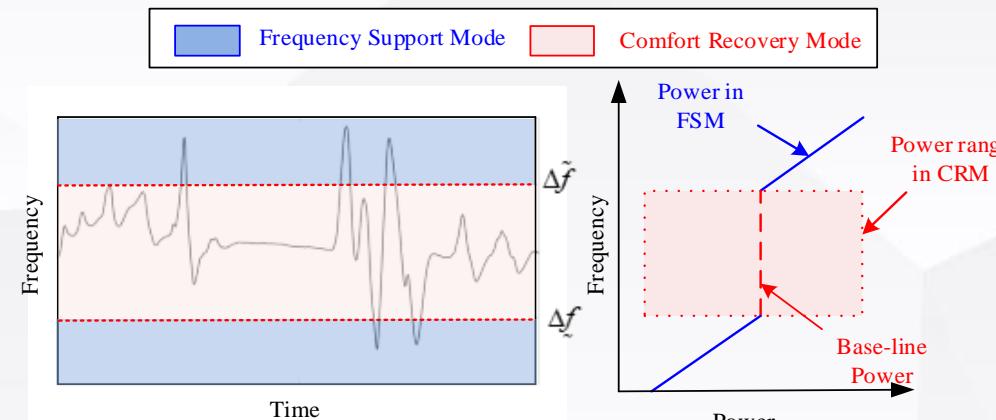
- 1) Centralized trading
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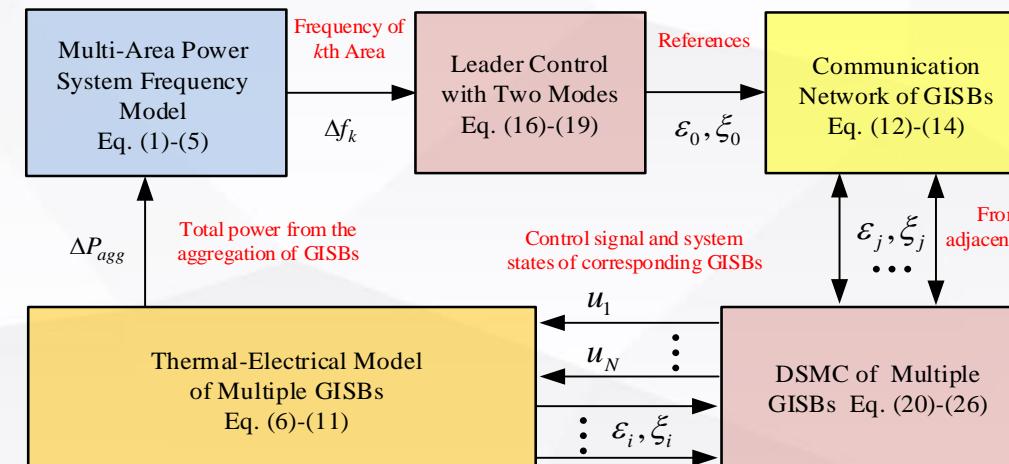
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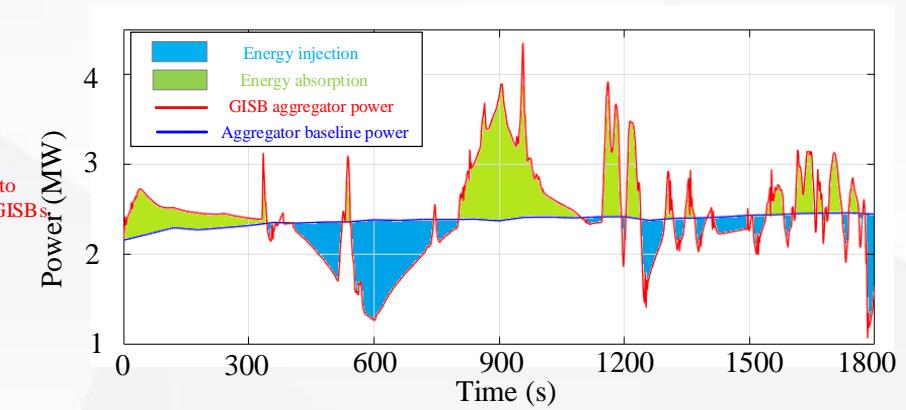
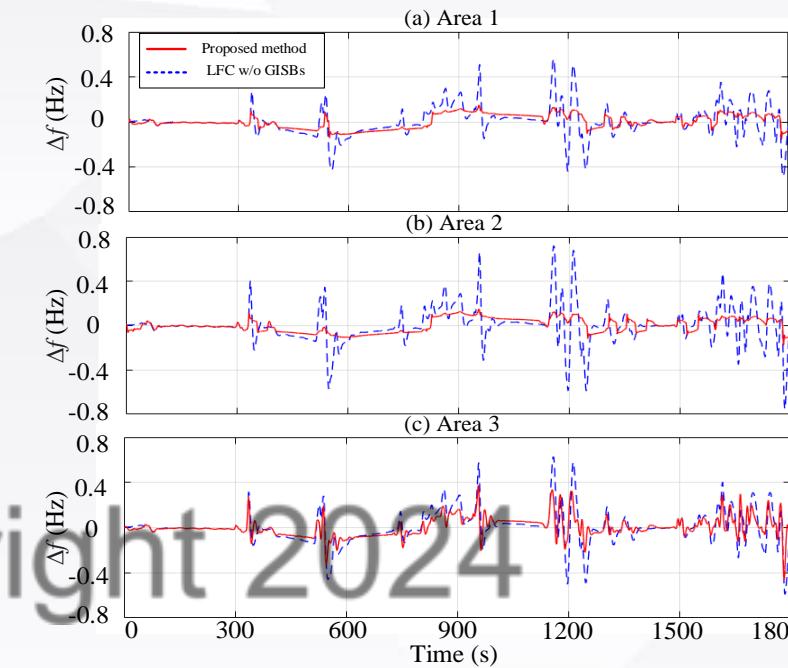
Thermostatically Controlled Loads (TCLs) for frequency support



Leader control mode: f support mode and comfort recover mode



Leader-follower consensus controller



Y. Wang, Y. Xu, and Y. Tang, "Distributed Aggregation Control of Grid-Interactive Smart Buildings for Power System Frequency Support," *Applied Energy*, 2019.

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- 2) Grid-tied mode

3. Operation

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- 2) Volt/Var regulation

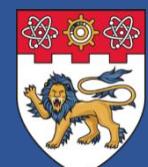
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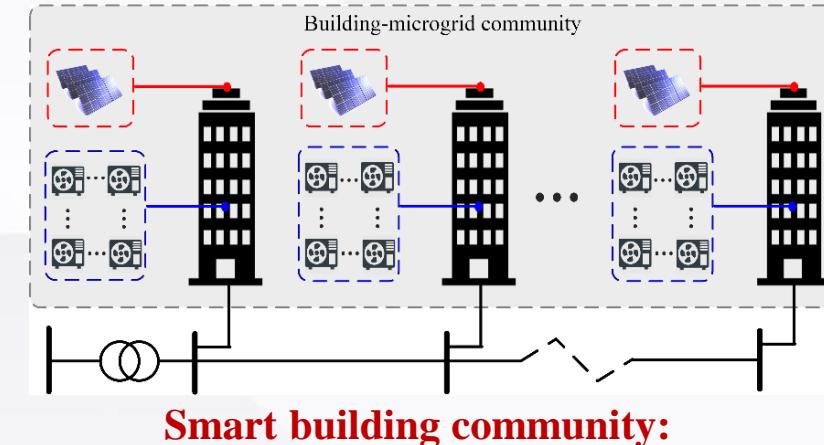
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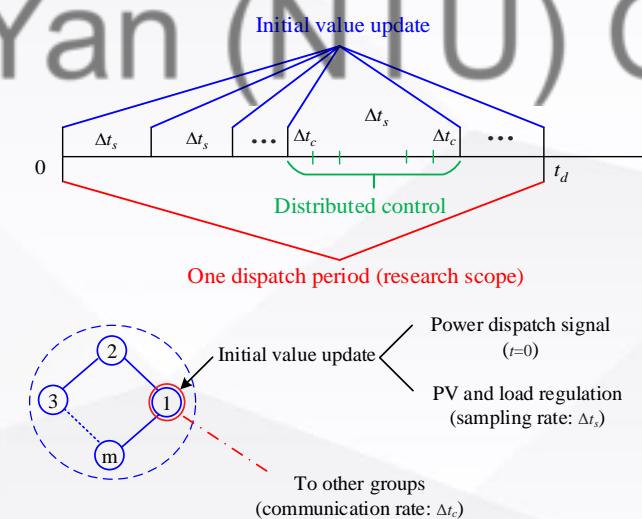
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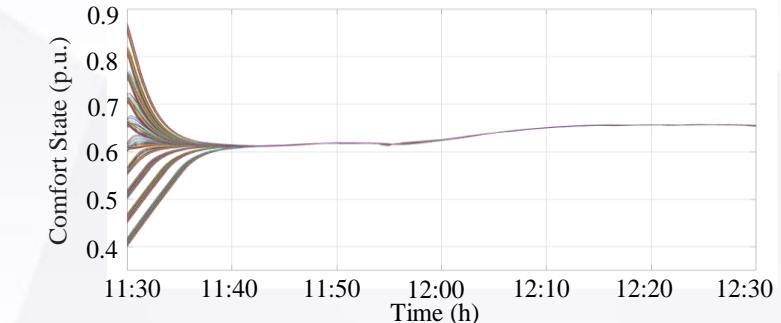
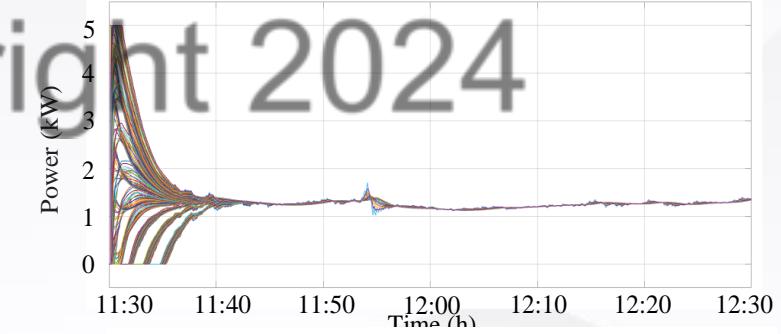
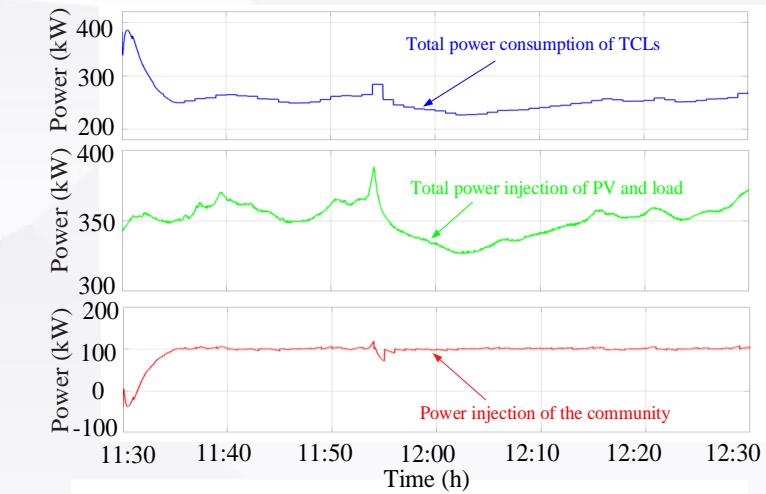
Ancillary Service Support from Smart Building Community



Smart building community:
TCLs+PVs



Initial value updating scheme



1. REIDS Project

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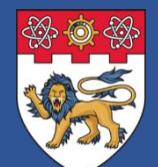
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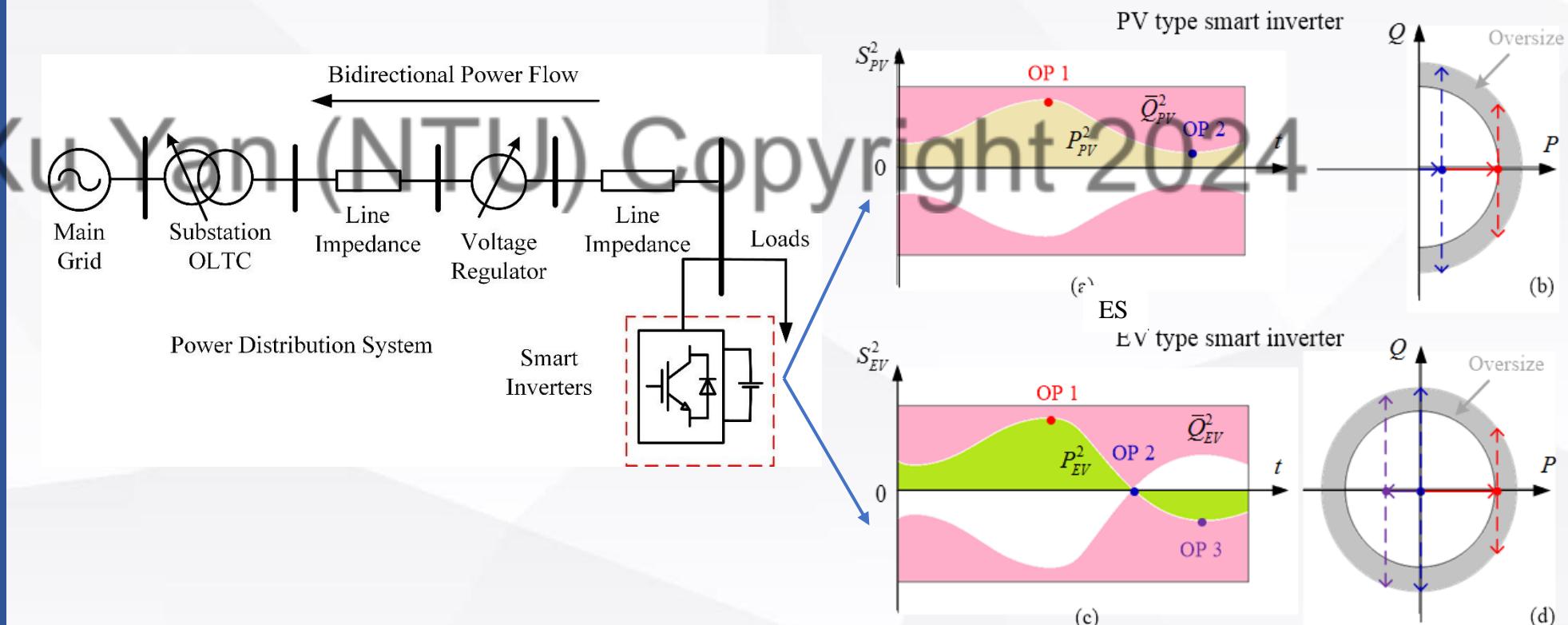
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- Real-time Voltage/Var Control (VVC) Support from DERs

- Existing Challenges: High PV penetration level, massive EV charging.
- Voltage quality issues: Voltage rise, drop and fast fluctuations.
- Potential solutions: inverter-assisted voltage/var support



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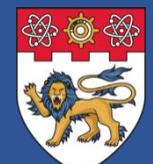
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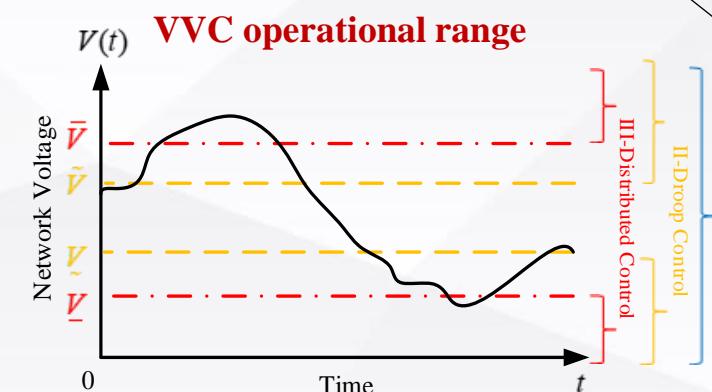
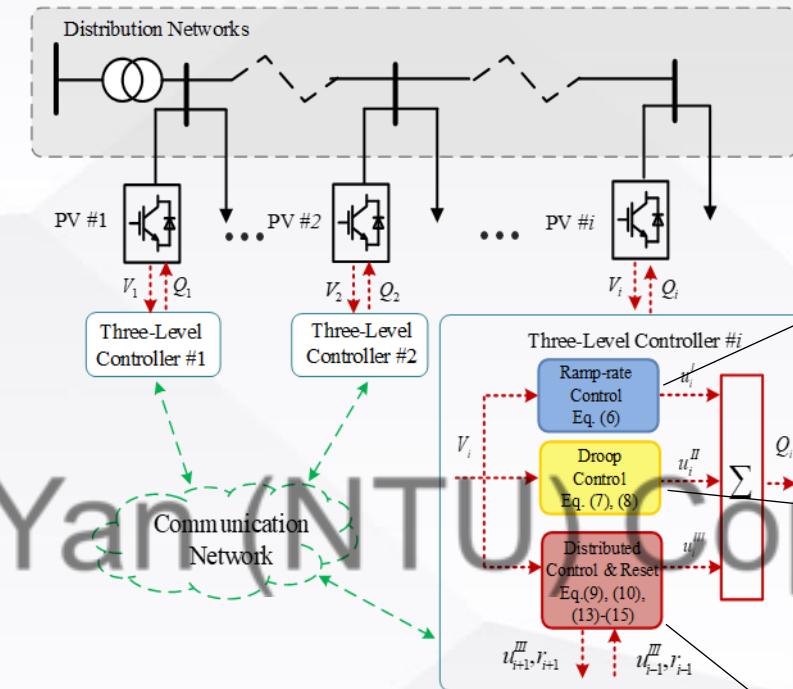
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Real-Time Coordinated Voltage/Var Control Controller



Controller design:

Level I: Ramp-rate Control \rightarrow smooth voltage fluctuation

$$u_i^I(t) = K_i^I [V_i(t) - \frac{\sum_{j=t-\omega}^t V_i(j)}{T(t) - T(t-\omega)}]$$

Level II: Droop Control \rightarrow immediate voltage support

$$u_i^{II}(t) = \begin{cases} K_i^{II} (V_i(t) - \tilde{V}), & V_i(t) > \tilde{V} \\ 0, & \tilde{V} \leq V_i(t) \leq \tilde{V} \\ K_i^{II} (V_i(t) - \tilde{V}), & V_i(t) < \tilde{V} \end{cases}$$

Level III: Distributed Control \rightarrow voltage regulation to acceptable range

$$\dot{u}_i^{III}(t) = G_i^{III} [\sum_{j=1}^N a_{ij} (u_j^{III}(t) - u_i^{III}(t))] + e(t)$$
$$e(t) = \begin{cases} K_i^{III} (V_i(t) - \bar{V}), & V_i > \bar{V} \\ 0, & \bar{V} \leq V_i \leq \bar{V} \\ K_i^{III} (V_i(t) - \underline{V}), & V_i < \underline{V} \end{cases}$$

Dynamic
consensus

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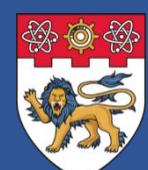
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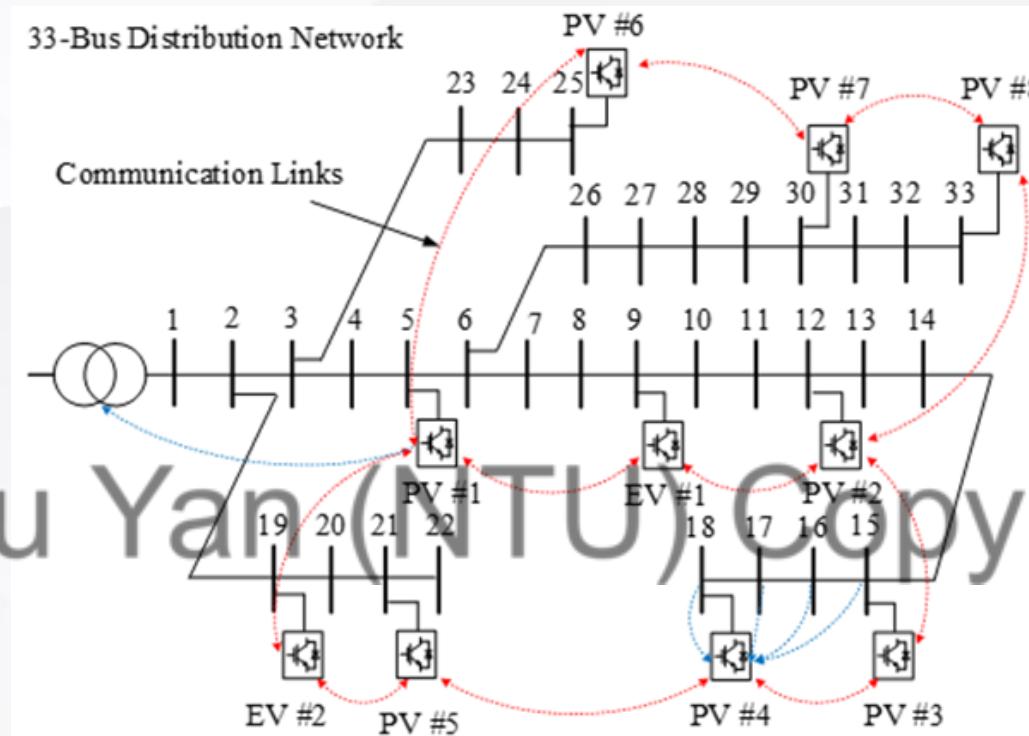
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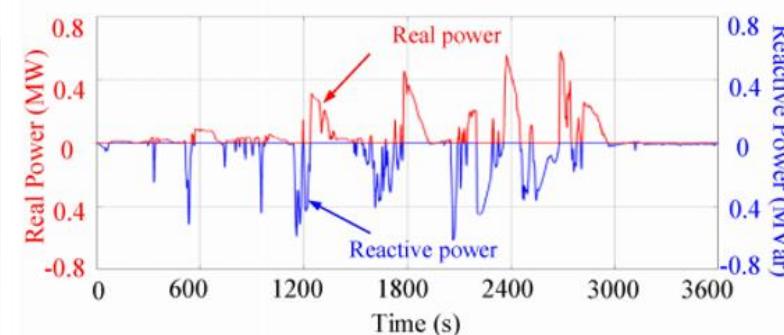


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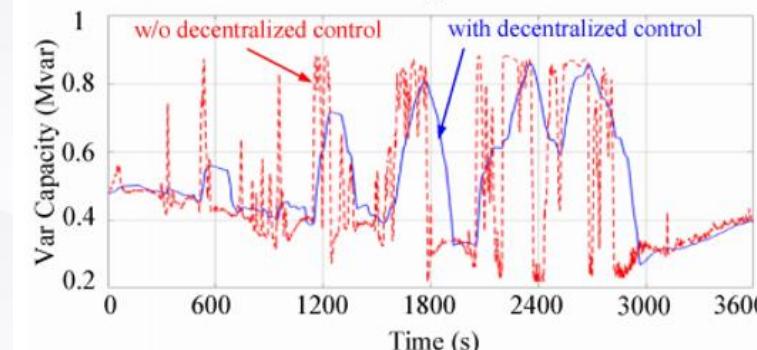
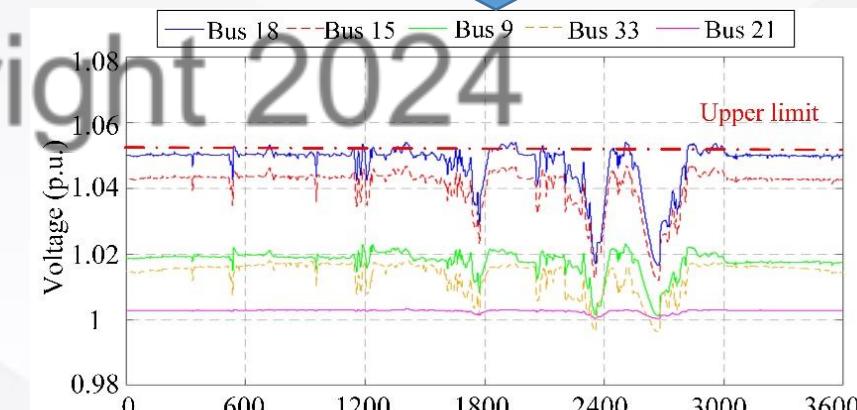
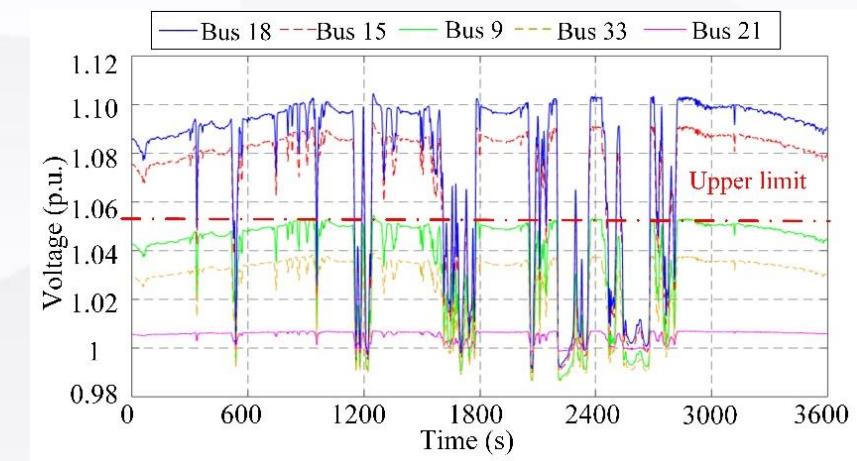
■ Simulation Tests



Effectiveness of ramp-rate control



Real-time voltage/var control from inverters



1. REIDS Project

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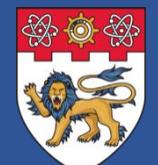
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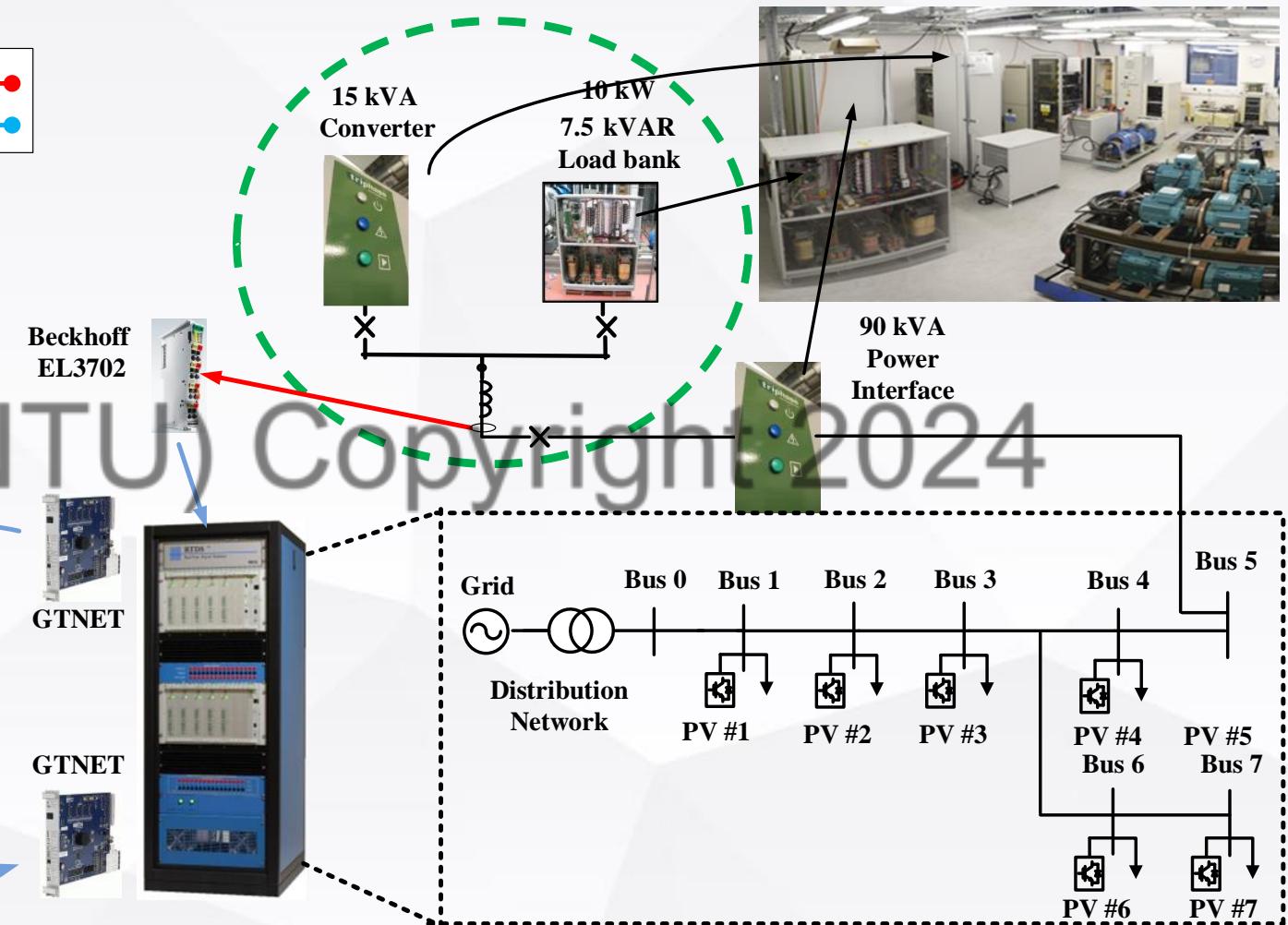
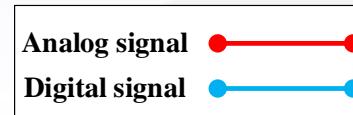
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Power Hardware-in-the-Loop (PHiL) Test



1. REIDS Project

2. Control

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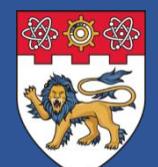
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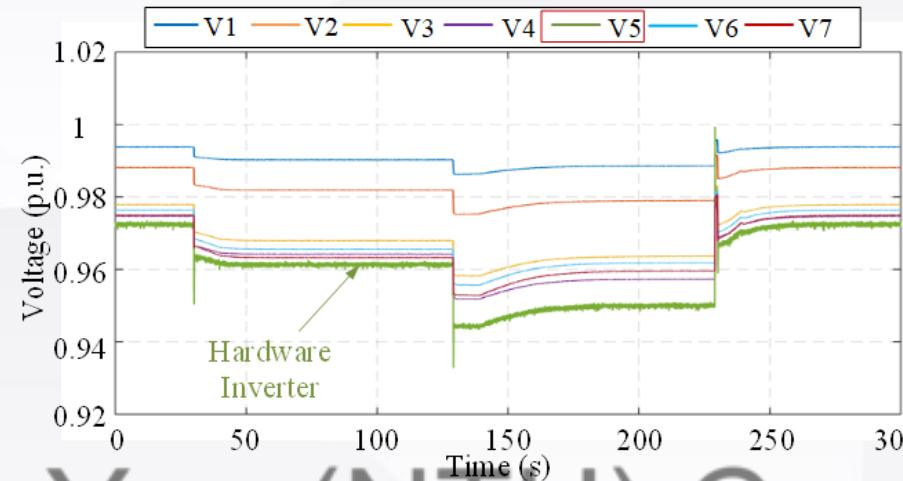
- 1) Centralized trading
- 2) P2P trading

6. Planning

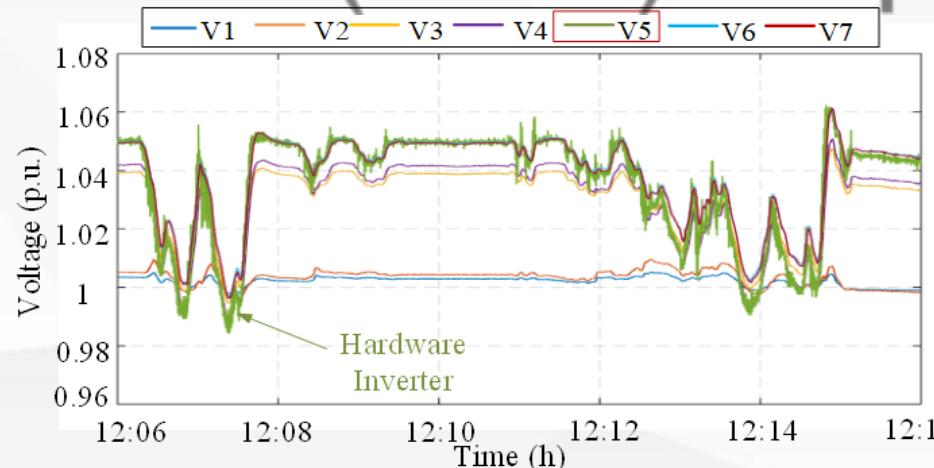
- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm



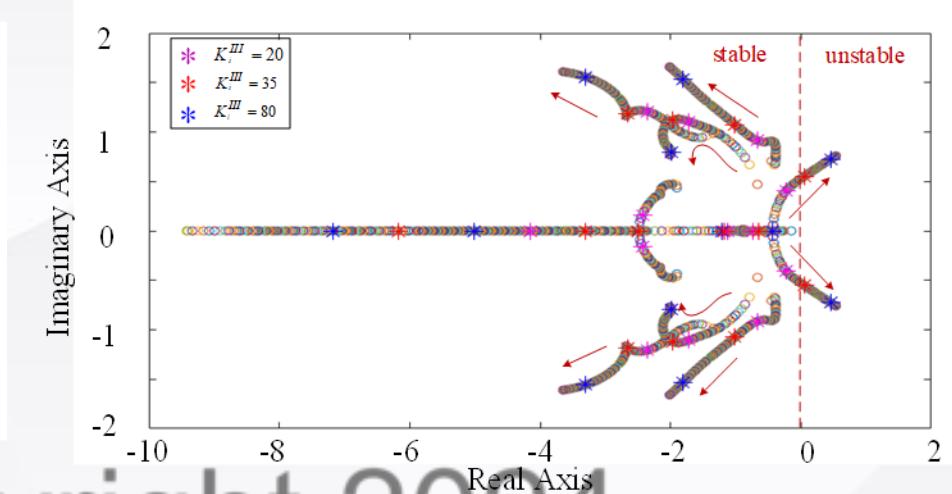
■ Power HiL Results and Eigenvalues



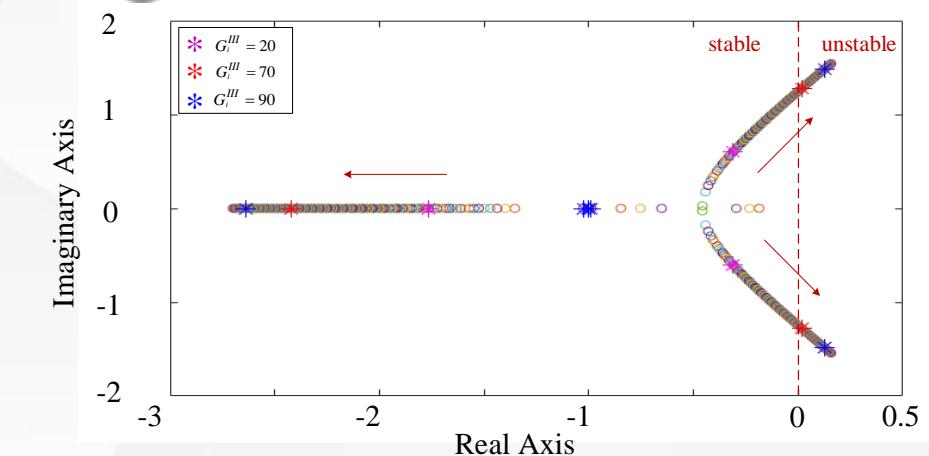
Voltage profiles under step load changes



Voltage profiles under real PV and load data



Trace of eigenvalues under different control gains



1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

4. Hierarchy coordination

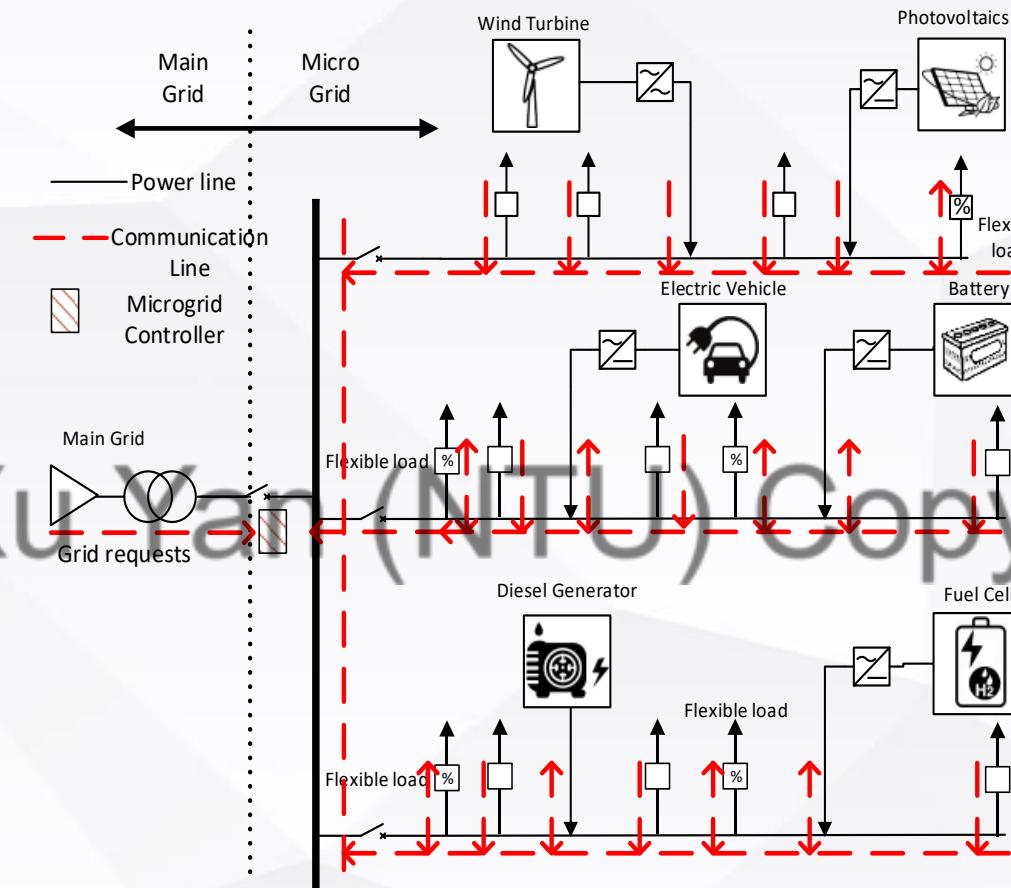
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■ Operation of DER - Energy Dispatch & Volt/Var Regulation in Microgrid



- Network model:
 - 1) Linearized Dist-Flow
 - 2) Second-order cone programming (SOCP) model

- Control variables:

- 1) Micro-turbine
- 2) Energy storage
- 3) Demand response
- 4) Capacitor banks
- 5) On-load tap changers
- 6) PV inverters

Active power resource

Reactive power resource

- Parameters:

- 1) Load demand
- 2) Wind and PV output
- 3) Electricity price
- 4) Network parameters (R,X,B)

Uncertain

- State variables:

- 1) Bus voltage
- 2) Branch power flow
- 3) Power exchange with main grid

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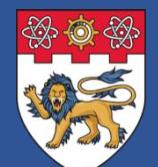
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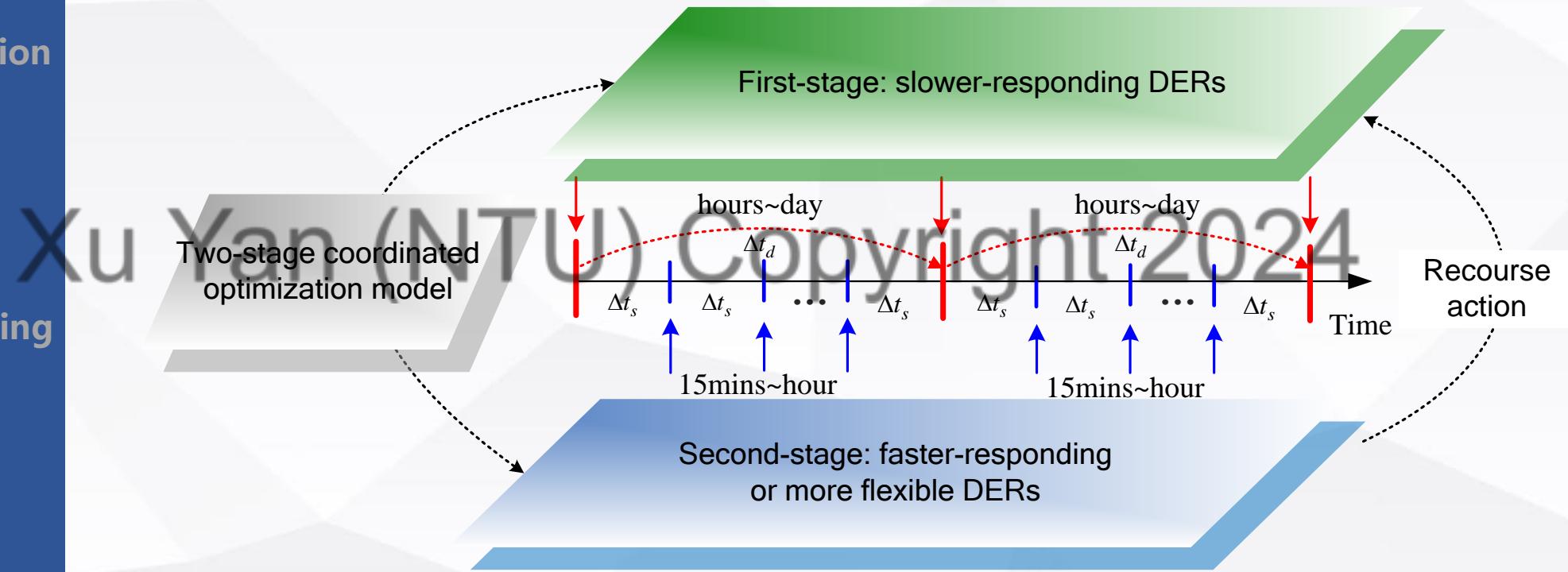
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- Two-stage coordinated operation – Temporal Coordination of DERs
- Principle: coordinate different DERs in different timescales against uncertainty.**
- **First-stage:** slower-responding DER in longer timescale.
 - **Second-stage:** faster-responding or more flexible DER in shorter timescale.



- **Frist-stage decisions** are implemented before uncertainty realizes and will be fixed in the second-stage.
- **Second-stage decisions** will be re-optimized and implemented after uncertainty realizes, therefore it is a recourse action to the first-stage decision.

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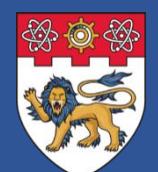
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Optimization Methods

Method	Stochastic Programming	Robust Optimization (RO)
Uncertainty Modeling	Probabilistic scenarios based on probability distribution function (PDF)	Uncertainty set with bounds and budgets
Inputs	Point prediction	Interval prediction
Model	Optimize under expectation $\min_{x \in F} \{ f(x) + E[Q(x, \xi)] \}$	Optimize under worst case $\min_{\mathbf{x}} \left(\mathbf{c}^T \mathbf{x} + \max_{\mathbf{d} \in \mathcal{D}} \min_{\mathbf{y} \in \Omega(\mathbf{x}, \mathbf{d})} \mathbf{b}^T \mathbf{y} \right)$
Advantages	<ul style="list-style-type: none">Simpler formulation and solution process	<ul style="list-style-type: none">No need for PDFFully robust within the uncertainty sets
Disadvantages	<ul style="list-style-type: none">Need for PDFProbabilistic robustness	<ul style="list-style-type: none">Complex formulation and solution processMay be conservative

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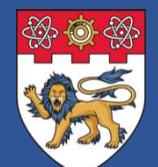
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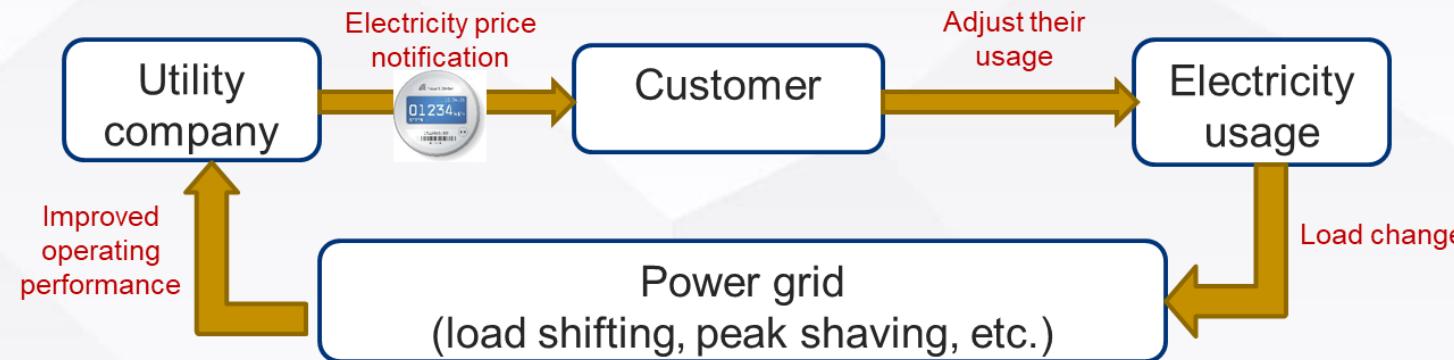
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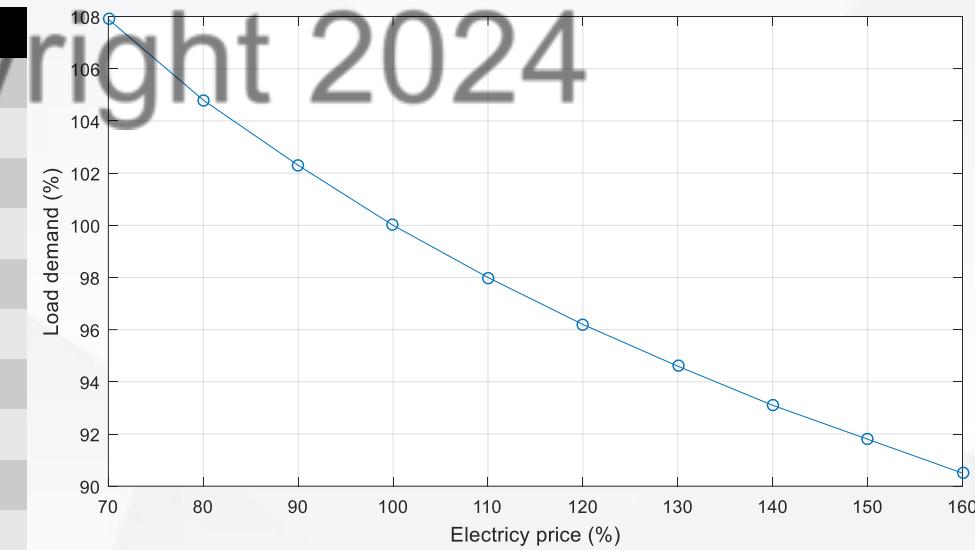


- Robustly Coordinated Energy Management
- Day-ahead Price-based Demand Response & Hourly-ahead Microturbine

Price-based Demand Response (PBDR)



Level	Price Rate (%)	Load Rate (%)
1	70	107.9
2	80	104.8
3	90	102.3
4	100	100.0
5	110	98.0
6	120	96.2
7	130	94.6
8	140	93.1
9	150	91.8
10	160	90.5



$$P_t^D = A \Pr_t^\varepsilon$$

where ε is **price elasticity** of electric demand, and A is a constant value modeling the relationship between the price and load demand. E.g., the price elasticity of load is -0.38 for Australian power systems. ⁵³

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▪ Robustly Coordinated Energy Management Day-ahead Price-based Demand Response & Hourly-ahead Microturbine

Two-Stage Operation Framework

Day-ahead 24-hour electricity prices and predicted wind turbine outputs, PV outputs and load demands

First Stage: Day-ahead PBDR

Hourly demands prediction with PBDR enabled

Hourly wind turbine and PV outputs prediction

Second Stage: Hourly micro-turbine outputs adjustment

Two-Stage Robust Optimization (TSRO) model

$$\min_{\mathbf{x}} \mathbf{c}^T \mathbf{x} + \max_{\mathbf{u}} \min_{\mathbf{y}} \mathbf{d}^T \mathbf{y} + \mathbf{e}^T \mathbf{u}$$

s.t.

$$A\mathbf{x} \geq \mathbf{b}$$

$$\mathbf{y} \in O(\mathbf{x}, \mathbf{u}) = \{\mathbf{F}\mathbf{x} + \mathbf{G}\mathbf{y} \leq \mathbf{v}, \mathbf{H}\mathbf{x} + \mathbf{I}\mathbf{y} + \mathbf{J}\mathbf{u} = \mathbf{w}\}$$

$$\mathbf{u} \in U$$

Objective function

$$\begin{aligned} \min_{\alpha} -C_{rev}^{pr} + \max_{R_{WT}, R_{PV}, R_D^{unc}} \min_{P_{MT}, V, P, Q} C_{MT} + C_{WT} + C_{PV} \\ + C_{grid} - C_{rev}^{unc}. \end{aligned}$$

Uncertainty modeling – uncertainty set

$$\begin{aligned} U_{WT} = \{R_{WT,n,t} \in \mathbb{R}^{n_{wt}} : \\ \mu_{WT,l} \leq \frac{\sum_{n \in N_{WT}} \sum_{t \in T} R_{WT,n,t}}{\sum_{n \in N_{WT}} \sum_{t \in T} R_{WT,n,t}^{pr}} \leq \mu_{WT,u}, \\ R_{WT,n,t}^{low} \leq R_{WT,n,t} \leq R_{WT,n,t}^{up}, \forall n, t\}, \end{aligned}$$

$$\begin{aligned} U_{PV} = \{R_{PV,n,t} \in \mathbb{R}^{n_{pv}} : \\ \mu_{PV,l} \leq \frac{\sum_{n \in N_{PV}} \sum_{t \in T} R_{PV,n,t}}{\sum_{n \in N_{PV}} \sum_{t \in T} R_{PV,n,t}^{pr}} \leq \mu_{PV,u}, \\ R_{PV,n,t}^{low} \leq R_{PV,n,t} \leq R_{PV,n,t}^{up}, \forall n, t\}, \end{aligned}$$

$$\begin{aligned} U_{LD} = \{P_D^{unc} \in \mathbb{R}^{n_{ld}} : \\ \mu_{LD,l} \leq 1 + \frac{1}{n_i n_t} \sum_{i \in N_D} \sum_{t \in T} \sum_{j \in J} \alpha_{j,t} R_{D,i,j,t}^{unc} \leq \mu_{LD,u}, \\ R_{D,i,j,t}^{low} \leq 1 + R_{D,i,j,t}^{unc} \leq R_{D,i,j,t}^{up}, \forall i, j, t\}. \end{aligned}$$

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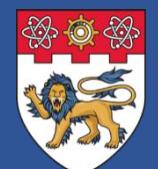
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▪ Robustly Coordinated Energy Management Day-ahead Price-based Demand Response & Hourly-ahead Microturbine

Modelling for Price-based DR

(9)*

$$C_{rev} = C_{rev}^{pr} + C_{rev}^{unc}$$

(10)*

$$C_{rev}^{pr} = \sum_{t \in T} \sum_{i \in N_D} P_{D,i,t}^{pr} \sum_{j \in J} \alpha_{j,t} L_j P_{r,j}$$

(11)*

$$C_{rev}^{unc} = \sum_{t \in T} \sum_{i \in N_D} P_{D,i,t}^{pr} \sum_{j \in J} \alpha_{j,t} L_j P_{r,j} R_{D,i,j,t}^{unc}$$

(12)*

$$\alpha_{j,t} \in \{0, 1\}, \forall j, t$$

(13)*

$$\sum_{j \in J} \alpha_{j,t} = 1, \forall t$$

(14)*

$$\sum_{t \in T} \sum_{i \in N_D} P_{D,i,t}^{pr} \sum_{j \in J} \alpha_{j,t} L_{j,t} P_{r,j,t} \leq \sum_{t \in T} \sum_{i \in N_D} P_{D,i,t}^{pr} P_{r_0,t}$$

(15)*



- Considering the characteristics of the uncertain load demands, in (9), the revenue from the demands is split into two parts i.e. the predicted revenue based on the predicted load demands and the uncertain revenue difference from the predicted one.
- Constraints (10) and (11) support the calculation functions of these two revenue items respectively.
- Constraint (12) denotes the decision variable for each PBDR level is binary.
- Constraint (13) guarantees that only one PBDR level decision can be carried out for each hour.
- Constraint (14) and (15) guarantees the bills for the customers cannot increase and the energy which the customers can use cannot decrease. These mean that the proposed PBDR does not reduce the customers' economic benefits.

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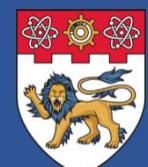
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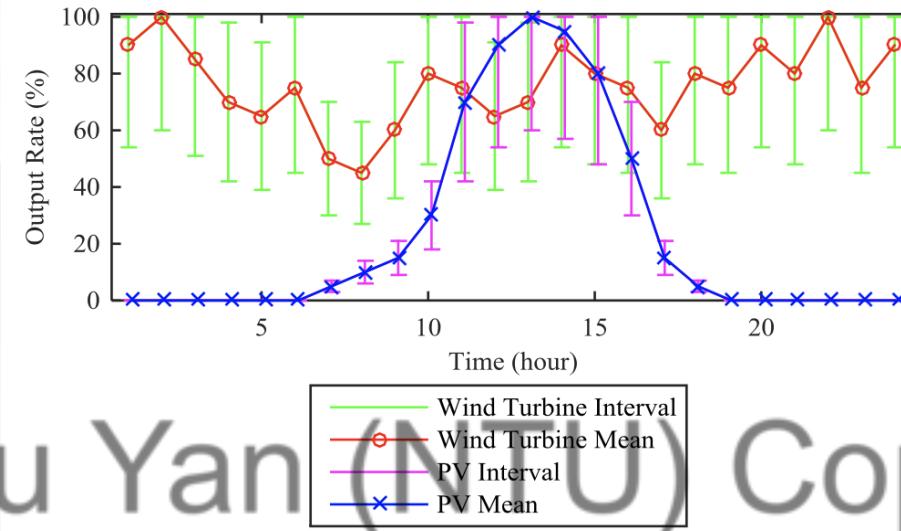
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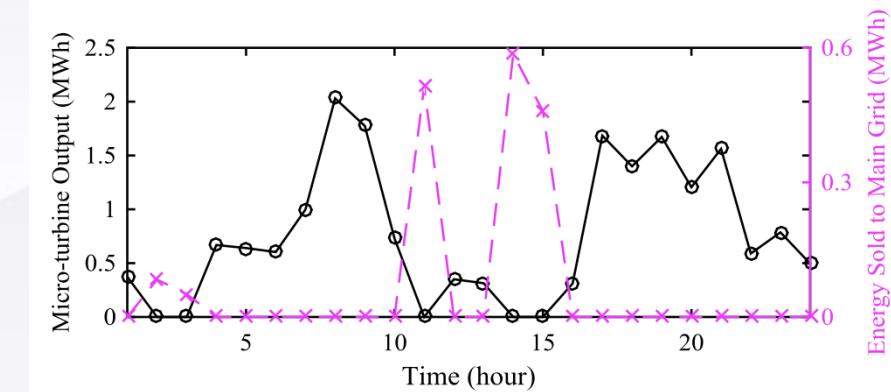


- Robustly Coordinated Energy Management
- Day-ahead Price-based Demand Response & Hourly-ahead Microturbine

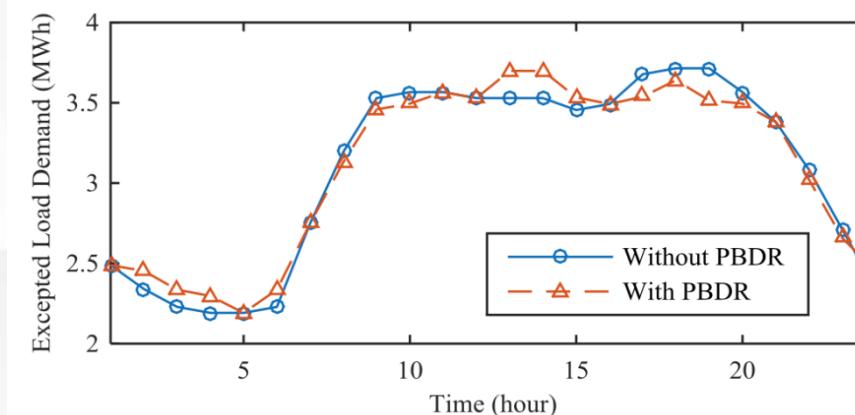
Day-ahead Interval Prediction



Hourly Microturbine Dispatch



Day-ahead PBDR Decision



Strategy	Average Profit (\$)	Micro-Turbine Generation (MWh)	Energy Bought from Main Grid (MWh)	Energy Sold to Main Grid (MWh)	Average Maximal Voltage Deviation (%)	TSRO beat Single in profit (%)	TSRO beat Single in voltage deviation (%)
Deviation Group 1: $\sigma_{WT} = 5\%M_{WT}$; $\sigma_{PV} = 5\%M_{PV}$; $\sigma_D = 1\%M_D$							
TSRO	3484.56	18.148	0.000	0.704	1.51%	100%	85.2%
Single	3465.65	17.612	0.970	1.225	1.52%		
Deviation Group 2: $\sigma_{WT} = 10\%M_{WT}$; $\sigma_{PV} = 10\%M_{PV}$; $\sigma_D = 2\%M_D$							
TSRO	3479.21	18.514	0.000	0.796	1.52%	100%	93.6%
Single	3437.12	17.612	1.989	1.970	1.60%		
Deviation Group 3: $\sigma_{WT} = 20\%M_{WT}$; $\sigma_{PV} = 20\%M_{PV}$; $\sigma_D = 4\%M_D$							
TSRO	3464.49	19.564	0.009	1.055	1.54%	100%	99.5%
Single	3378.48	17.612	4.064	3.246	1.83%		

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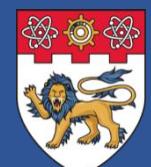
4. Hierarchy coordination

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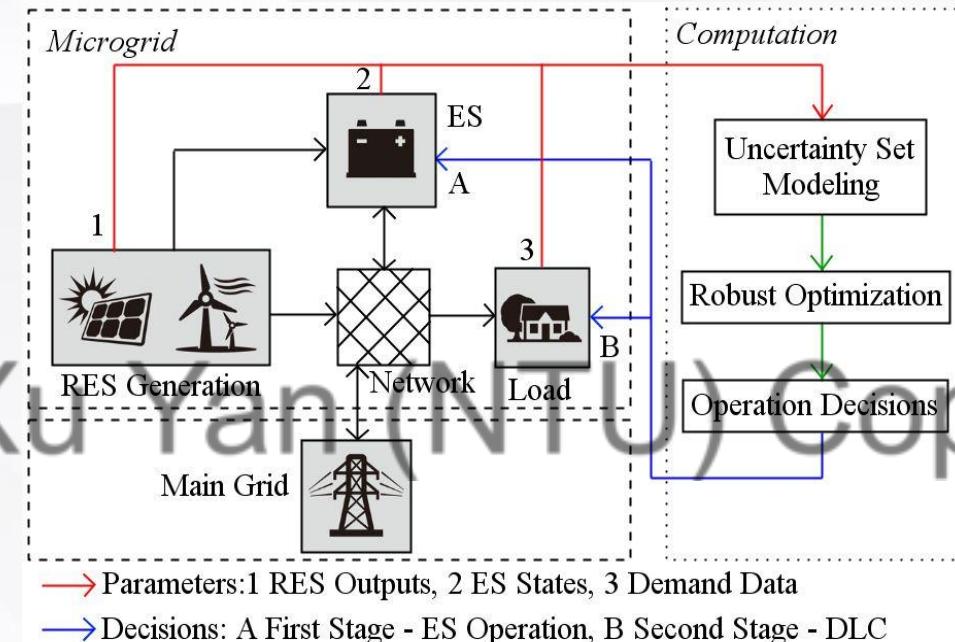
6. Planning

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- Robustly Coordinated Energy Management
- Hourly-ahead energy storage & 15min-ahead direct load control (DLC)

Two-stage coordination framework



Two-stage robust optimization model

$$\min_{\alpha_{dis}, \alpha_{ch}} C_{ES} + \max_{P_{WT}, P_{PV}, K_{DLC}, V, P, Q \in O} \min_{C_{WT} + C_{PV} + C_{grid}} - C_{rev}$$

ESS economic model

$$C_{ES,dis}E_{dis} + C_{ES,ch}E_{ch} = C_{ES,OM}E_{stored}.$$

$$E_{stored} = \eta_{dis}E_{dis} = \eta_{ch}E_{ch}, \eta_{dis} > 1, \eta_{ch} < 1.$$

$$\frac{C_{ES,dis}}{\eta_{dis}} + \frac{C_{ES,ch}}{\eta_{ch}} = C_{ES,OM}.$$

ESS operation model

$$P_{ES,dis,m} = P_{dis,m}^{\max} \sum_{j \in J_{dis}} \alpha_{dis,m,j} L_{dis,m,j}. \quad P_{ES,ch,m} = P_{ch,m}^{\max} \sum_{j \in J_{ch}} \alpha_{ch,m,j} L_{ch,m,j}.$$

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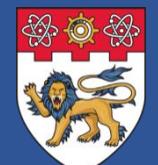
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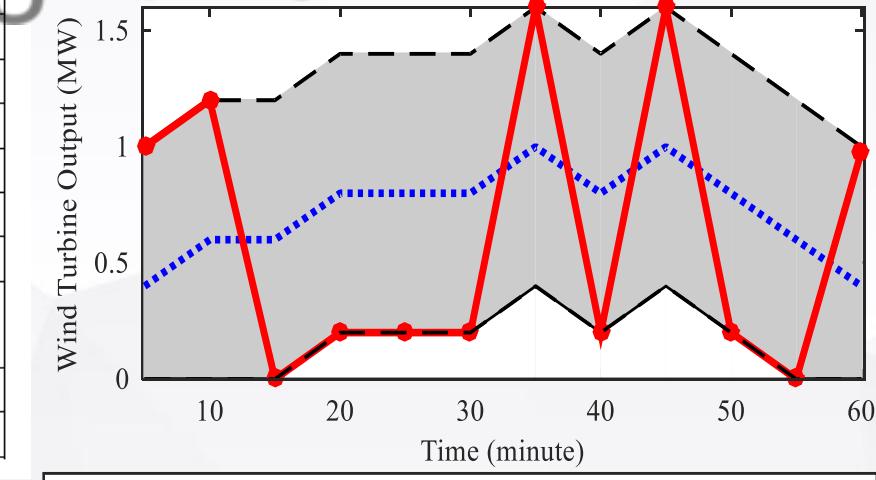
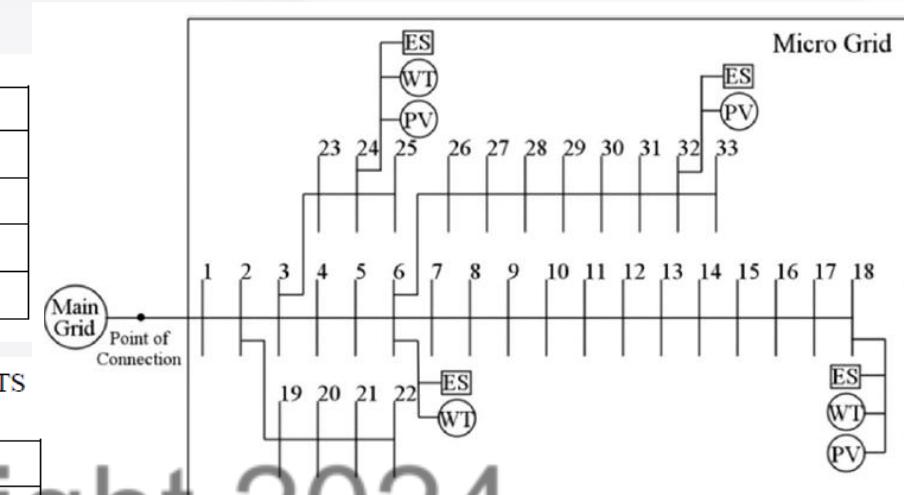
- Robustly Coordinated Energy Management
- Hourly-ahead energy storage & 15min-ahead direct load control (DLC)

UNCERTAINTY BUDGET SETS UNDER TESTS

Test No	1	2	3	4	5	6
$\mu_{WT,l}$	95%	90%	85%	80%	75%	70%
$\mu_{WT,u}$	105%	110%	115%	120%	125%	130%
$\mu_{PV,l}$	97.5%	95%	92.5%	90%	87.5%	85%
$\mu_{PV,u}$	102.5%	105%	107.5%	110%	112.5%	115%

SOLUTION RESULTS FOR BASE CASE UNDER DIFFERENT UNCERTAINTY SETS

	Test No	1	2	3	4	5	6
ES Discharging	ES 1	0%	10%	0%	10%	10%	10%
	ES 2	0%	0%	10%	0%	0%	0%
	ES 3	20%	20%	40%	20%	40%	40%
	ES 4	30%	20%	20%	30%	30%	30%
DLC under Worst Case	0-15 min	0%	0%	0%	0%	0%	0%
	15-30 min	46%	0%	43%	39%	38%	38%
	30-45 min	0%	0%	0%	0%	31%	0%
	45-60 min	3%	6%	2%	2%	0%	0%
Profit under Worst Case (\$)		192.39	187.94	184.45	179.86	177.30	174.29
Iteration Number		5	5	3	3	3	2
Solution Time (s)		61.39	15.96	12.04	13.84	18.34	7.01



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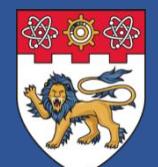
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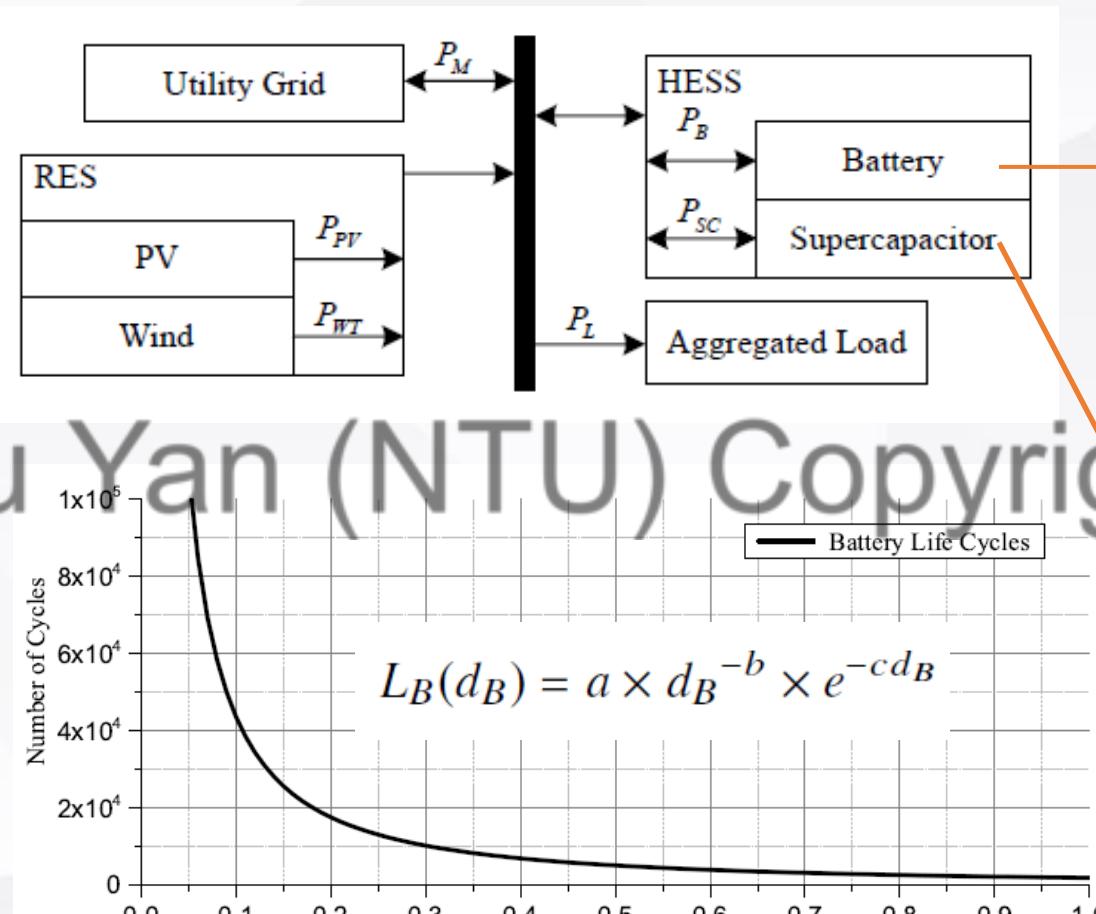
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Two-Stage Dispatch of Hybrid Energy Storage considering battery health



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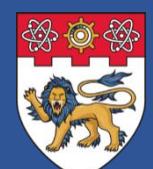
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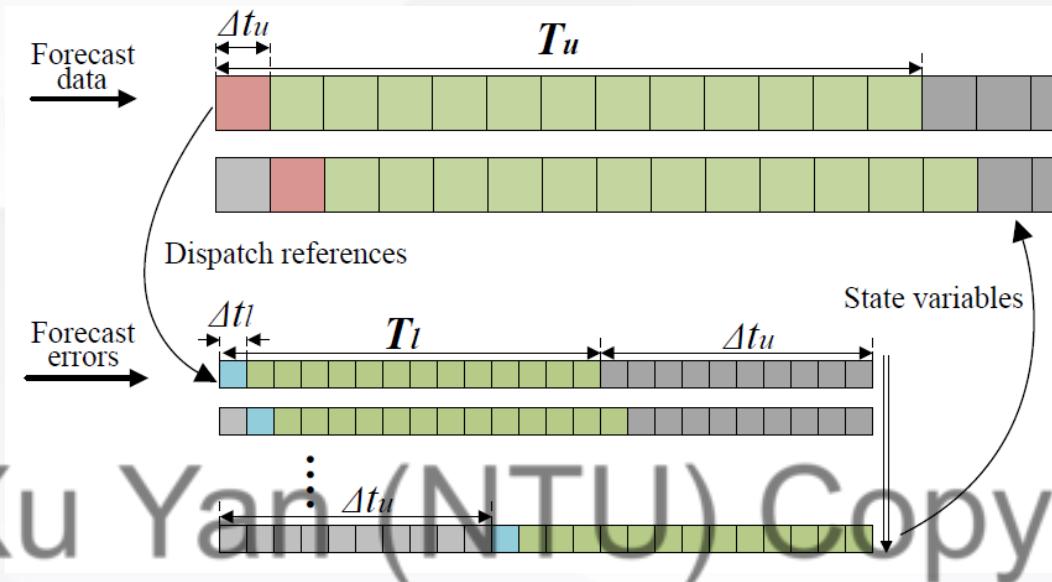
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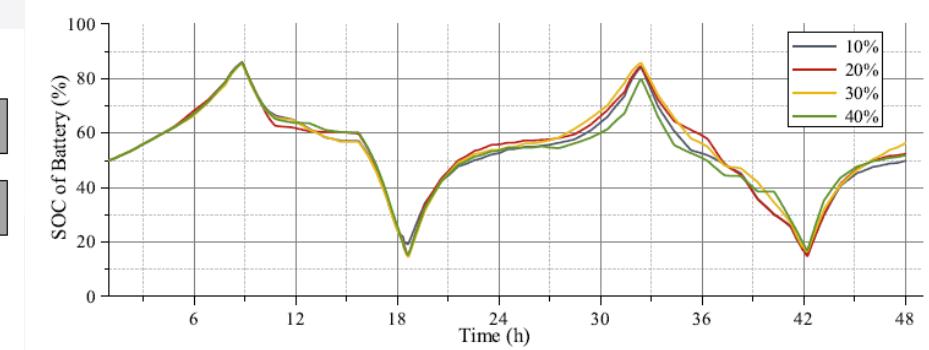
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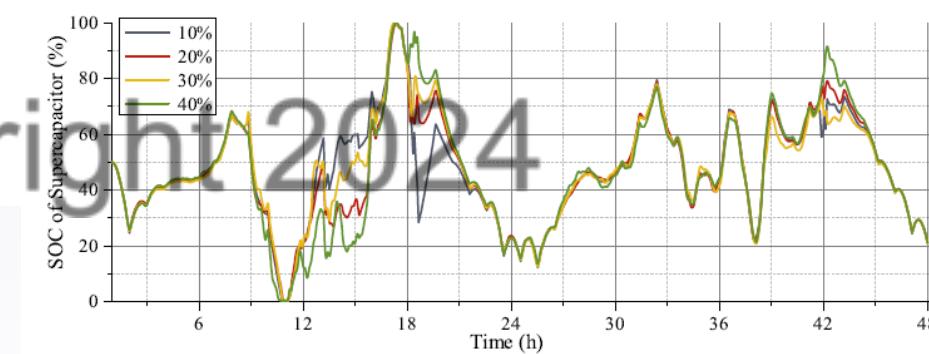
Two-Stage Dispatch of Hybrid Energy Storage considering battery health



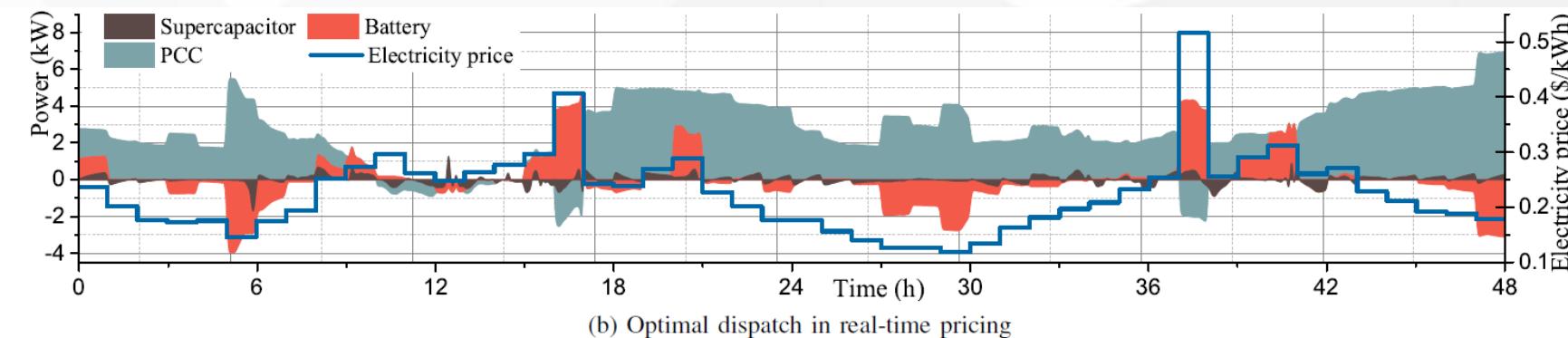
- ✓ First-stage: battery dispatch with SOH degradation cost
- ✓ Second-stage: supercapacitor dispatch



(a) SOC of battery



(b) SOC of supercapacitor



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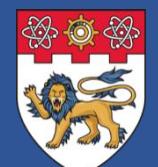
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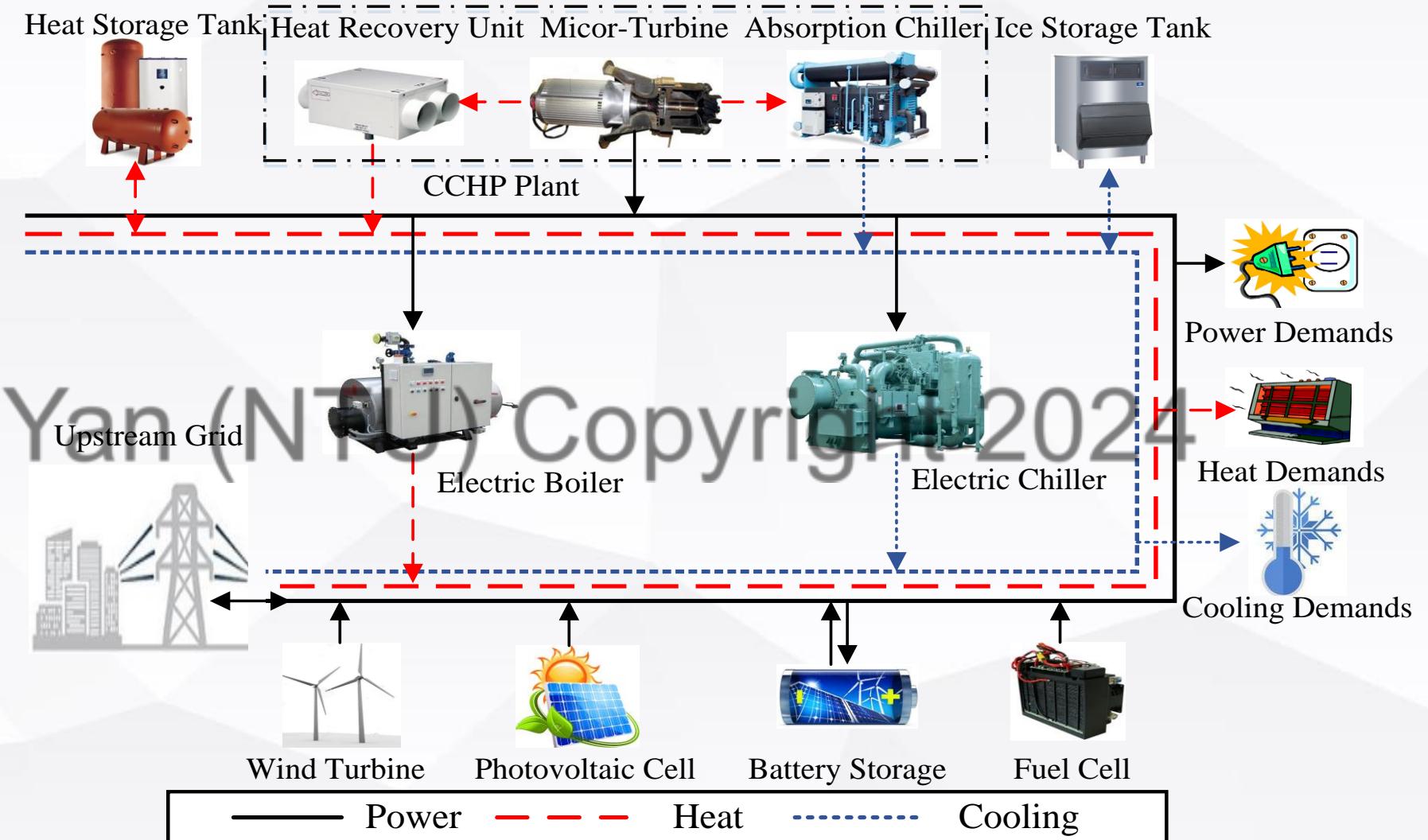
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Multi-Energy Microgrid



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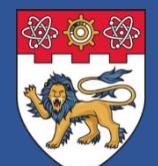
4. Hierarchy coordination

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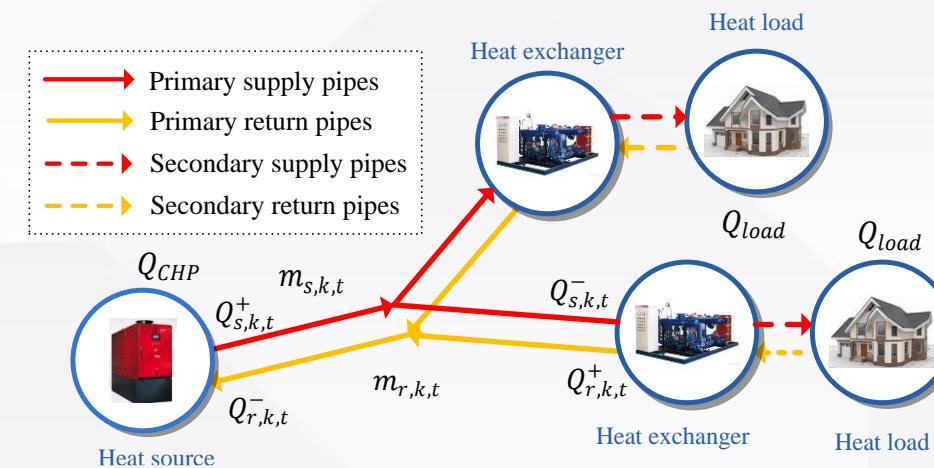
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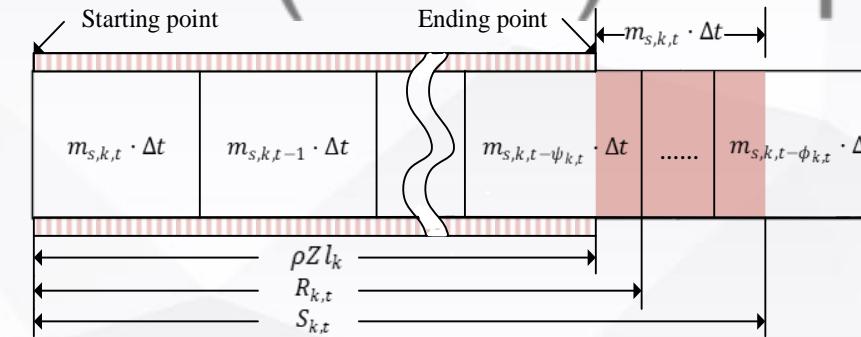
- 1) DG planning
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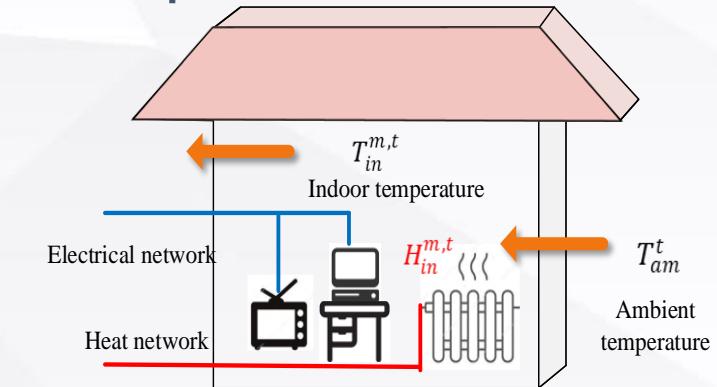
Multi-Energy Microgrid – Modeling of thermal part



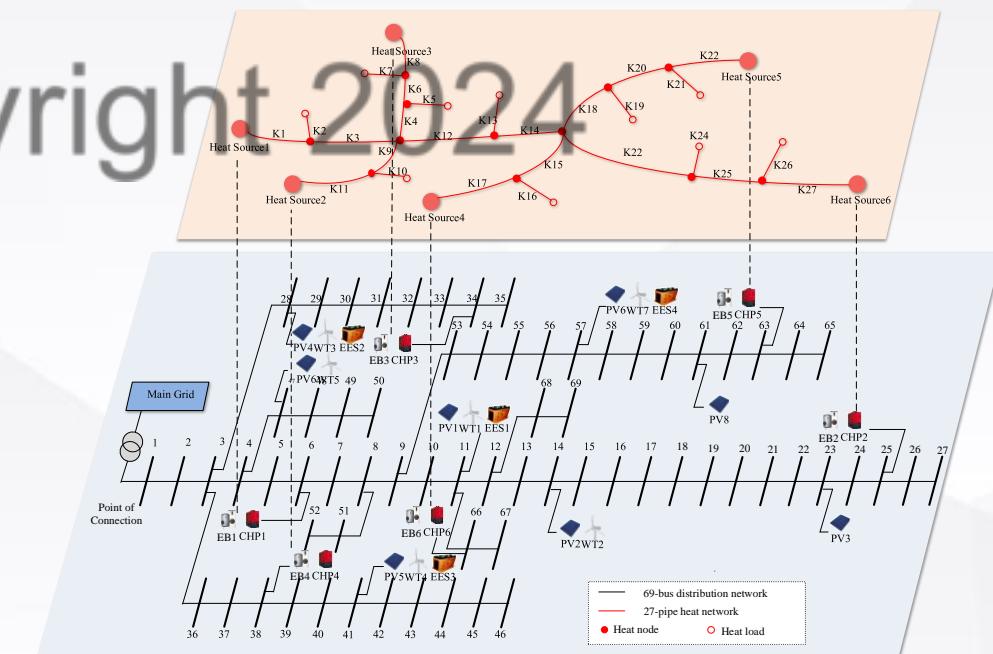
District Heat Network



Vertical section of a pipe



Thermal conduction of a building



Coupled electric-thermal network

Y. Chen, Y. Xu*, Z. Li, "Optimally Coordinated Dispatch of Combined-Heat-and-Electrical Network," *IET Gen. Trans. & Dist.*, 2019.

Z. Li and Y. Xu*, "Optimal coordinated energy dispatch for a multi-energy microgrid in grid-connected and islanded modes," *Applied Energy*, 2017. Web-of-Science Highly Cited Paper & 2018 Applied Energy Highly Cited Paper Award

1. REIDS Project

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- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

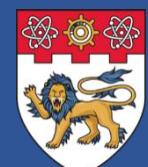
4. Hierarchy coordination

5. Trading

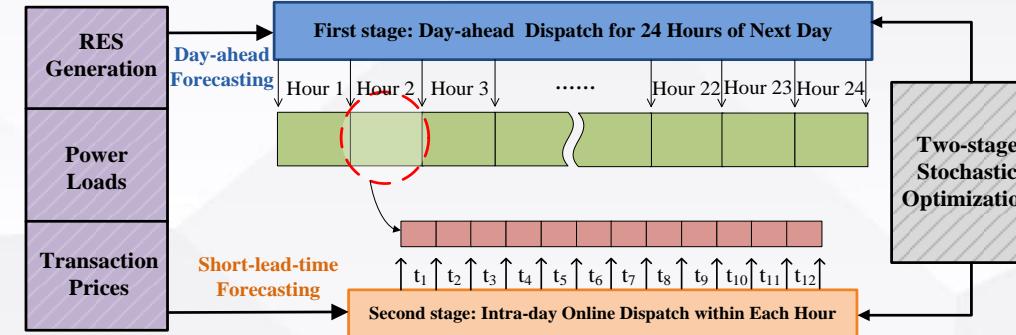
- 1) Centralized trading
- 2) P2P trading

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm



■ Multi-Energy Dispatch – Two-Stage Coordinated Operation



Temporally-coordinated Stochastic Operation Framework

$$\text{MIN } F_G = C_{FC} + C_{OM} + C_{EX} + C_{ST} + C_{SD} - C_{HR}$$

$$C_{FC} = \sum_{t \in N_T} \sum_{i \in N_M} (\gamma_G P_{MT}^{t,i} / \eta_{MT}^{t,i}) \Delta t$$

$$C_{EX} = \sum_{t \in N_T} (\gamma_B P_{BUY}^{t,1} - \gamma_S P_{SELL}^{t,1}) \Delta t$$

$$C_{OM} = \sum_{t \in N_T} \sum_{i \in N_W} [\gamma_{WT} P_{WT}^{t,i} + \dots + \sum_{i \in N_H} \gamma_{TST} (P_{TSTC}^{t,i} + P_{TSTD}^{t,i})] \Delta t$$

$$C_{ST} = \sum_{t \in N_T} \sum_{i \in (N_M \cup N_E)} \max\{0, U_{CG}^{t,i} - U_{CG}^{t-1,i}\} C_{CG}^U$$

$$C_{SD} = \sum_{t \in N_T} \sum_{i \in (N_M \cup N_E)} \max\{0, U_{CG}^{t-1,i} - U_{CG}^{t,i}\} C_{CG}^D$$

$$C_{HR} = \sum_{t \in N_T} \sum_{i \in N_M} \gamma_{HR} H_L^{t,i} \Delta t$$

$$\min_{z, y_1, y_2 \dots y_n} F(z) + \sum_{n \in N_S} \chi_n L(y_n)$$

$$\text{s.t. } z \in F_A$$

$$y_n \in \Omega(z, \omega_n), \forall n$$

Two-Stage Stochastic Optimization model

$$U_{CG}^{t,i} \cdot P_{CG}^{min,i} \leq P_{CG}^{t,i} \leq U_{CG}^{t,i} \cdot P_{CG}^{max,i}$$

$$R_{CG}^{down,i} \Delta t \leq P_{CG}^{t,i} - P_{CG}^{t-1,i} \leq R_{CG}^{up,i} \Delta t$$

$$1 - \Delta V_{BUS}^{\max} \leq V_{BUS}^{t,i} \leq 1 + \Delta V_{BUS}^{\max}$$

$$P_{PF}^{t,b+1} = P_{PF}^{t,b} - P_{PF}^{t,0,b+1} - P_L^{t,i} + \dots - P_{PT}^{t,i}, b \in Br(i), \forall i, t$$

$$Q_{PF}^{t,b+1} = Q_{PF}^{t,b} - Q_{PF}^{t,0,b+1} - Q_L^{t,i}, b \in Br(i), \forall i, t$$

$$V_{BUS}^{t,i+1} = V_{BUS}^{t,i} - (R^b P_{PF}^{t,b} + X^b Q_{PF}^{t,b}) / V_0, b \in Br(i, i+1), \forall i, t$$

$$H_L^{t,i} = H_{MT}^{t,i} + H_{PT}^{t,i} + P_{TSTD}^{t,i} - P_{TSTC}^{t,i}$$

$$\xi_{ES}^{min,i} Cap_{ES}^i \leq E_{ES}^{t,i} \leq \xi_{ES}^{max,i} Cap_{ES}^i$$

1. REIDS Project

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- 2) Volt/Var regulation

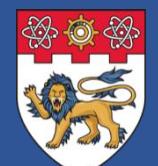
4. Hierarchy coordination

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- 2) P2P trading

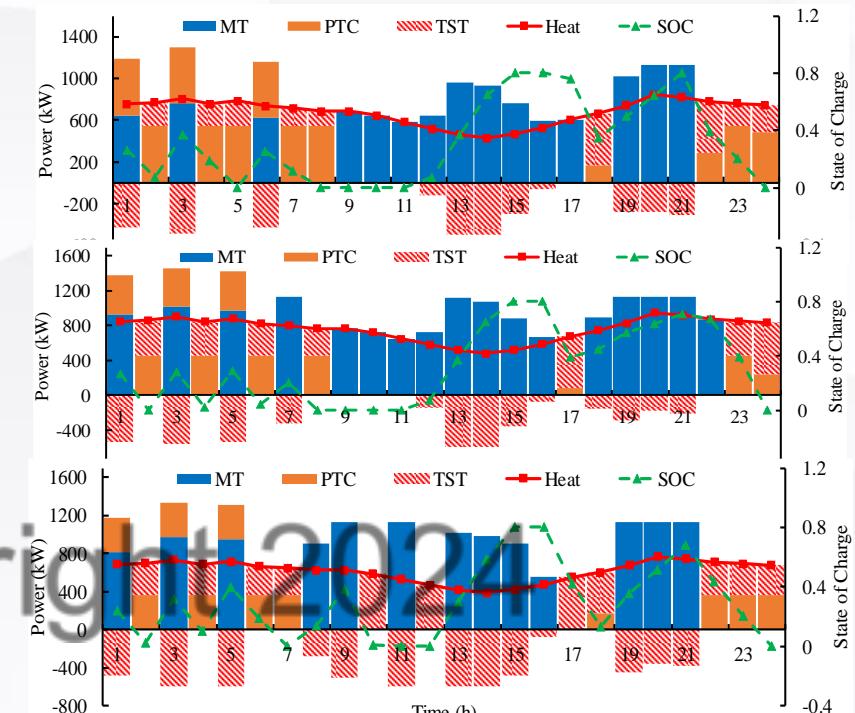
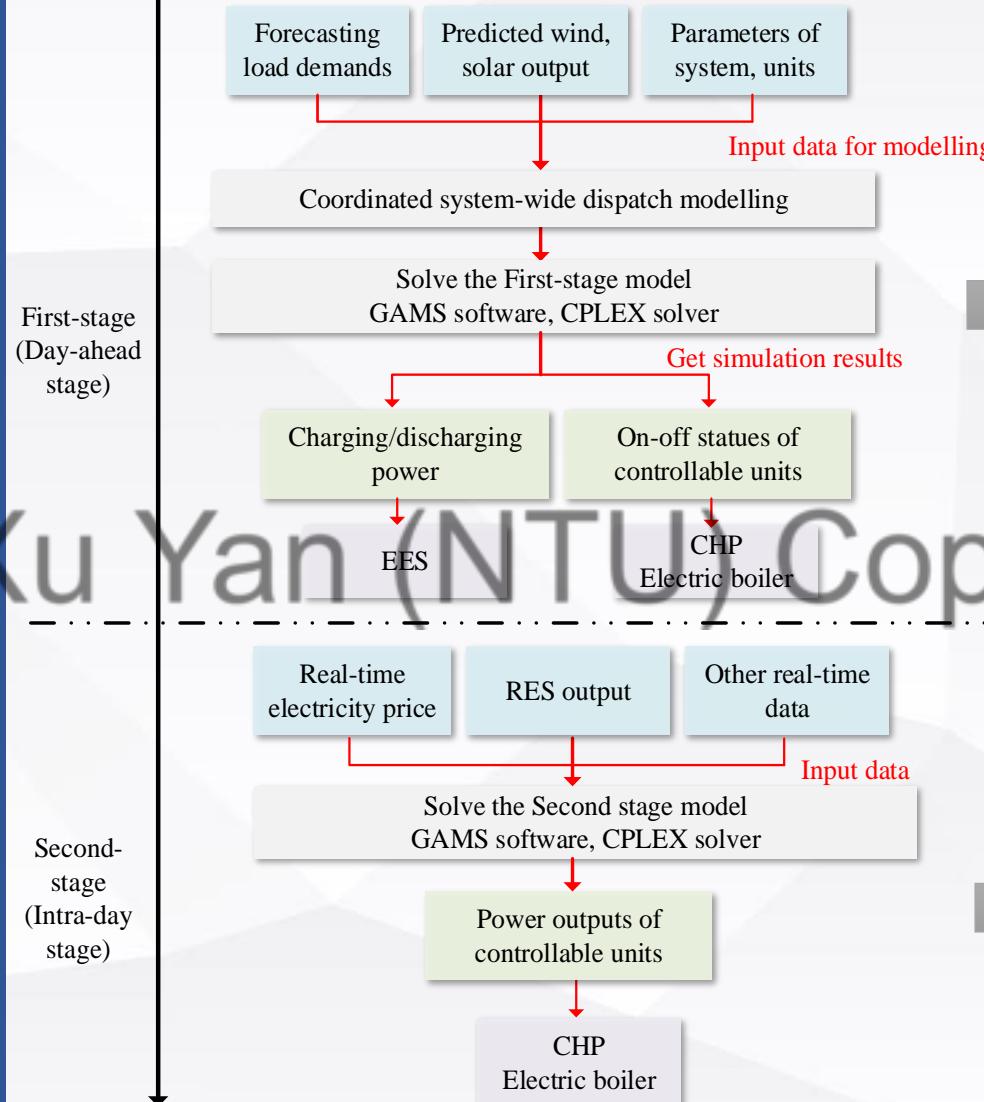
6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm

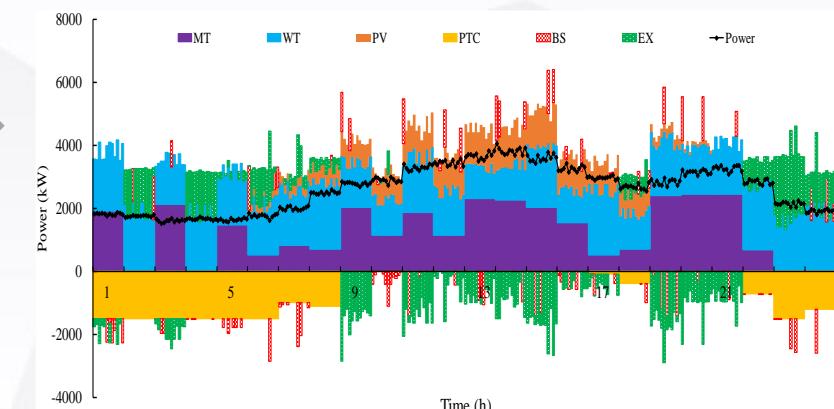


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Multi-Energy Dispatch – Two-Stage Coordinated Operation



Day-ahead dispatch results



Intra-day dispatch results

Z. Li and Y. Xu*, "Temporally-Coordinated Optimal Operation of a Multi-energy Microgrid under Diverse Uncertainties," *Applied Energy*, 2019.

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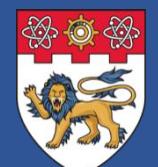
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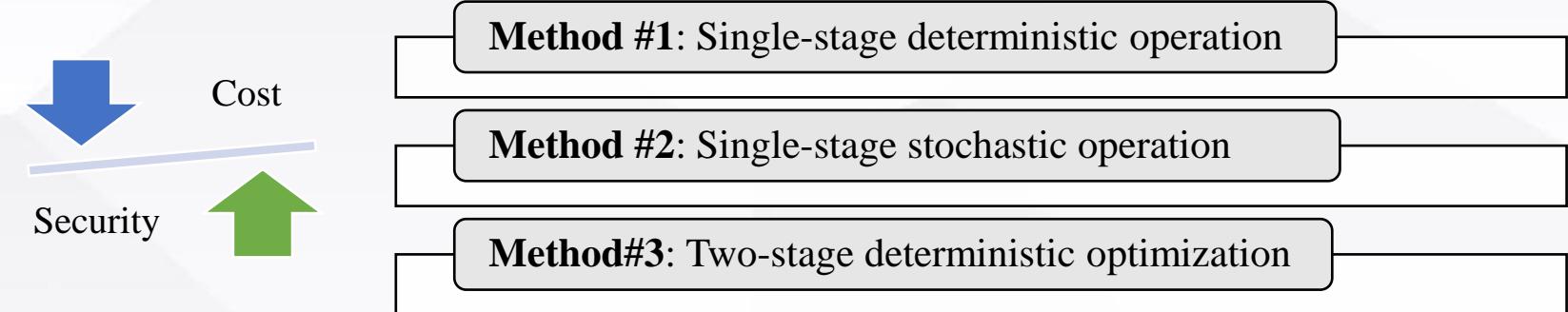
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Multi-Energy Dispatch – Two-Stage Coordinated Operation



Item	Method #1	Method #2	Method #3	Our Method
Uncertainty level 1 (Lower Uncertainty)				
Average cost (\$)	2183.46	2149.65	2468.20	2440.22
Average voltage violation (%)	30.40	16.50	0	0
Uncertainty level 2 (Medium Uncertainty)				
Average Cost (\$)	2218.89	2188.97	2483.19	2450.78
Average voltage violation (%)	74.70	49.80	0	0
Uncertainty level 3 (High Uncertainty)				
Average Cost (\$)	2341.64	2282.66	2556.04	2508.65
Voltage violation (%)	97.20	77.90	0	0

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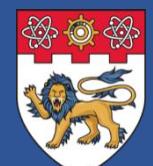
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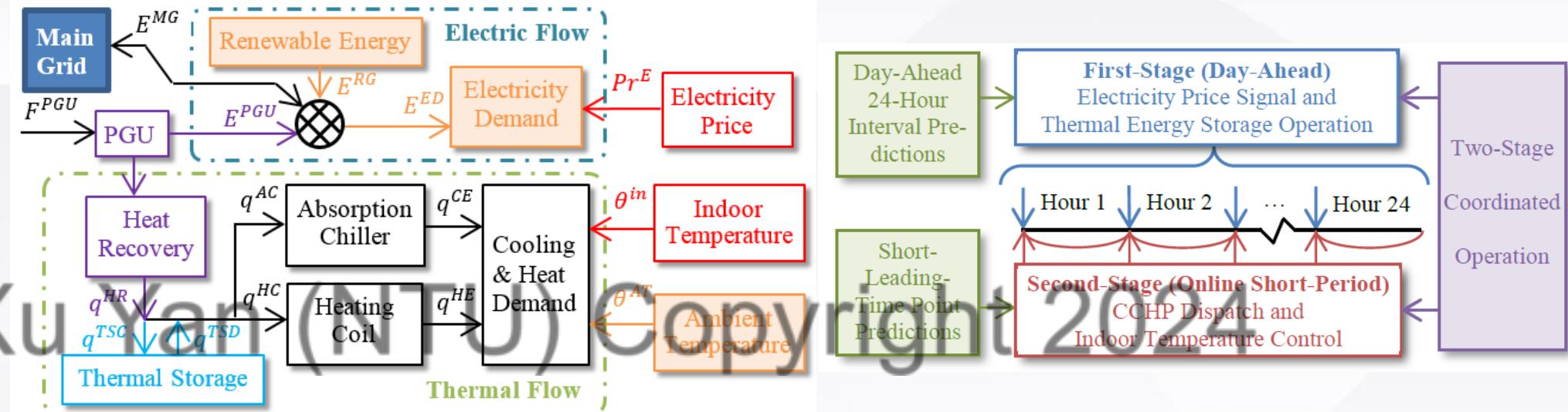
- 1) Centralized trading
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- Multi-Energy Demand Response
indoor temperature control (thermal load) and **price-based DR (electric load)**
to counteract uncertain renewable power generation, load, and ambient temperature



Day-ahead robust optimization model

$$\begin{aligned} & \min_x \max_u \min_y (C_{CCHP} + C_{OM} + C_{grid} - C_{rev}^e - C_{rev}^{thm}) \quad (48) \\ & \text{s.t.} \quad (10)-(47) \end{aligned}$$

Intra-day optimization model

$$\begin{aligned} & -C_{rev}^e + \min_y (C_{CCHP} + C_{OM} + C_{grid} - C_{rev}^{thm}) \quad (49) \\ & \text{s.t.} \quad (10)-(14), (25)-(46) \end{aligned}$$

- 1) x is the *first-stage control variables*, denoting the day-ahead operation decisions including the electricity price $\alpha_{j,t}$ as well as the thermal storage operation state $\beta_{m,t}^{TSC/D}$ and $q_{m,t}^{TSC/D}$;
- 2) y is the *second-stage control variables*, expressing the intra-day operation decisions including the CCHP electric power output $P_{m,t}^{CCHP}$ and the indoor temperature setpoint $\theta_{m,k,t}^{in}$;
- 3) u is the *uncertain variables* which include the renewable power outputs $P_{n,t}^{WT/PV}$, the electric load demand $P_{0,i,t}^{ED}$ and the ambient temperature $\theta_{m,k,t}^{am}$.

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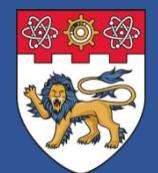
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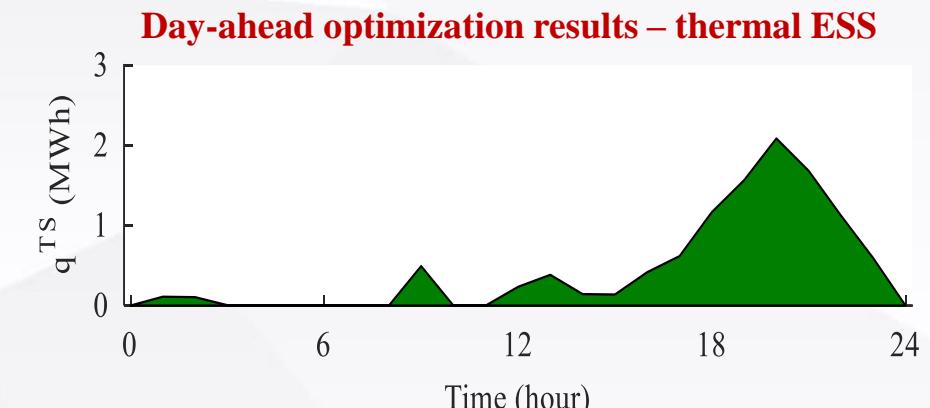
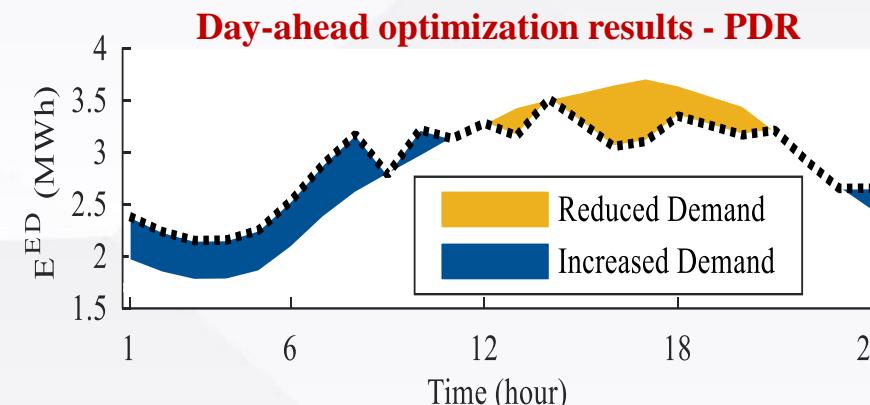
- 1) Centralized trading
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6. Planning

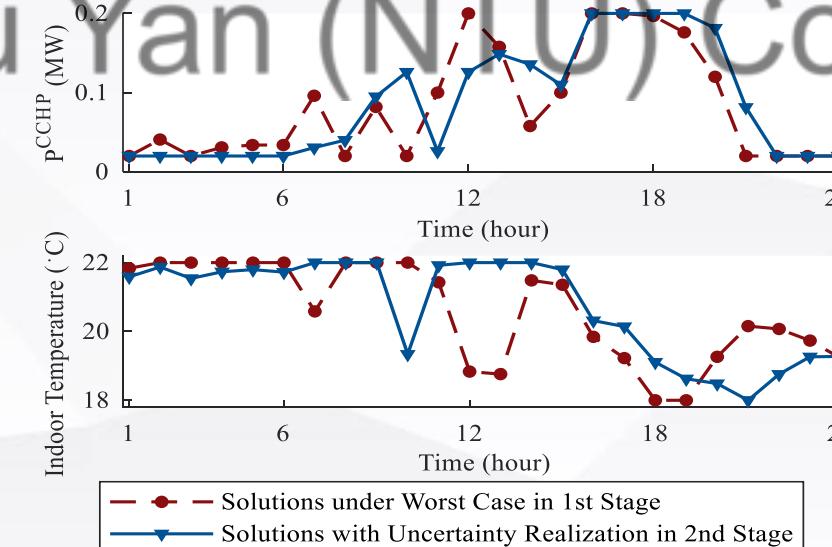
- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm



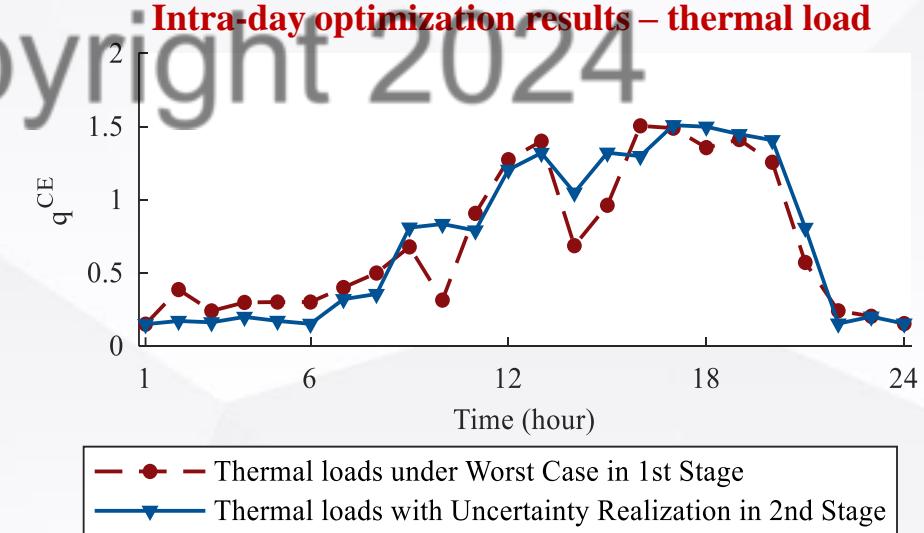
■ Multi-energy demand response



Intra-day results – CCHP and indoor temperature



Intra-day optimization results – thermal load



1. REIDS Project

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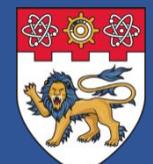
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▪ Robustness VS Conservativeness

Robustness:

Possibility of a feasible solution (or no operating constraint violation) whatever uncertainties realize (**Advantage**)

- Full Robustness: Always a feasible solution

Conservativeness:

Compromise in optimization process when considering uncertainties (**Drawback**)

Design of Uncertainty Budgets

- Larger Budgets
 - > Higher Robustness
 - > Higher Conservativeness
- Uncertainty Degree Analysis

Robustness under Different Uncertainty Budgets

UNCERTAINTY SETS WITH DIFFERENT UNCERTAINTY BUDGETS

Uncertainty Set Group No	$\underline{\mu}^{PV}$	$\bar{\mu}^{PV}$	$\underline{\mu}^{EL}$	$\bar{\mu}^{EL}$	$\underline{\mu}^{HE}$	$\bar{\mu}^{HE}$
1	0.95	1.05	0.98	1.02	0.99	1.01
2	0.9	1.1	0.96	1.04	0.98	1.02
3	0.8	1.2	0.94	1.06	0.97	1.03

FEASIBILITY CHECK RESULTS IN ISLANDED MODE

Method	Deterministic Method	Proposed Robustly Coordinated Operation		
Uncertainty Set Group No	N. A.	1	2	3
Optimized Total Operating Cost in Day-Ahead Stage (\$)	5993	6387	6586	6822
MCS Group 1: $\sigma^{PV} = 5\% \hat{P}^{PV}$, $\sigma^{EL} = 2\% \hat{P}^{EL}$, $\sigma^{HE} = 1\% \hat{q}^{HE}$				
Average Total Operating Cost of Feasible Cases (\$)	6020	6036	6044	6034
Infeasible Case Rate (%)	0.1%	0.0%	0.0%	0.0%
MCS Group 2: $\sigma^{PV} = 10\% \hat{P}^{PV}$, $\sigma^{EL} = 4\% \hat{P}^{EL}$, $\sigma^{HE} = 2\% \hat{q}^{HE}$				
Average Total Operating Cost of Feasible Cases (\$)	6051	6056	6064	6052
Infeasible Case Rate (%)	12.5%	1.6%	1.0%	0.0%
MCS Group 3: $\sigma^{PV} = 20\% \hat{P}^{PV}$, $\sigma^{EL} = 8\% \hat{P}^{EL}$, $\sigma^{HE} = 4\% \hat{q}^{HE}$				
Average Total Operating Cost of Feasible Cases (\$)	6097	6095	6103	6087
Infeasible Case Rate (%)	25.9%	6.5%	5.7%	0.0%

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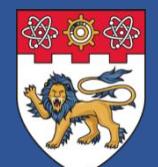
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5. Trading

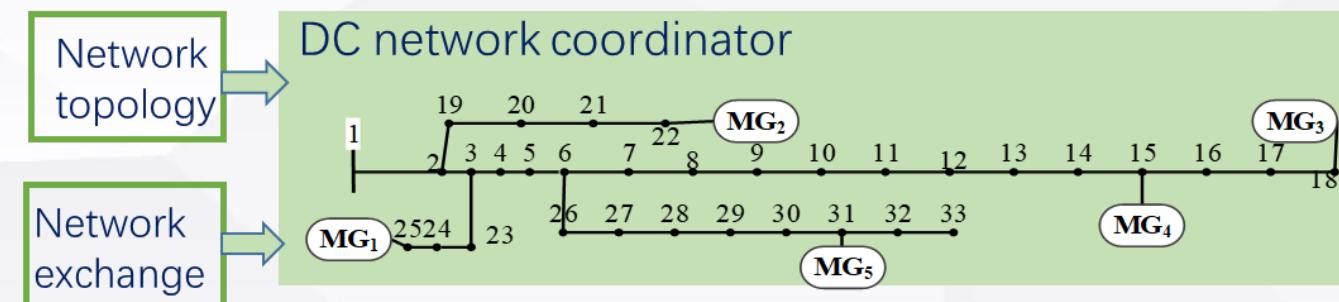
- 1) Centralized trading
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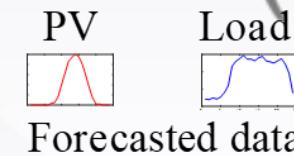
- 1) DG planning
- 2) ESS planning
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▪ Robustly Coordinated Energy Management Distributed robust optimization for Networked-Hybrid AC/DC Microgrids



Interval forecasting
Uncertainty modeling



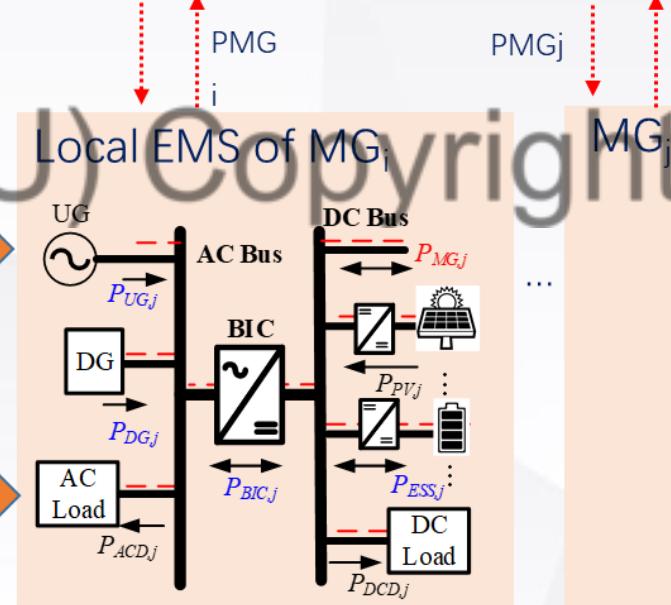
Affinely adjustable robust optimization

$$p_{UG,i}(t) = P_{UG,i}(t) - \beta_{UG,i}(t)\xi_i(t), \forall t \in \mathcal{T}$$

$$p_{DG,i}(t) = P_{DG,i}(t) - \beta_{DG,i}(t)\xi_i(t), \forall t \in \mathcal{T}$$

$$p_{ESS,i}(t) = P_{ESS,dc,i}(t) - P_{ESS,c,i}(t) - \beta_{ESS,i}(t)\xi_i(t), \forall t \in \mathcal{T}$$

$$\beta_{DG,i} + \beta_{UG,i} + \beta_{ESS,i} = 1, \forall t \in \mathcal{T}$$



Individual MG

$$\begin{aligned} \min_{\mathbf{P}_i(t), \beta_i(t), \forall t \in \mathcal{T}} & \mathbb{E} \sum_{t \in \mathcal{T}} f(\mathbf{P}_i(t), \beta_i(t)) = \\ & \sum_{t \in \mathcal{T}} [a_{DG,0,i} P_{DG,i}^2(t) + a_{DG,1,i} P_{DG,i}(t) + a_{DG,2,i} + \\ & a_{DG,0,i} \beta_{DG,i}^2(t) + b_{PV,i} P_{PV,i}(t) + \lambda(t) P_{UG,i}(t) + \\ & c_{ESS,dc,i} P_{ESS,dc,i}(t) + c_{ESS,c,i} P_{ESS,c,i}(t)] \Delta t \end{aligned}$$

Networked-MG

$$\begin{aligned} \min_{\mathbf{P}_j(t), \beta_j(t), \forall t \in \mathcal{T}} & \mathbb{E} \sum_{t \in \mathcal{T}} \{f(\mathbf{P}_i(t), \beta_i(t)) + \sum_{j:k \rightarrow j} l_{jk}(t) r_{jk}\} \\ & P_{jk}(t), l_{jk}(t), v_{jk}(t), \forall j \in \mathcal{N}, j \rightarrow k, t \in \mathcal{T} \end{aligned}$$

1. Affinely adjustable robust optimization modeling

2. Model convexification

3. Distributed solution based on ADMM

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
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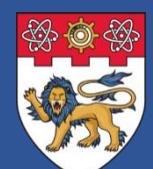
4. Hierarchy coordination

5. Trading

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- 2) P2P trading

6. Planning

- 1) DG planning
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- 3) PRO algorithm



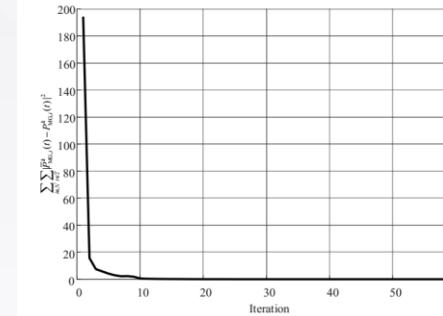
■ Simulation results

A 3 networked microgrid system in an IEEE 4 bus system

Scenario I: centralized deterministic;

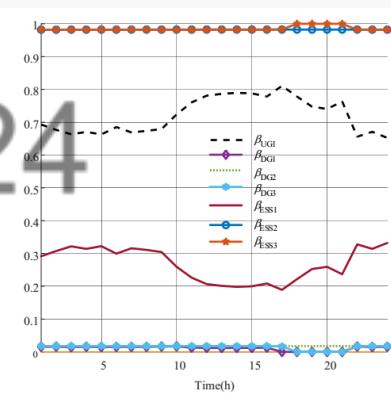
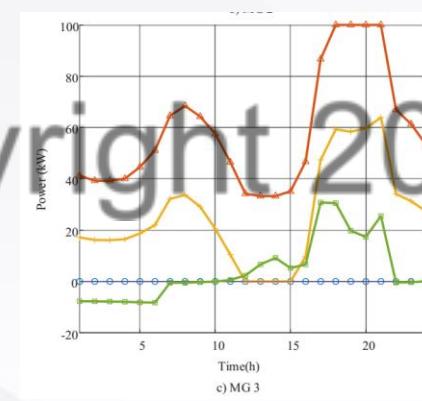
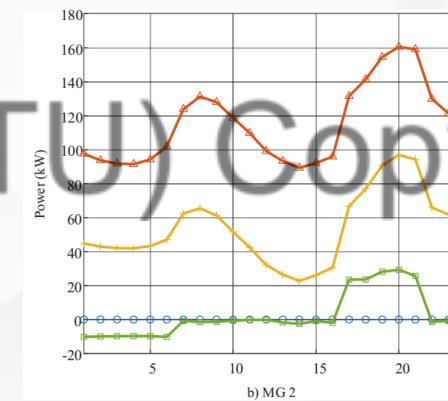
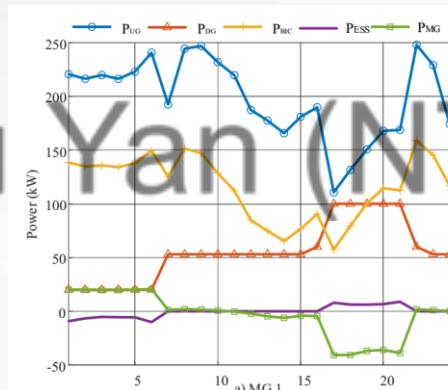
Scenario II: centralized stochastic; (100)

Scenario III: proposed

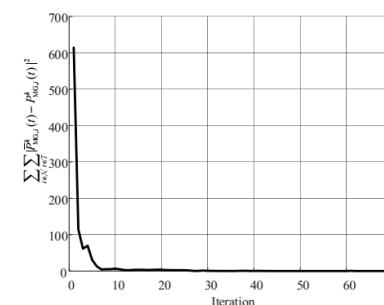
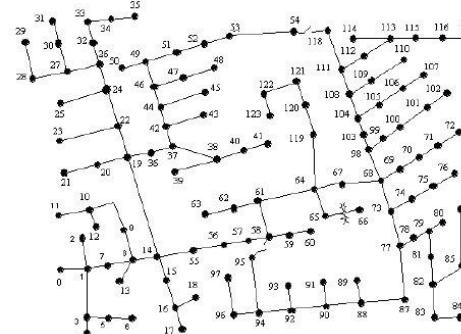


COMPARISON RESULTS UNDER CASE I (A SYSTEM OF THREE NETWORKED MGs)

	Scenario i	II	III
Objective value(\$)	2,484.84	2,483.89	2,580.33
Running time(s)	0.17	308.14	4.85
Number of decision variables	864	2232	2520
Number of constraints	792	73008	1944



A 30 networked microgrid system in a revised IEEE 123 bus system



COMPARISON RESULTS UNDER CASE II(A SYSTEM OF 30 NETWORKED MGs)

	Scenario i	II	III
Objective value(\$)	17,849.00	17,840.87	17,849.24
Running time(s)	1.28	471.37	368.92
Number of decision variables	16008	666168	31848
Number of constraints	13800	734520	23880

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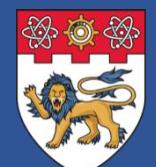
4. Hierarchy coordination

5. Trading

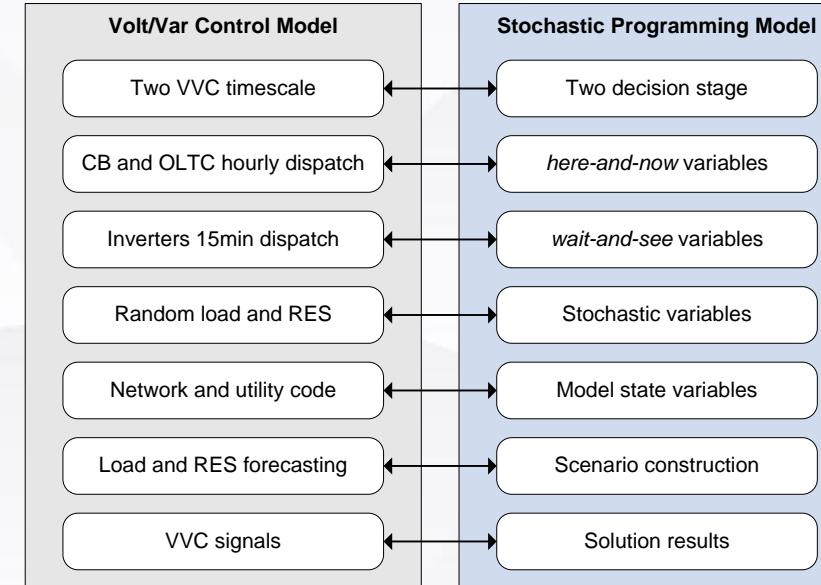
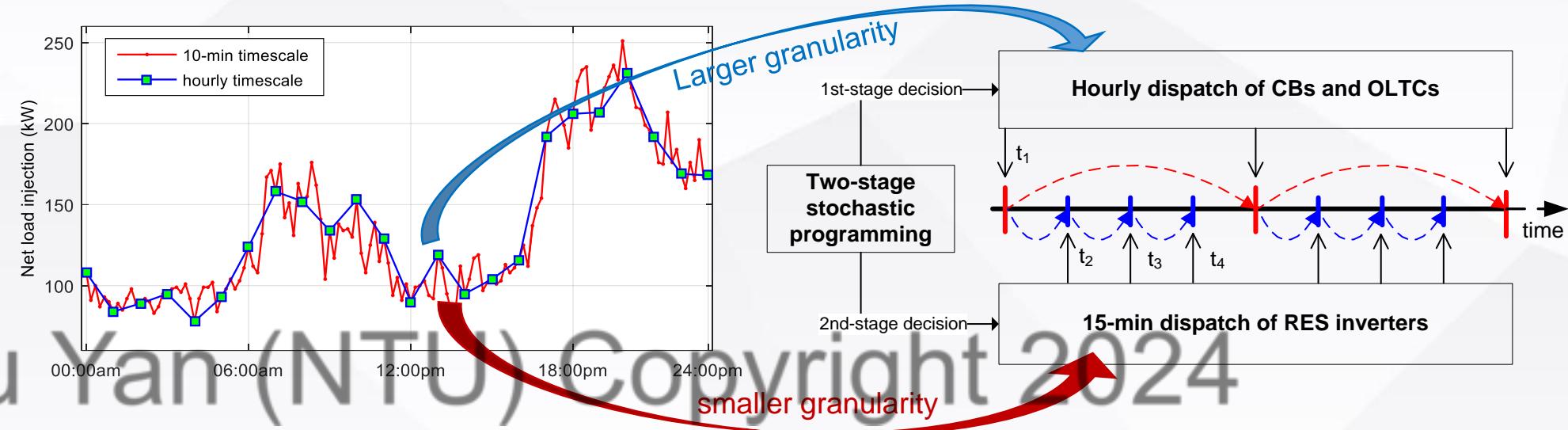
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- Two-stage Coordinated Volt/Var Regulation under uncertainty
Hourly dispatch of CB and OLTC & 15min dispatch of PV inverters



- **First-Stage:** Slow switching devices such as OLTCs and CBs are scheduled one day ahead.
- **Second-Stage:** Fast responding devices such as PV-associated inverters are updated to operate in short time-window.

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■ Mathematical modeling

A. Stochastic Model

The VVC is realized at two coordinated timescales and the mathematical model of (5)–(21) is formulated into a two-stage stochastic programming model as follows:

$$\min_{x \in F} \{f(x) + E [Q(x, \xi)]\} \quad (22)$$

where $f(x)$ is the first-stage problem, i.e., the long-term (hourly timescale) VVC, and x is the first-stage decision vector; $Q(x, \xi)$ is optimal value of the second-stage problem, i.e., the short-term (15-min timescale) VVC: $\min_{y \in \Omega(x, \xi)} g(y)$, where y is the second-stage decision vector, ξ is the random vector, and $E[Q(x, \xi)]$ is the expected value of the second-stage problem.

C. Scenario Construction

The stochastic variations of RES generation and load from their predicted values are assumed to respectively follow the Beta distribution and the normal distribution [5], [6], [20].

The Beta distribution is defined by two shape parameters: α and β which represent the prediction error (stochastic variation) for a predicted power \hat{P} [20]:

$$f_{\hat{P}}(y) = y^{\alpha-1} \cdot (1-y)^{\beta-1} \cdot N \quad (27)$$

where f is the Beta distribution function and y is the occurrence of the active power value, N is the normalization factor.

B. Deterministic Equivalent

Assuming ξ has a finite number of possible realizations, called scenarios, denoted as ξ_1, \dots, ξ_K with respective possibilities of ρ_1, \dots, ρ_k , then the expectation term in (22) can be written as:

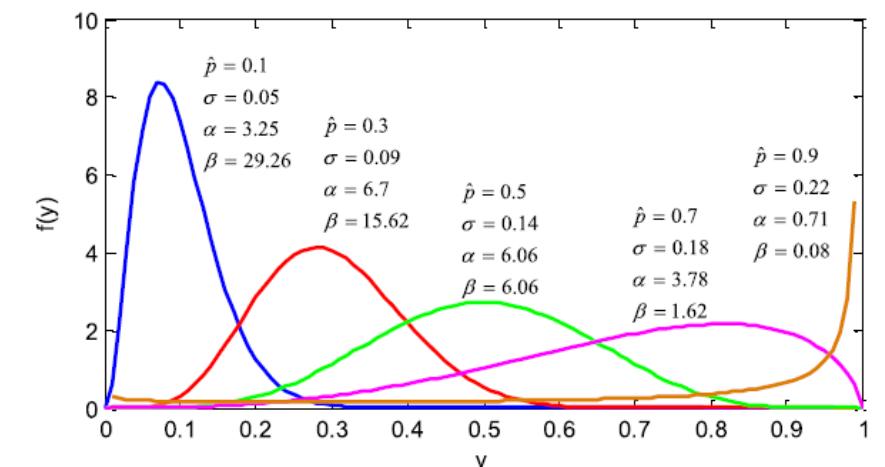
$$E [Q(x, \xi)] = \sum_{k=1}^K \rho_k Q(x, \xi_k) \quad (23)$$

Then, the original two-stage stochastic programming model can be reformulated as the following *deterministic equivalence*:

$$\min_{x, y_1, \dots, y_K} f(x) + \sum_{k=1}^K \rho_k g(y_k) \quad (24)$$

$$\text{s.t. } x \in F \quad (25)$$

$$y_k \in \Omega(x, \xi_k), \forall k \quad (26)$$



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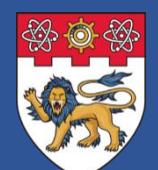
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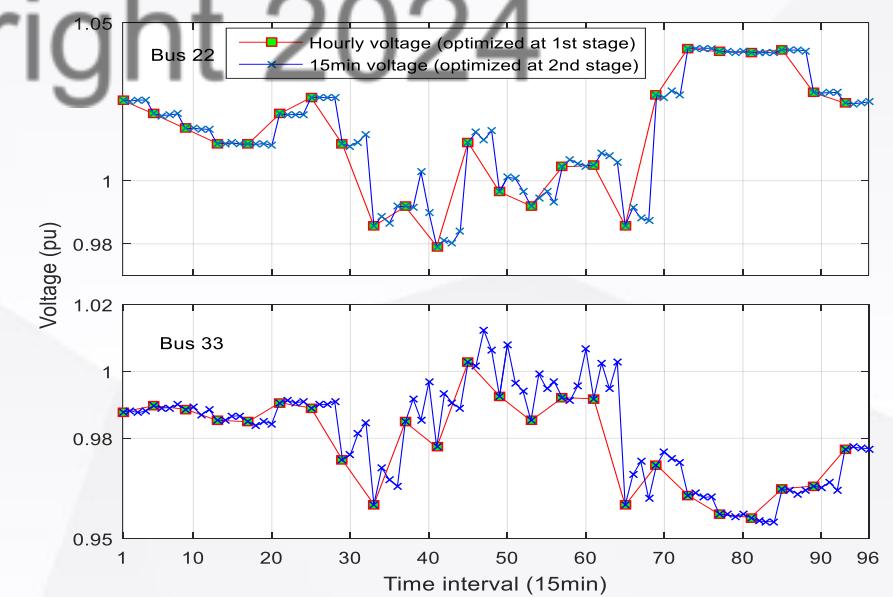
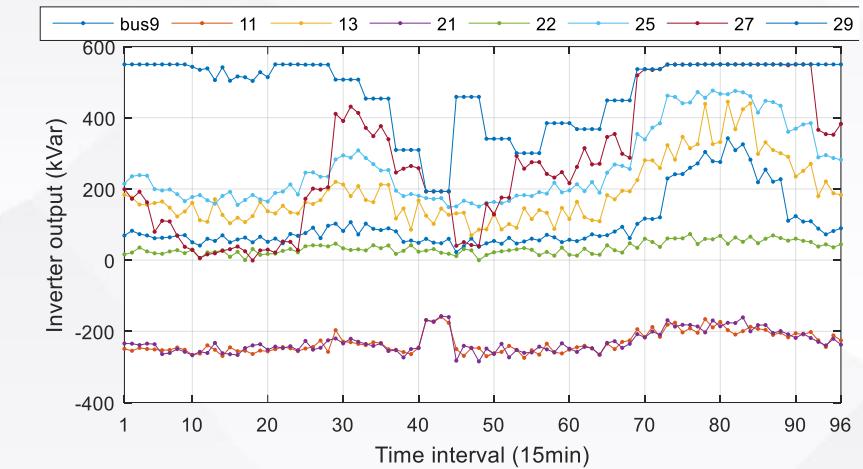
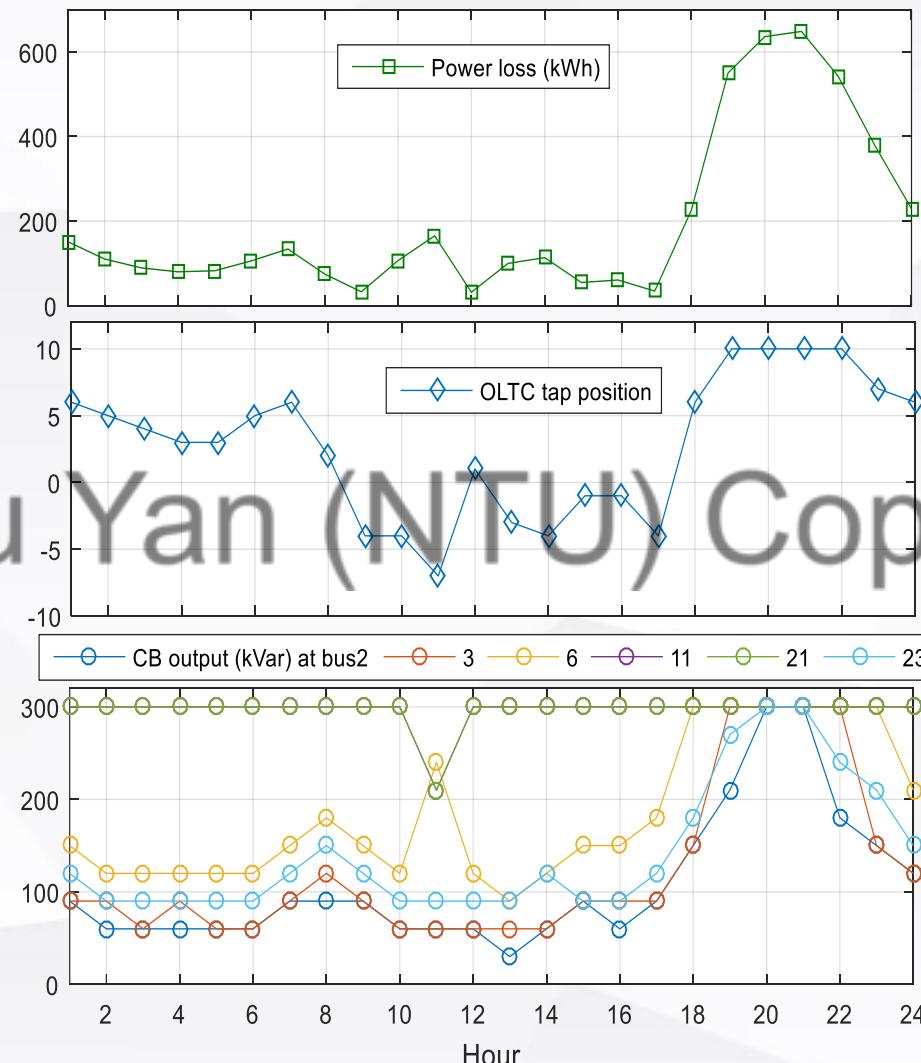
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■ Simulation Results



Y. Xu*, Z.Y. Dong, et al, “Multi-timescale coordinated voltage/var control of high renewable-penetrated distribution networks,” *IEEE Trans. Power Syst.*, 2018.

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

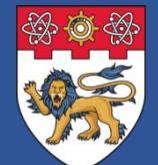
4. Hierarchy coordination

5. Trading

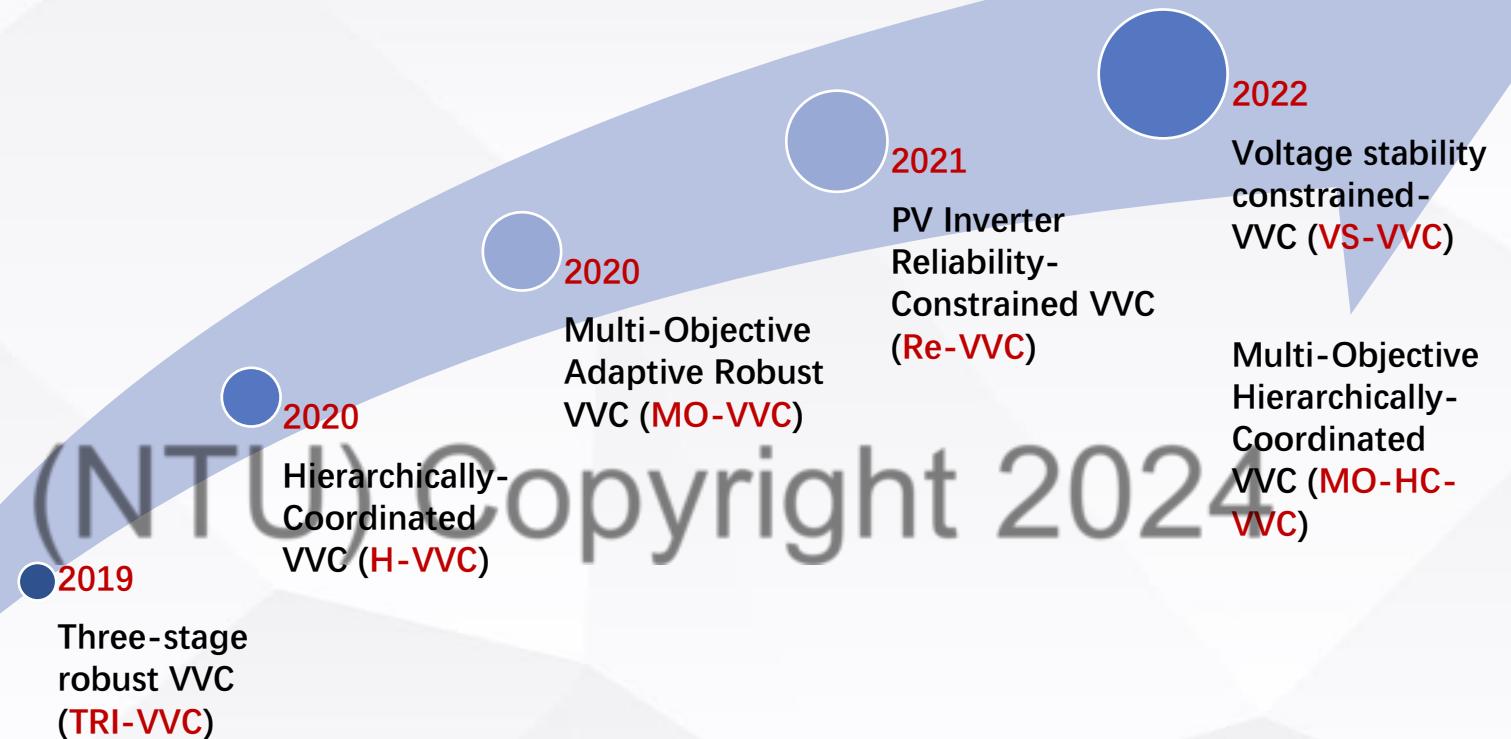
- 1) Centralized trading
- 2) P2P trading

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) PRO algorithm



Continued research in PV Inverter-based Volt/Var Control



- 2019** - C. Zhang, Y. Xu*, Z.Y. Dong, "Three-Stage Robust Inverter-Based Voltage/Var Control for Distribution Networks with High PV," *IEEE Trans. Smart Grid*, 2019. – [Web-of-Science Highly Cited Paper](#)
- 2020** - C. Zhang and Y. Xu*, "Hierarchically-Coordinated Voltage/VAR Control of Distribution Networks using PV Inverters," *IEEE Trans. Smart Grid*, 2020. – [2021 IEEE TSG Outstanding Paper Award](#)
- 2020** - C. Zhang, Y. Xu*, Z.Y. Dong, "Multi-Objective Adaptive Robust Voltage/VAR Control for High-PV Penetrated Distribution Networks," *IEEE Trans. Smart Grid*, 2020.
- 2021** - Q. Chai, C. Zhang, Y. Xu, and Z.Y. Dong, "PV Inverter Reliability-Constrained Volt/Var Control of Distribution Networks," *IEEE Trans. Sustainable Energy*, 2021.
- 2022** - C. Zhang, Y. Xu*, Y. Wang, "Three-Stage Hierarchically-Coordinated Volt-age/Var Control based on PV Inverters Considering Network Voltage Stability," *IEEE Trans. Sustainable Energy*, 2022.
- 2022** - R. Xu, C. Zhang, Y. Xu, Z.Y. Dong, and R. Zhang, "Multi-Objective Hierarchically-Coordinated Volt/Var Control for Active Distribution Networks with Droop-Controlled PV Inverters," *IEEE Trans. Smart Grid*, 2022.

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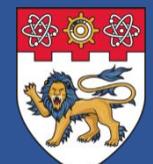
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■ Multi-Objective Adaptive Robust Voltage/VAR Regulation

- Minimizing voltage deviation conflicts with minimizing network power loss.
- Multi-objective “min-max-min” problem

$$\min_x \max_u \min_y [f_1(x, u, y), f_2(x, u, y)]$$

s.t.

$$Ax \geq b$$

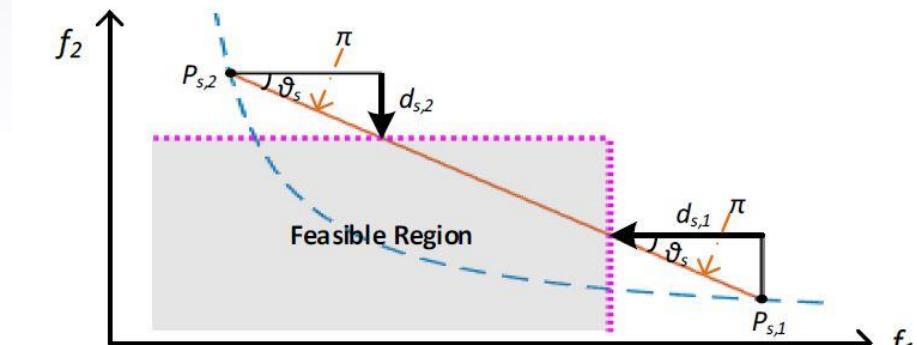
$$Cx + Dy \leq v$$

$$\begin{matrix} Ex + Gy + Hu = w \\ u \in U \end{matrix}$$

Key point:

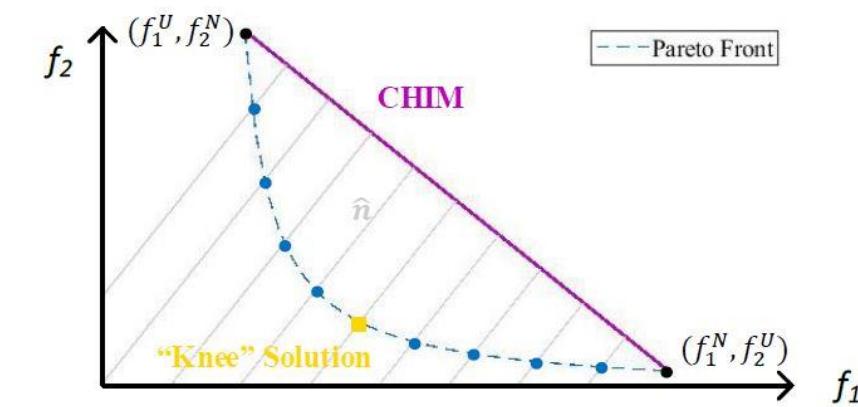
- 1) **Voltage deviation index**: load-weighted voltage deviation index (LVDI)
- 2) **Which MOP algorithm is more efficient** to generate accurate Pareto front and get a fair trade-off?
 - a) Classic Weighted-Sum (CWS)
 - b) Classic ϵ -Constrained (CeC)
 - c) Adaptive Weighted-Sum (AWS)
 - d) Normal Boundary Intersection (NBI)

Adaptive Weighted Sum (AWS)



Reduced feasible region used in AWS algorithm.

Normal Boundary Intersection (NBI)



Pareto front generated by NBI algorithm.

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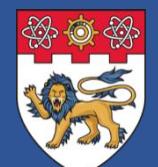
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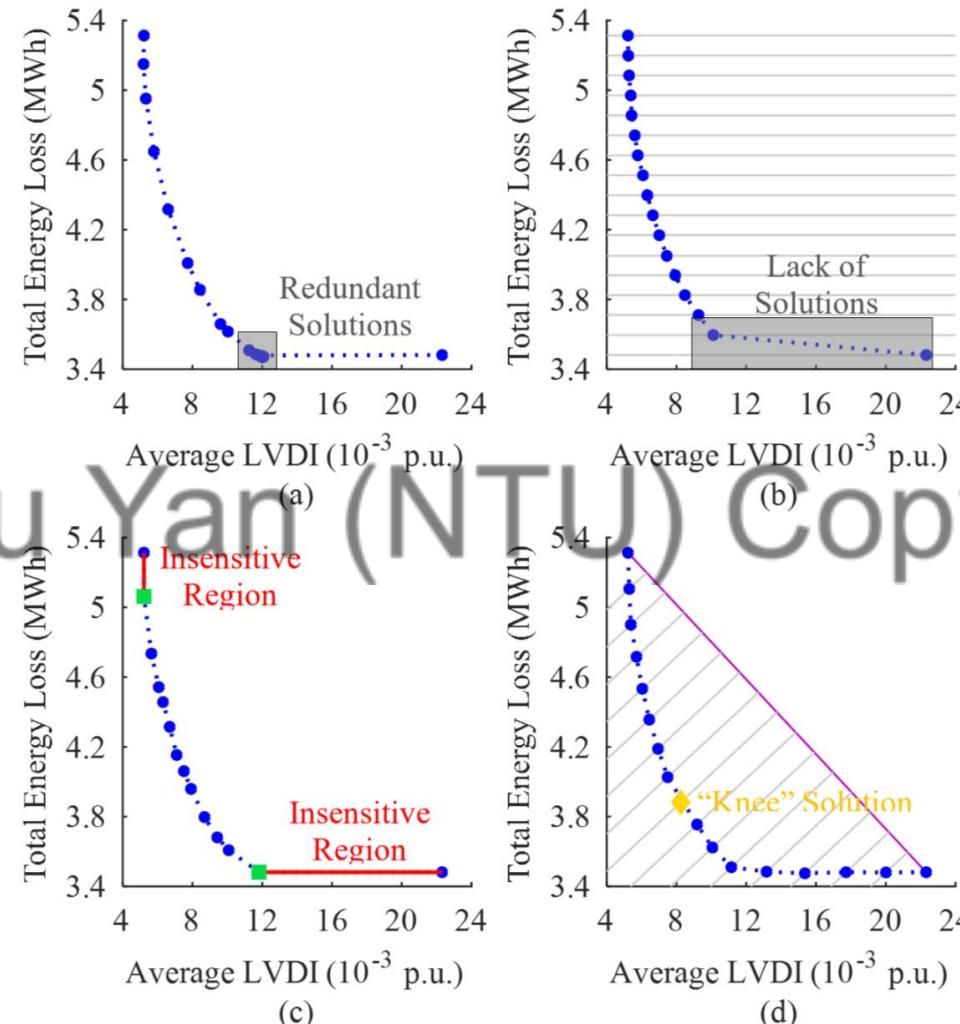
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Multi-Objective Adaptive Robust Voltage/VAR Regulation



(a) CWS; (b) CeC; (c) AWS; (d) NBI

C. Zhang, Y. Xu*, Z.Y. Dong, "Multi-Objective Adaptive Robust Voltage/VAR Control for High-PV Penetrated Distribution Networks," *IEEE Trans. Smart Grid*, 2020.

COMPUTATION EFFICIENCY COMPARISON

Method	CWS	CeC	AWS	NBI
Number of Solutions	17	17	14	17
MOP Processing Time (s)	53	62	44	60
GUROBI Solver Time (s)	569	2344	869	2384
Total Time (s)	622	2406	913	2444

The AWS and NBI algorithms are suggested depending on different optimization requirements.

- ✓ If a relatively accurate Pareto front with high computation efficiency is required, the **AWS** algorithm is preferred.
- ✓ If a more accurate Pareto front with evenly distributed solutions or the “knee” solution is required, the **NBI** algorithm is preferred.

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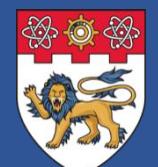
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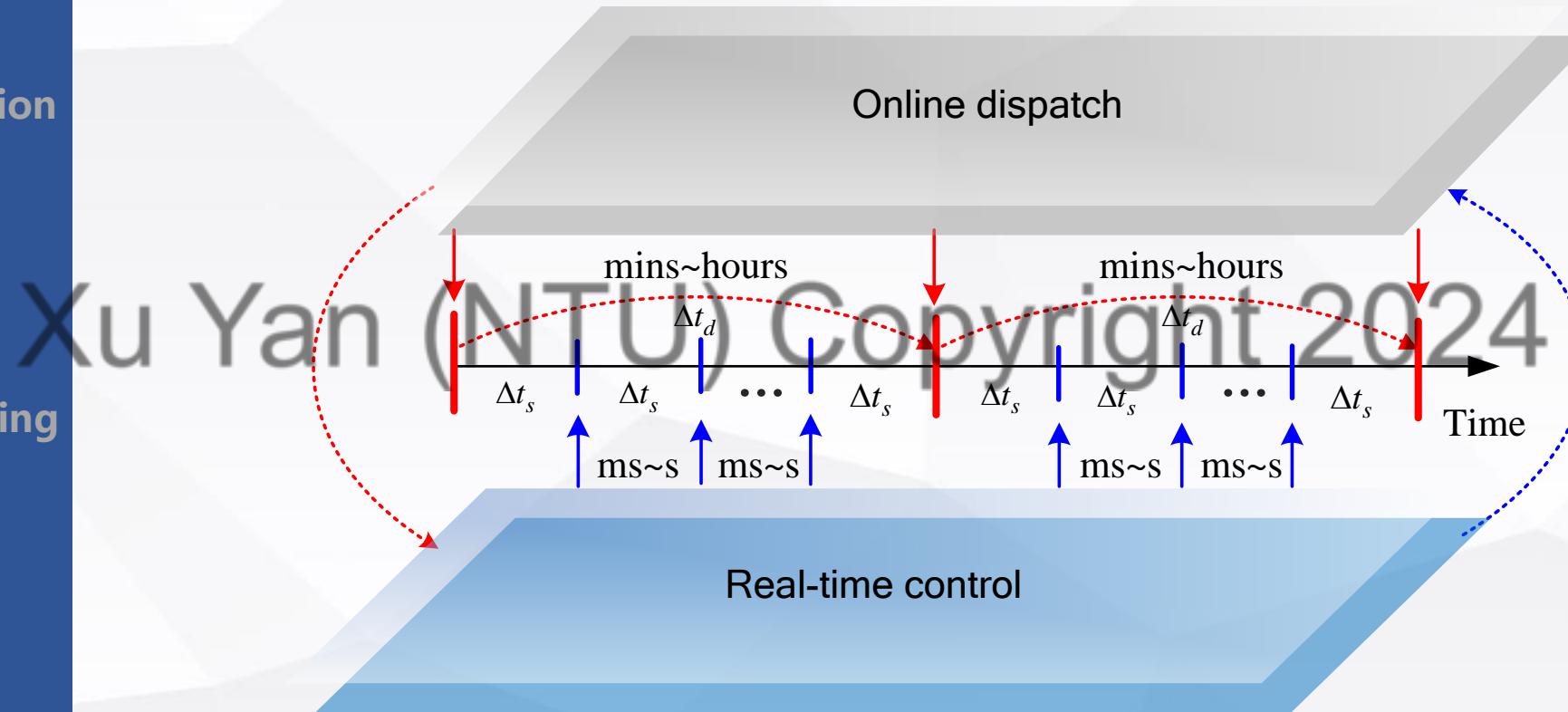
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- Hierarchically coordinated operation and control of DERs
 - ✓ Operational optimization and real-time control are traditionally **decoupled**.
 - ✓ Existing two-stage coordination methods are **all for operational timeframe** (e.g., day-ahead & hourly-ahead or hourly-ahead & 15mins-ahead).



- ✓ Need to coordinate the operation level and control level for enhanced system performance, i.e., **optimizing the operation decisions considering the real-time controllers' effects, or simultaneously optimizing operational variables and controller parameters**.

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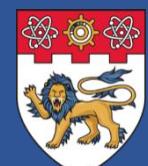
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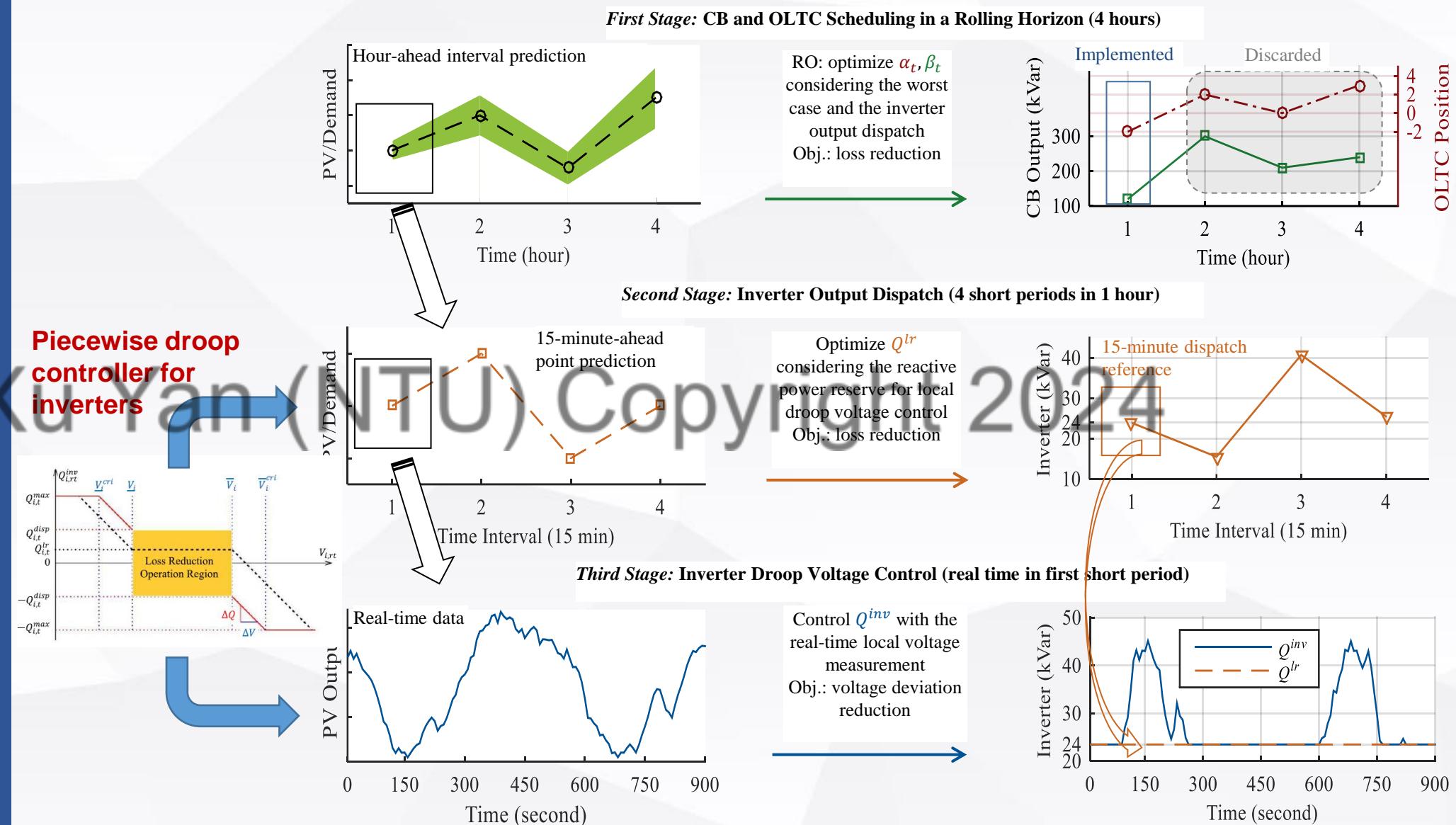
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■ Three-Stage Robust Volt/Var Control (TRI-VVC)



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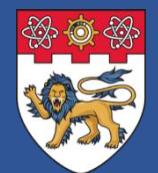
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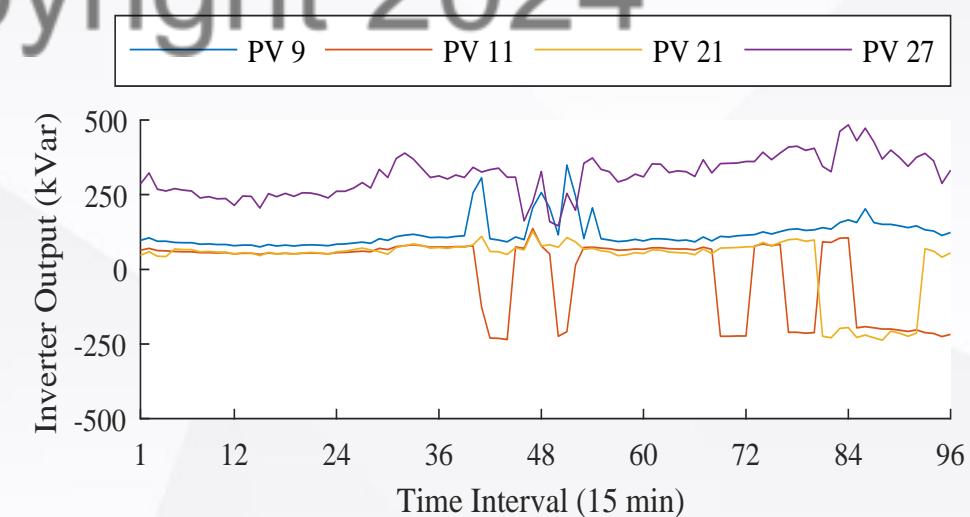
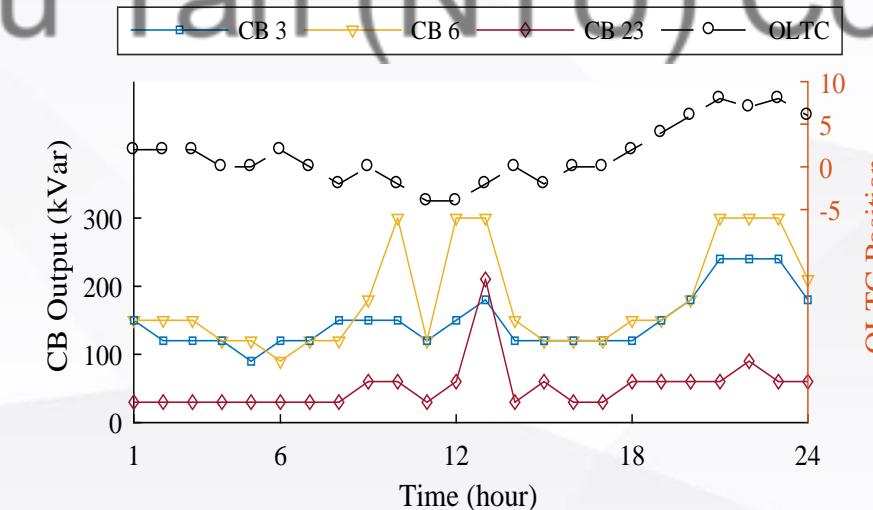
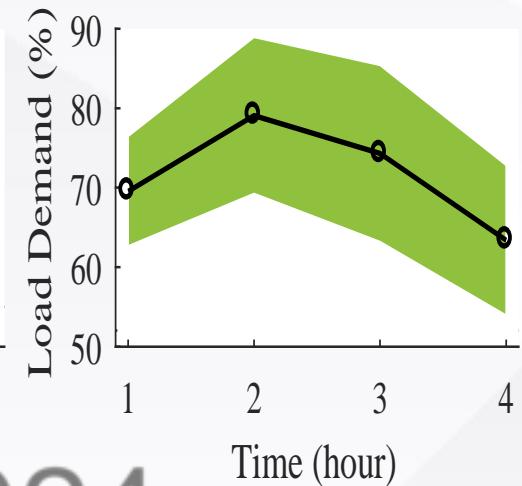
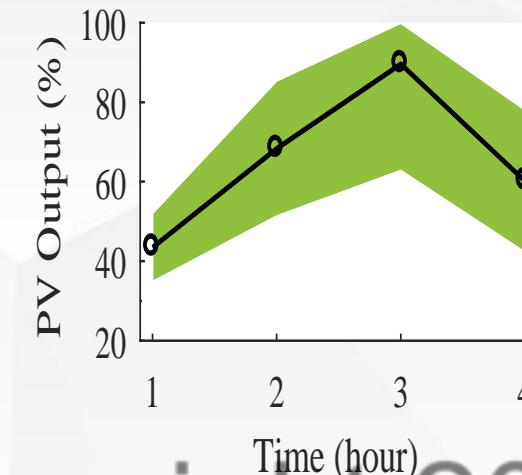
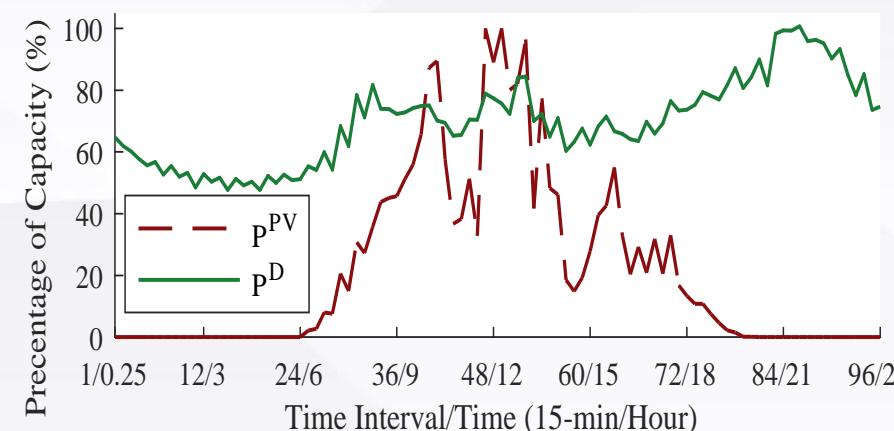
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■ Simulation Results



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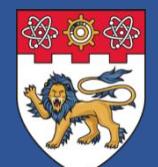
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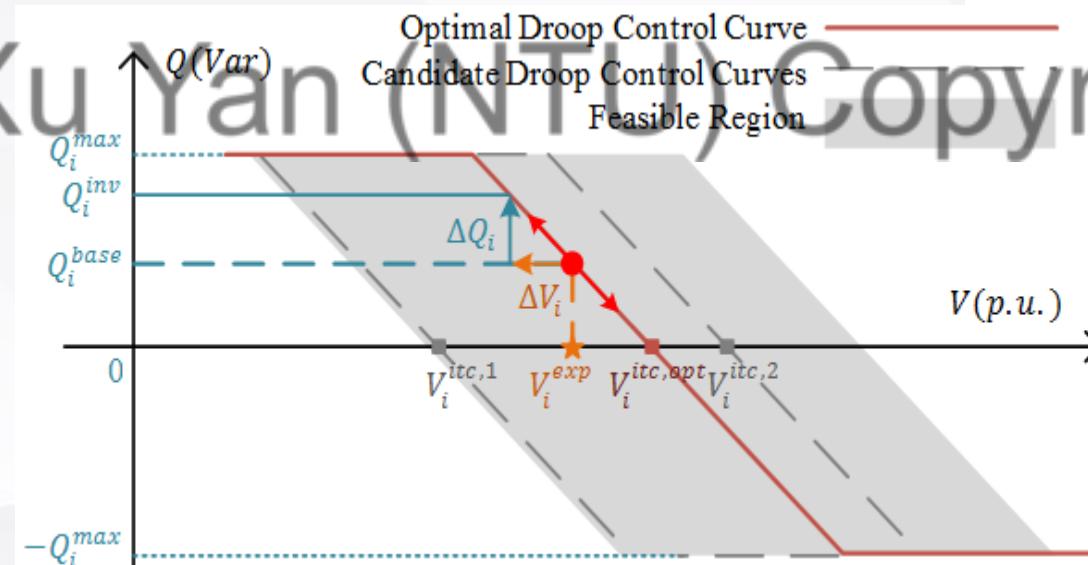
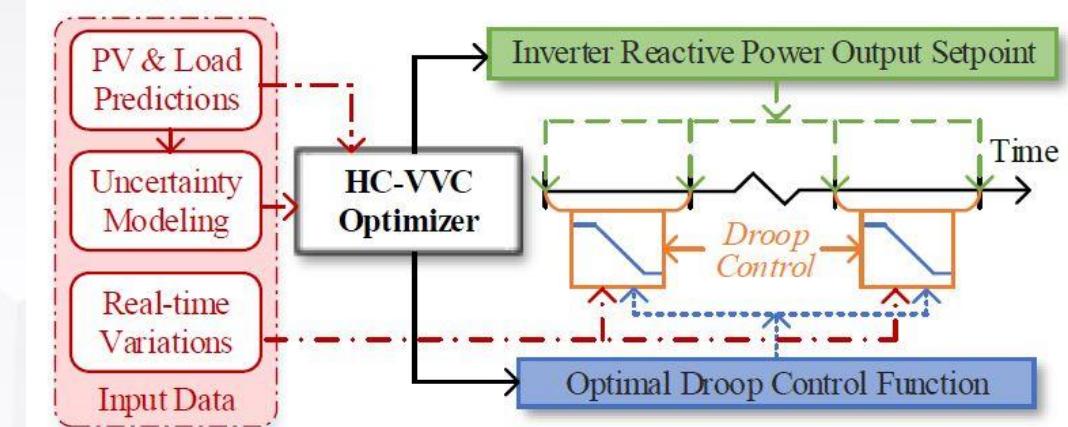
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▪ Hierarchically-Coordinated Voltage/VAR Control (HC-VVC)

- ✓ Central VVC considers the network level information (power flow)
- ✓ Local VVC focuses on the real-time variation (bus voltage)



linear droop controller for inverters

Inverter Droop Control Model

- The central VVC hierarchy implements the base reactive power output setpoint of each inverter, i.e. Q_i^{base} under the expected operating condition.
- The local VVC hierarchy implements the local droop control by adjusting the reactive power output responding to the local voltage deviation. $\Delta Q = f(\Delta V)$

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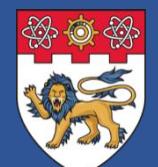
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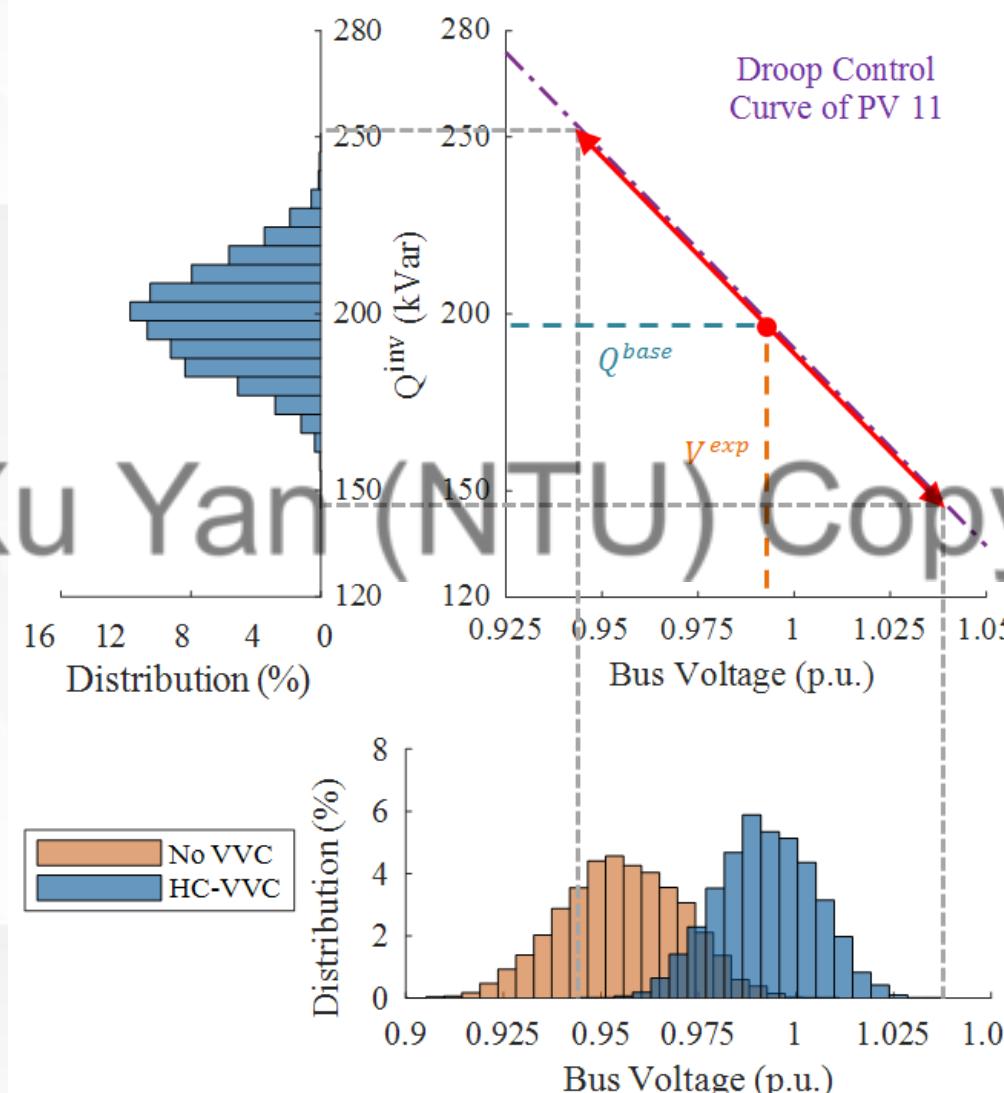
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▪ Hierarchically-Coordinated Voltage/VAR Control (HC-VVC)



Voltage control results:

In response to the local bus voltage variation, the inverter reactive power output moves along the droop control curve.

The mean bus voltage magnitude with the HC-VVC is very close to 1 p.u.

COMPARISON RESULTS FOR DIFFERENT VVC METHODS

Method	#1	#2	#3	HC-VVC
Average Power Loss (kW)	24.1	32.9	110.3	26.7
Voltage Violation Rate (%)	3.4%	0.2%	51.8%	0.1%
Average Voltage (p.u.)	0.990	0.998	0.971	0.993
Average Absolute Voltage Deviation (p.u.)	0.012	0.010	0.029	0.009

Comparison with other VVC methods

HC-VVC: least voltage violation rate; least voltage magnitude deviation; second least average power loss; second average voltage close to 1 p.u.

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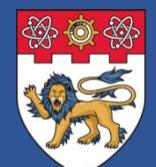
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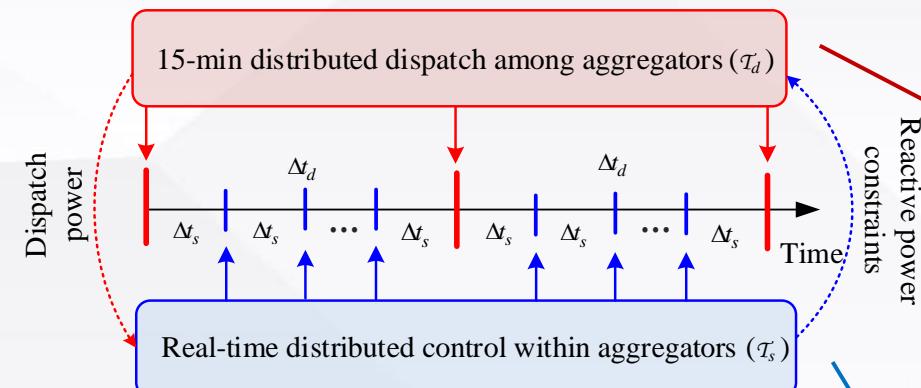
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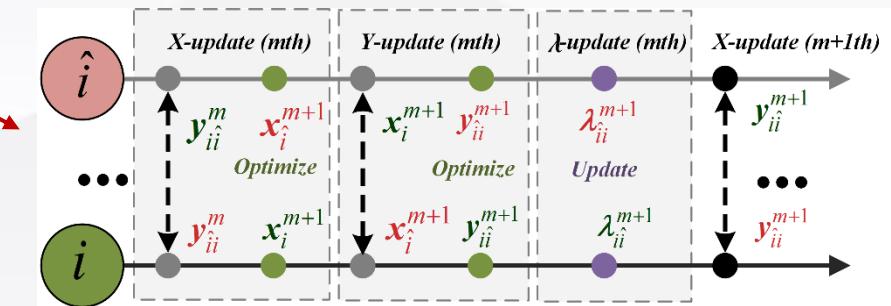


▪ Fully Distributed Two-Level Volt/Var Control

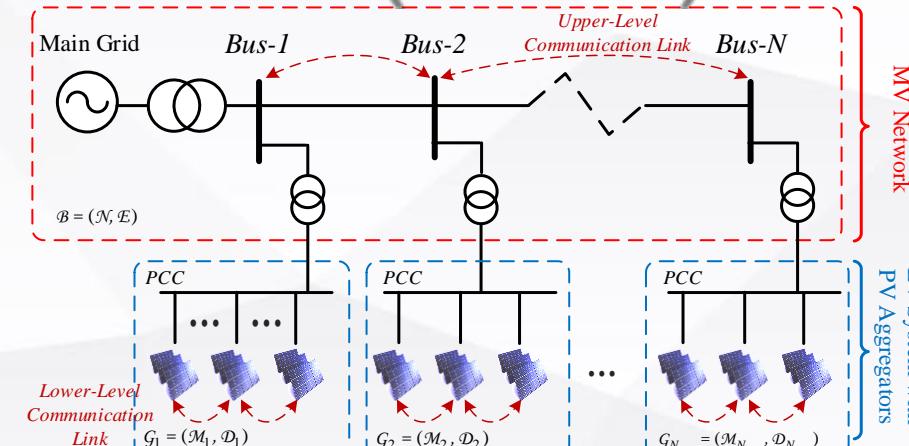
Two-level VVC with time scale coordination



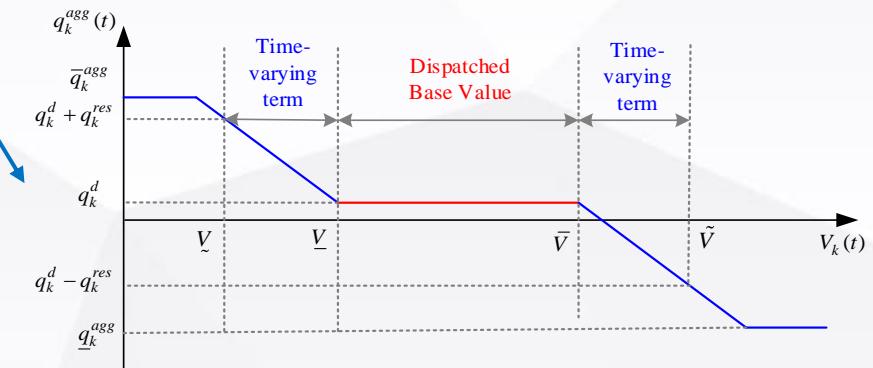
Distributed dispatch by ADMM



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Distributed real-time voltage control



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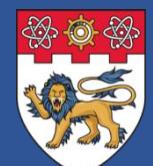
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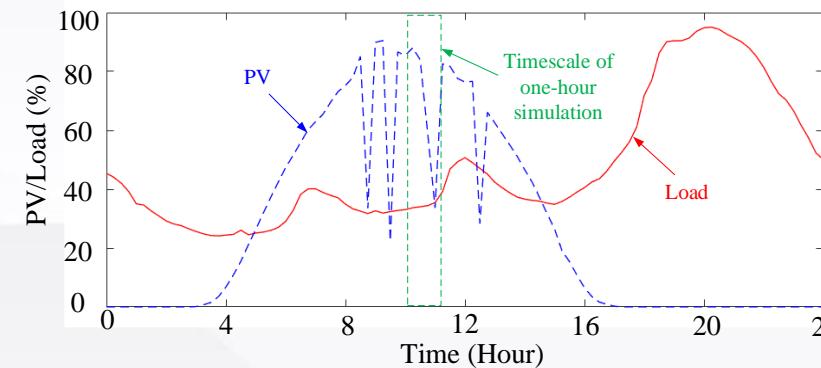
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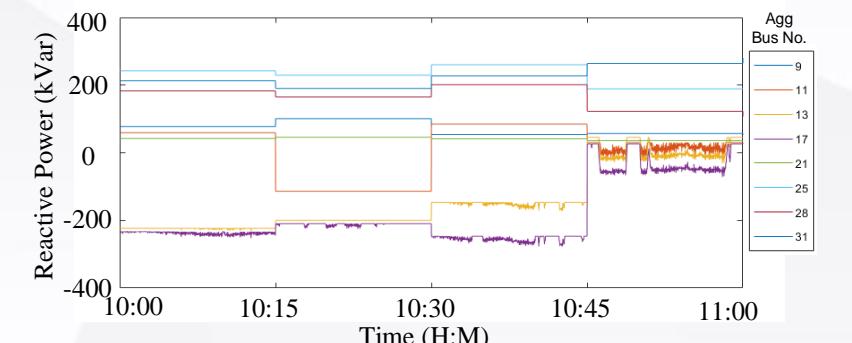
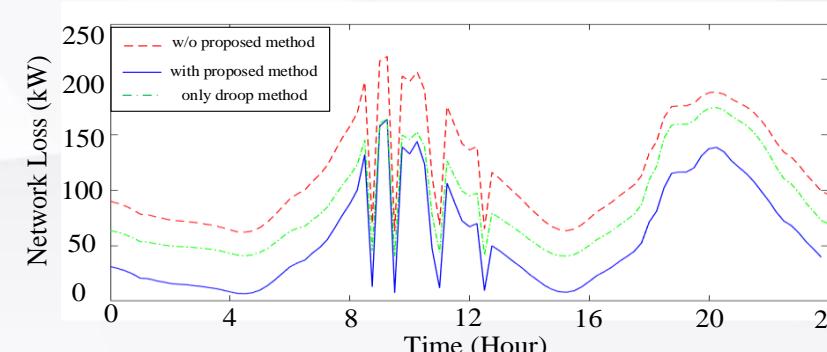
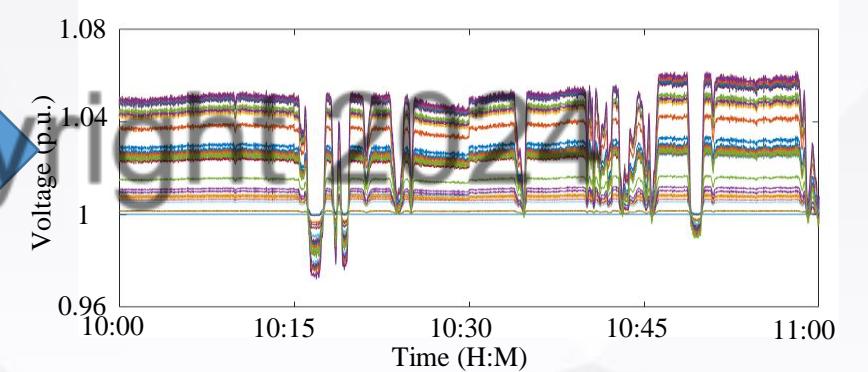
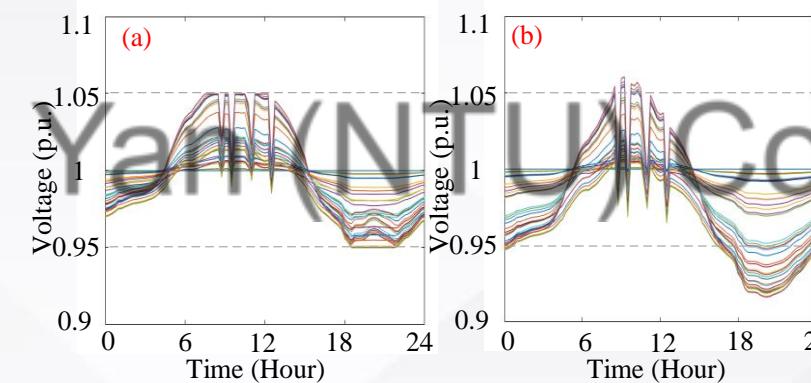
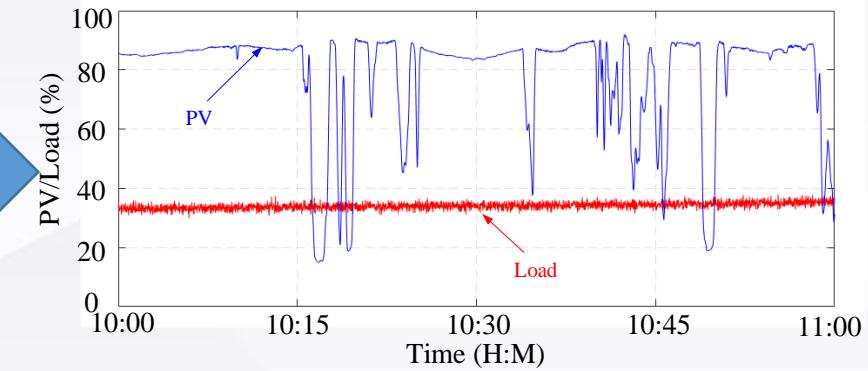
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■ Simulation Results

24-hour simulation with 15 minutes sampling



One-hour simulation with 1 second sampling



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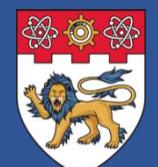
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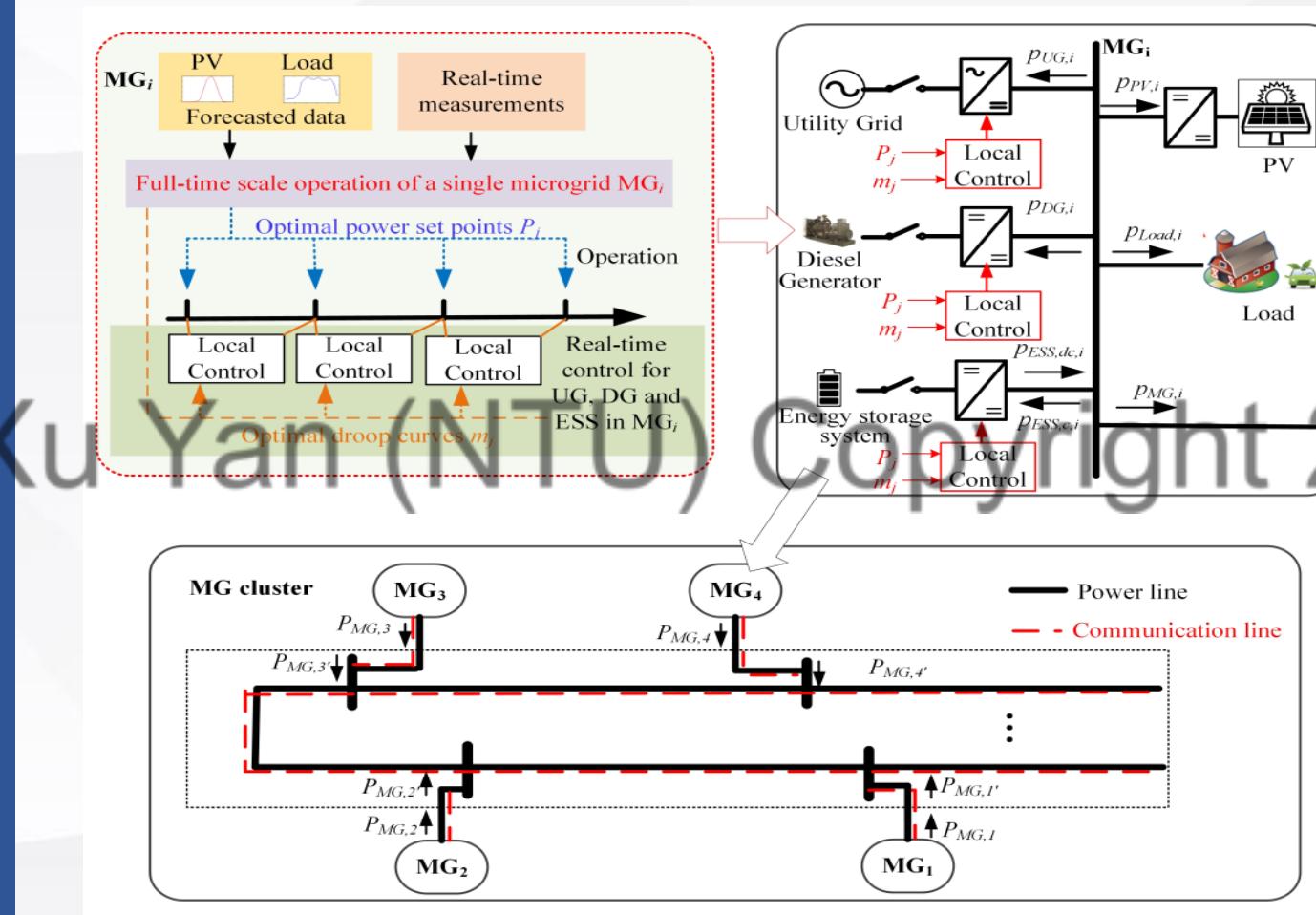
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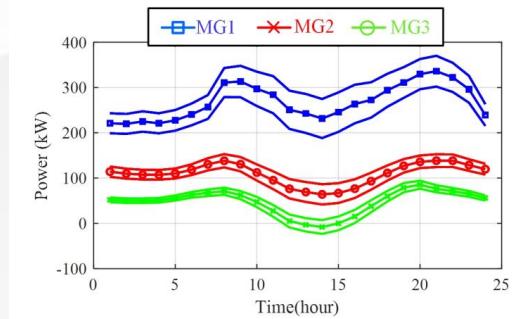
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Hierarchically Coordinated Operation and Control for DC microgrid clusters



$$\min_{\mathbf{P}_j(t), \beta_j(t), P_{jk}(t), l_{jk}(t), v_j(t)} \mathbb{E} \sum_{t \in \mathcal{T}} \{f(\mathbf{P}_i(t), \beta_i(t)) + \sum_{j:j \rightarrow k} l_{jk}(t)r_{jk}\}$$
$$p_{UG,i} - P_{UG,i} = \beta_{UG,i}\xi_i$$
$$p_{DG,i} - P_{DG,i} = \beta_{DG,i}\xi_i$$
$$p_{ESS,i} - P_{ESS,dc,i} + P_{ESS,c,i} = \beta_{ESS,i}\xi_i$$
$$\beta_{UG,i} + \beta_{DG,i} + \beta_{ESS,i} = 1$$
$$m_{UG,i} = \frac{k_i}{\beta_{UG,i}}, m_{UG,i} \in \left(0, \frac{\Delta V_{max}}{P_{UG,max}}\right)$$
$$m_{DG,i} = \frac{k_i}{\beta_{DG,i}}, m_{DG,i} \in \left(0, \frac{\Delta V_{max}}{P_{DG,max}}\right)$$
$$m_{ESS,i} = \frac{k_i}{\beta_{ESS,i}}, m_{ESS,i} \in \left(0, \frac{\Delta V_{max}}{P_{ESS,max}}\right)$$



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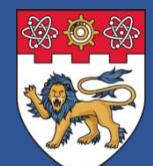
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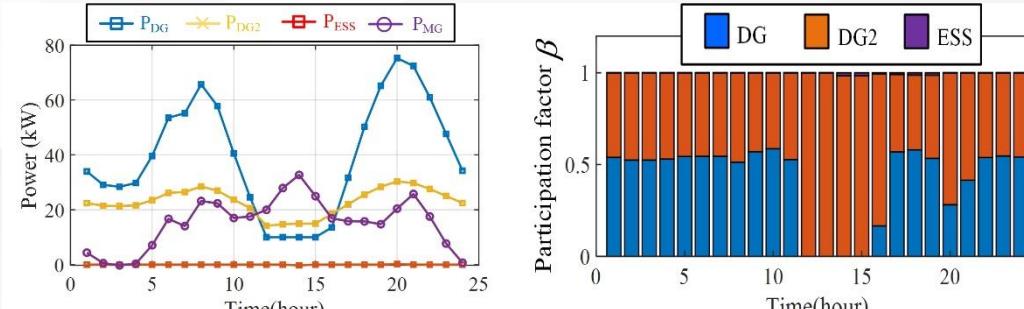
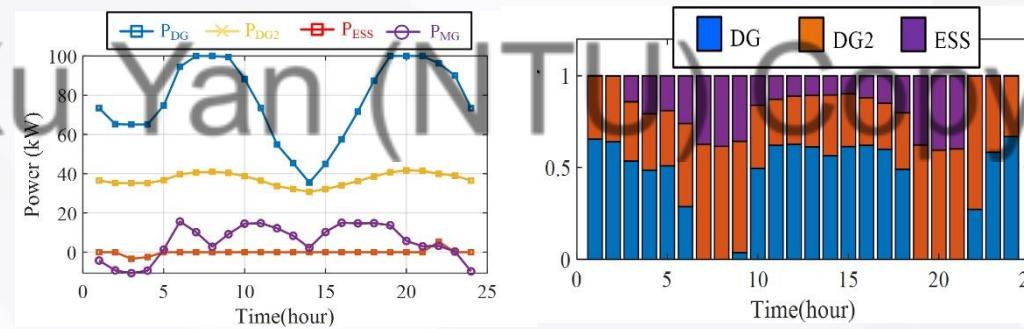
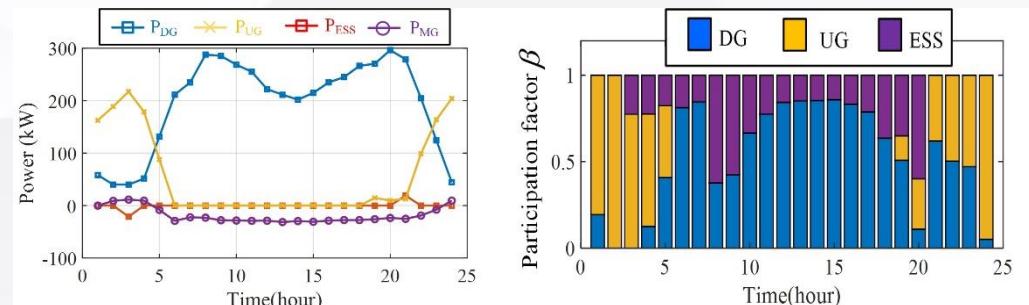
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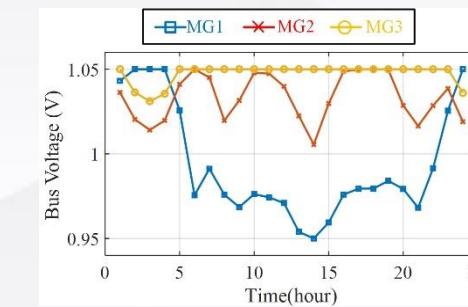
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■ Hierarchically Coordinated Operation and Control for DC microgrid clusters

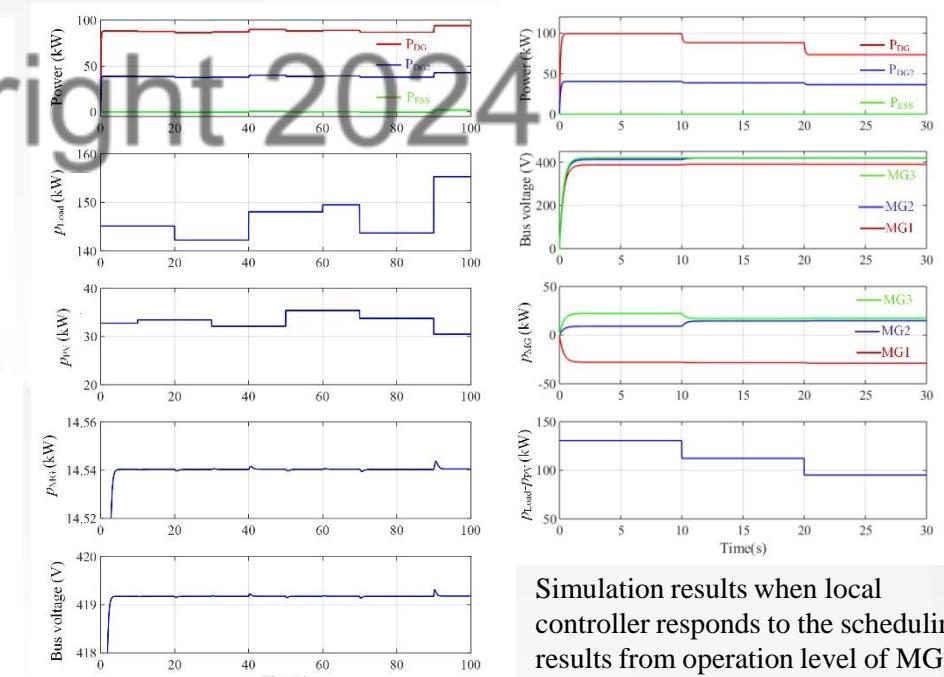
Dispatch results



Q. Xu, Y. Xu*, et al, " A Hierarchically Coordinated Operation and Control Scheme for DC Microgrid Clusters under Uncertain," *IEEE Transactions on Sustainable Energy*, 2020.



Real-time control results



Simulation results when local controller responds to the scheduling results from operation level of MG2 at 9h, 10h and 11h (which is at 10s, 20s and 30s in the simulation)

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- 2) Volt/Var regulation

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- 1) Design
- 2) Energy trading
- 3) Ancillary service

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) Joint planning

Continued research works in local energy markets

A centralized market structure may no longer be applicable with the emergence of a significant number of prosumers. P2P energy trading offers a promising solution.

Fully-Decentralized Local Energy Market (P2P) [2]

The uncertain behaviours of flexible consumers pose a great challenge to system operation, while their flexibility offers opportunities to locally accommodate the uncertain renewable generation.

Centralized Local Energy Market [1]

Partially-Decentralized Local Energy Market (community-based) [3]

The existing regulations may not accommodate end-to-end energy trading. The aggregator can coordinate the DERs within a certain region and provide energy services at scale, which makes their market entry more possible to be supported by regulatory and policy bodies. On the other hand, small-scale end users may not have the means or interest in participating in P2P energy trading as well.



Local Ancillary Service Market [4][5]

The penetration of DERs coupled with the rise of P2P markets leads to a significant challenge in distribution network operation. Luckily, inverter-interfaced DERs hold both technical potential and economic incentives to provide distribution systems with fast and flexible Var supports.

[1] Y. Zou, Y. Xu*, and C. Zhang, "A Risk-Averse Adaptive Stochastic Optimization Method for Transactive Energy Management of a Multi-Energy Microgrid," *IEEE Transactions on Sustainable Energy*, 2023.

[2] Y. Zou, Y. Xu*, X. Feng, and H. D. Nguyen, "Peer-to-Peer Transactive Energy Trading in a Reconfigurable Multi-Energy Network," *IEEE Transactions on Smart Grid*, 2022.

[3] Y. Zou, Y. Xu*, and J. Li, "Aggregator-Network Coordinated Peer-to-Peer Multi-Energy Trading via Adaptive Robust Stochastic Optimization," *IEEE Transactions on Power Systems*, 2024.

[4] Y. Zou, and Y. Xu*, "Design of Robust Var Reserve Contract for Enhancing Reactive Power Ancillary Service Market Efficiency," *CSEE Journal of Power and Energy Systems*, 2023.

[5] Y. Zou, and Y. Xu*, "DER-Inverter Based Reactive Power Ancillary Service for Supporting Peer-to-Peer Transactive Energy Trading in Distribution Networks," *IEEE Transactions on Power Systems*, 2024.

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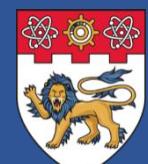
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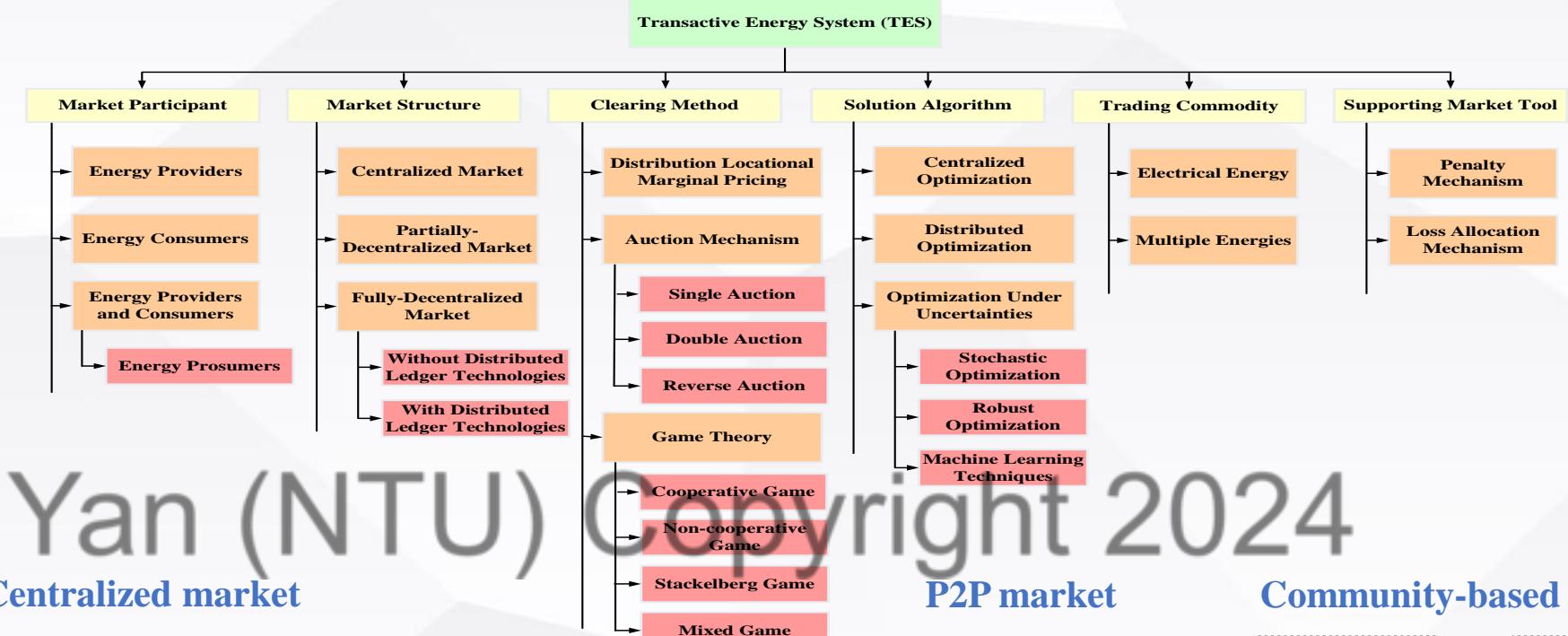
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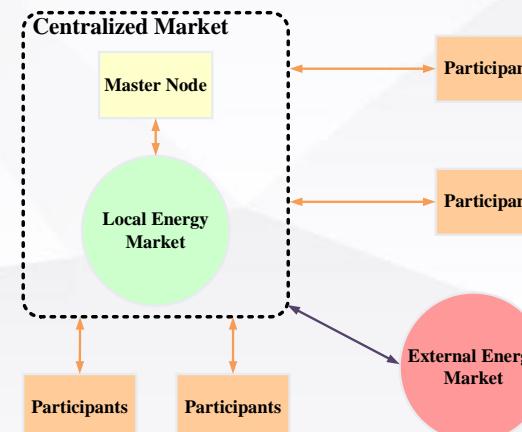
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■ Transactive Energy System (TES) Classification

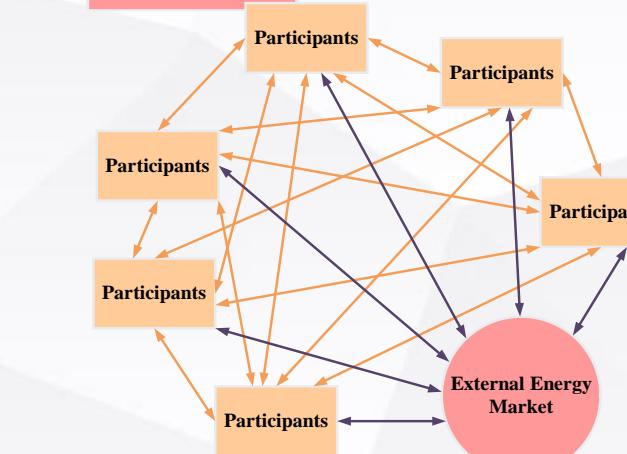


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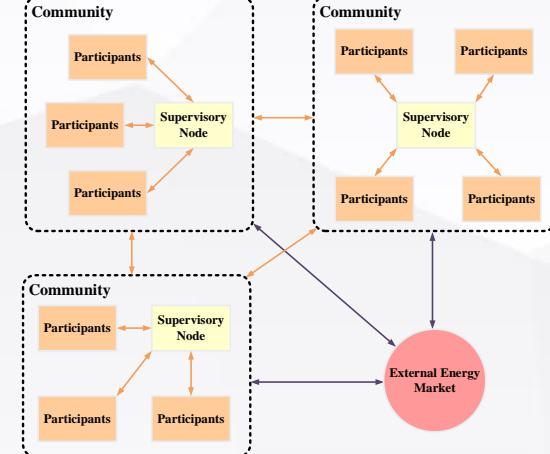
Centralized market



P2P market



Community-based market



1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

4. Hierarchy coordination

5. Trading

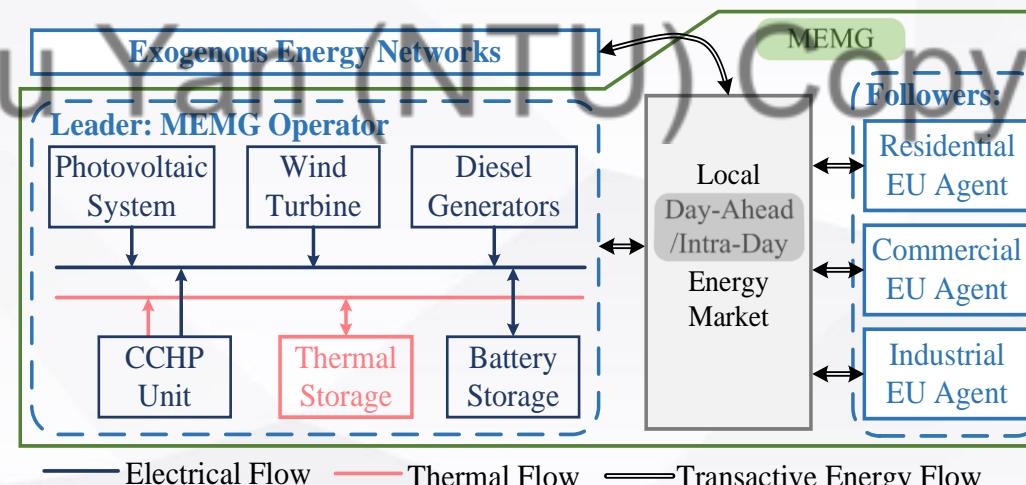
- 1) Design
- 2) Energy trading
- 3) Ancillary service

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) Joint planning

Centralized Local Market: Risk-Averse Transactive Energy Management

Main motivation: The uncertain behaviours of flexible consumers is challenging MES operation, while their flexibility offers opportunities to locally accommodate the uncertain renewable generation.



Strategy of the MEMG operator:

- To schedule all the physical DER units;
- To determine the energy trading prices for desired demand-side response. **(as a price maker)**

Strategy of the energy user (EU) agents:

- To transact with the MEMG operator; **(as price takers)**
- To trade energies with the exogenous energy networks.

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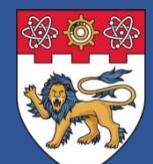
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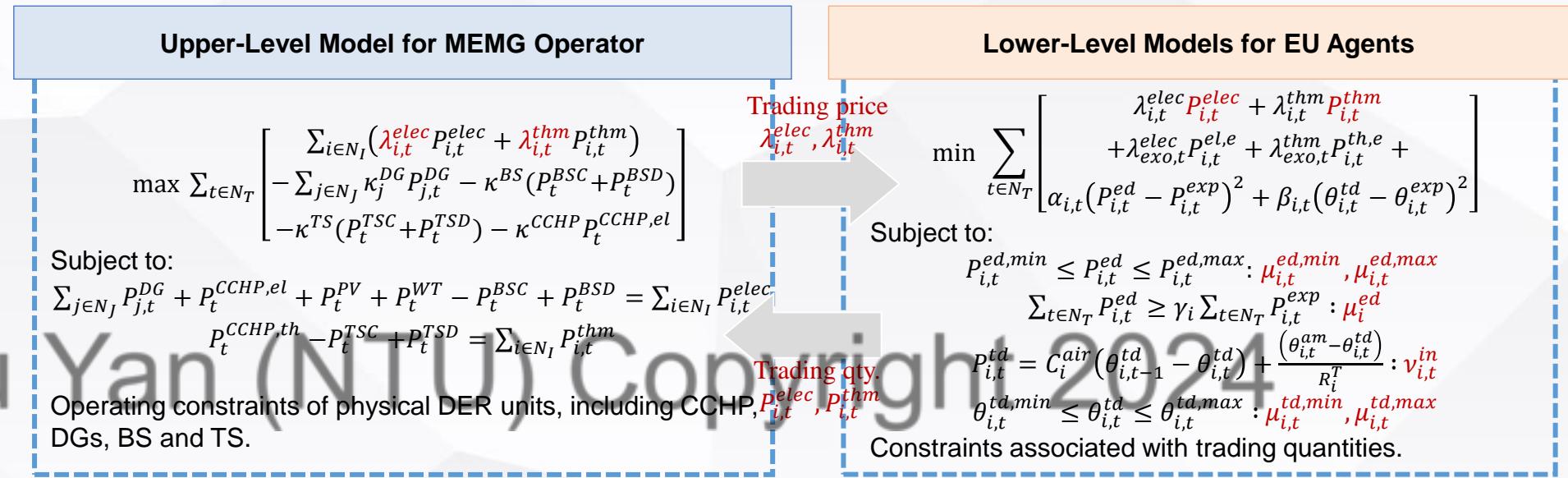
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Mathematical Formulation

The interactions between the MEMG operator and EU agents are captured by a **Stackelberg game**, which is expressed as a **bi-level model**.



Risk aversion towards uncertainties:

$$\max_{x \in \chi, y_s \in \Omega, \eta \in \mathcal{R}} c^T x + \sum_{s \in N_s} \pi_s \mathcal{L}(x, d_s) + \rho \cdot CVaR_\vartheta$$

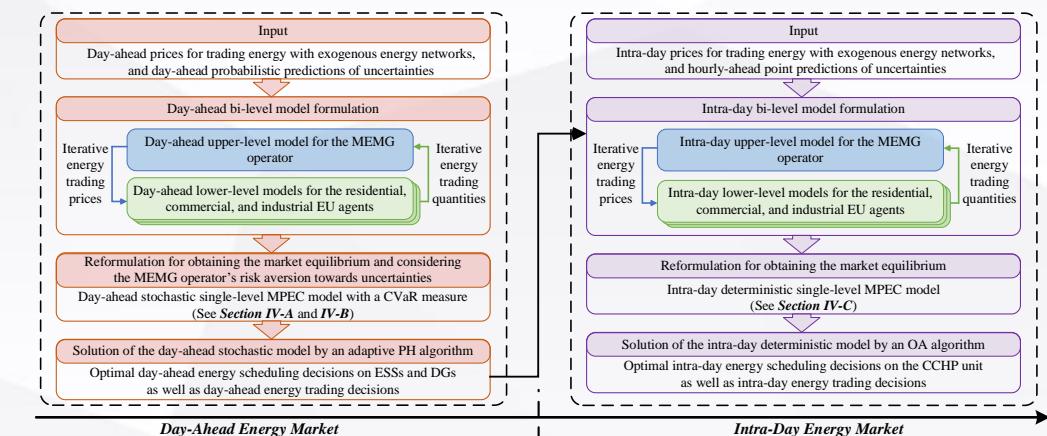
Subject to:

$$x \in \chi$$

$$\mathcal{L}(x, d_s) = \max_{y_s \in \Omega(x, d_s)} b^T y_s$$

$$CVaR_\vartheta = \max_{\eta \in \mathcal{R}} \{\eta + \frac{1}{1-\vartheta} \sum_{s \in N_s} [f_P^s - \eta]^- \pi_s\}$$

where $\Omega(x, d_s) = \{y_s | Ax + By_s \geq r, Ex + Fy_s = d_s\}$, $f_P^s = c^T x + \mathcal{L}(x, d_s)$ denotes the profit under scenario s.



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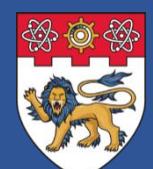
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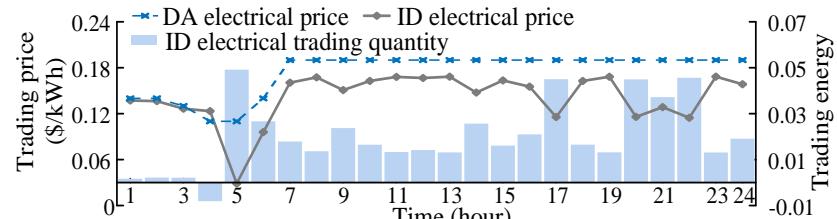
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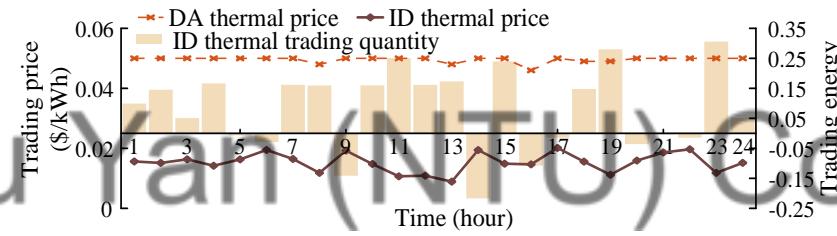


■ Simulation Results

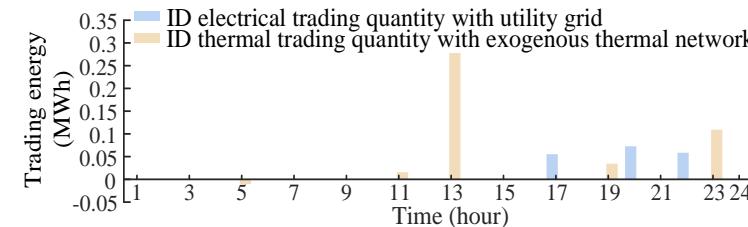
□ Intra-day energy trading



(a) Intra-day electrical trading between MEMG operator and residential agent



(d) Intra-day thermal trading between MEMG operator and residential agent



(f) Intra-day energy trading between MEMG operator and exogenous networks

- MEMG operator uses price signals to guide users' behaviors, thereby reducing reliance and impact on external grids.

□ Computation performance

Computational Performance for Day-Ahead Stochastic MILP

Solution Approach	No. of Variables	Solution Time (s)	Objective Value (\$)	Optimality Accuracy
Direct Use of GUROBI	14862 continuous 4641 binary for all scenarios	79.70 Hours	7501.01	100%
PH Algorithm 1*	3938 continuous	≥16.03 Hours	N/A	N/A
PH Algorithm 2 ⁺	2781 binary for each scenario	2.82 Hours	7478.15	99.7%
Adaptive PH Algorithm [#]	3.56 Hours	7492.69	99.9%	

Computational Performance for the Intra-Day Bilinear Problem

Bilinear Term Linearization Approach	Step Size (\$/kWh)	Convergence Tolerance	Average Time (s)
Price Discretizing	0.001	N/A	191.95
OAAlgorithm	→ 0	10 ⁻⁵	13.51

- Problem scale is reduced by adaptive PH algorithm through scenario decomposition. Bilinear terms of price times quantity are efficiently handled by OA algorithm.

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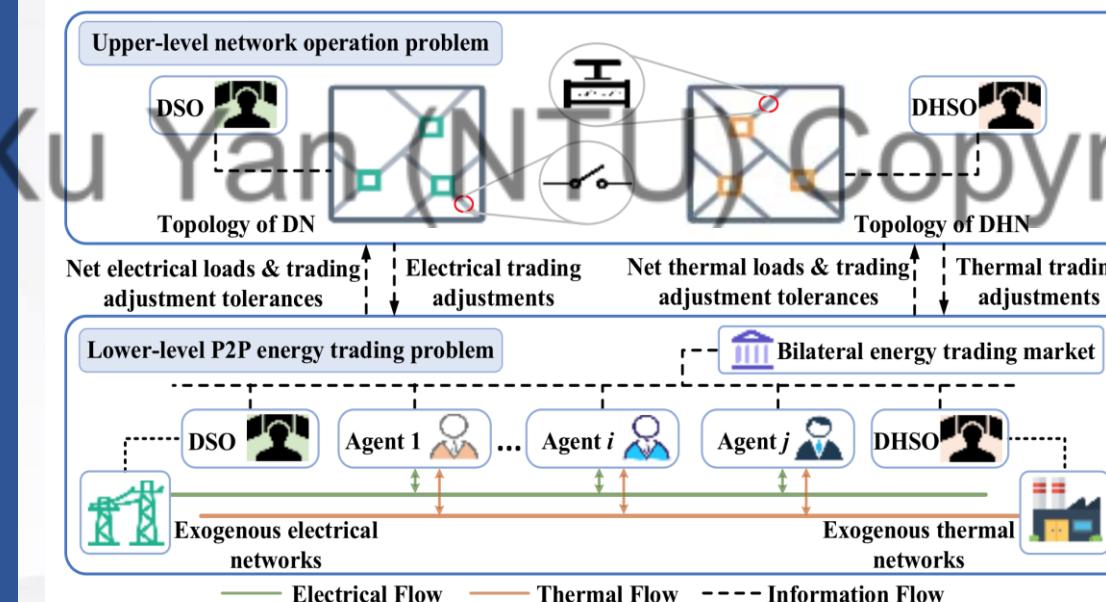
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P2P Transactional Energy Trading in A Reconfigurable Multi-Energy Network

Main motivation: P2P trading can address operational complexities arising from the emergence of prosumers, facilitating local energy balance, but it may also worsen network operation, e.g., voltage drops and line congestion.



Strategy of DSO and DHSO (at upper level):

- To reconfigure the DN and DHN;
- To request the lower-level agents to make necessary trading adjustments.

Strategy of nodal agents (at lower level):

- To schedule the local DERs (e.g., CCHP, ESS, flexible loads);
- To transact with other agents or exogenous networks in a bilateral manner;
- To submit the current net loads to the DSO and DHSO.

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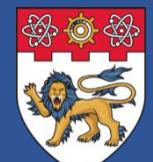
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■ Mathematical Formulation

A. Lower-level P2P energy trading problem

Modeling for P2P energy trading

- Objective function:

$$C_i = \sum_{t \in N_T} (C_{i,t}^{Gen} + C_{i,t}^{Bill} + C_{i,t}^{Disc} + C_{i,t}^{Ser}) + C_i^{P2P}$$

$$\tilde{C}_i = \sum_{t \in N_T} (C_{i,t}^{Gen} + C_{i,t}^{Bill} + C_{i,t}^{Disc})$$

$$\max \prod_{i=1}^N (\tilde{C}_i - C_i)^{\mathcal{MP}_i}$$

where \mathcal{MP}_i is a positive value denoting the bargaining power of agent i .

- Key constraints:

$$e_{ij,t}^{DN} + e_{ji,t}^{DN} = 0, \forall t, \forall i, \forall j \in \mathcal{N} \setminus i$$

$$e_{ij,t}^{DHN} + e_{ji,t}^{DHN} = 0, \forall t, \forall i, \forall j \in \mathcal{N} \setminus i$$

$$\phi_{ij}^{P2P} + \phi_{ji}^{P2P} = 0, \forall i, \forall j \in \mathcal{N} \setminus i$$

$$\tilde{C}_i \geq C_i, \forall i$$

B. Upper-level network operation problem

Modeling for reconfigurable DN operation

- Objective function:

$$\min \sum_{t \in N_T} \left(\sum_{mn \in N_{Br}^{DN}} PL_{mn,t}^{Loss} + \partial \sum_{m \in N_{Ag}^{DN}} |\Delta e_{m,t}^{DN}| \right)$$

- Constraints:

- Linearized DistFlow with reconfiguration variables
- Spanning tree constraints:

$$\theta_{mn,t} + \theta_{nm,t} = \mathcal{K}_{mn,t}, \quad \forall mn \in N_{Br}^{DN}, \forall t$$

$$\sum_{n \in \{N_m^{DN} \cup N_m^{DN-}\}} \theta_{mn,t} \leq 1, \forall m \in N_{Ag}^{DN}, \forall t$$

$$\sum_{n \in \{N_m^{DN} \cup N_m^{DN-}\}} \theta_{mn,t} = 0, \forall m \in N_{St}^{DN}, \forall t$$

- Spanning tree constraints (to strictly ensure radality)

$$\sum_{n \in N_m^{DN+}} F_{mn,t} + D_{m,t} = \sum_{n \in N_m^{DN-}} F_{nm,t}$$

$$-\mathcal{K}_{mn,t} M \leq F_{mn,t} \leq \mathcal{K}_{mn,t} M, \forall m \in N_{Ag}^{DN}, \forall t$$

Nash bargaining theory with the concept of bargaining power

- Nash product: to maximize agents' benefits from participating in P2P energy trading (i.e., $\tilde{C}_i - C_i$)

- Bargaining power \mathcal{MP}_i :

- ❖ If $\mathcal{MP}_i = 1$ for $\forall i$, all agents will be awarded with the equal benefits regardless of their market contributions.
(traditional Nash bargaining theory)

- ❖ If \mathcal{MP}_i is set as

$$\mathcal{MP}_i = \frac{\sum_{t \in N_T} (| \sum_{j \in \mathcal{N} \setminus i} e_{ij,t}^{DN} | + | \sum_{j \in \mathcal{N} \setminus i} e_{ij,t}^{DHN} |)}{\sum_{h \in \mathcal{N}} \sum_{t \in N_T} (| \sum_{j \in \mathcal{N} \setminus h} e_{hj,t}^{DN} | + | \sum_{j \in \mathcal{N} \setminus h} e_{hj,t}^{DHN} |)}$$

then the allocated benefit for each agent will be directly proportional to the respective P2P trading contribution.

Modeling for reconfigurable DHN operation

- Objective function:

$$\min \sum_{t \in N_T} \left(\sum_{gk \in N_{Pi}^{DHN}} HL_{gk,t}^{Loss} + \partial \sum_{g \in N_{Ag}^{DHN}} |\Delta e_{g,t}^{DHN}| \right)$$

- Constraints:

- Linearized thermal flow model with reconfiguration variables, independent of mass flow rate and water temperature.
- Valve switching constraints (XOR operation):

$$\sum_{gk \in N_{Pi}^{DHN}} (\mathcal{V}_{gk,t} + \mathcal{V}_{gk,(t-1)} - 2\xi_{gk,t}) \leq N^{VA}, \forall t$$

$$\xi_{gk,t} - \mathcal{V}_{gk,t} \leq 0, \forall gk, \forall t$$

$$\xi_{gk,t} - \mathcal{V}_{gk,(t-1)} \leq 0, \forall gk, \forall t$$

$$\mathcal{V}_{gk,t} + \mathcal{V}_{gk,(t-1)} - \xi_{gk,t} \leq 1, \forall gk, \forall t$$

$$\xi_{gk,t} \geq 0, \forall gk, \forall t$$

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■ Simulation Results

□ Lower-level P2P trading results

Benefit Distribution for four Representative Agents based on Traditional Nash Bargaining Theory

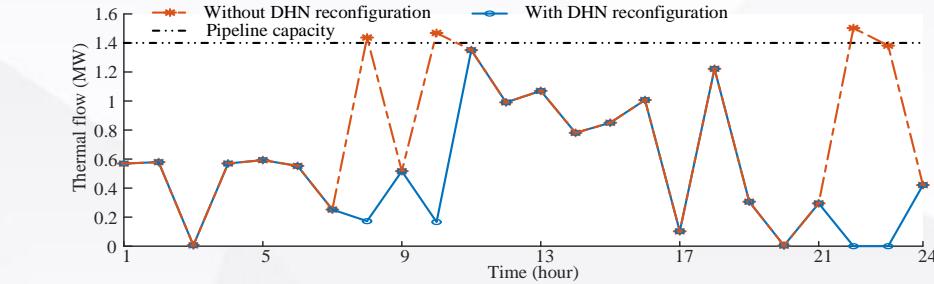
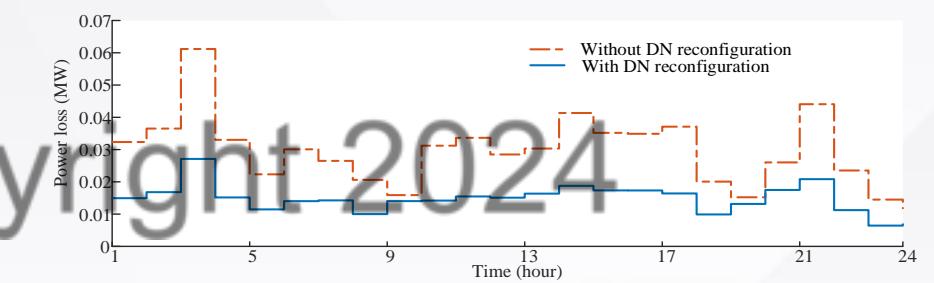
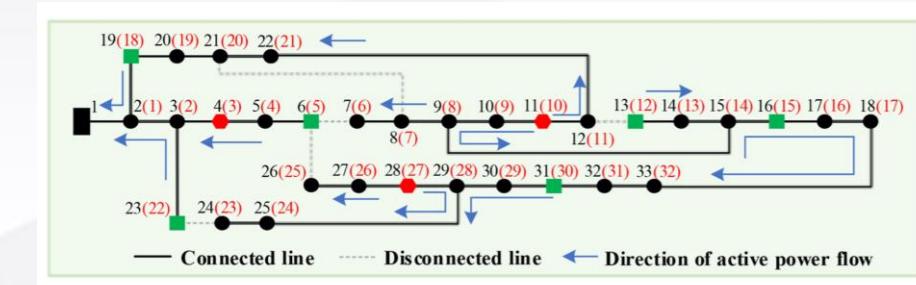
	Item	Agt. 3	Agt. 6	Agt. 22	Agt. 34
With P2P trading	Cost without P2P trading (\$)	-71.4	988.0	-325.5	329.6
	Social cost* (\$)	1435.5	64.8	24.8	15.6
	P2P payments (\$)	-1723.9	706.2	-567.3	97.0
	Total cost b+c (\$)	-288.4	771.0	-542.5	112.6
	P2P trading contribution (MWh)	26.92	4.33	4.04	6.59
	Market power	1.0	1.0	1.0	1.0
Benefit from P2P trading a-d (\$)		217.0	217.0	217.0	217.0
Benefit per P2P contrib. g/e (\$/MWh)		8.06	50.16	53.66	32.94

Benefit Distribution for four Representative Agents based on Modified Nash Bargaining Theory

	Item	Agt. 3	Agt. 6	Agt. 22	Agt. 34
With P2P trading	Cost without P2P trading (\$)	-71.4	988.0	-325.5	329.6
	Social cost (\$)	1435.5	64.8	24.8	15.6
	P2P payments (\$)	-2554.4	754.9	-507.6	57.7
	Total cost b+c (\$)	-1118.9	819.7	-482.8	73.3
	P2P trading contribution (MWh)	26.92	4.33	4.04	6.59
	Market power	0.1178	0.0189	0.0177	0.0288
Benefit from P2P trading a-d (\$)		1047.5	168.3	157.3	256.3
Benefit per P2P contrib. g/e (\$/MWh)		38.91	38.91	38.91	38.91

➤ Proposed mechanism ensures a fairer benefit allocation after P2P trading. Each agent obtains an equal benefit per P2P trading contribution.

□ Upper-level network operation results



➤ P2P energy trading can be facilitated by network reconfiguration, in terms of alleviating network operation violations as well as reducing line losses.

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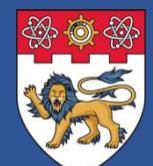
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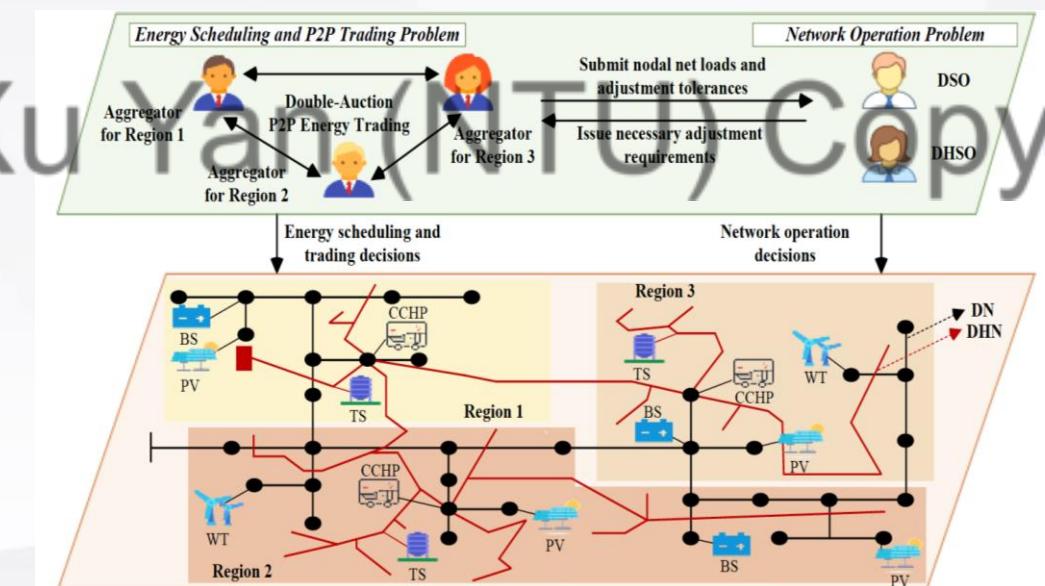
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Community-Based Market: Aggregator-Network Coordinated P2P Trading

Main motivation: The existing regulations may not accommodate end-to-end energy trading. And small-scale end users may not have the means or interest in participating in P2P energy trading as well.



Distributed energy resources (DERs)

- Invested and owned by private entities
- Managed by corresponding aggregators

Aggregators

- Manage (internal coordination + external trading) contracted geographically adjacent or dispersed DERs

Multi-energy networks

- Owned by the network asset companies
- Operated by a distribution system operator (DSO) and a district heating system operator (DHSO)

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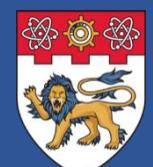
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▪ Mathematical Formulation

A. Double-auction P2P trading among aggregators

Modeling for dynamic double-auction negotiation

□ Augmented Lagrangian:

$$\mathcal{L}_m(x_{m,t}, \hat{e}_{m,t}, \lambda_{m,t}) = \sum_{t \in N_T} \left[\frac{\varrho}{2} \|e_{m,t} - \hat{e}_{m,t}\|_2^2 + (\lambda_{m,t})^T (e_{m,t} - \hat{e}_{m,t}) \right]$$

s.t., $\hat{e}_{mn,t} + \hat{e}_{nm,t} = \mathbf{0}$, $\forall t, \forall m \in N_M, \forall n \in N_M \setminus m$

DER operational constraint

Power balance constraints

□ Dynamic P2P negotiations:

Update of P2P trading quantity $e_{m,t}$:

$$\{x_{m,t}^{[\tau+1]}\}_{t \in N_T} = \underset{x_{m,t} \in \mathcal{X}_{m,t}}{\operatorname{argmin}} \mathcal{L}_m(x_{m,t}, \hat{e}_{m,t}^{[\tau]}, \lambda_{m,t}^{[\tau]})$$

Update of auxiliary variable $\hat{e}_{m,t}$:

$$\hat{e}_{mn,t}^{[\tau+1]} = -\hat{e}_{nm,t}^{[\tau+1]} = \frac{e_{mn,t}^{[\tau+1]} - e_{nm,t}^{[\tau+1]}}{2} + \frac{\lambda_{mn,t}^{[\tau]} - \lambda_{nm,t}^{[\tau]}}{2\varrho}$$

Update of P2P trading price $\lambda_{m,t}$:

$$\lambda_{m,t}^{[\tau+1]} = \lambda_{m,t}^{[\tau]} + \varrho [e_{m,t}^{[\tau+1]} - \hat{e}_{m,t}^{[\tau+1]}]$$

□ Market equilibrium:

$$|e_{mn,t}^{[\tau+1]}|, \lambda_{mn,t}^{[\tau+1]} = |e_{nm,t}^{[\tau+1]}|, \lambda_{nm,t}^{[\tau+1]}, \forall t, \forall m \in N_M, \forall n \in N_M \setminus m$$

B. Network operation problem

Modeling for three-phased unbalance DN operation

$$\min_{x^{BSO}} \sum_{t \in N_T} \left[\sum_{ij \in \mathcal{E}^{DN}} (\lambda_t^{DN,b} PL_{ij,t}^{Loss} + \kappa^D \omega_{ij,t} + \kappa^C \varpi_{ij,t}) \right] \\ + \partial \sum_{i \in \mathcal{N}_{Agg}^{DN}} \mathbf{1}^T |\Delta e_{i,t}^{DN}|$$

Linearized three-phase DistFlow model

$$\Delta e_{i,t}^{DN} - P_{i,t}^{Net*} = \sum_{j \in \mathcal{N}_i^{DN+}} \mathbf{PL}_{ij,t} - \sum_{j \in \mathcal{N}_i^{DN-}} \mathbf{PL}_{ji,t}, \forall t$$

$$P_{i,t} = \sum_{j \in \mathcal{N}_i^{DN+}} \mathbf{PL}_{ij,t} - \sum_{j \in \mathcal{N}_i^{DN-}} \mathbf{PL}_{ji,t}, \forall i \in \mathcal{N}_{SS}^{DN}, \forall t$$

$$Q_{i,t} = \sum_{j \in \mathcal{N}_i^{DN+}} \mathbf{QL}_{ij,t} - \sum_{j \in \mathcal{N}_i^{DN-}} \mathbf{QL}_{ji,t}, \forall i \in \mathcal{N}^{DN}, \forall t$$

$$\begin{bmatrix} 2\operatorname{Re}(\tilde{z}_{ij}^* s_{ij,t}) - (1 - \mathcal{K}_{ij,t}) \mathbf{M} \leq \mathbf{U}_{i,t} - \mathbf{U}_{j,t} \\ \leq 2\operatorname{Re}(\tilde{z}_{ij}^* s_{ij,t}) + (1 - \mathcal{K}_{ij,t}) \mathbf{M} \end{bmatrix}, \forall ij \in \mathcal{E}^{DN}, \forall t$$

Unbalanced voltage:

$$\max_{\varphi \in \Phi} \left| \frac{U_{\varphi,i,t} - \tilde{U}_{i,t}}{\tilde{U}_{i,t}} \right| \leq \epsilon, \forall i \in \mathcal{N}_{Agg}^{DN}, \forall t$$

$$\tilde{U}_{i,t} = \frac{1}{3} \sum_{\varphi \in \Phi} U_{\varphi,i,t}, \forall i \in \mathcal{N}_{Agg}^{DN}, \forall t$$

Three-phase power loss:

$$PL_{ij,t}^{Loss} = \frac{s_{ij}^H \tilde{r}_{ij} s_{ij,t}}{V_0^2}, \forall ij \in \mathcal{E}^{DN}, \forall t$$

Other constraints are similar to those in the single-phase distribution network modeling.

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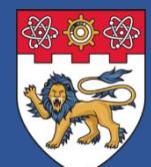
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▪ Uncertainty Handling

□ Scenario-Based Ambiguity Set

The uncertain renewable generation is captured by

$$\mathcal{F} = \left\{ \mathbb{P} \in \mathcal{P}_0(\mathbb{R}^{|U|} \times S) \middle| \begin{array}{l} (\tilde{\mathbf{u}}, \tilde{s}) \sim \mathbb{P} \\ \mathbb{E}_{\mathbb{P}}[\tilde{\mathbf{u}} | \tilde{s} \in S] \in \mathcal{Q} \\ \mathbb{P}[\tilde{\mathbf{u}} \in U_s | \tilde{s} = s] = 1, \forall s \in S \\ \mathbb{P}[\tilde{s} = s] = p_s, \forall s \in S \\ \mathbf{p} \in \mathcal{P} \end{array} \right\}$$

The scenario-based ambiguity set is a highly generalized formulation.

Remark 1: It provides a unified uncertainty formulation for SO, RO and DRO. A RSO model with the scenario-based ambiguity set can shrink to a SO model when U_s is reduced to the sample vector $\hat{\mathbf{u}}_s$ for each scenario s . The RSO can become a RO model when $|S| = 1$.

Remark 2: It encompasses most existing ambiguity sets. For instance, a Wasserstein metric-based ambiguity set can be mapped into the format of a scenario-based ambiguity set as:

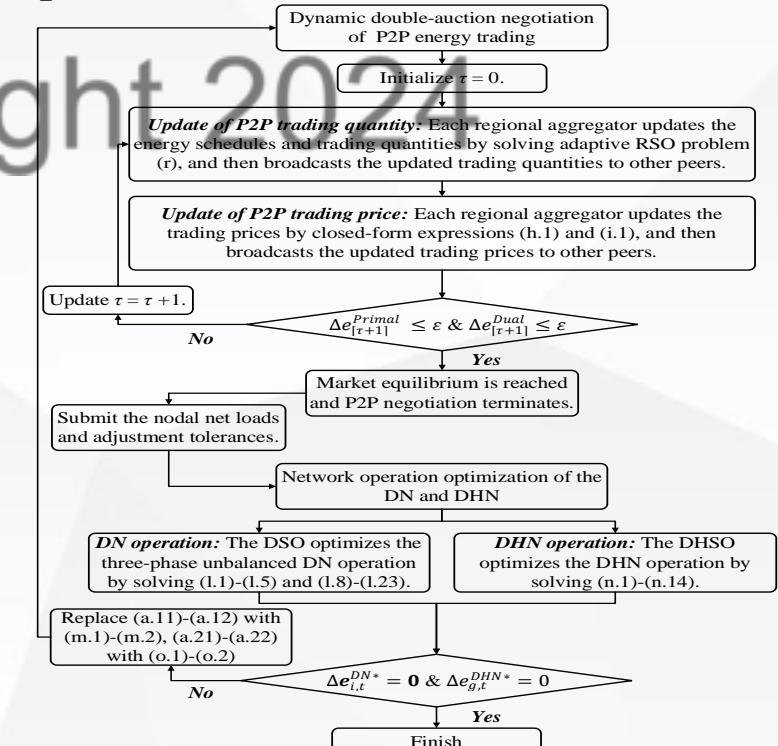
$$\mathcal{F}_W^1 = \left\{ \mathbb{P} \in \mathcal{P}_0(\mathbb{R}^{|U|} \times S) \middle| \begin{array}{l} (\tilde{\mathbf{u}}, \tilde{s}) \sim \mathbb{P} \\ \mathbb{E}_{\mathbb{P}}[d(\tilde{\mathbf{u}}, \hat{\mathbf{u}}_{\tilde{s}}) | \tilde{s} \in S] \leq \Gamma \\ \mathbb{P}[\tilde{\mathbf{u}} \in U_s | \tilde{s} = s] = 1, \forall s \in S \\ \mathbb{P}[\tilde{s} = s] = 1/|S|, \forall s \in S \end{array} \right\}$$

□ Adaptive Robust Stochastic (RSO) Optimization

Based on the developed scenario-based ambiguity set for uncertainties, the update of trading quantity during dynamic double-auction negotiation is rewritten as:

$$\begin{aligned} \left\{ \mathbf{x}_{m,t}^{NA,[\tau+1]}, \mathbf{x}_{m,t}^{A,[\tau+1]} \right\}_{t \in N_T} &= \\ \operatorname{argmin}_{(\mathbf{x}_{m,t}^{NA}, \mathbf{x}_{m,t}^A) \in \mathcal{X}_{m,t}} \sup_{\mathbb{P} \in \mathcal{F}_W^{2,m}} \mathbb{E}_{\mathbb{P}} &\left[\mathcal{L}_m \left((\mathbf{x}_{m,t}^{NA}, \mathbf{x}_{m,t}^A), \hat{\mathbf{e}}_{m,t}^{[\tau]}, \lambda_{m,t}^{[\tau]} \right) \right] \end{aligned}$$

□ Implementation



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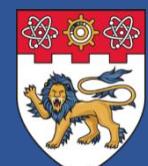
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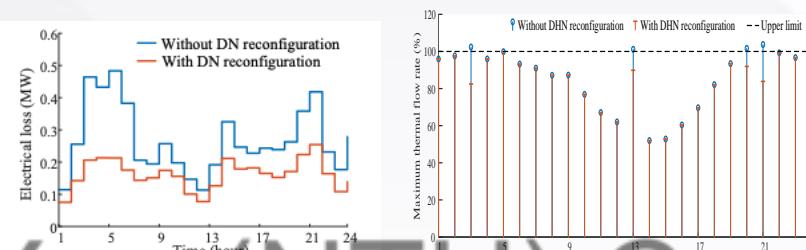


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■ Simulation Results

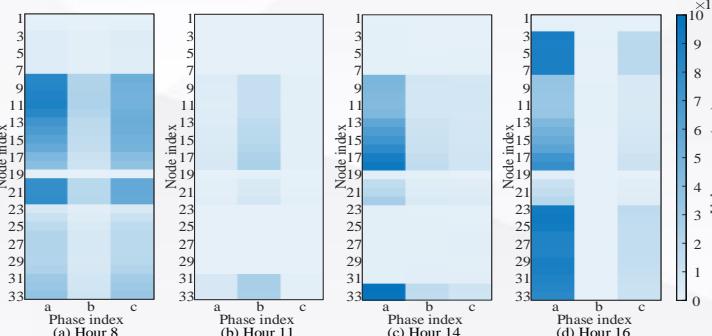
□ Coordination between aggregators and networks

Regional aggregator (RA)		RA 1	RA 2	RA 3	Total
a	Cost without P2P trading (\$)	2778.2	3042.8	5329.6	11150.6
b	Social cost (\$)	3022.6	3689.2	3862.9	10574.7
c	With P2P trading	-304.3	-857.2	1161.5	0
d	P2P payments (\$)	2718.3	2832.0	5024.4	10574.7
e	Benefit from P2P trading [a-d] (\$)	59.9	210.8	305.2	575.9



➤ The double-auction P2P trading mechanism is incentive compatible, and the coordination between aggregators and networks helps reduce network losses and prevent possible network operation issues.

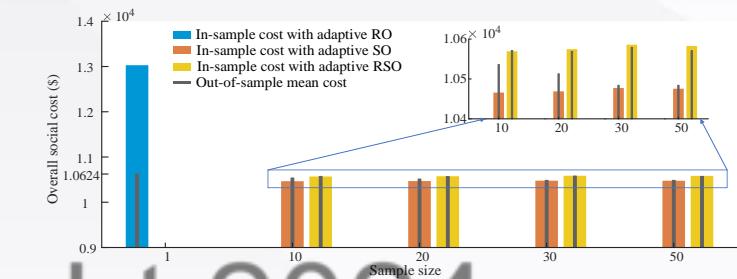
□ Accuracy



➤ Voltage errors stay below 10^{-3} .

□ Performance of adaptive RSO approach

Sample size	Percentage of feasible out-of-sample cases				
	1*	10	20	30	50
Adaptive RO	100%	-	-	-	-
Adaptive SO	-	35.4%	76.3%	85.9%	92.7%
Adaptive RSO	-	98.2%	100%	100%	100%



➤ Adaptive RSO offers a superior performance for uncertainty handling than adaptive RO and SO.

□ Scalability

Index	No. of aggregators	Lower-layer energy scheduling and P2P trading				
		No. of variables*	No. of iterations	Time		
Case 1	3	4057	83	271.79s		
Case 2	5	7599	96	287.01s		
Upper-layer DN operation		Upper-layer DHN operation				
Index	Nodes	No. of variables	Time	Nodes	No. of variables	Time
Case 1	33	24072	210.69s	23	4488	5.09s
Case 2	123	86400	244.75s	37	7416	7.88s

➤ The proposed aggregator-network coordinated P2P trading method is scalable in practice.

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

4. Hierarchy coordination

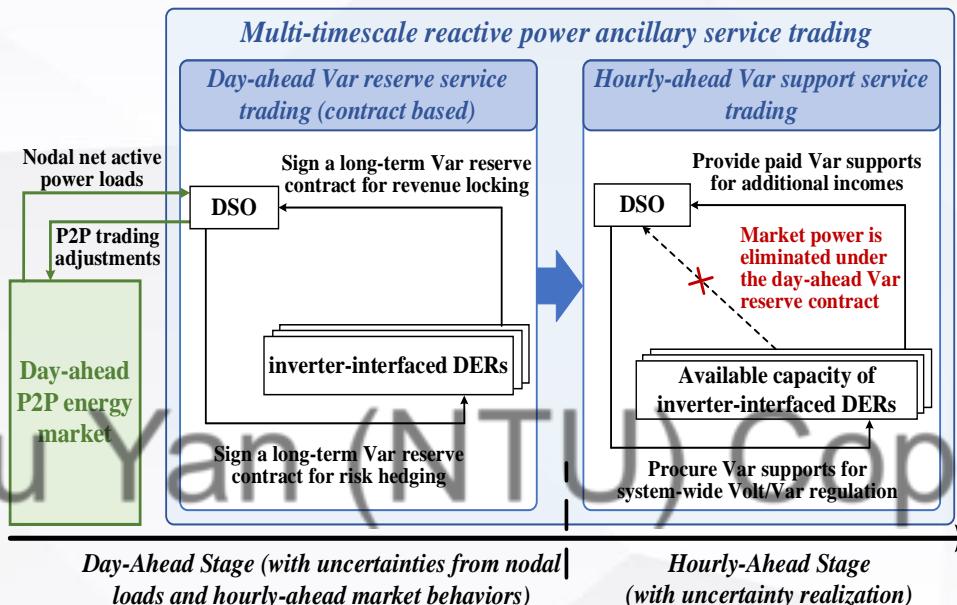
5. Trading

- 1) Design
- 2) Energy trading
- 3) Ancillary service

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) Joint planning

Reactive Power Ancillary Services for Supporting P2P Energy Trading



□ Day-ahead P2P energy market

After P2P negotiation, each agent is required to submit their respective nodal net active power loads to the DSO.

□ Reactive power ancillary service market

Day-ahead Var reserve service trading:

DSO: has a clear incentive to sign a day-ahead Var reserve contract with some DERs for eliminating potential market power.

DERs: are also in favour of a day-ahead contract for revenue protection.

Causes for market power (must-run capacity):

- 1) **system configuration deficiency**
- 2) **market structure flaws**

Hourly-ahead Var support service trading:

DSO: needs Var supports for system-wide voltage regulation and loss reduction, after uncertainty realization.

DERs: have incentives to provide available inverter capacity for additional profit earning.

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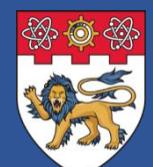
4. Hierarchy coordination

5. Trading

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- 2) Energy trading
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- 3) Joint planning



Mathematical Formulation

Day-ahead Var reserve service trading: a two-stage robust optimization problem

$$\begin{aligned} \min_x \sum_{i \in \mathcal{I}} \pi^{RSV} Q_i^{RSV} + \sum_{t \in \mathcal{T}} \sum_{m \in \mathcal{N}_{Ag}^{DN}} \partial |\Delta e_{m,t}^{DN}| + \\ \max_u \min_y \sum_{t \in \mathcal{T}} (\sum_{h \in \mathcal{N}_{St}^{DN}} \pi_t^{HV,Q} |Q_{h,t}^{HV}| + \sum_{i \in \mathcal{I}} \pi_{i,t}^{INV} |Q_{i,t}^{INV,ST}| + \sum_{mn \in \mathcal{E}^{DN}} \pi_t^{HV,P} PL_{mn,t}) \end{aligned}$$

Market clearing based on a uniform price auction:

$$\begin{aligned} 0 \leq Q_i^{RSV} \leq r_i^{DER} \mathcal{B} Q_i^{DER}, \forall i \in \mathcal{I} \\ r_i^{DER} \mathcal{B} P_i^{DER} \leq \pi^{RSV}, \forall i \in \mathcal{I} \end{aligned}$$

Uncertainty sets for nodal power loads and hourly-ahead market behaviors:

$$U^{MRKT} = \left\{ \begin{array}{l} a_{i,t}^{INV}, N^{INV} - n^{MP} \leq \sum_{i \in \mathcal{I}} a_{i,t}^{INV} \leq N^{INV}, \forall t \\ \pi_{i,t}^{INV}, \underline{\pi}_{i,t}^{INV} \leq \pi_{i,t}^{INV} \leq \bar{\pi}_{i,t}^{INV}, \forall i \in \mathcal{I}, \forall t \end{array} \right\}$$

$$U^{Load} = \left\{ \begin{array}{l} p_{m,t}^{Net} \leq P_{m,t}^{Net} \leq \bar{P}_{m,t}^{Net}, \forall m \in \mathcal{N}_{Ag}^{DN}, \forall t \\ Q_{m,t}^L \leq q_{m,t}^L \leq \bar{Q}_{m,t}^L, \forall m \in \mathcal{N}^{DN}, \forall t \\ p_{m,t}^{AcLoad}, \mu^{AcLoad} \leq \frac{\sum_{t \in \mathcal{T}} \sum_{m \in \mathcal{N}_{Ag}^{DN}} p_{m,t}^{Net}}{\sum_{t \in \mathcal{T}} \sum_{m \in \mathcal{N}_{Ag}^{DN}} \check{p}_{m,t}^{Net}} \leq \bar{\mu}^{AcLoad} \\ p_{m,t}^{ReLoad}, \mu^{ReLoad} \leq \frac{\sum_{t \in \mathcal{T}} \sum_{m \in \mathcal{N}^{DN}} q_{m,t}^L}{\sum_{t \in \mathcal{T}} \sum_{m \in \mathcal{N}^{DN}} \check{q}_{m,t}^L} \leq \bar{\mu}^{ReLoad} \end{array} \right\}$$

Xu Yan (NTU) Copyright 2024

Hourly-ahead Var support service trading: a non-cooperative game

Distribution system operator (DSO):

$$\begin{aligned} \min_{\{y, \phi_{i,t}^{INV}\}} \sum_{h \in \mathcal{N}_{St}^{DN}} \pi_t^{HV,Q} |Q_{h,t}^{HV}| + \sum_{i \in \mathcal{I}} \phi_{i,t}^{INV} \\ + \sum_{mn \in \mathcal{E}^{DN}} \pi_t^{HV,P} PL_{mn,t} \end{aligned}$$

s.t.

$$f_t^{DSO}(x^*, y, u^\dagger) \leq 0$$

Inverter-interfaced DERs:

$$\begin{aligned} \max_{\{\ddot{Q}_{i,t}^{INV,ST}, \dot{\phi}_{i,t}^{INV}\}} \ddot{\phi}_{i,t}^{INV} - [\mathcal{C}_{i,t}^{INV}(Q_{i,t}^{INV}) - \mathcal{C}_{i,t}^{INV}(Q_i^{RSV*})] \\ \text{s.t.} \quad Q_{i,t}^{INV} = Q_i^{RSV*} + |\ddot{Q}_{i,t}^{INV,ST}| \\ |\ddot{Q}_{i,t}^{INV,ST}| \leq a_{i,t}^{INV} (\bar{Q}_{i,t}^{INV} - Q_i^{RSV*}) \\ \mathcal{C}_{i,t}^{INV}(Q_{i,t}^{INV}) = \mathcal{C}_{i,t}^{INV,PL}(Q_{i,t}^{INV}) + \mathcal{C}_{i,t}^{INV,LT}(Q_{i,t}^{INV}) \end{aligned}$$

Dynamic negotiation based on Nash Mechanism:

$$\begin{aligned} Q_{i,t}^{INV,ST} &= \frac{1}{2} (\mathcal{B} Q_{i,t}^{PSO2INV} + \mathcal{B} Q_{i,t}^{INV2DSO}), \forall i \in \mathcal{I} \\ \phi_{i,t}^{INV} &= \frac{1}{2} \mathcal{B} P_{i,t}^{INV2DSO} (\mathcal{B} Q_{i,t}^{PSO2INV} + \mathcal{B} Q_{i,t}^{INV2DSO}) \\ &+ (\mathcal{B} P_{i,t}^{PSO2INV} - \mathcal{B} P_{i,t}^{INV2DSO})^2, \forall i \in \mathcal{I} \end{aligned}$$

Reactive power cost incurred by additional power loss in the inverter:

$$\Delta P_{i,t}^{INV,Loss} = \begin{cases} \xi_{INV}^{PL,0} + \xi_{INV}^{PL,1} Q_{i,t}^{INV} + \xi_{INV}^{PL,2} (Q_{i,t}^{INV})^2, & \text{if } P_{i,t}^{INV} = 0 \\ \xi_{INV}^{PL,1} (S_{i,t}^{INV} - P_{i,t}^{INV}) + \xi_{INV}^{PL,2} (Q_{i,t}^{INV})^2, & \text{if } P_{i,t}^{INV} \neq 0 \end{cases}$$

Reactive power cost reflecting inverter lifetime degradation by higher thermal stress:

$$\begin{aligned} \mathcal{C}_{i,t}^{INV,LT}(Q_{i,t}^{INV}) &= \\ \xi_{INV}^{LT,0} + \xi_{INV}^{LT,1} Q_{i,t}^{INV} + \xi_{INV}^{LT,2} (Q_{i,t}^{INV})^2 + \xi_{INV}^{LT,3} (Q_{i,t}^{INV})^3 & \end{aligned}$$

1. REIDS Project

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- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

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- 2) Volt/Var regulation

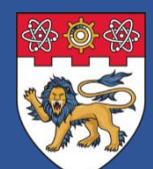
4. Hierarchy coordination

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- 3) Ancillary service

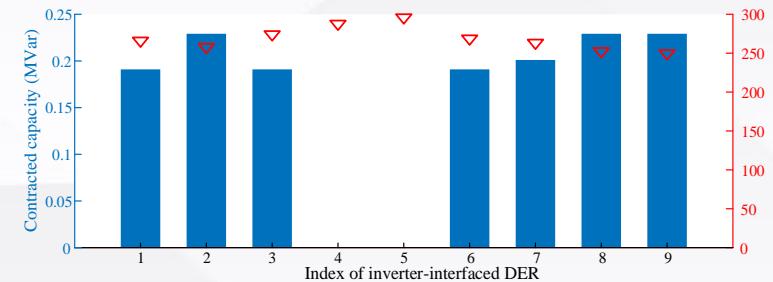
6. Planning

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- 2) ESS planning
- 3) Joint planning



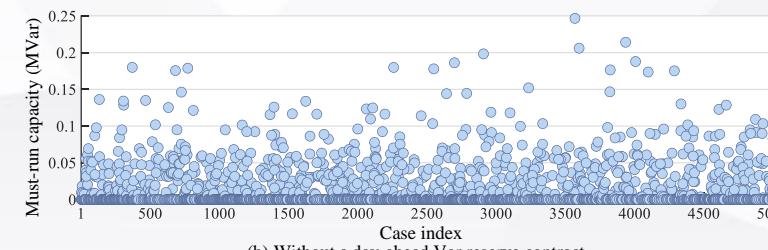
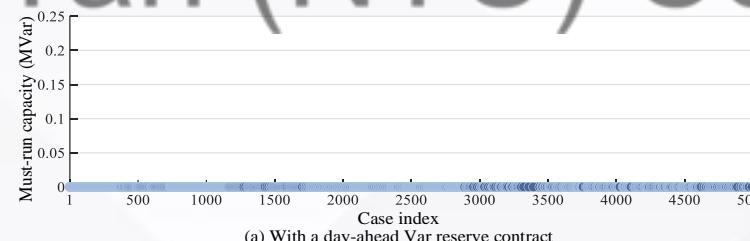
■ Simulation Results

□ Settlement for day-ahead Var reserve service



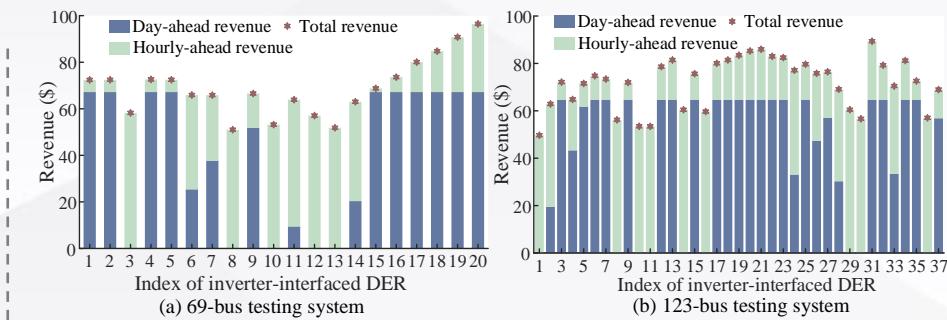
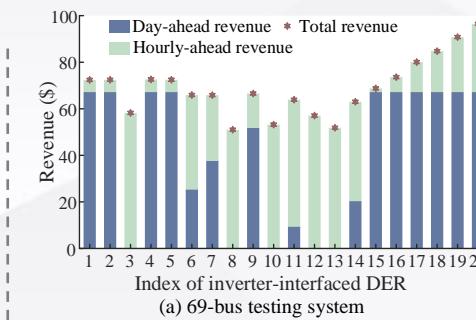
- Uniform price auction motivates DERs to reduce their Var costs, thereby lowering their bidding prices and increasing the likelihood of being selected in the market.

□ Potential market power issue



- Robust day-ahead Var reserve contract prevents DERs from gaining market power and manipulating reactive market prices.

□ Revenue from Var ancillary service trading



- DERs are incentivized to participate in both day-ahead and hourly-ahead trading, thereby providing operational support for distribution systems.

□ Scalability

Distribution network (DN)	33-bus DN	69-bus DN	123-bus DN
Participants in the reactive power ancillary service trading	1 DSO & 9 DERs	1 DSO & 20 DERs	1 DSO & 37 DERs
Day-ahead problem	Algorithm C&CG	Algorithm C&CG	Algorithm C&CG
	No. of iterations 5	4	3
	Solution time 108.2s	120.3s	236.6s
Hourly-ahead problems	Algorithm Algorithm 1	Algorithm 1	Algorithm 1
	No. of iterations 113	261	165
	Solution time 39.8s	110.4s	129.2s
	Parallel solution time 4.0s	5.3s	3.4s

- The framework and methods are highly scalable.

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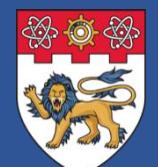
4. Hierarchy coordination

5. Trading

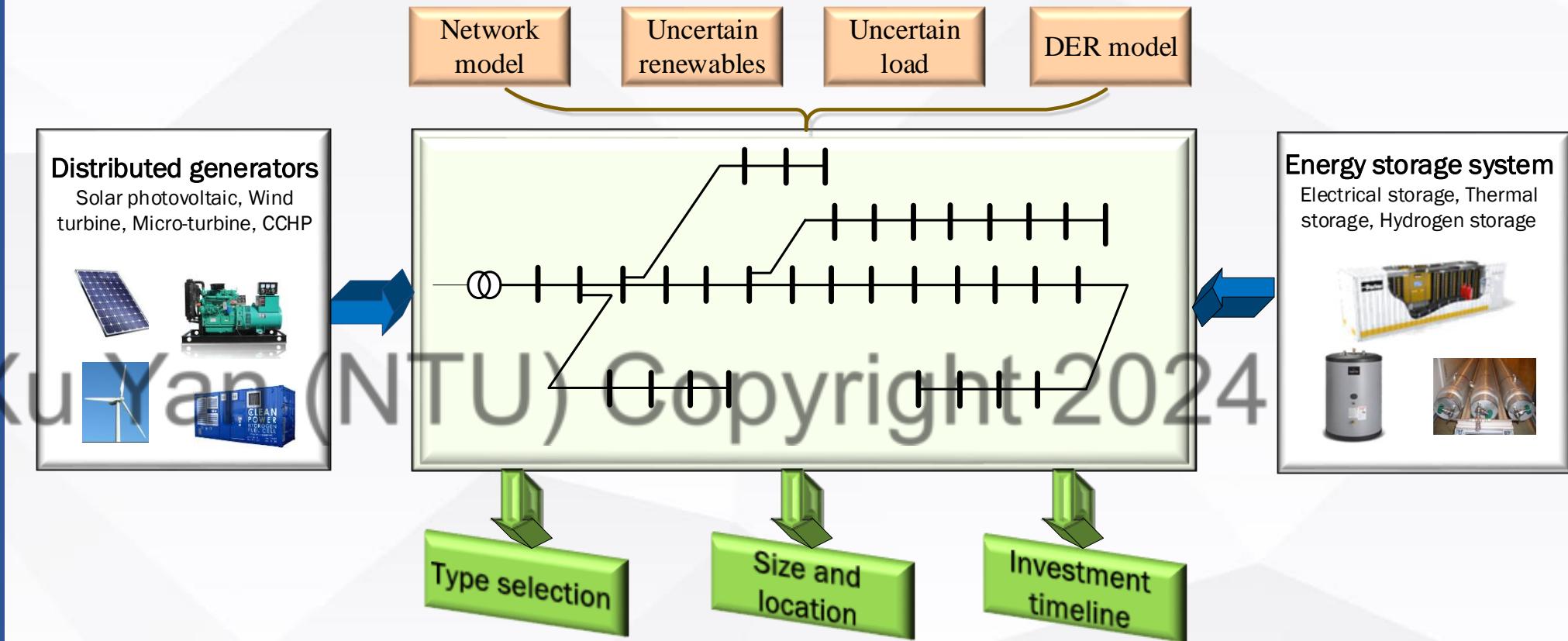
- 1) Review
- 2) Centralized trading
- 3) P2P trading

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) Joint planning



Optimal Planning of DERs in Microgrid



Objective: Minimize total investment costs

Constraints: operational limits
network constraints
component constraints, etc.

Variables: size, site, type, installation year, etc.

Stochastic programming
Robust optimization
Probability-weighted robust optimization
...

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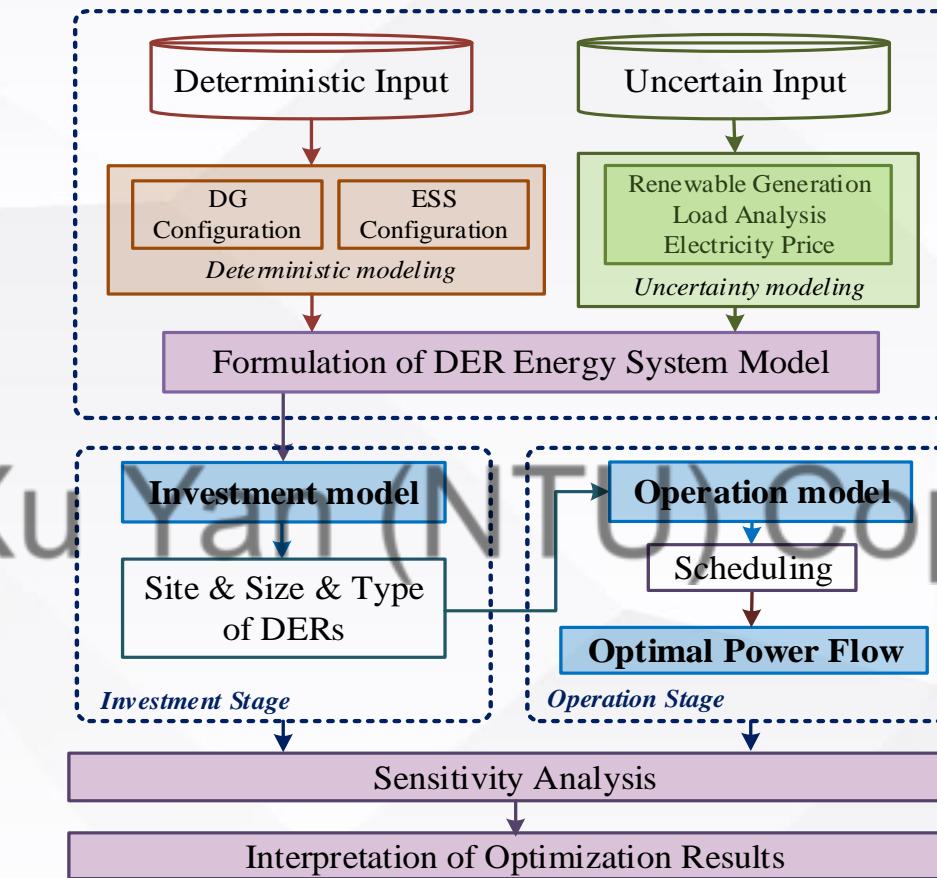
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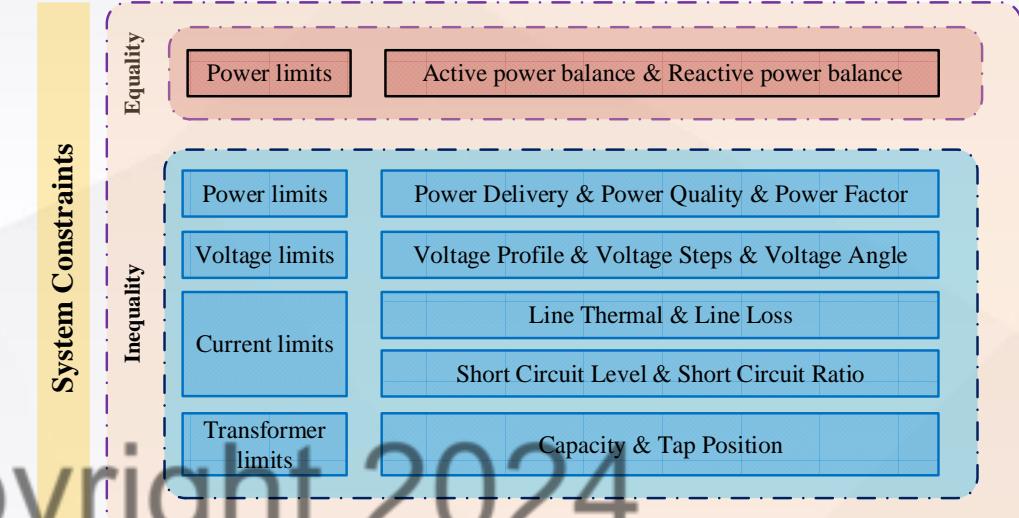
- 1) DG planning
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- 3) Joint planning

Optimal Planning of DERs in Microgrid



Two-stage framework of the DER planning

R. Leng, Z. Li, and Y. Xu, "A comprehensive literature review for optimal planning of distribution energy resources in distribution grid," *Proc. IEEE ISGT-Asia 2022*, 1-5 Nov. Singapore.



The constraints of distributed generator planning

	Objective
Technical	<ul style="list-style-type: none">Maximization of system reliabilityMinimization in system lossesMinimization of voltage deviationMinimization of absolute active power flow
Economical	<ul style="list-style-type: none">Maximization of social welfareMaximization of system annual profitMinimization of investment and operation cost
Environmental	<ul style="list-style-type: none">Minimization of gas emissions

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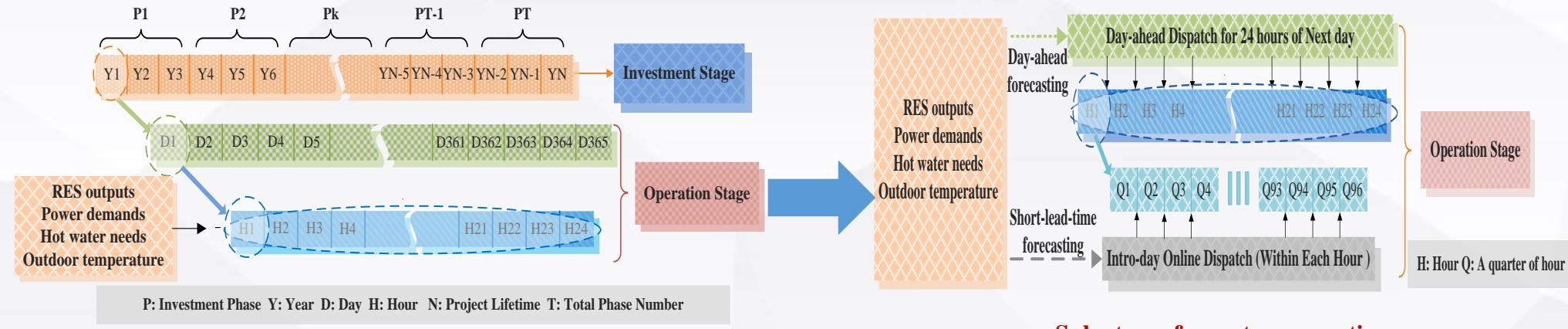
- 1) Review
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Optimal Placement of Heterogeneous Distributed Generators



Proposed two-stage DG placement method

$$NPV_s = \max_{z \in CF_z, x \in CG_x} \left\{ \underbrace{-F(z)}_{\text{Investment Stage}} + \underbrace{G(x)}_{\text{Operation Stage}} \right\}$$

$$\min G(x|c) = \min_w \{ S(w|c) + E[Q(w|c, \omega)] \}$$

$$s.t. \quad w \in CS_w \mid z$$

$$Q(w|c, \omega) = \min_y L(y|c)$$

$$y \in CL(w, \omega)$$

System multi-stage operation model

Year/Bus	3	6	9	12	18	22	25	27	30	33
CCHP unit: Cap-65										
1-4	65	195	65	130	0	0	130	65	0	65
5-8	65	195	65	195	0	65	130	65	65	65
9-12	65	195	65	195	65	65	130	65	65	130
Electric boiler: A										
1-4	123.2	96	90.7	0	146.8	41.5	167.8	92.9	0	0
5-8	123.2	96	128.1	0	146.8	88.5	214.8	92.9	0	0
9-12	138.5	96	129.6	0	146.8	120.4	216.2	92.9	0	0
Electric boiler: B										
9-12	0	0	0.0	57.1	0	66.7	74.1	0	0	0
Electric chiller: A										
1-4	200.2	0	68.4	0	105.8	0.0	141.3	0	0	48.25
Electric chiller: B										
1-4	0	0	25.0	0	0	50.7	74.3	0	0	0
5-8	0	0	50.3	0	0	103.8	115.2	0	0	0
9-12	0	0	90.9	0	0	143.0	115.2	0	0	0
Photovoltaics: B										
1-12	137.6	137.6	136.2	122.2	118.9	137.7	181.6	181.6	177.8	169
Wind turbine: A										
1-12	80	0	0	0	0	80	80	0	80	0
Wind turbine: B										
1-12	0	240	120	0	240	0	240	0	120	0

1. REIDS Project

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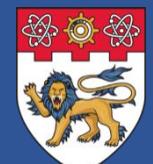
4. Hierarchy coordination

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- 3) Joint planning



■ Probability-Weighted Robust Optimization (PRO) for DG Planning

Problems identification: Robust optimization only considers the worst case under a single day profile, while stochastic programming cannot cover full spectrum of uncertainties and thus full operational robustness.

Our aims: to ensure a full robustness for the short-term operation under the uncertainties over the long-term planning horizon.

Probability-Weighted Uncertainty Sets

$$U_v^D = \{\underline{\mu}_{y,v}^D \leq \sum_{t \in T} \sum_{i \in I} h \times P_{i,t,y,v}^D \leq \bar{\mu}_{y,v}^D, \forall y, \\ P_{i,t,y,v}^D \leq \underline{P}_{i,t,y,v}^D \leq \bar{P}_{i,t,y,v}^D, \forall i, t, y\} \text{ with } \rho_v, \forall v = 1, 2, \dots, n_v$$

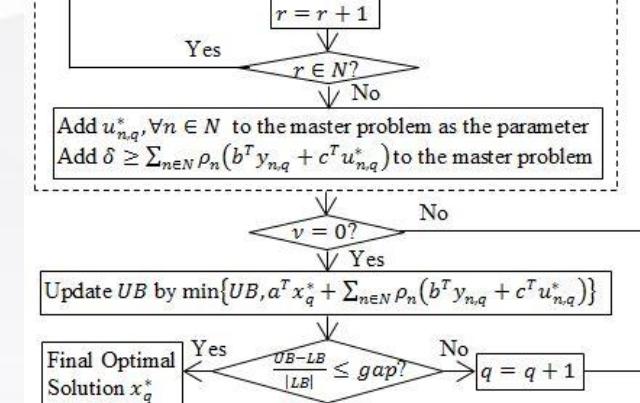
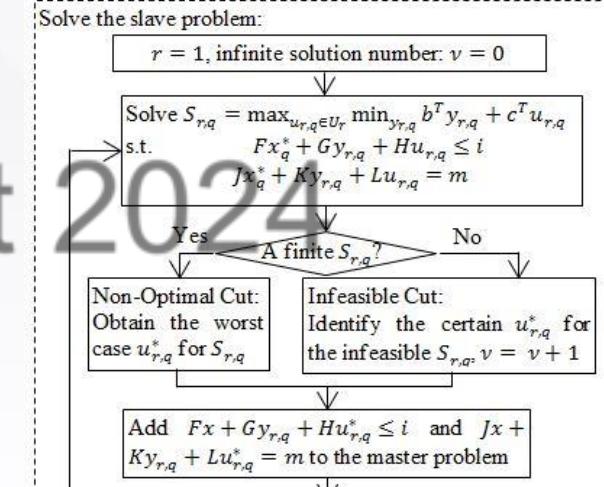
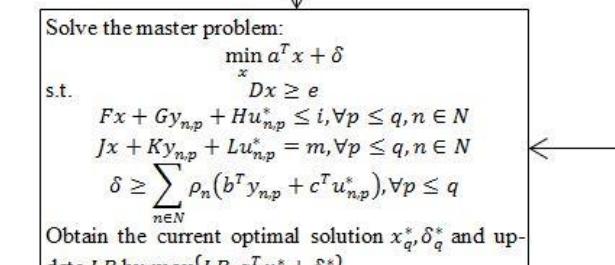
PRO Formulation

$$\min_x a^T x + \sum_{n \in N} \rho_n (\max_{u_n \in U_n} \min_{y_n} b^T y_n + c^T u_n) \\ \text{s.t.} \\ Dx \geq e \\ Fx + Gy_n + Hu_n \leq i, \forall n \\ Jx + Ky_n + Lu_n = m, \forall n$$

C. Zhang, Y. Xu*, Z.Y. Dong, "Probability-Weighted Robust Optimization for Distributed Generation Planning in Microgrids," *IEEE Trans. Power Syst.*, 2018.

Solution Algorithm

Initialize the lower bound LB as $-\infty$, the upper bound UB as $+\infty$, $u_{n,0} = u_{n,mean}, \forall n \in N$ and the iteration number $q = 0$



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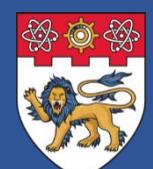
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■ Probability-Weighted Robust Optimization (PRO) for DG Planning

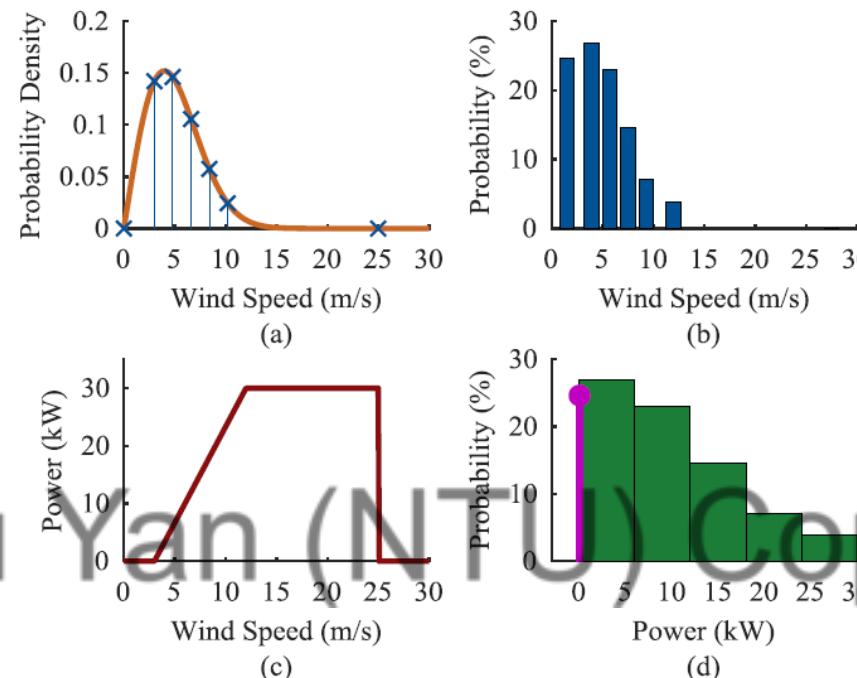


Fig. 3 (a) Wind speed probability density; (b) Wind speed probability; (c) Wind power generation function; (d) Wind power probability.

COMPARISON BETWEEN DIFFERENT METHODS

DG Planning Method	PRO	RO			
Uncertainty Profile Case	N/A	1	2	3	4
Voltage Violation Rate	0%	8.12%	0%	3.12%	11.44%
Profit in NPV (M\$)	23.51	24.71	23.43	24.50	24.74

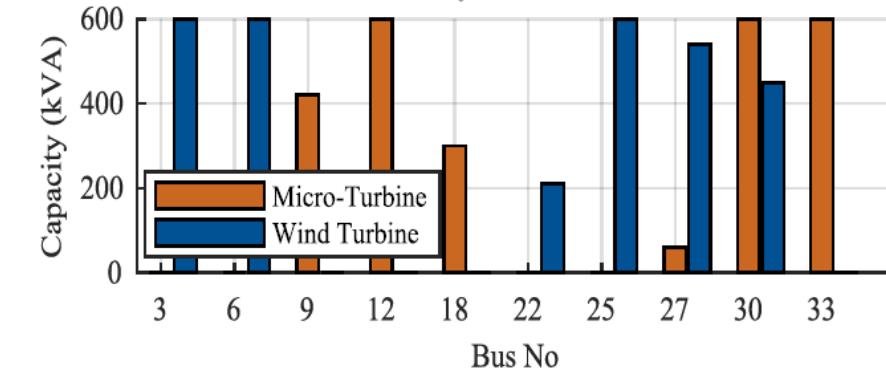
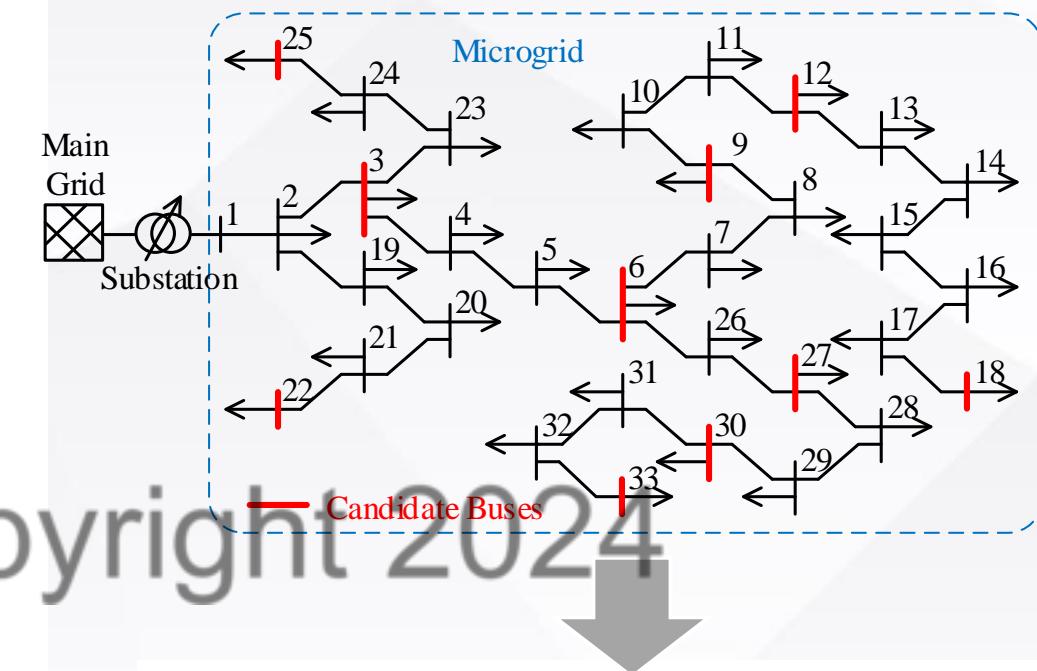


Fig. 4 DG planning decisions.

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- 2) Volt/Var regulation

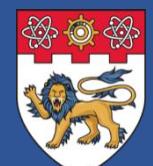
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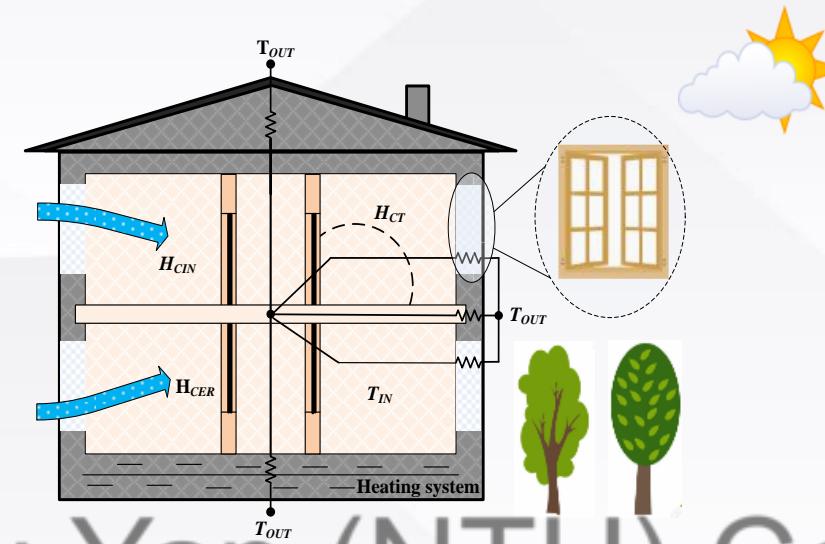
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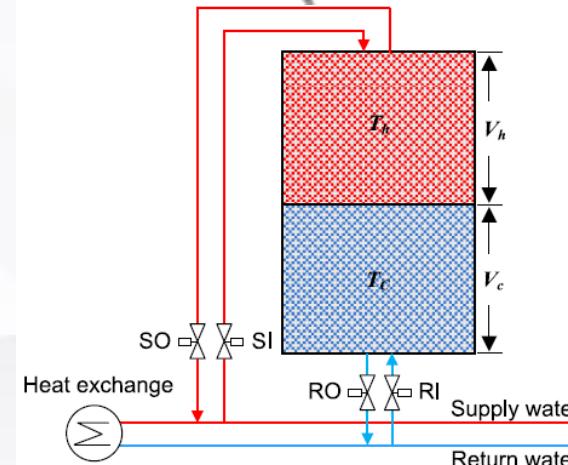


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Optimal Deployment of Heterogeneous Energy Storage



Typical structure of a room in a residential building



Structure of the thermal storage

$$\max_{z \in Z, x \in X, \eta_{\text{VaR}} \in \mathcal{R}} [C_{\text{EDP}} - \rho_{RK} C_{\text{VaR}}(\alpha)(C_{\text{EDP}})]$$

$$\text{s.t., } C_{\text{EDP}} = \frac{1}{365 \times N_p} \cdot \frac{dr(1+dr)^{N_p}}{(1+dr)^{N_p} - 1}$$

$$\cdot \left[\underbrace{-F(z)}_{\text{Investment Stage}} + \underbrace{G(x)}_{\text{Operation Stage}} \right]$$

$$C_{\text{VaR}}(\alpha)(C_{\text{EDP}}) = \eta_{\text{VaR}} + \frac{1}{1-\alpha CL} E \times [\max(C_{\text{EDP}} - \eta_{\text{VaR}}, 0)]$$

Risk-averse objective function

$$\min_x G(x) = \min_{w, y_1, y_2, \dots, y_q} [S(w) + \sum_{q \in N_Q} c_q L(y_q)]$$

$$\text{s.t. } w \in CS_w \mid z$$

$$y_q \in CL(w, \omega_q), \forall q$$

Proposed multi-stage stochastic deployment model

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

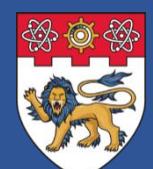
4. Hierarchy coordination

5. Trading

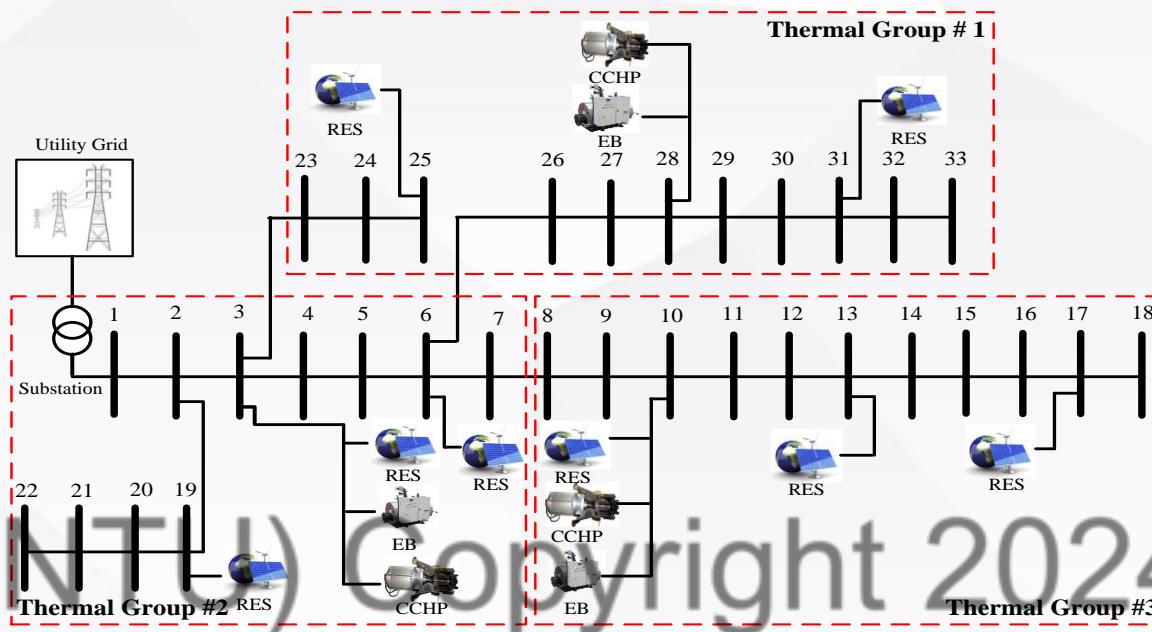
- 1) Review
- 2) Centralized trading
- 3) P2P trading

6. Planning

- 1) DG planning
- 2) ESS planning
- 3) Joint planning



■ Planning results



Deployment Results For Battery Storage (kWh)

Year/Bus	3	6	18	22	25	27	30	33
1-3	1500	0	0	1500	1500	0	0	0
4-6	1500	466.0	101.7	1500	1500	0	0	473.2
7-9	1500	466.0	101.7	1500	1500	378.0	81.19	473.2

Deployment Results For Thermal Storage (kWh)

Year 1-9	Group 1	Group 2	Group3
Cooling storage tank	0	0	0
Heat storage tank	1800	1800	1800

1. REIDS Project

2. Control

- 1) Islanded mode
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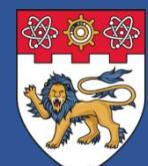
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Joint Planning of Utility-Owned Distributed Energy Resources in an Unbalanced Active Distribution Network Considering Asset Health Degradation

Research motivation: DERs asset health will degrade along with the service period. The asset health degradation of DER will cause nameplate capacity decrease and incur the extra cost of operation and maintenance.

Our aims: proposes a new planning method for utility-owned distributed generators and energy storage systems in an unbalanced active distribution network considering asset health degradation.

- WT blade erosion



- PV module degradation



- DG capacity drop modeling by Wiener model:

$$\Gamma_{cap}^{q,y} = \Gamma_{cap}^{q,y-\Delta y} + \lambda_{cap}^q a(y - \Delta y)^{a-1} \Delta y + \sigma_{cap}^q Y \sqrt{\Delta y}$$

- DG O&M cost increase modeling by Wiener model:

$$\chi_{om}^{q,y,d,t} = \chi_{om}^{q,y,d,t-\Delta t} + \lambda_{om}^q b(t - \Delta t)^{b-1} \Delta t + \sigma_{om}^q Y \sqrt{\Delta t}$$

Proposed DG health degradation model based on the Wiener model

R. Leng, Z. Li, **Y. Xu***, Joint Planning of Utility-Owned Distributed Energy Resources in an Unbalanced Active Distribution Network Considering Asset Health Degradation[J]. *IEEE Transactions on Smart Grid*, 2024.

● The linearized three-phase power flow

Active power balance:

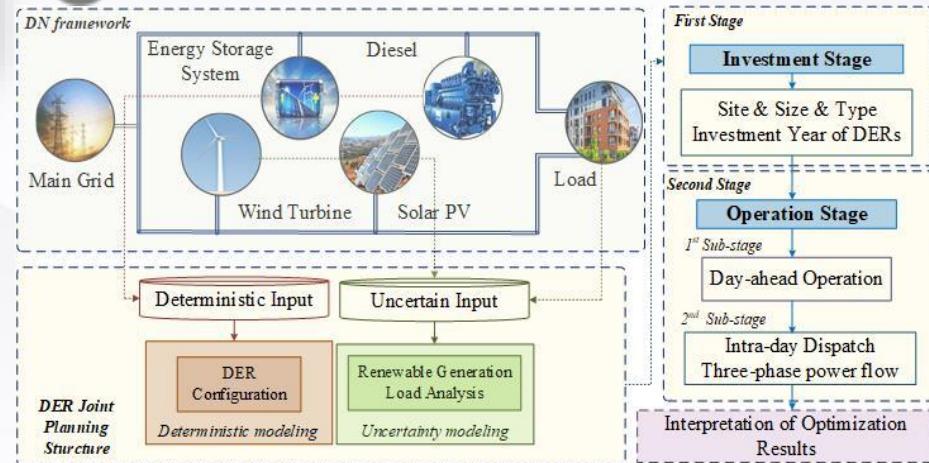
$$\begin{aligned} P_{flw}^{p,y,d,t,br+1} &= P_{flw}^{p,y,d,t,br} - P_{flw}^{p,y,d,t,0,br+1} - P_{LD}^{p,y,d,t,i} + P_{DE}^{p,y,d,t,i} \\ &\quad + P_{PV}^{p,y,d,t,i} + P_{WT}^{p,y,d,t,i} + P_{BSD}^{p,y,d,t,i} - P_{BSC}^{p,y,d,t,i} \end{aligned}$$

Reactive power balance:

$$Q_{flw}^{p,y,d,t,br+1} = Q_{flw}^{p,y,d,t,br} - Q_{flw}^{p,y,d,t,0,br+1} - Q_{LD}^{p,y,d,t,i} + Q_{WT,PV}^{p,y,d,t,i}$$

Voltage Constraint:

$$\begin{bmatrix} V_a^{y,d,t,i+1} \\ V_b^{y,d,t,i+1} \\ V_c^{y,d,t,i+1} \end{bmatrix} = \begin{bmatrix} V_a^{y,d,t,br} \\ V_b^{y,d,t,br} \\ V_c^{y,d,t,br} \end{bmatrix} - \bar{Z}_{i \rightarrow j} \begin{bmatrix} P_{flw,a}^{y,d,t,br} - jQ_{flw,a}^{y,d,t,br} \\ P_{flw,b}^{y,d,t,br} - jQ_{flw,b}^{y,d,t,br} \\ P_{flw,c}^{y,d,t,br} - jQ_{flw,c}^{y,d,t,br} \end{bmatrix} - \bar{Z}_{i \rightarrow j}^* \begin{bmatrix} P_{flw,a}^{y,d,t,br} + jQ_{flw,a}^{y,d,t,br} \\ P_{flw,b}^{y,d,t,br} + jQ_{flw,b}^{y,d,t,br} \\ P_{flw,c}^{y,d,t,br} + jQ_{flw,c}^{y,d,t,br} \end{bmatrix}$$



The proposed DERs joint planning framework

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

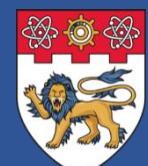
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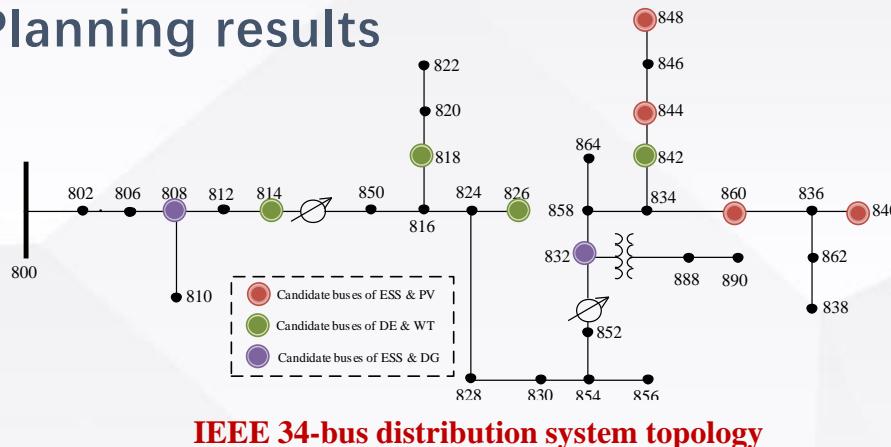
- 1) DG planning
- 2) ESS planning
- 3) Joint planning



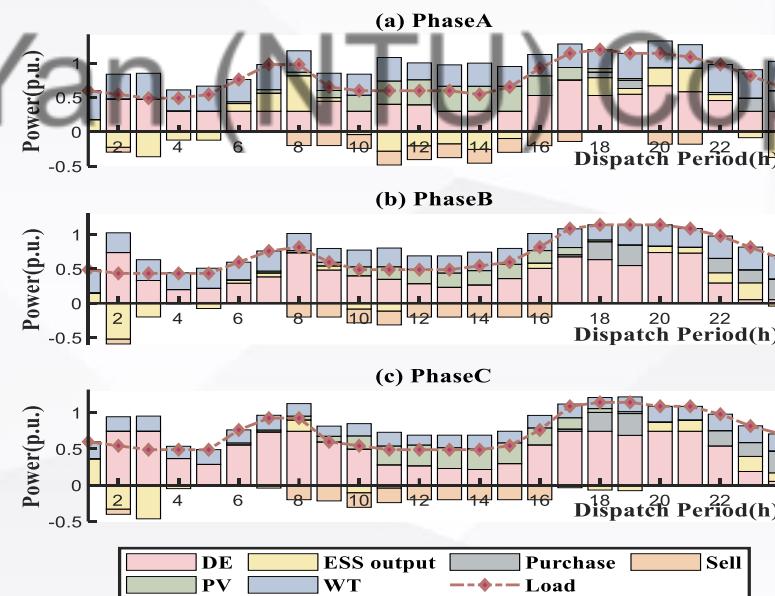
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Joint Planning of Utility-Owned Distributed Energy Resources in an Unbalanced Active Distribution Network Considering Asset Health Degradation

■ Planning results



IEEE 34-bus distribution system topology



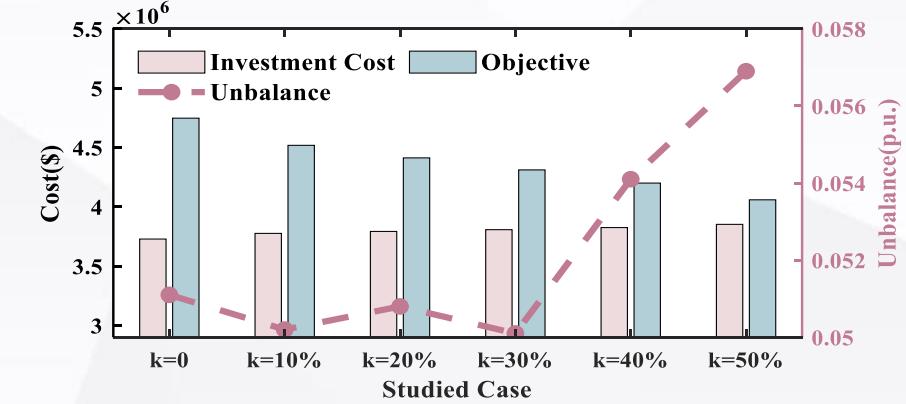
Simulation results for operation stage in year 2034-Spring/Fall

DERs deployment results

Year	Phase /bus	DE (kW)				WT (kW)		
		808	814	826	842	808	814	826
1-4	A	0	50	0	0	50	200	0
	B	150	0	0	0	200	50	70
	C	80	0	280	0	0	0	200
5-8	A	0	240	120	0	50	200	0
	B	180	0	0	270	200	70	70
	C	80	0	0	250	40	0	200
9-12	A	0	240	120	160	50	200	0
	B	200	0	0	400	200	70	70
	C	90	0	330	290	40	0	200

TABLE V. ESS AND PV GENERATORS DEPLOYMENT RESULTS

Year	Phase/ bus	ESS (kWh)			
		808	860	840	844
1-4	A	0	0	0	0
	B	240	0	0	0
	C	0	240	0	0
5-8	A	0	0	0	0
	B	240	0	0	0
	C	0	240	0	0
9-12	A	0	240	0	240
	B	240	0	240	0
	C	0	240	240	0
Year	Phase	PV (kW)			
1-12	A	200	0	0	165
	B	183	0	200	0
	C	0	180	200	0



Comparison results for different degradation parameters

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

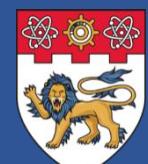
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Real-Option Based Planning of Utility-Owned Distributed Energy Resources for Islanded Distribution Networks in Southeast Asia

● Research challenges and contributions in this paper

DERs planning for islanded DNs in Southeast Asia

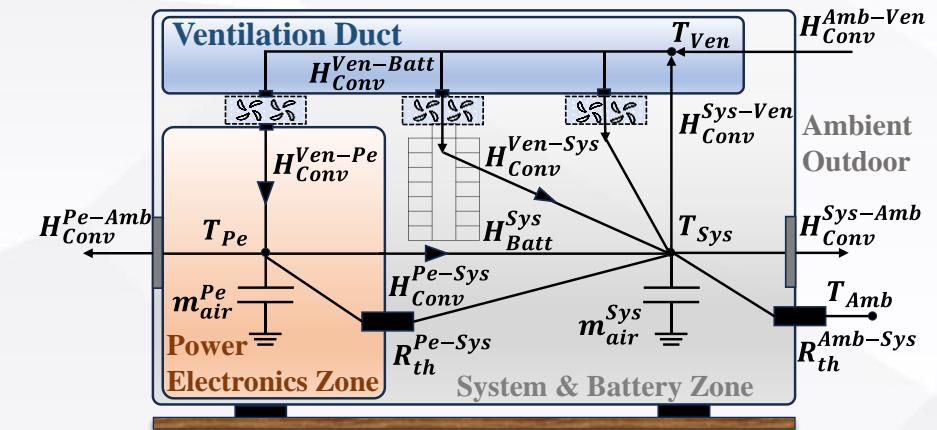
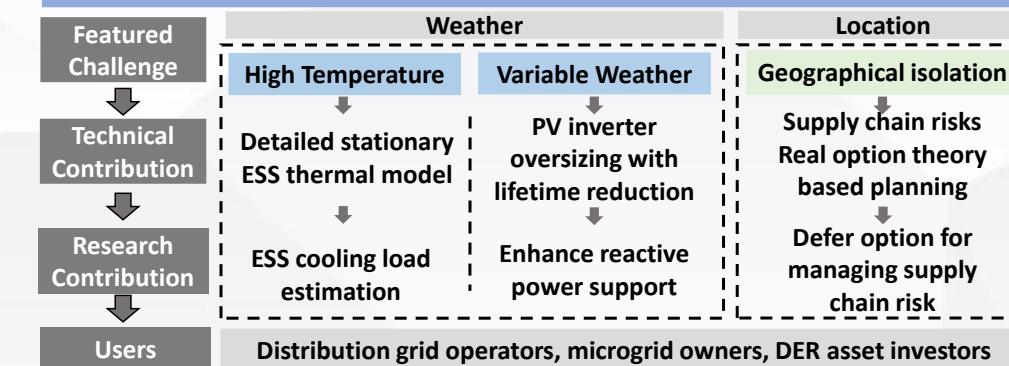


Illustration of the ESS container system thermal management

● Supply Chain Risk Model

Supply chain risk degree:

$$\Theta_{Ma}^q = \frac{y_q [\Upsilon + (n-1)(1+\varpi\delta_q^2)]}{2\mu_{Ma}^q [2\Upsilon + (n-1)(1+\varpi\delta_q^2)] [\Upsilon + n(1+\varpi\delta_q^2)] (2+\varepsilon)}$$

Warehouse disruption risk degree:

$$\lambda_{wa}^{q,d} = \max\{0, [\lambda_{wa}^{q,d-1} + \min\{(1-\lambda_{wa}^{q,d-1}), (\frac{1}{\partial^{q,d}})\}] \cdot [1 - \Lambda^{q,d} \frac{\psi^{q,d}}{100}]\}$$

Real option valuation:

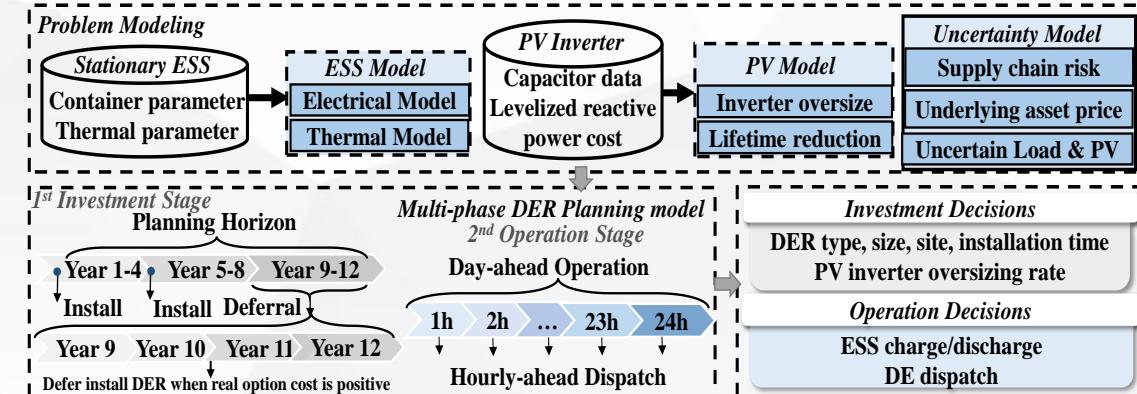
$$C_{DERopt}^y = S_{DER}^y \cdot N(d_1) - K_{DER}^y \cdot e^{-r_f T} \cdot N(d_1 - \sigma_{DER} \sqrt{T})$$

$$d_1 = \ln(S_{DER}^y / K_{DER}^y) + (r_f + 0.5\sigma_{DER}^2)T / \sigma_{DER} \sqrt{T}$$

$$S_{DER}^y(t + \Delta t) = S_{DER}^y(t) + \mu_{DER}t + \sigma_B Y \sqrt{\Delta t}$$

Multistage and multiphase framework for DER joint planning:

In the investment stage, the entire planning period is divided into multiple planning sub-horizons. The operation stage involves the day-ahead operation and hourly ahead dispatch.



The proposed DER planning framework

1. REIDS Project

2. Control

- 1) Islanded mode
- 2) Grid-tied mode

3. Operation

- 1) Energy dispatch
- 2) Volt/Var regulation

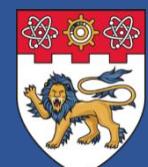
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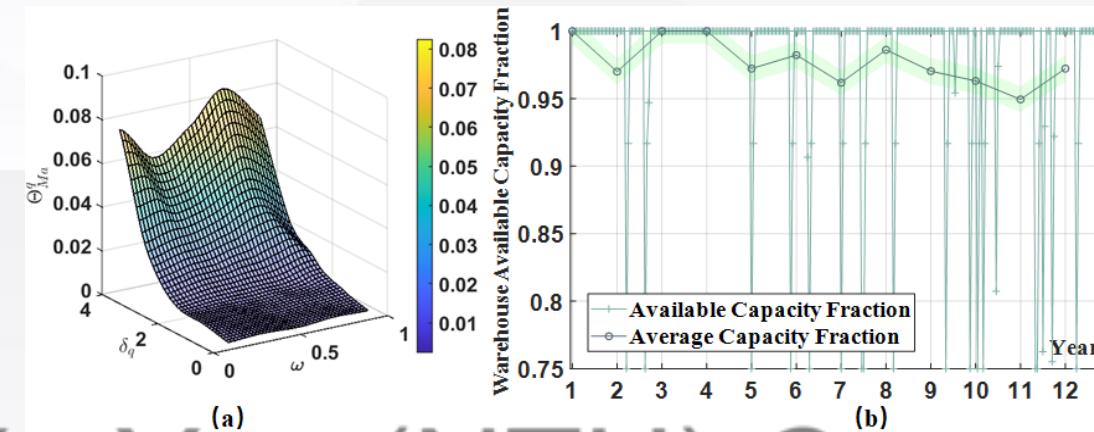
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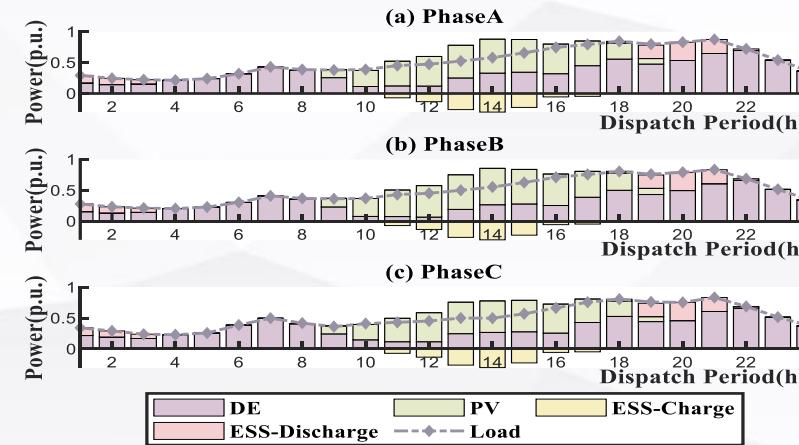
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Real-Option Based Planning of Utility-Owned Distributed Energy Resources for Islanded Distribution Networks in Southeast Asia

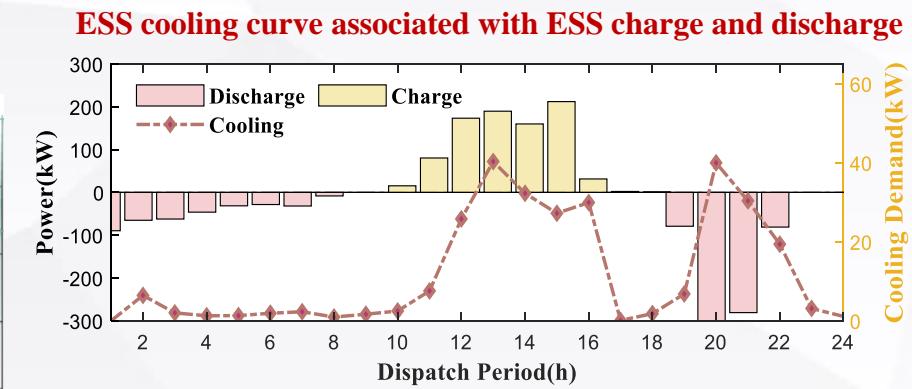
■ Simulation results



Supply chain risk parameters. (a) Joint impact of ω , δ_q and supply risk degree $\theta_{M_a}^q$ at n=4. (b) Warehouse Capacity Fraction Curve for 12 years.

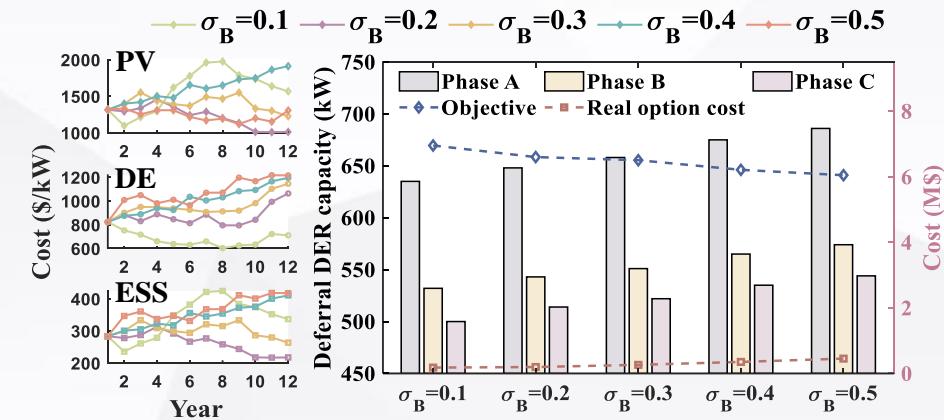


Simulation results for the operation stage in June 2035



PV inverter oversizing results in the final planning year

Phase A		Phase B		Phase C	
Bus	OS%	Bus	OS%	Bus	OS%
808	28%	808	60%	808	60%
860	49%	840	23%	860	19%
840	60%	848	60%	844	60%
848	60%	832	42%	832	60%



Sensitivity results for different volatility values

Y. Xu, Y. Wang, C. Zhang, and Z. Li, "Coordination of Distributed Energy Resources in Microgrids: Optimisation, control, and hardware-in-the-loop validation," IET Press, 2021



Coordination of Distributed Energy Resources in Microgrids Optimisation, control, and hardware-in-the-loop validation

Yan Xu, Yu Wang, Cuo Zhang and Zhengmao Li



Foreword

A microgrid is composed of a medium/low-voltage distribution system with distributed energy resources (DERs) such as distributed generators (DGs), energy storage systems (ESSs), and controllable loads, which can operate either connected or disconnected from the main grid. Microgrids are an effective means to integrate renewable energy through smart grid technologies. In the past couple of decades, microgrids have been widely researched and developed and are starting to be widely deployed.

Due to the significantly diverse temporal and spatial characteristics of different DERs and the significant operational uncertainties from intermittent renewable energy-based DERs, the planning, operation, and control of DERs in microgrids present challenging problems. Thus, this book focuses on coordination aspects of DERs in the context of microgrids, presenting various advanced techniques for optimal planning, operation, and control of DERs for secure, economic, and robust microgrid operation. Major topics covered in this book include:

- Comprehensive mathematical modelling of DERs and microgrids.
- Optimal sizing and siting of DERs in microgrids.
- Robust and stochastic optimisation for active and reactive power dispatch of DERs in microgrids.
- Distributed coordinated control of DERs in microgrids in grid-connected and islanded modes.
- Power and controller hardware-in-the-loop tests for validation of control algorithms.

Written by a dedicated research team that has been working on DERs and microgrids for over ten years, this book is a systematic presentation of the authors' original research work and insights on these topics. With a balanced presentation of theory and practice, it can be a valuable reference for researchers, engineers, and graduate students in the areas of DERs and microgrids.

Claudio Cañizares, PhD, P.Eng., FIEEE, FRSC, FCAE

University Professor and Hydro One Endowed Chair

Executive Director, Waterloo Institute for Sustainable Energy (WISE)

University of Waterloo, Canada

Editor-in-Chief, *IEEE Transactions on Smart Grid*

IEEE Division VII Director-Elect

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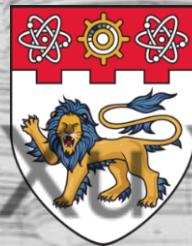
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■ Publications Microgrid Planning

1. R. Leng and **Y. Xu***, Real-Option Based Planning of Utility-Owned Distributed Energy Resources for Islanded Distribution Networks in Southeast Asia,” *IEEE Trans. Smart Grid, 2024*.
2. R. Leng, Z. Li, and **Y. Xu***, “Joint Planning of Utility-Owned Distributed Energy Resources in an Unbalanced Active Distribution Network Considering Asset Health Degradation,” *IEEE Trans. Smart Grid, 2024*.
3. Z. Li, **Y. Xu***, et al, “Optimal Deployment of Heterogeneous Energy Storage System in a Residential Multi-Energy Microgrid with Demand Side Management,” *IEEE Trans. Industrial Informatics, 2020*. – **Web-of-Science Highly Cited Paper**
4. Z. Yan, T. Zhao, **Y. Xu***, et al, “Data-driven Robust Planning of Electric Vehicle Charging Infrastructure for Urban Residential Carparks,” *IET Gen. Trans. & Dist., 2020*.
5. Z. Li, **Y. Xu***, et al, “Optimal Placement of Heterogeneous Distributed Generators in a Grid-Connected Multi-Energy Microgrid under Uncertainties,” *IET Renewable Power Generation, 2019*.
6. C. Zhang, **Y. Xu***, Z.Y. Dong, et al, “Probability-Weighted Robust Optimization for Distributed Generation Planning in Microgrids,” *IEEE Trans. Power Syst., 2018*.
7. **Y. Xu**, Z.Y. Dong, K.P. Wong, et al, “Optimal capacitor placement to distribution transformers for power loss reduction in radial distribution systems,” *IEEE Trans. Power Systems, 2013*.

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