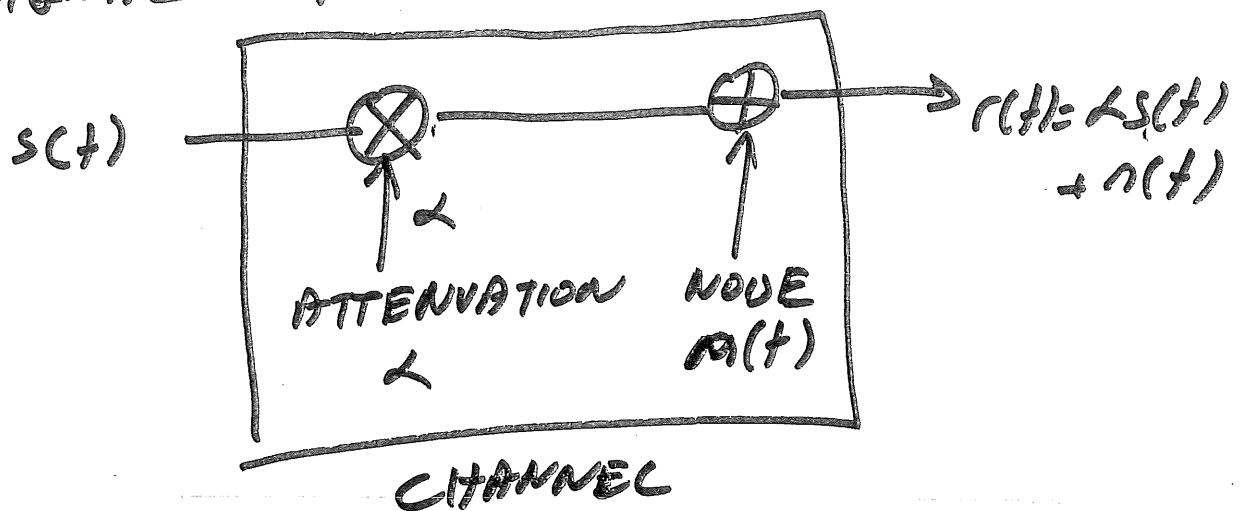


TRANSMISSION LOSSES

①

- ⇒ ADDITIVE NOISE
- ⇒ SIGNAL ATTENUATION

→ FILTERS
→ AMPLIFIERS



- ⇒ SIMPLE SOLUTION = USING AMPLIFIERS TO BOOST THE LEVEL OF THE SIGNAL
- ⇒ ~~can~~ (ALSO AMPLIFIES NOISE) *

$$S_{\text{NO}}(f) = \frac{N_0}{2} \text{ W/Hz}$$

AMPLIFIERS ARE IDENTIFIED WITH NOISE FIGURE

NOISE FIGURE ⇒ RATIO OF THE OUTPUT NOISE POWER P_{NO} TO THE OUTPUT NOISE POWER OF AN IDEAL (NOISELESS) AMPLIFIER ($T_0 = 290^\circ\text{K}$)

↓ better

$$\text{NOISE FIGURE} \Rightarrow F = \left(1 + \frac{T_e}{T_0} \right)$$

$T_e \Rightarrow$ EFFECTIVE NOISE TEMPERATURE

TRANSMISSION LOSSES

(2)

$$\text{Loss} \quad \left| \quad L = \frac{P_T}{P_R} \right. \begin{array}{l} \Rightarrow \text{Transmitted power} \\ \Rightarrow \text{Received power} \end{array}$$

or in dB

$$L_{dB} = 10 \log L = 10 \log P_T - 10 \log P_R$$

WIRED
 \Rightarrow COAXIAL CABLE OF 1CM DIAMETER \Rightarrow LOSS $2dB/km$ at 1MHz

LOSS INCREASES WITH AN INCREASE IN FREQ.

LINE OF SIGHT COMM.

$$L = \left(\frac{4\pi d}{\lambda} \right)^2$$

$$\lambda = \frac{c}{f} \text{ wavelength}$$

$c = 3 \times 10^8 \text{ m/sec}$, speed of light

d = distance in meters

$L = \left(\frac{4\pi d}{\lambda} \right)^2 \Rightarrow L$ is called FREE-SPACE PATH LOSS

LINK BUDGET ANALYSIS

3

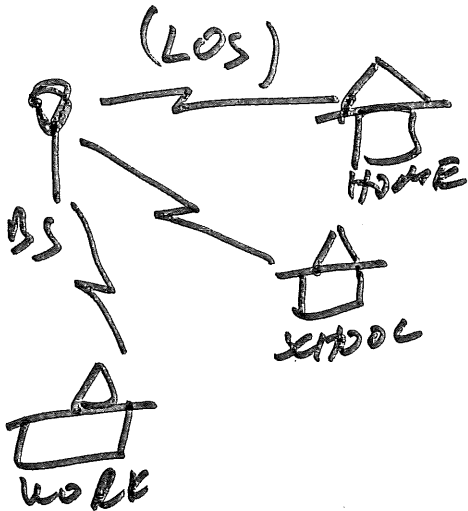
⇒ HOW FAR CAN IT GO?

⇒ WHAT WILL BE THE THROUGHPUT?

⇒ INPUTS ⇒

- 1) OUTPUT POWER
- 2) AVAILABLE BW
- 3) RECEIVER SENSITIVITY
- 4) ANTENNA GAINS
- 5) RADIO TECHNOLOGY
- 6) ENVIRONMENTAL CONDITIONS

LINE OF SIGHT (LOS) LINK BUDGET



RECEIVED POWER (dBm)

$$= \text{TX POWER (dBm)} + \text{GAINS (dB)} - \text{LOSSES (dBm)}$$

⇒ WHAT IS THE RECEIVER SENSITIVITY

⇒ LOWEST POWER LEVEL AT WHICH THE RECEIVER CAN DETECT AN RF SIGNAL AND DEMODULATE DATA. THIS VALUE IS INDEPENDENT OF TX.

⇒ THE AMOUNT RECEIVED POWER EXCEEDS RECEIVER SENSITIVITY IS CALLED LINK MARGIN.

$$\text{LINK MARGIN} = \text{RECEIVED POWER} - \text{RECEIVE SENSITIVITY}$$

FREE SPACE PATH LOSS (FSPL)

(4)

$$FSPL = L(dB) = 10 \log_{10} \left(\frac{4\pi d f}{c} \right)^2$$

$$FSPL(dB) = 20 \log_{10}(d) + 20 \log_{10}(f) + 20 \log_{10} \left(\frac{4\pi}{c} \right)$$

$$= 20 \log_{10}(d) + 20 \log_{10}(f) - 147.55$$

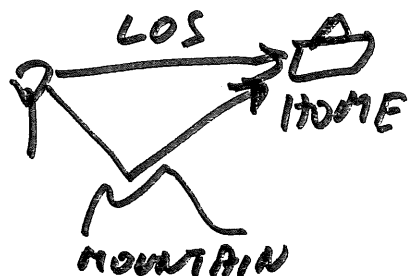
$f \Rightarrow \text{Hz}$ $d \Rightarrow \text{meters}$ $c = 3 \times 10^8 \text{ m/s}$

EXAMPLE

<u>DISTANCE</u>	<u>FSPL(dB)</u>		<u>f</u>
	<u>900MHz</u>	<u>2.4GHz</u>	
1km	91.53	100.05	107.72
5km	105.55	114.03	121.70
10km	111.53	120.05	127.72
50km	125.51	134.03	141.70

MULTIPATH AND FADE MARGIN

\Rightarrow WAVES TRAVELS DIFFERENT PATHS AND CAUSE UNWANTED INTERFERENCE.



\Rightarrow FADING CAN CAUSE A SIGNAL REDUCTION OF MORE THAN 30 dB

\Rightarrow IN REAL SYSTEM WE ADD FADE MARGIN TO OVERCOME FADING IN LINK BUDGET.

FOR RAYLEIGH FADING MODEL
TIME AVAILABILITY

<u>FADE MARGIN</u>
8 dB
18 dB
28 dB

90%
95%
99.9%

SIGNAL TO NOISE RATIO

(5)

- ⇒ MODULATION ALSO DETERMINE THE SYSTEM RELIABILITY.
- ⇒ TRADE OFF BETWEEN DATA RATES AND DISTANCE.
- ⇒ 64 QAM REQUIRES HIGH SNR
BPSK " " LESS SNR

<u>EXAMPLE</u> ⇒ (GIVEN BW, GIVEN PER)	<u>DATARATE</u>	<u>SNR</u> <u>dB</u>
<u>MODULATION & CODING</u>		
BPSK $1/2$	6 Mbps	8 dB
QPSK $1/2$	12 Mbps	11 dB
16 QAM $1/2$	24 Mbps	16 dB
64 QAM $3/4$	54 Mbps	25 dB

DESIGN EXAMPLE

DISTANCE = 5 km

FREQ = 5.8 GHz

LINK = Point to Point \Rightarrow (FREE SPACE) SENSITIVITY

54 Mbps \Rightarrow -72 dBm
RECEIVER

LOS \Rightarrow YES

TX POWER = +23 dBm = 200 mW

ANTENNA GAIN \Rightarrow TX = 10 dBi
 \Rightarrow RX = 10 dBi

24 Mbps \Rightarrow -82 dBm

$$10 \log_{10}(200 \text{ mW}) = 23 \text{ dBm}$$

CALCULATE RECEIVE POWER?

FIRST PATH LOSS \Rightarrow 5.8 GHz \Rightarrow 5 km \Rightarrow 121.70 dB

RECEIVED POWER = TX POWER + ANTENNA GAINS
- LOSSES

$$= 23 + 10 + 10 - 121.70 \text{ dB}$$

$$= -78.7$$

MAXIMUM CHANNEL NOISE FOR 54 Mbps \Rightarrow SNR = 25

MAXIMUM CHANNEL NOISE = REC. POWER - SNR (dB)

$$= -78.7 - 25$$

$$= -103.7$$

OUR RECEIVED POWER $-78.7 < -72 \text{ dBm}$ so
54 Mbps can not be supported

\Rightarrow 24 Mbps $-82 \text{ dBm} < -78.7$ so we can
support 24 Mbps.