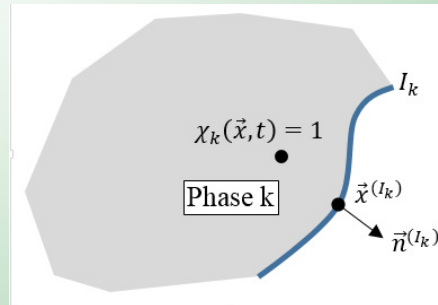


Instantaneous equations of multiphase flows

- A short introduction to tensorial notation

➡ Lecture Notes: III.1

DNS formulations

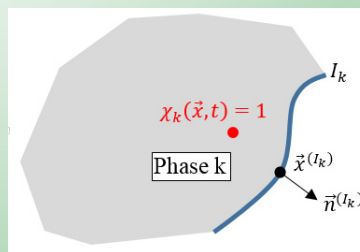


- Approach 1: multi-domain
- Approach 2: multi-fluid
- Approach 3: one-fluid

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DNS approach 1: multi-domain

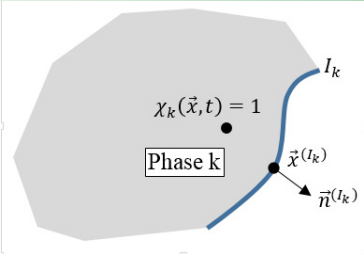


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DNS approach 1: multi-domain

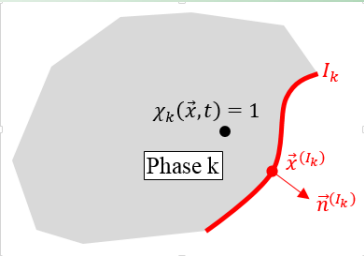
- For each phase, k , the continuity, momentum, scalars ($x \in k^{\text{th}}$ phase)



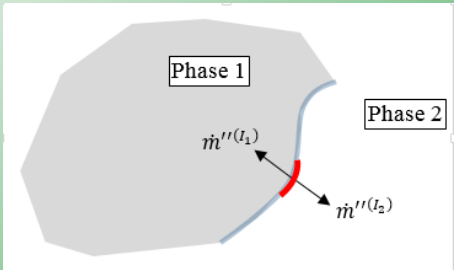
$$\frac{\partial \rho_k}{\partial t} + \frac{\partial}{\partial x_j} (\rho_k U_{k,j}) = 0$$
$$\frac{\partial}{\partial t} (\rho_k U_{k,i}) + \frac{\partial}{\partial x_j} (\rho_k U_{k,j} U_{k,i}) = \frac{\partial \sigma_{k,ij}}{\partial x_j} + \rho_k g_i ; \sigma_{k,ij} = -p_k \delta_{ij} + \tau_{k,ij}$$
$$\frac{\partial}{\partial t} (\rho_k Q_k) + \frac{\partial}{\partial x_j} (\rho_k U_{k,j} Q_k) = -\frac{\partial J_{Q_k,j}}{\partial x_j} + \rho_k S_{Q_k}$$

DNS approach 1: multi-domain

- Jump conditions (the balance of transports) at the interface:



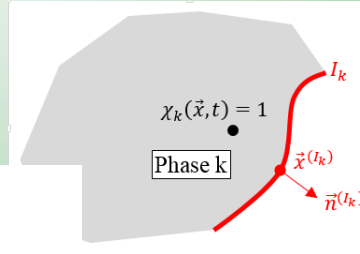
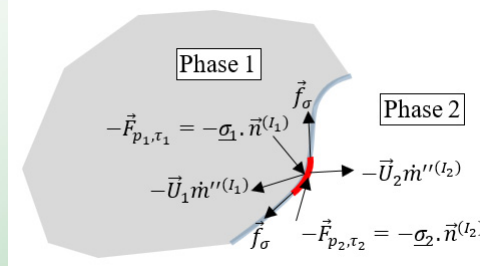
$$\dot{m}''^{(I_k)} = -\rho_k (\vec{U}_k - \vec{U}^{(I_k)}) \cdot \hat{n}^{(I_k)}$$
$$\sum_{k=1}^2 \dot{m}''^{(I_k)} = 0$$



Mass balance per unit interface area

DNS approach 1: multi-domain

- Jump conditions (the balance of transports) at the interface:



momentum balance per unit interface area

$$-\sum_{k=1}^2 (\sigma_k \cdot \hat{n}^{(I_k)} + \dot{m}''^{(I_k)} \vec{U}_k) + \vec{f}_{\sigma} = 0$$

Chap 3



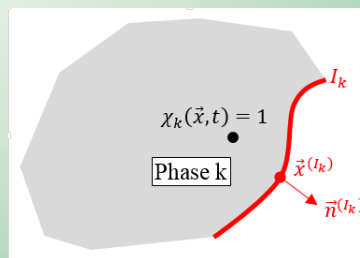
Energy equation jump condition? (HW)

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DNS approach 1: multi-domain

- Interface location closure:

$$\frac{d\vec{x}^{(I_k)}}{dt} = \vec{U}^{(I_k)}$$



+ A simple model (no breakup, evaporation, etc.):

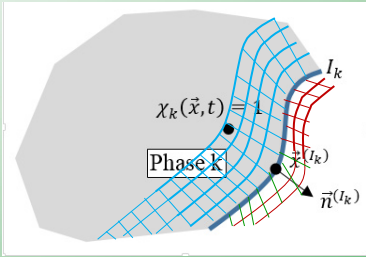
$$\vec{U}^{(I_k)} = \lim_{\vec{x} \rightarrow \vec{x}^{(I_k)}} \vec{U}_k$$

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DNS approach 1: multi-domain

- Features:
 - not defined in all space,
 - needs interface-fitted dynamic mesh,

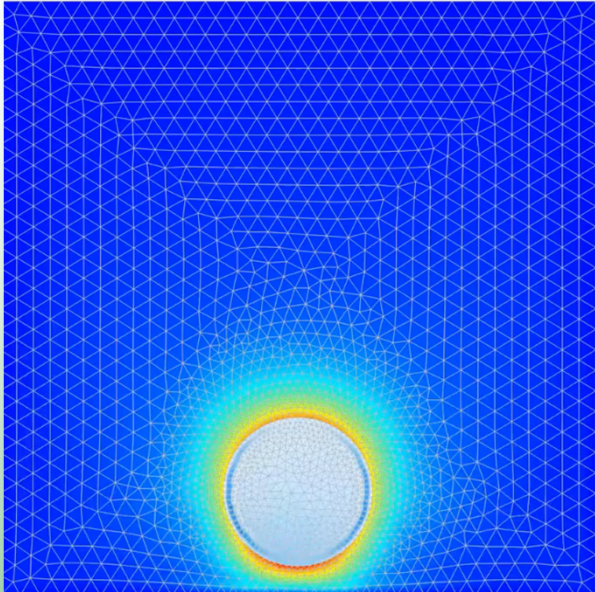


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DNS approach 1: multi-domain

Rising bubble benchmark
▶



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DNS approach 1: multi-domain

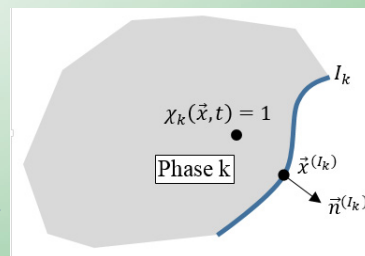
- Features:
 - not defined in all space,
 - needs **interface-fitted dynamic** mesh,
 - highest **accuracy** (does not need approximation of the delta function)
 - highest **computational costs**

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DNS approach 2: multi-fluid

- based on the generalized variables $Q_k \chi_k$
- see references [3] (section 2.3), [Naud 2003] (chap 3), and [Kataoka 1986] for the **derivation** of the equations
- derivation using **indicator function advection** equation



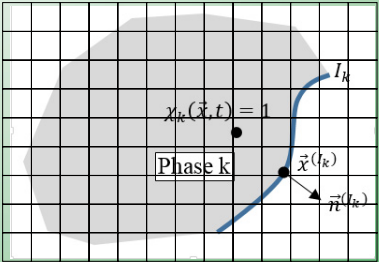
$$\frac{\partial \chi_k}{\partial t} + U_j^{(I_k)} \frac{\partial \chi_k}{\partial x_j} = 0$$

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DNS approach 2: multi-fluid

- For each phase, k, the indicator function advection:



volume flow rate to phase k
across the interface I_k

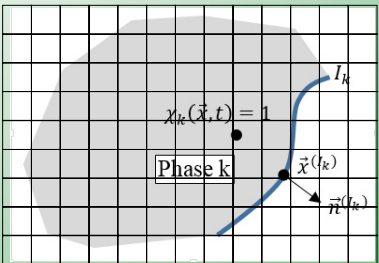
$$\frac{\partial \chi_k}{\partial t} + U_j^{(I_k)} \frac{\partial \chi_k}{\partial x_j} = 0 \Rightarrow \frac{\partial \chi_k}{\partial t} + U_{k,j} \frac{\partial \chi_k}{\partial x_j} = \frac{S_m^{(I_k)} / \rho_k}{(U_{k,j} - U_j^{(I_k)})} \frac{\partial \chi_k}{\partial x_j}$$

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DNS approach 2: multi-fluid

- For each phase, k, the continuity, momentum, scalars all over the domain:



mass transfer rate to phase k
across the interface I_k

$$\frac{\partial}{\partial t} (\rho_k \chi_k) + \frac{\partial}{\partial x_j} (\rho_k U_{k,j} \chi_k) = \frac{S_m^{(I_k)}}{\rho_k (U_{k,j} - U_j^{(I_k)})} \frac{\partial \chi_k}{\partial x_j}$$

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DNS approach 2: multi-fluid

- For each phase, k, the continuity, momentum, scalars all over the domain:

mass transfer rate to phase k
across the interface I_k

$$\frac{\partial}{\partial t}(\rho_k \chi_k) + \frac{\partial}{\partial x_j}(\rho_k U_{k,j} \chi_k) = \overbrace{\rho_k (U_{k,j} - U_j^{(I_k)}) \frac{\partial \chi_k}{\partial x_j}}^{S_m^{(I_k)}}$$
$$\frac{\partial}{\partial t}(\rho_k U_{k,i} \chi_k) + \frac{\partial}{\partial x_j}(\rho_k U_{k,j} U_{k,i} \chi_k) = \frac{\partial}{\partial x_j}(\sigma_{k,ij} \chi_k) + \rho_k \chi_k g_i + \underbrace{\left(-\sigma_{k,ij} \frac{\partial \chi_k}{\partial x_j} \right)}_{S_{U_i}^{(I_k)}}$$
$$\frac{\partial}{\partial t}(\rho_k Q_k \chi_k) + \frac{\partial}{\partial x_j}(\rho_k U_{k,j} Q_k \chi_k) = -\frac{\partial}{\partial x_j}(J_{Qk,j} \chi_k) + \rho_k \chi_k S_{Qk} + \underbrace{\left(J_{Qk,j} \frac{\partial \chi_k}{\partial x_j} \right)}_{S_Q^{(I_k)}} + \underbrace{Q_k S_m^{(I_k)}}_{\text{momentum transfer by phase change}}$$

momentum transfer due to pressure and viscous stress at the interface I_k

momentum transfer by phase change

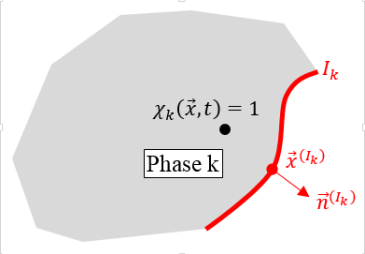
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DNS approach 2: multi-fluid

- Closures:

Models for interface transfer source terms, $S_m^{(I_k)}$, $S_{U_i}^{(I_k)}$, and $S_Q^{(I_k)}$ satisfying jump condition constraints



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DNS approach 2: multi-fluid

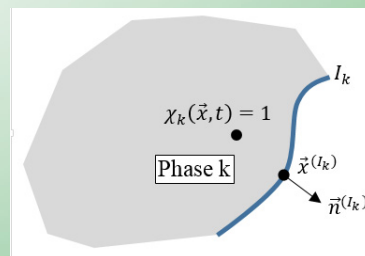
- Features:
 - defined in all space (does not need **interface-fitted** mesh),
 - the **interface transfer source terms** appears at the interface only and are zero inside the phases,
 - interface transfer source terms can be described by **delta functions** [Naud 2003],
 - the numerics needs **approximation** of the **delta function**
 - the basis of the **Eulerian-Lagrangian** formulation

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DNS approach 3: one-fluid

- based on the generalized variable $Q = \sum_{k=1}^N Q_k \chi_k$, see reference [Kataoka 1986]
- the governing equations are derived using $\sum_{k=1}^N$ (5.3) applying the jump condition constraints

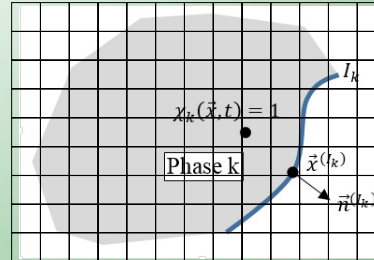


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DNS approach 3: one-fluid

- The one-fluid continuity, momentum, scalars all over the domain:



$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_j} (\rho U_j) = 0 \quad ; \quad \left(\sum_{k=1}^N S_m^{(I_k)} = 0 \right)$$

surface tension force $F_{\sigma,i}$

$$\frac{\partial}{\partial t} (\rho U_i) + \frac{\partial}{\partial x_j} (\rho U_i U_j) = \frac{\partial \sigma_{ij}}{\partial x_j} + \rho g_i + \sum_{k=1}^N \overbrace{[S_{U_i}^{(I_k)} + U_{k,i} S_m^{(I_k)}]}^{S_{Q_m}^{(I)}}$$

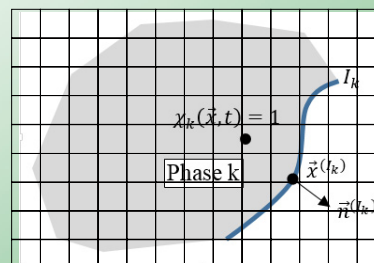
$$\frac{\partial}{\partial t} (\rho Q) + \frac{\partial}{\partial x_j} (\rho U_j Q) = - \frac{\partial J_{Q,j}}{\partial x_j} + \rho S_Q + \sum_{k=1}^N \overbrace{[S_Q^{(I_k)} + Q_k S_m^{(I_k)}]}$$

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DNS approach 3: one-fluid

- The indicator function advection for each phase k:



$$\frac{\partial \chi_k}{\partial t} + U_j \frac{\partial \chi_k}{\partial x_j} = \overbrace{\left(U_j - U_j^{(I_k)} \right) \frac{\partial \chi_k}{\partial x_j}}^{S_{\chi}^{(I_k)}}$$

- Can be recast as: $\frac{\partial}{\partial t} (\rho_k \chi_k) + \frac{\partial}{\partial x_j} (\rho_k \chi_k U_j) = S_m^{(I_k)}$
- The secondary generalized properties, like density, viscosity, etc.:

$$Q = \sum_{k=1}^N Q_k \chi_k$$

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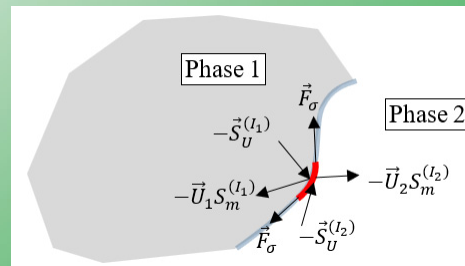
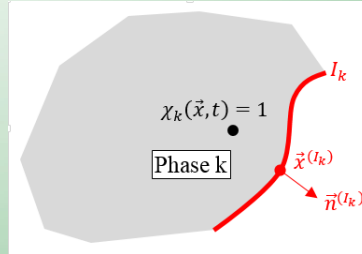
DNS approach 3: one-fluid

● Closures:

Models for interface transfer source terms, including $S_{\chi}^{(I_k)}$, surface tension, f_{σ} , and $S_{Qm}^{(I)}$ satisfying jump condition constraints

$$-\sum_{k=1}^N \left[S_{U_i}^{(I_k)} + U_{k,i} S_m^{(I_k)} \right] + F_{\sigma,i} = 0$$

momentum balance per unit fluid volume ►



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DNS approach 3: one-fluid

● Features:

- defined in all space (does not need **interface-fitted mesh**),
- the **interface transfer source terms** appears at the interface only and are zero inside the phases,
- the **surface tension force** is described using a **delta function** and **surface curvature**, see reference [1] (appendix A, section 2.4.2),
- the numerics needs **approximation** of the **delta function**
- simpler and more **widely used** for DNS than approach 2

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DNS approach 3: one-fluid

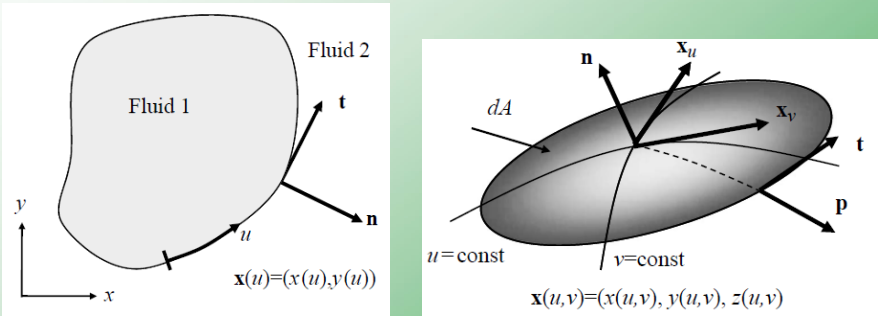
- Example: VOF method



Spray atomization ▲

DNS approach 3: one-fluid

- Details of formulation
 - The parametric description of an interface:



➡ Lecture Notes: III.3

Appendices

- Summary of DNS approaches: “chap3-DifferentDNSFormulationsSummary.pdf”
- Optional
 - The proofs in 2D (intermediate): “chap3-2DProofs.pdf”
 - The proofs in 3D (advanced): “chap3-3DProofs.pdf”
- HW#3 (optional)
 - Practice of using the tensorial notation
 - Derivation of some important relations

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