



Eulerian averaged equations and models

- Key relations of averaging

➡ Lecture Notes: V.1

- The multifluid model

- Ensemble averaging the multifluid instantaneous equations

$$\langle (5.3a) \rangle \rightarrow \frac{\partial}{\partial t} \langle \rho_k \chi_k \rangle + \frac{\partial}{\partial x_j} \langle \rho_k U_{k,j} \chi_k \rangle = \langle S_m^{(I_k)} \rangle$$

$$\text{Volume fraction } \alpha_k \langle \rho \rangle|_k = \bar{\rho}_k \quad (7.2) \quad (10.2) \quad \frac{\partial \bar{\rho}_k}{\partial t} + \frac{\partial}{\partial x_j} (\bar{\rho}_k \tilde{U}_{k,j}) = \langle S_m^{(I_k)} \rangle \equiv \sum_{q=1}^N (\dot{m}_{qk} - \dot{m}_{kq}) \quad (13.5)$$

Chap 5

Interphase mass coupling: needs modeling

By E. Amani

Eulerian averaged equations and models

The multifluid model

- Usually p and T are assumed at (phase) equilibrium, which is called **mechanical and thermal (local) homogeneity**, and are the same for all phases.

However, velocity is determined per phase

$$\begin{aligned}
 \langle (5.3b) \rangle &\rightarrow \frac{\partial}{\partial t} \langle \rho_k \chi_k U_{k,i} \rangle + \frac{\partial}{\partial x_j} \langle \rho_k U_{k,j} U_{k,i} \chi_k \rangle = \frac{\partial}{\partial x_j} \langle \sigma_{k,ij} \chi_k \rangle \\
 &\quad + \langle \rho_k \chi_k \rangle g_i + \langle S_{U_i}^{(I_k)} \rangle + \langle U_{k,i} S_m^{(I_k)} \rangle \quad \text{Reynolds stress: needs modeling} \\
 \frac{\partial}{\partial t} (\bar{\rho}_k \tilde{U}_{k,i}) + \frac{\partial}{\partial x_j} (\bar{\rho}_k \tilde{U}_{k,j} \tilde{U}_{k,i}) &= \frac{\partial \bar{\sigma}_{k,ij}}{\partial x_j} + \bar{\rho}_k g_i - \frac{\partial}{\partial x_j} (\bar{\rho}_k \widetilde{U_{k,j}'' U_{k,i}'}) + \\
 &\quad \langle S_{U_i}^{(I_k)} \rangle + \langle U_{k,i} S_m^{(I_k)} \rangle \quad (15.5)
 \end{aligned}$$

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Interphase momentum coupling: need modeling

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The multifluid model

- **Unclosed terms**

$$\begin{aligned}
 \langle S_U^{(I_k)} \rangle &= \sum_{q=1}^N F_{qk} = \sum_{q=1}^N \left(\overset{\text{Drag force}}{F_{qk}^{\text{drag}}} + \overset{\text{Lift force}}{F_{qk}^{\text{lift}}} + \overset{\text{Wall lubrication force}}{F_{qk}^{\text{td}}} + \overset{\text{Undisturbed flow force}}{F_{qk}^{\text{wall}}} + \overset{\text{Turbulent dispersion force}}{F_{qk}^{\text{vm}}} + \overset{\text{Virtual mass force}}{F_{qk}^0} + \dots \right) \quad (16.5) \\
 \langle U_k S_m^{(I_k)} \rangle &= \sum_{q=1}^N (\dot{m}_{qk} U_k - \dot{m}_{kq} U_q) \quad (17.5)
 \end{aligned}$$

- **Note 1:** $F_{kq} = -F_{qk}$
- **Note 2:** For **dilute flows** where the presence of a phase (carrier-phase) is dominant $\sum_{q=1}^N F_{qk} = F_{ck}$

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The multifluid model

- **Note 1:** $\mathbf{F}_{kq} = -\mathbf{F}_{qk}$
- **Note 2:** For **dilute flows** where the presence of a phase (carrier-phase) is dominant $\sum_{q=1}^N \mathbf{F}_{qk} = \mathbf{F}_{ck}$
- **Note 3:** The modeling of **interphase coupling terms** are highly **problem dependent**. This will be discussed in chapters 6 and 9.
- **Note 4:** The 1st and 4th terms of the RHS Eq. (15.5) can be recast as (see Capecelatro (2013) for a proof)

$$\frac{\partial \overline{\sigma}_{k,ij}}{\partial x_j} + \left\langle S_{U_i}^{(I_k)} \right\rangle = \alpha_k \frac{\partial \langle \sigma_{ij} \rangle_{|k}}{\partial x_j} + \left\langle S_{U_i}'^{(I_k)} \right\rangle \quad (18.5)$$

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The same as Eq. (16.5) excluding F_{qk}^0 By E. Amani

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The multifluid model

- Similarly, for scalar transport equations, starting from Eq. (5.3c), Reynolds flux: needs modeling

$$\frac{\partial}{\partial t} (\bar{\rho}_k \tilde{Q}_k) + \frac{\partial}{\partial x_j} (\bar{\rho}_k \tilde{U}_{k,j} \tilde{Q}_k) = \frac{\partial \bar{J}_{Q_k,j}}{\partial x_j} - \frac{\partial}{\partial x_j} (\bar{\rho}_k \overline{U_{k,j}'' Q_k''}) + \bar{\rho}_k \tilde{S}_{Q_k}$$

$$\left\langle S_{Q_k}^{(I_k)} \right\rangle + \left\langle Q_k S_m^{(I_k)} \right\rangle \quad (19.5)$$

Interphase scalar coupling: need modeling

Averaged source term: usually needs modeling

- **Summary**

$$\sum_{k=1}^N \alpha_k = 1 \quad (20.5)$$

Unknowns	Equations
α_k (N)	Eq. (13.5) (N)
$\tilde{U}_{k,i}$ (3N)	Eq. (15.5) (3N)
\bar{p} (1)	Eq. (20.5) (1)
4N+1	4N+1

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The drift-flux model

- **Exercise: Show that summing Eqs. (13.5) and (15.5) over all phases yields**

$$\frac{\partial \rho_m}{\partial t} + \frac{\partial}{\partial x_j} (\rho_m U_{m,j}) = 0 \tag{21.5}$$

$$\frac{\partial}{\partial t} (\rho_m U_{m,i}) + \frac{\partial}{\partial x_j} (\rho_m U_{m,j} U_{m,i}) = \frac{\partial \bar{\sigma}_{ij}}{\partial x_j} + \rho_m g_i - \frac{\partial}{\partial x_j} \sum_{k=1}^N (\underbrace{\bar{\rho}_k U_{km,j} U_{km,i}}_{\text{Drift velocity: needs modeling}}) - \frac{\partial}{\partial x_j} (\underbrace{\rho_m \widetilde{U''_{m,j} U''_{m,i}}}_{\text{Reynolds stress: needs modeling}}) + \underbrace{\langle F_{\sigma_i} \rangle}_{\text{Averaged surface tension: needs modeling}} \tag{22.5}$$

Eulerian averaged equations and models

The drift-flux model

- **Summary:**

Unknowns	Equations
α_k (N)	Eq. (21.5) (1), Eq. (13.5) (N-1)
$U_{m,i}$ (3)	Eq. (22.5) (3)
\bar{p} (1)	Eq. (20.5) (1)
N+4	N+4

- **Note 1: In many cases, $\langle F_{\sigma_i} \rangle$ is neglected.**
- **Note 2: If $U_{km} = 0$, the model is called the **homogeneous model** and there is no relative velocity between phases.**

The Population Balance Model (PBM)

- **Trade-off between the multifluid and drift-flux**

