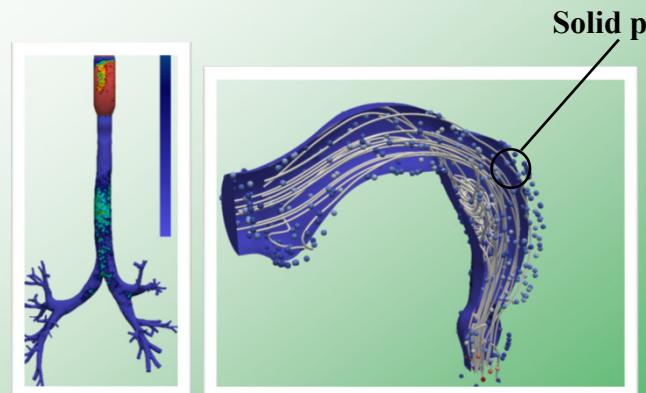


Particle

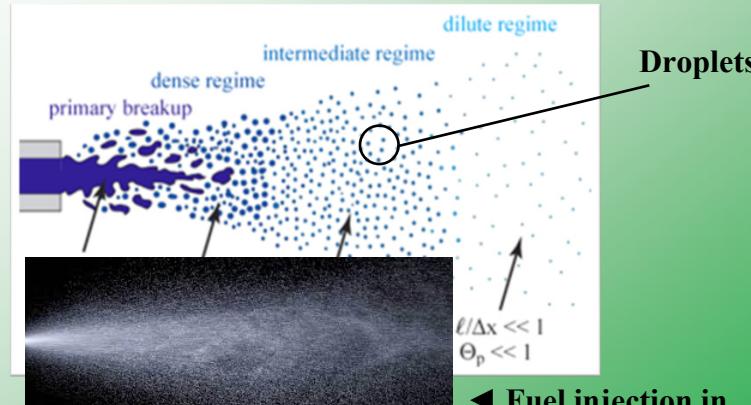
- Particle: solid particle, droplet, or bubble



▲ Pulmonary Drug Delivery

Particle

- Particle: solid particle, droplet, or bubble



Chap 7

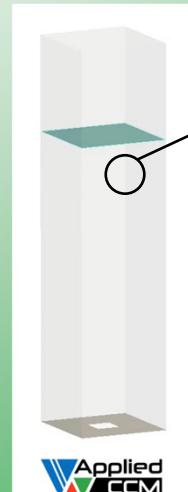
By E. Amani

Particle

- Particle: solid particle, droplet, or bubble



Bubble column reactor ▲▶



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By E. Amani

Key concepts and definitions

- Particle concentration and volume fraction

➡ Lecture Notes: VII.2

- Particle spacing – isolated particle assumption

➡ Lecture Notes: VII.3

- Particle time scales – Stokes number

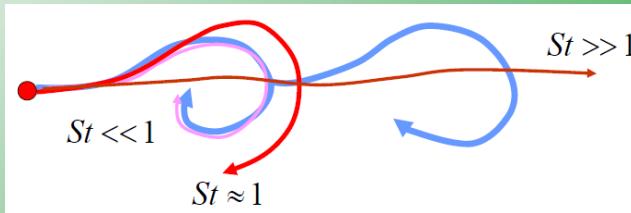
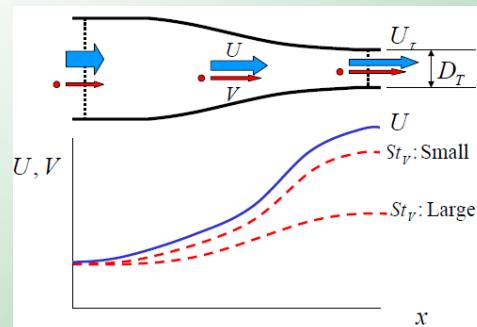
➡ Lecture Notes: VII.4

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Stokes number effect

- Physical interpretation



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Stokes number effect

- Application: flow visualization

Flow past a wing,
visualization by
smoke particles ►



Convection within a
small water droplet ▼



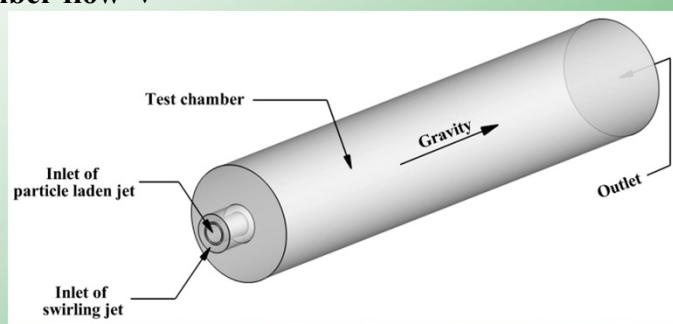
Chap 7

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Stokes number effect

- Application: particle transport

combustion
chamber flow ▼



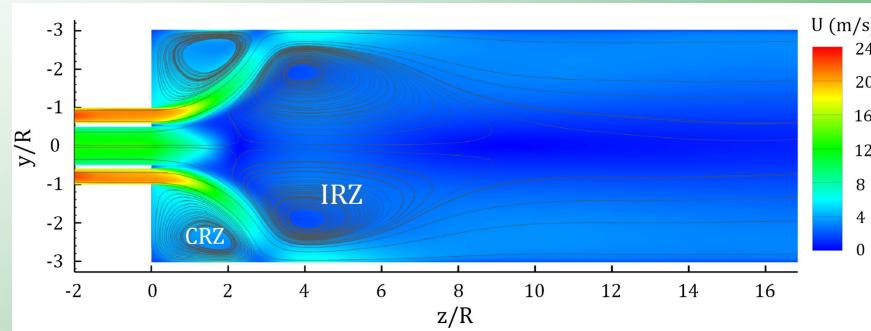
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Stokes number effect

- Application: particle transport

combustion
chamber flow ▼



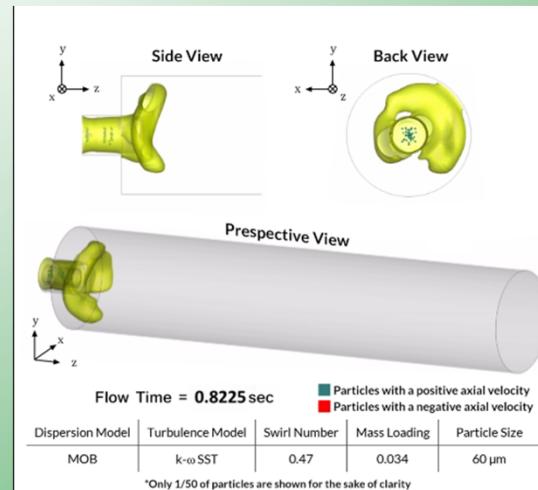
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Stokes number effect

- Application: particle transport

Particles in a
combustion
chamber flow ►



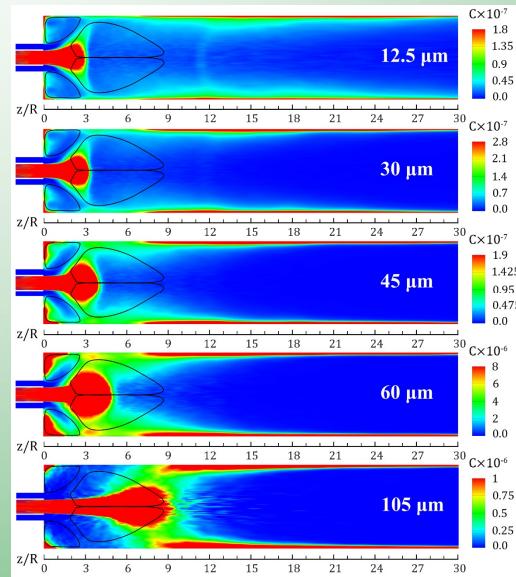
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Stokes number effect

Concentration
of particles ►

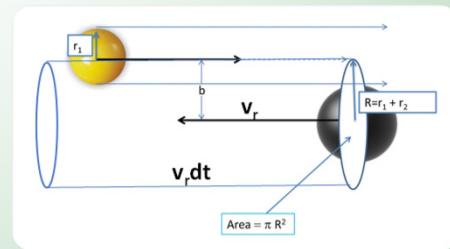
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Collision time scale

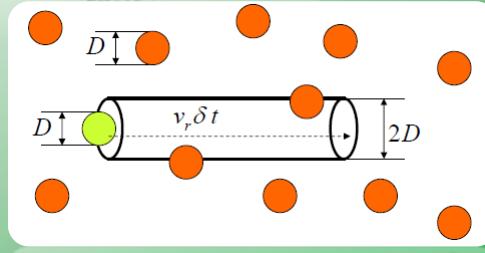
- The collision cylinder



◀ For two particles

For one particle
and a group of
particles (in an
average sense) ►

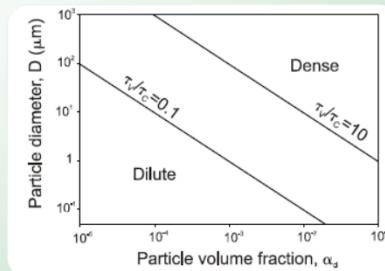
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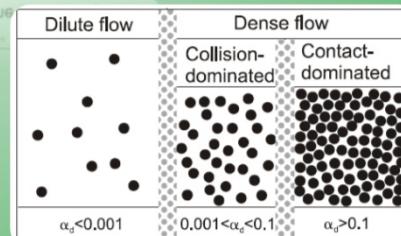
Collision time scale

- Dilute and dense flow regimes



◀ For Glass particles
in air with a
fluctuating velocity
magnitude of 1 m/s

Only based on
the volume
fraction value ►

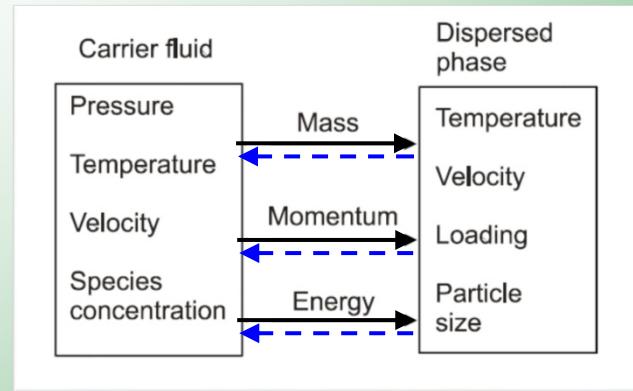


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General particle-laden flow regimes

- Coupling: Fluid-particle interaction



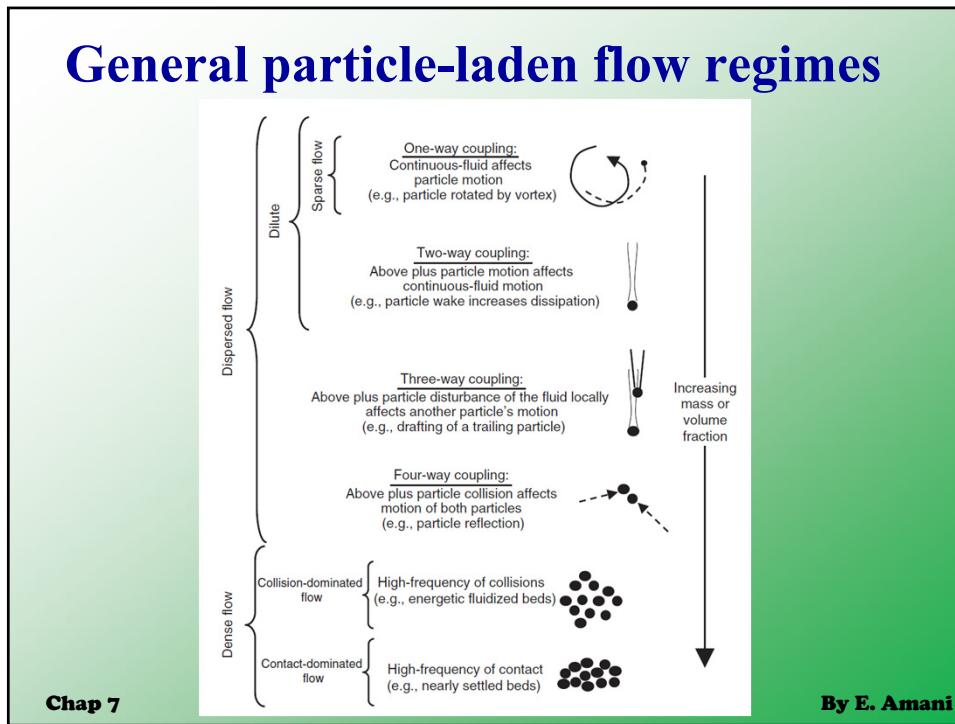
One-way coupling →

Two-way coupling ←→

Chap 7

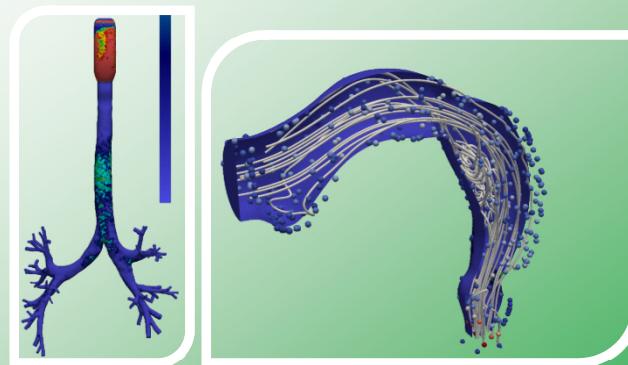
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General particle-laden flow regimes



General particle-laden flow regimes

- One-way coupling regime



▲ Pulmonary Drug Delivery ▲

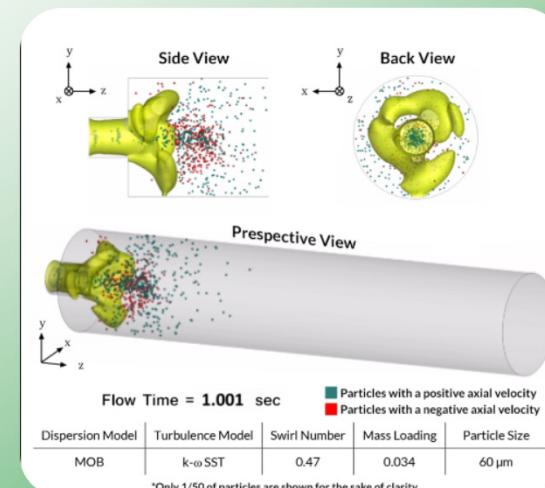
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General particle-laden flow regimes

- Two-way coupling regime

Particles in a combustion chamber flow ►



Chap 7

MOB

 $k-\omega$ SST

0.47

0.034

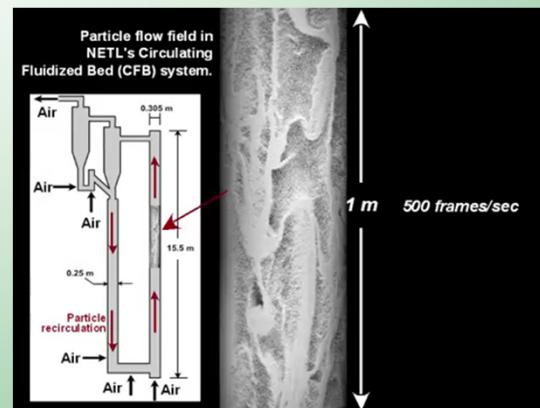
60

 μm

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General particle-laden flow regimes

- Collision-dominated regime



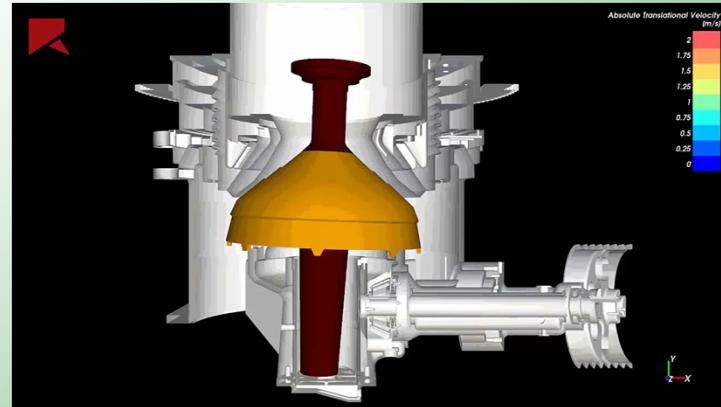
Energetic fluidized beds ▲

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General particle-laden flow regimes

- Contact-dominated regime



Crusher ▲

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Key concepts and definitions

- The coupling

➡ Lecture Notes: VII.5

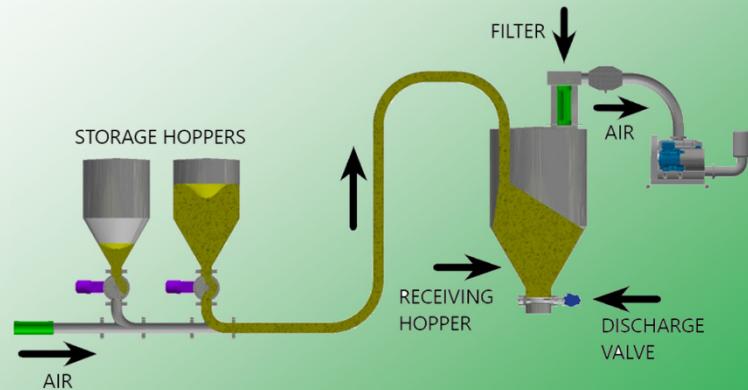
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Pneumatic particle transport

- Modes:

- Dilute-phase pneumatic conveying



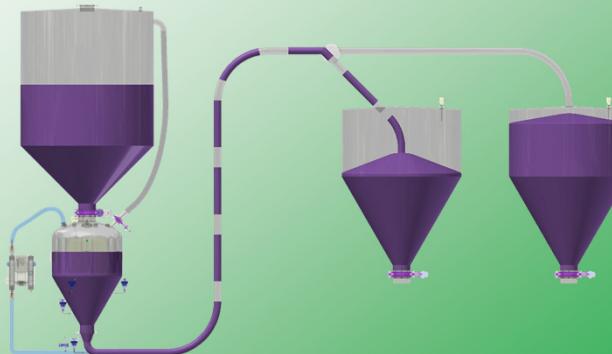
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Pneumatic particle transport

- Modes:

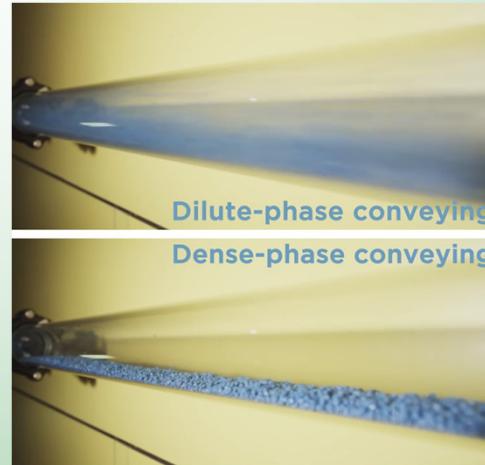
- Dilute-phase pneumatic conveying
- Dense-phase pneumatic conveying



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Pneumatic particle transport



Chap 7

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Pneumatic particle transport

- Applications:
 - Pharmaceutical industries



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Pneumatic particle transport

- **Applications:**
 - Pharmaceutical industries
 - Mining industries



Chap 7



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Pneumatic particle transport

- **Applications:**
 - Pharmaceutical industries
 - Mining industries
 - Agriculture industries



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Pneumatic particle transport

- **Applications:**

- **Pharmaceutical industries**
- **Mining industries**
- **Agriculture industries**
- **Tire industries**



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Pneumatic particle transport

- **Applications:**

- **Pharmaceutical industries**
- **Mining industries**
- **Agriculture industries**
- **Tire industries**
- **...**

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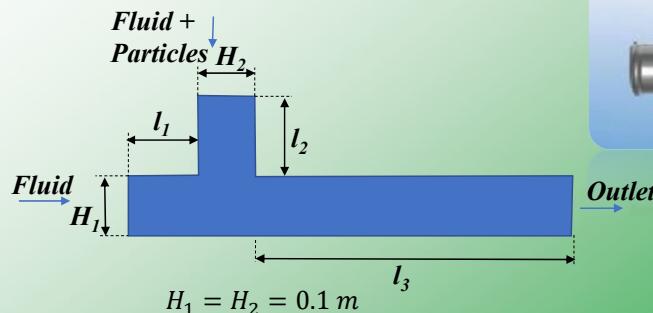
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Case study #3: Conveying T-junction

- Pneumatic conveying T-junction

- Problem definition

1. Geometry



Chap 7

Depth: $W \rightarrow \infty$

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Case study #3: Conveying T-junction

- Pneumatic conveying T-junction

- Problem definition

1. Geometry

2. Boundary conditions

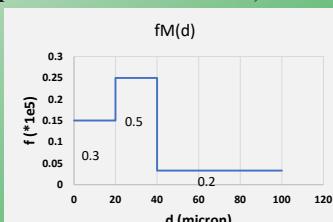
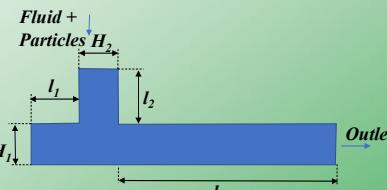
- i) Inlets:

(1) Fluid: air $\dot{m}'_a = 0.7 \frac{\text{kg}}{\text{s.m}}$ ($\dot{m}'_a = \dot{m}_a/W$), $I = 5\%$

(2) Fluid + Particles: air ($\dot{m}'_a = 0.7 \frac{\text{kg}}{\text{s.m}}$, $I = 5\%$), Sand Particles ($\dot{m}'_p = 0.07, 0.7 \frac{\text{kg}}{\text{s.m}}$, in equilibrium with the fluid)

ii) Walls

iii) Outlets



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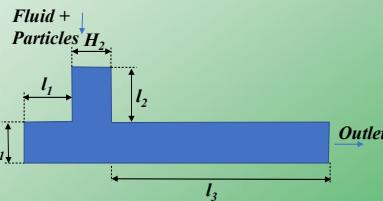
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Case study #3: Conveying T-junction

● Pneumatic conveying T-junction

- Problem definition

1. Geometry
2. Boundary conditions
3. Material properties



$$\rho_{air} = 1.225 \frac{kg}{m^3}, \quad \mu_{air} = 1.8 \times 10^{-5} Pa.s$$

$$\rho_p = 1500 \frac{kg}{m^3}$$

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Case study #3: Conveying T-junction

● Pneumatic conveying T-junction

- Eulerian-Lagrangian simulation

1. Preliminary analysis
2. Solution using ANSYS Fluent (Chap 9)

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Case study #3: Conveying T-junction

● Preliminary analysis

$\alpha_p = ?$

$$\text{HW#7: } \alpha_p = \frac{c}{b}, \quad c = \frac{\dot{m}_p''}{\rho_p}, \quad b = \left(\frac{\dot{m}_c''}{\rho_c} + \frac{\dot{m}_p''}{\rho_p} \right)$$

$$\dot{m}_c'' = \frac{0.7}{0.1} = 7 \frac{kg}{m^2 s}, \quad \dot{m}_p'' = \frac{0.07}{0.1} = 0.7 \frac{kg}{m^2 s} \rightarrow \alpha_p = 8.16 \times 10^{-5}, \alpha_c = 1 - \alpha_p = 0.999918$$

Continuous-phase flow regime (laminar vs. turbulent)?

$$Re_{D_H} = \frac{\rho_c \bar{u}_c D_H}{\mu_c}, \quad D_H = \lim_{W \rightarrow \infty} \left(\frac{4WH_1}{2H_1 + 2W} \right) = 2H_1 = 0.2 \text{ m}$$

$$\dot{m}_c'' = \bar{\rho}_c \bar{u}_c, \quad \bar{\rho}_c = \alpha_c \rho_c = 1.224 \frac{kg}{m^3} \rightarrow \bar{u}_c = 5.72 \frac{m}{s} \rightarrow Re_{D_H} = 77841 \text{ (Fully turbulent)}$$

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Case study #3: Conveying T-junction

● Preliminary analysis

Maximum number of particles in the computational domain (Depth=1m)?

$$N_{p,tot} = n_p \forall_p \\ \forall_p \sim 0.1 \times 1.6 \times 1 = 0.16 \text{ m}^3$$

$$n_p = \frac{\bar{\rho}_p}{m_p}, \quad m_p = \frac{\pi}{6} \rho_p d_p^3, \quad (d_p = 30 \mu m) \rightarrow m_p = 2.12 \times 10^{-13} \text{ kg}, \quad \bar{\rho}_p = \alpha_p \rho_p = 0.1224 \frac{kg}{m^3}$$

$$\rightarrow n_p = 5.77 \times 10^{11} \frac{\text{particles}}{m^3} \rightarrow N_{p,tot} = 9.23 \times 10^{10} \text{ particles}$$

Loading?

$$c = z = \frac{\bar{\rho}_p}{\bar{\rho}_c} = 0.1, \quad Z = \frac{\dot{m}_p}{\dot{m}_c} = 0.1$$

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Case study #3: Conveying T-junction

- Preliminary analysis

Isolated particles?

$$\frac{l}{d} = \left(\frac{\pi}{6\sigma_p} \right)^{1/3} = 18.58 \quad ? > 10 \text{ (Isolated particles)}$$

Stokes number?

$$\tau_F \sim \frac{H_1}{\tilde{u}_c} = 0.0175 \text{ s}$$

$$\tau_v \sim \frac{\rho_p d_p^2}{18\mu_c}, \quad (d_p = 30 \mu m) \rightarrow \tau_v = 4.167 \text{ ms}$$

$$St_v = \frac{\tau_v}{\tau_F} = 0.238 \quad ? \ll 1 \text{ (Particles are not tracer)}$$

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Case study #3: Conveying T-junction

- Preliminary analysis

Dense vs. dilute (collision modeling)?

$$\tau_c \sim \frac{\sqrt{\pi}}{4n_p d_p^2 u'}, \quad (d_p = 30 \mu m), u' = \frac{l}{100} \tilde{u}_c = 0.286 \rightarrow \tau_c = 2.98 \text{ ms}$$

$$\frac{\tau_v}{\tau_c} \sim 1.398 \quad ? < 10 \text{ (Collisions may be unimportant)}$$

One-way vs. two-way coupling?

$$\Pi_v = \frac{c}{1+St_v} = 0.081 \quad ? \ll 1 \text{ (Two-way coupling is probably unimportant)}$$

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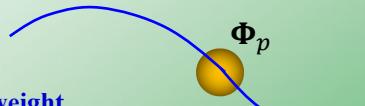
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The point-particle assumption

- Particle state vector

Particle primary properties Parcel weight
 $\Phi_p \equiv (x_p, u_p, d_p, T_p, \dots, \underbrace{u_s, T_s, \dots, w_p}_{\text{fluid properties seen by particle}})$ $w_p = 1 : \text{real particle}$

(41.7)



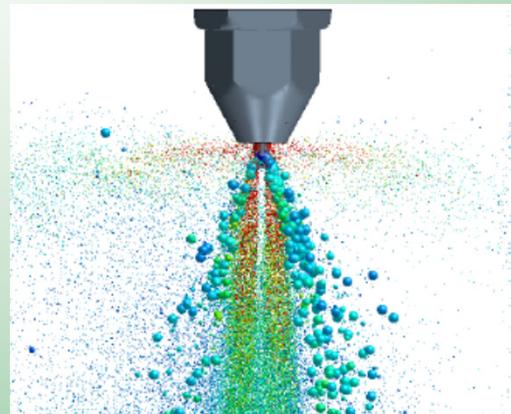
- Parcel (Computational particle) vs. real particle

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The size distribution

- Post-processing



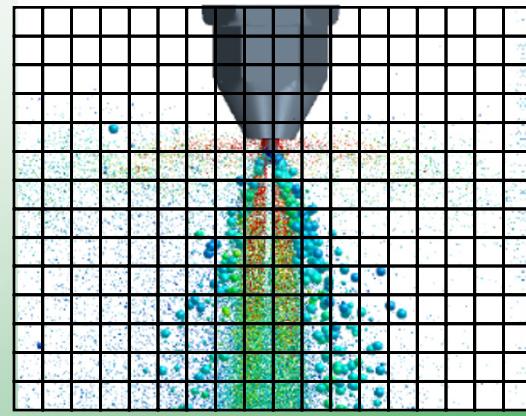
Water spray ▲

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The size distribution

- Post-processing



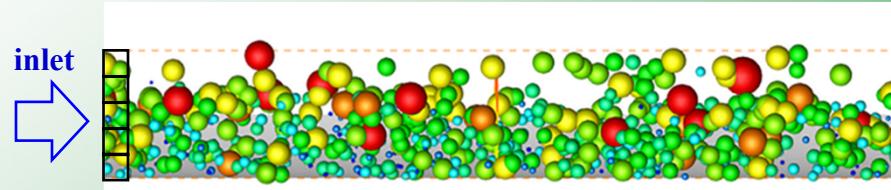
Water spray ▲

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The size distribution

- Setting boundary conditions



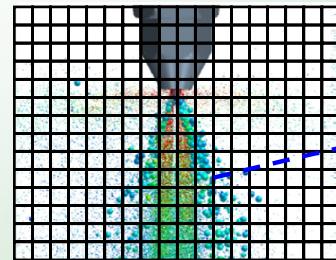
Gas-solid flow in a duct ▲

Chap 7

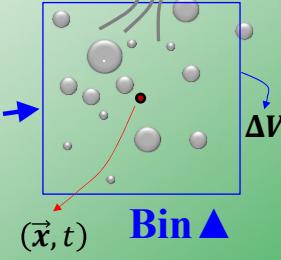
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The size distribution

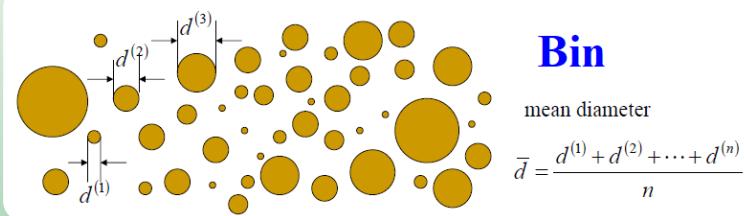
- The Probability Density Function (PDF)



Samples



Bin ▲

**Bin**

mean diameter

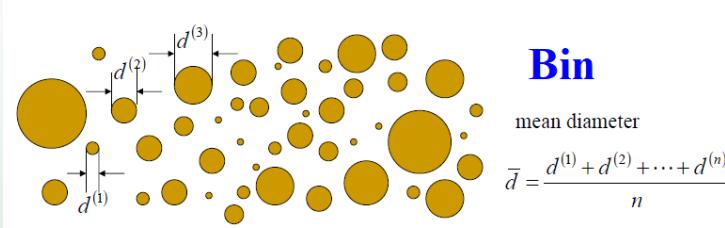
$$\bar{d} = \frac{d^{(1)} + d^{(2)} + \dots + d^{(n)}}{n}$$

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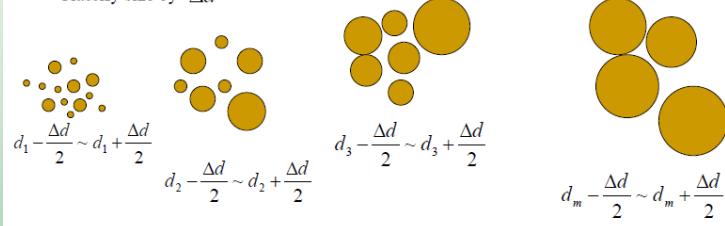
The size distribution

- The Probability Density Function (PDF)

**Bin**

mean diameter

$$\bar{d} = \frac{d^{(1)} + d^{(2)} + \dots + d^{(n)}}{n}$$

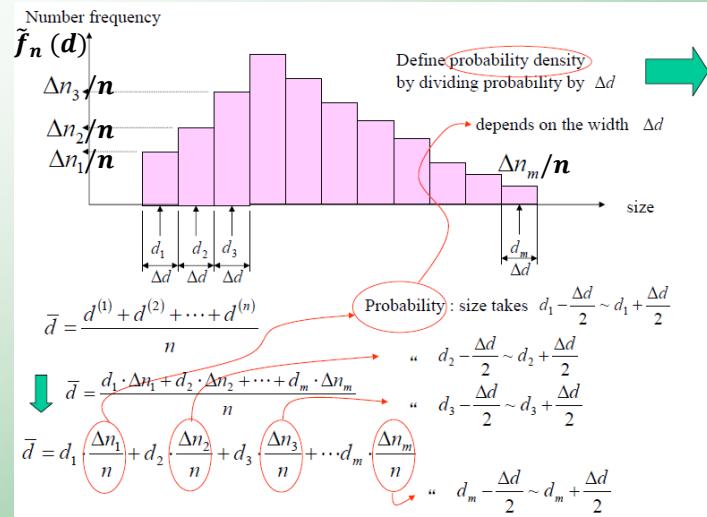
Classify size by Δd 

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The size distribution

- The Probability Density Function (PDF)



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The size distribution

- The Probability Density Function (PDF)

$$\frac{\Delta n_1}{n \cdot \Delta d} = f(d_1) \quad \frac{\Delta n_2}{n \cdot \Delta d} = f(d_2) \quad \frac{\Delta n_3}{n \cdot \Delta d} = f(d_3) \quad \dots \quad \frac{\Delta n_m}{n \cdot \Delta d} = f(d_m)$$

$$\bar{d} = d_1 \cdot \frac{\Delta n_1}{n} + d_2 \cdot \frac{\Delta n_2}{n} + d_3 \cdot \frac{\Delta n_3}{n} + \dots + d_m \cdot \frac{\Delta n_m}{n}$$

$$\bar{d} = d_1 \cdot f(d_1) \cdot \Delta d + d_2 \cdot f(d_2) \cdot \Delta d + d_3 \cdot f(d_3) \cdot \Delta d + \dots + d_m \cdot f(d_m) \cdot \Delta d$$

$$\bar{d} = \lim_{m \rightarrow \infty} \sum_{i=1}^m d_i \cdot f(d_i) \cdot \Delta d = \int_0^{\infty} d \cdot f(d) \cdot dd$$

probability density

probability density function, pdf

frequency distribution

Chap 7

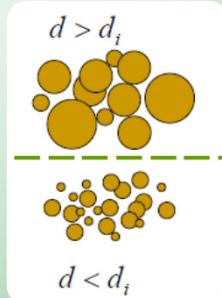
Lecture Notes: VII.9

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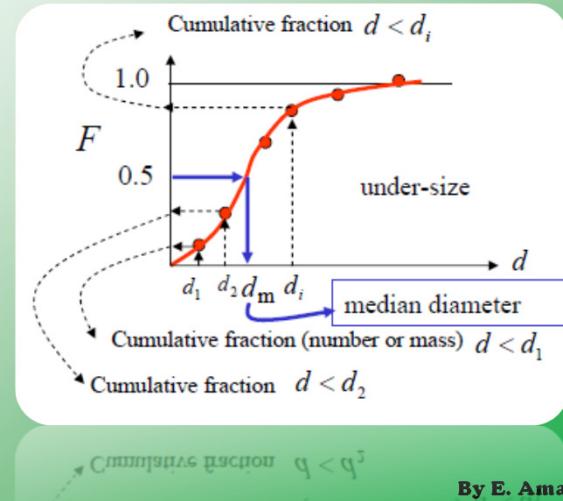
The size distribution

- The Cumulative Distribution Function (CDF)

$$F = \int_0^d f(d) \cdot dd$$

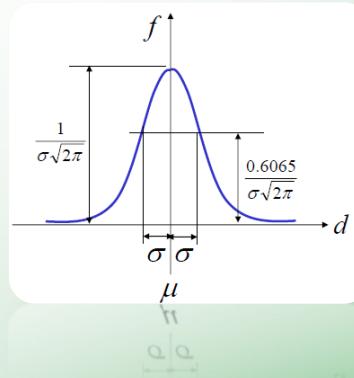


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 $q < q^*$ 

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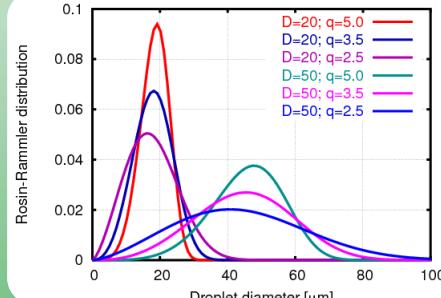
Analytical distribution functions



◀ The normal distribution

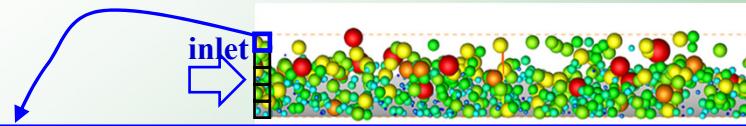
The Rosin-Rammler distribution ►

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Sample problem



For a particle-laden flow, the size distribution PDF of particles at the injection location is given by the following so-called "exponential distribution":

$$f(d) = \begin{cases} \lambda e^{-\lambda d} & ;d \geq 0 \\ 0 & ;d < 0 \end{cases}$$

where $\lambda = 2.5 \times 10^4 \text{ m}^{-1}$.

Hint: $\int xe^{\alpha x} dx = -\frac{e^{\alpha x}}{\alpha^2} + \frac{xe^{\alpha x}}{\alpha}$, $\int_0^\infty x^n e^{-ax} dx = \frac{n!}{a^{n+1}}$ ($a > 0, n = 0, 1, 2, \dots$)

- a) What is the particle mean diameter?
- b) 95% of particles have a diameter smaller than $d_{95\%}$. What is $d_{95\%}$?
- c) Obtain the mass-based PDF, $f_M(d)$?
- d) D is the diameter that particles with $d_p > D$ contain only 5% of the total mass. Is D smaller, equal, or greater than $d_{95\%}$ obtained in part (b)?

Lecture Notes: VII.10

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Hands-on practice

• HW#7:

- A sample preliminary EL analysis
- Working with size distributions
- ...

Size range (μm)	Number of particles	Size range (μm)	Number of particles
5-15	56	40-45	41
15-20	62	45-50	38
20-25	73	50-60	38
25-30	79	60-70	21
30-35	58	70-80	12
35-40	39	80-95	15
32-40	38	80-92	12
30-32	28	10-80	15

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