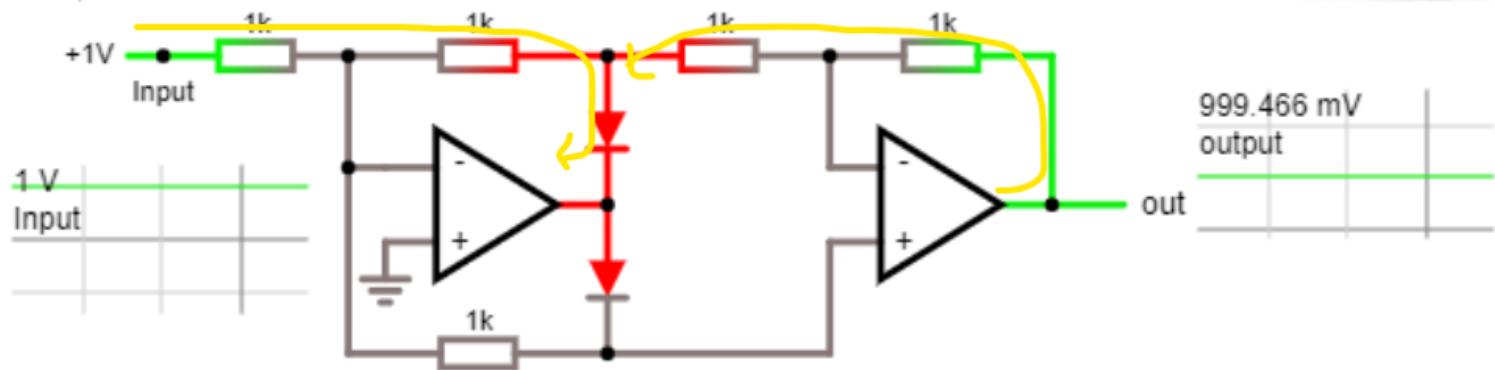


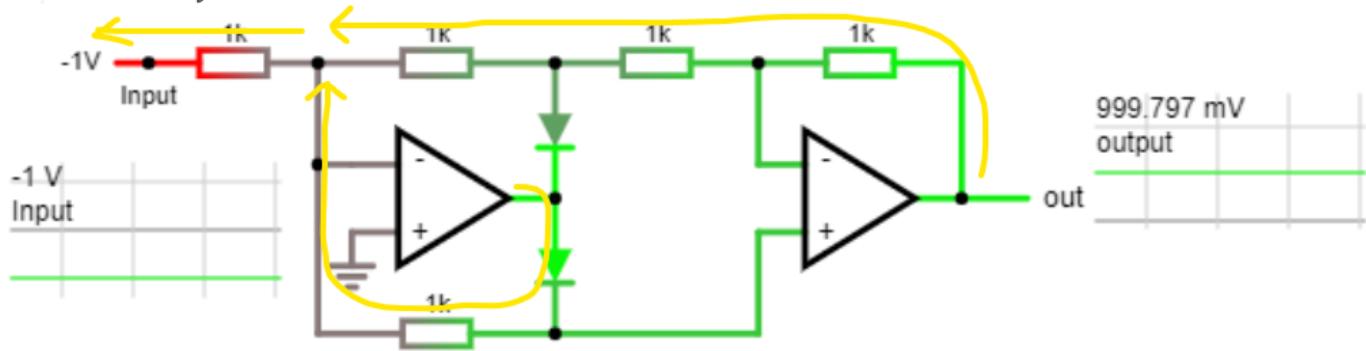
(1) Precision Rectifier

a) Operation:



For a positive voltage, due to the virtual short of the input terminals of each op amp the only conduction path is 'into' the output of OP₁ (or the OV at node 1 or diode D₁)

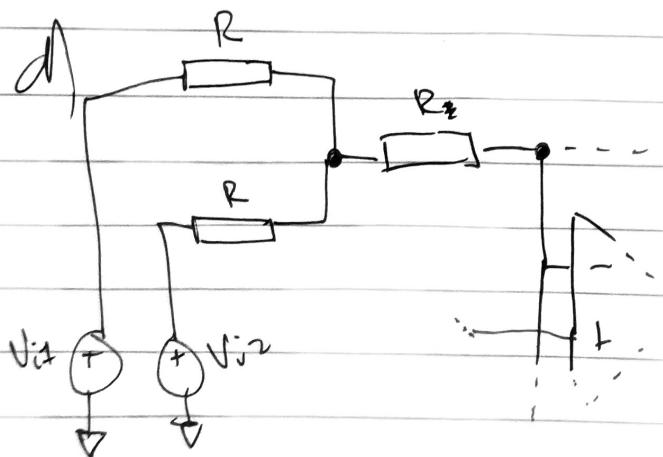
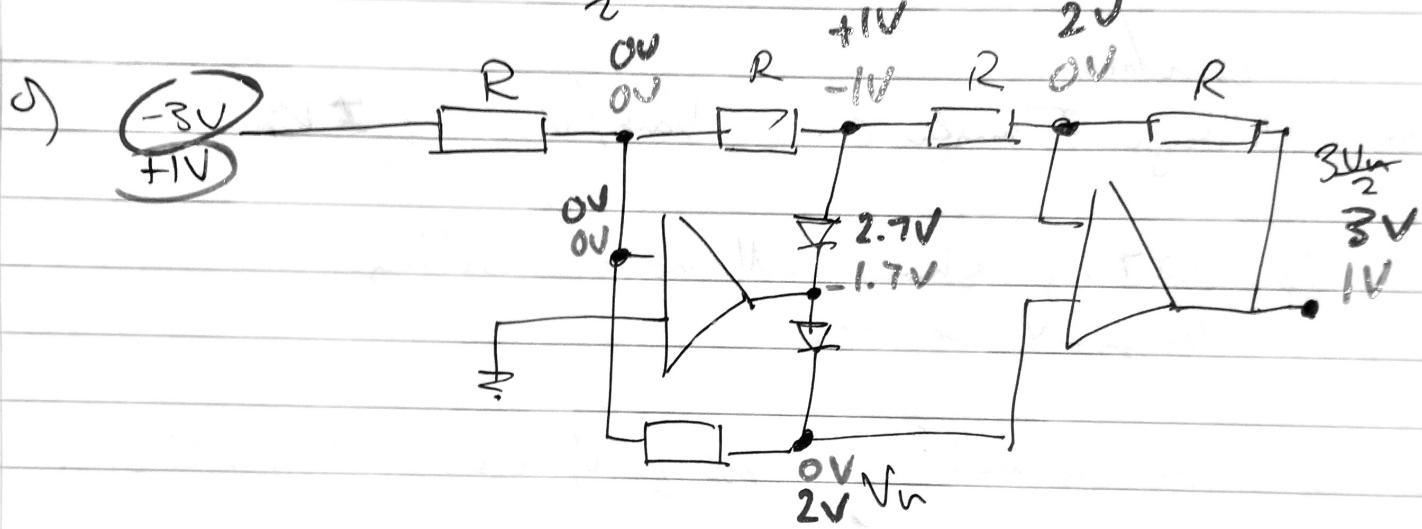
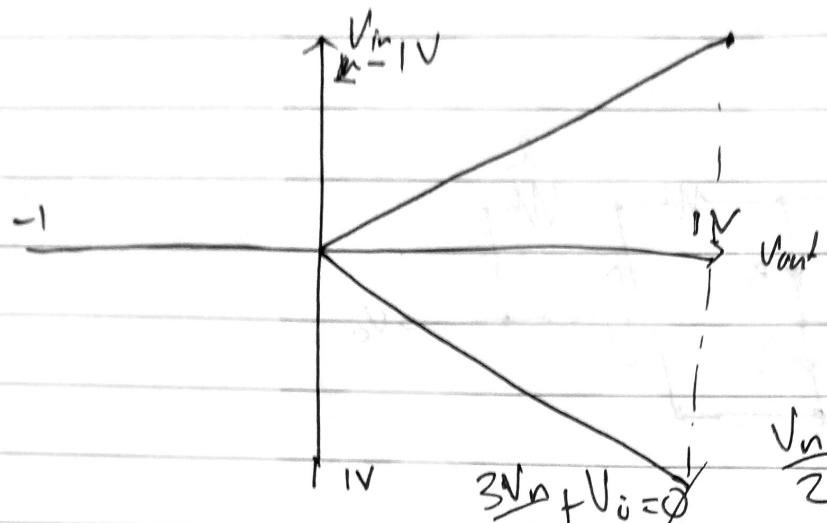
With current flowing from each branch into OP₁, with that node being at -V_{in}, the required voltage at OP₂ out is -V_{in}.



For -ve V_{in} (the virtual short still remains)

the conduct path is along the top branch and from the output of OP₁ to node 1, due to the reverse bias of D₂ block conduction.

The voltage at bottom node in inverting i/p of OP₂ are virtually shorted and OV at inverting i/p of OP₂ ($\frac{1}{3} V_{in}$) is dropped across the top branch resulting in V_{out} = -V_{in} ie rectified.



2) This is a computer monitor trigger.

a) Assume: $V_{O(\text{off})} = \pm 13V$, R_1, R_2 ?

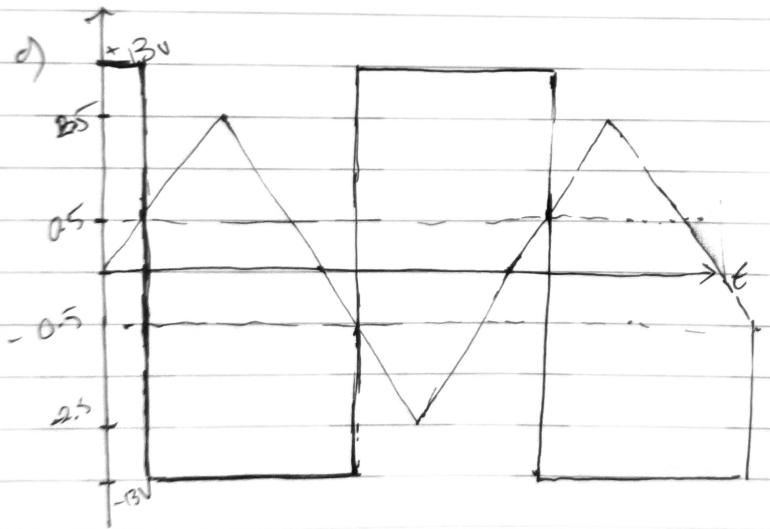
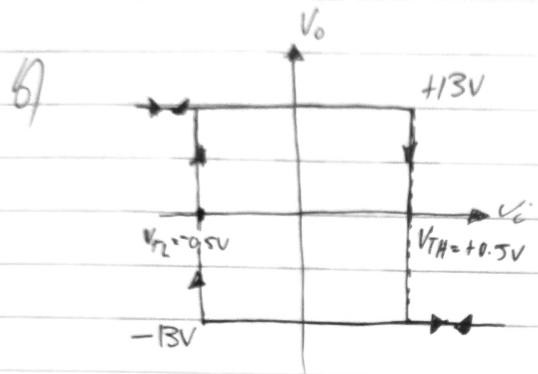
~~$\Delta V = V_{TH} - V_{OL} = 26V$~~ but given hysteresis of $\pm 1V$

~~$\Delta V = V_T - V_{OL} = 26V$~~ $|V_T - V_{OL}| = 1V$ ($v = \pm 0.5V$)

$$\Delta V_T = \left(\frac{R_1}{R_1 + R_2} \right) \cdot (V_{O(\text{on})} - V_{O(\text{off})})$$

~~$\frac{R_1}{R_1 + R_2} = \frac{1}{26}$~~ $\frac{R_1}{R_1 + R_2} = \frac{1}{26}$

$$\therefore R_1 = 1K \quad \text{and} \quad R_2 = 25K$$



3. Hysteresis is how the state of a system depends on its previous states:

In electrical circuits, hysteresis can be included to reduce/prevent unwanted, high speed switching.

Examples of this are a Schmitt trigger, using positive feedback in -ve input

and a latching relay for higher current applications.

4. An opamp has 3 internal stages.

- The input stage, a differential configuration with moderate gain, this is key is minimizing input mismatch

- The gain stage, for voltage amplification. For stability it needs roll off at $\sim 1/\text{Hz}$. So a key note is the Miller Effect.
 - this accounts for the increase in equivalent capacitors.

- The output stage, this provides a low output impedance & a high current. This provides the power amplification for output. Key is protection circuitry.

$$5) GB = 2 \text{ MHz}, V_{\text{sup}} = \pm 10 \text{ V} \quad V_{\text{in-pp}} = 1 \text{ V}$$

gain peak = 10x, input $\Rightarrow 120 \text{ kHz}$

a) • calc required GB, $\geq 2 \text{ MHz}$ enough.

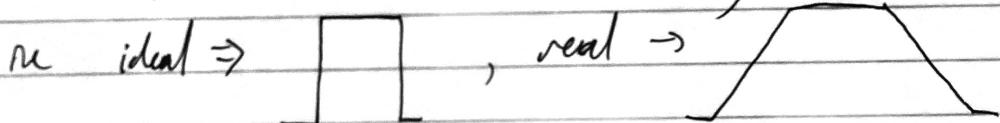
b) \Rightarrow Slow Date

c) • other important parameter \rightarrow closure suitable.

$$a) GBP = A \times BW = 1.2 \text{ MHz}$$

\therefore as the GBP is higher than required
the ~~gain~~ open-loop is suitable in this case.

b) Op amp's, being an active component, it cannot switch output values instantaneously



So if as the f increases the rate of this (the slow rate) will lead to distortion in the actual signal, even though the gain is preserved.

$$c) A = 1 \text{ V}, \omega = 2\pi \cdot 120 \text{ Hz}$$

$$\therefore SR = A \cdot 2\pi f = 1 \cdot 2\pi \cdot 120$$

$$SR = 753.98 \text{ V/}\mu\text{s} = 753.98 \text{ V/}\mu\text{s}$$

$$SR = 0.75389 \text{ V/}\mu\text{s}$$

Search for: min GBP $\geq 1.2 \text{ MHz}$, $SR = 1 \text{ V/}\mu\text{s}$

\Rightarrow TLV342: General purpose OP Amp, GBP: 2.3 MHz
 $SR = 1 \text{ V/}\mu\text{s}$.

$$R_1 = 2k \quad R_2 = 22k, \quad U_{os} \leq 4mV \quad I_B \leq 20\mu A$$

To minimize effect of I_B , $R_p \approx R_1/R_2$

$$R_1/R_2 = 95.5 \quad \text{choose } \underline{\underline{91\Omega}} \text{ (E24)}$$

$$R_a = R_1/R_2 - R_{af} = 46.5 \Omega, \quad \text{choose } \underline{\underline{47\Omega}} \text{ (E24)}$$

$$\text{Transistor Voltage, } V_{ID} = U_{os(max)} + (R_1/R_2) I_{os(max)} \\ = 6mV + (95.5) 30\mu A \\ V_{ID} = 4.03mV$$

So the common voltage will be $4.03mV$ at non-inverting input; $V_x = \pm 4.03mV$

$$V_x = V_y \left(\frac{R_a}{R_B + R_A} \right), \quad \text{but } V_y \Rightarrow \pm 15V$$

So to add some extra allowance for V_x , set to $\mp 15V$.

$$\frac{V_x}{V_y} = \frac{R_a}{R_B + R_A} = \frac{47mV}{15V} = \frac{1}{3212500} \quad R_B \approx \cancel{18.75k\Omega}$$

$$R_B \approx 2500k\Omega \quad \cancel{R_B} = 28125 \quad \cancel{R_B} \rightarrow 9k\Omega$$

$$R_B = 117,500 \Omega \Rightarrow 120k\Omega \quad (\cancel{22k})$$

To assume inverting as R_c varying in the nullifying voltages.

$$R_c \ll R_B$$

So choose a common potential value

$$\underline{\underline{5k\Omega}} \rightarrow 10k\Omega$$

$$\text{Final: } R_p = 91\Omega, R_A = 47\Omega, R_B = 120k\Omega, R_c = 5k\Omega \rightarrow 10k\Omega$$