

Ecu 303

Q1.  $V_{ce} = +10V$ ,  $V_{ce} = -10V$ ,  $R_E = 10\Omega$

$$V_{eq} = V_{ce}, I_{eq} \approx I_C = \frac{|V_{ce}|}{R_E} = 1A$$

$$P_{primary} = \frac{V_{eq} I_{eq}}{2} = \frac{10(1)}{2} = 5 \text{ watts}$$

$$\begin{aligned} P_{dc} &= |V_{ce}| + |V_{ce}| \cdot I_{ca} \\ &= 10 + 10 I_{eq} = 20 \text{ watts} \end{aligned}$$

$$\eta = \frac{\Sigma}{20} = 0.25 = 25\%$$

Q2. a)  $\%D_2 = \left| \frac{0.5}{5} \right| \times 100 = 10\%$

$$\%D_3 = \left| \frac{0.3}{5} \right| \times 100 = 6\%$$

$$\%D_4 = \left| \frac{0.2}{5} \right| \times 100 = 4\%$$

b)  $THD = \sqrt{0.1^2 + 0.08^2 + 0.04^2} = \underline{0.12323} = 12.328\%$

c)  $D_{2,3,4} = 0.2, 0.05, 0.04$

$$I_c = 4A \quad R_c = 8\Omega$$

$$THD = \sqrt{0.2^2 + 0.05^2 + 0.06^2} = 0.215$$

$$P_L = \frac{I_c^2 \cdot R_L}{2} = \frac{16 \cdot 8}{2} = 64 \text{ watts}$$

$$P = (1 + THD^2) P_L = (1 + 0.215^2) 64 = 66.95 \text{ watts}$$

Quench 3. a) 2N3904  $T_{\text{crossover}} = 65^\circ$

deraille:  $5 \text{ mV}/^\circ\text{C}$  above  $T_a = 25^\circ$

$$(65 - 25) \cdot 5 = 200 \text{ mW}$$

Max dissipation  $\Rightarrow @ T_a = 65^\circ\text{C} \Rightarrow 425 \text{ mW}$

b)  $R_{\theta T_a} = 200^\circ\text{C}/\text{W}$

$$R_{\theta T_c} = 03.3^\circ\text{C}/\text{W}$$

$$T_{j,\text{max}} = -55^\circ\text{C} \rightarrow 150^\circ\text{C}$$

$$V_{CC} = 10, R_1 = 10\text{k}, R_2 = 2\text{k2}$$

$$P_{\text{dc}} = V_{CC} \cdot I_{CQ}, \quad I_E \approx I_{CQ} \quad T_E = \frac{V_E}{R_E}$$

$$V_E = V_B - 0.7, \quad V_B = \frac{R_2}{R_1 + R_2} V_{CC} = 1.8$$

$$V_E = 1.1, \quad I_{CQ} = 0.001617 = 1.617 \text{ mA}$$

$$\underline{P_{\text{dc}} = 16.17 \text{ mW}}$$

$$T = 200 + 16.17 \times 10^{-3} + 65 = 68.234^\circ\text{C}$$

This is within the operating temperature  
 $\therefore$  does not require a heatsink

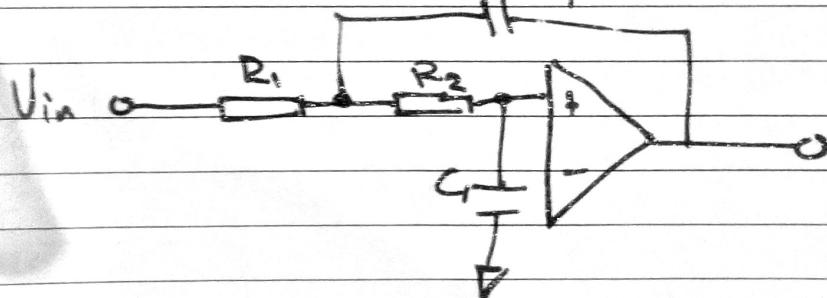
Quadrat. Low pass filter:

$f_c = 200\text{Hz}$ , sourced from Techwally

I chose a 2nd Order Active filter  
to make use of high input  $Z_i$

And a butterworth approximation to reduce eliminate  
passband ripple.

$$Q = \frac{1}{\sqrt{2}} \quad K_C = 1 \quad f_p = \frac{f_c}{C_2 K_p} = 200\text{Hz}$$

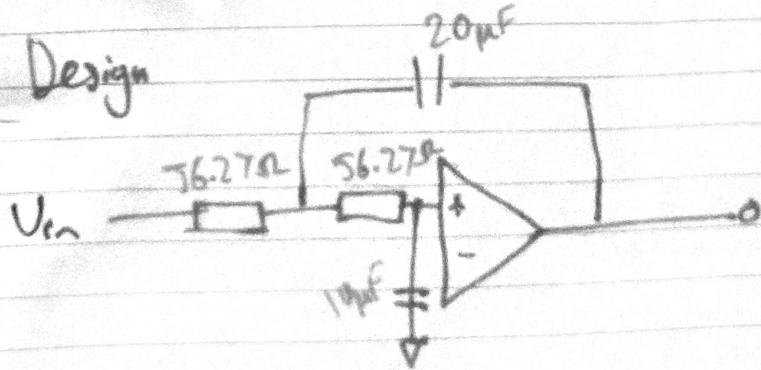


Next: Choose standard  $C_1$  value =  $10\mu\text{F}$

$$Q = 0.5 \sqrt{\frac{C_2}{C_1}} \Rightarrow C_1(2Q)^2 = 2C_1 = C_2, \quad C_2 = 20\mu\text{F}$$

$$f_p = \frac{1}{2\pi R \sqrt{C_1 C_2}}, \quad R = \frac{1}{f_p 2\pi \sqrt{C_1 C_2}} = 56.27\Omega$$

Final Design



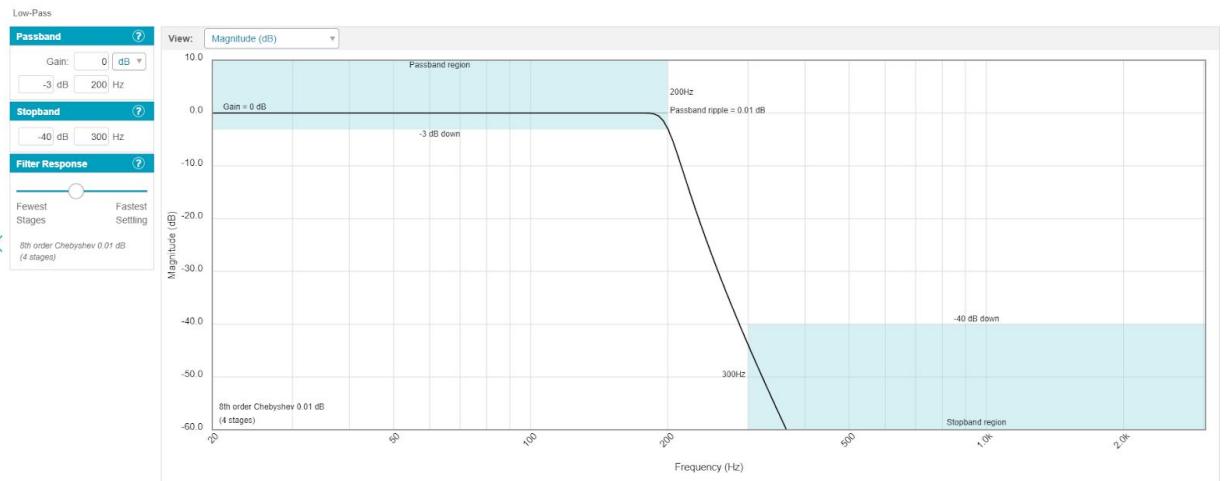
## Question 5

To keep from altering the passed signal a 0dB passband gain was chosen.

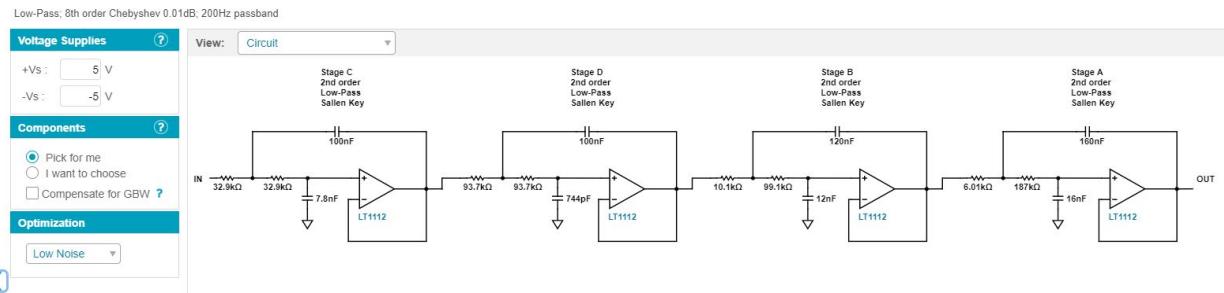
The passband ends at 200Hz with a -3dB point.

The stop band was chosen to be as close as possible (300Hz) while retaining a unity gain in the passband.

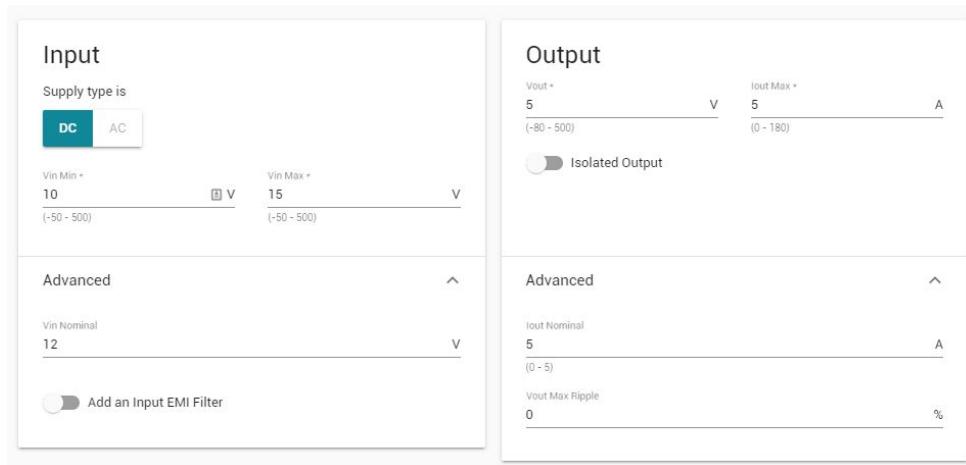
Note due to a slight Chebyshev approximation there is a 0.01dB ripple at the end of the passband



The resultant filter is a 4 stage, 8th order active filter. This is supplied with +5V as this is just signal filtering, but optimised for low noise output due to its audio application.



## Question 6

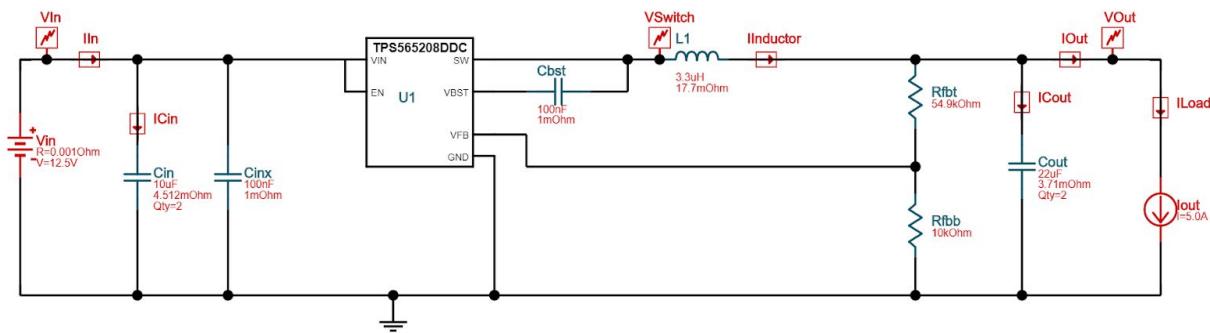


### Design Decisions:

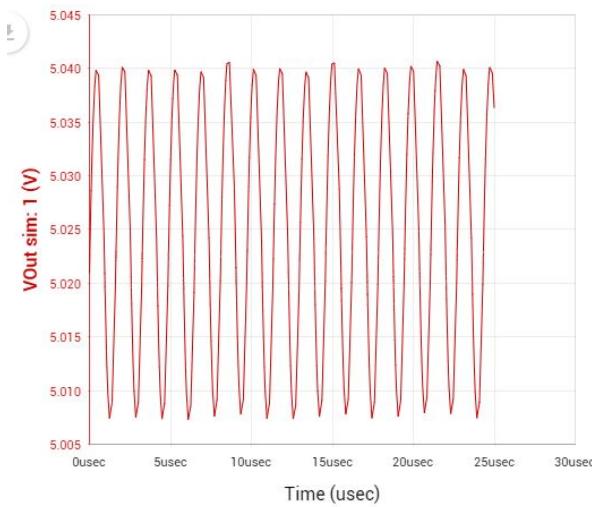
Given the required application of a charger. This was taken to be powered via an external DC voltage source, ie a large 12V battery etc. Also the closeness in input to out. The above figure shows a chosen voltage range of 10V - 15V but designed for a nominal 12V, this is the account for discharge voltage droop and accounting for issues with overvoltage

Output was selected to match 5V, 5A requirements and aimed 0% Vout ripple to design for a minimised ripple.

This resulted in TI Power Designer providing the below design, which I then simulated and evaluated.



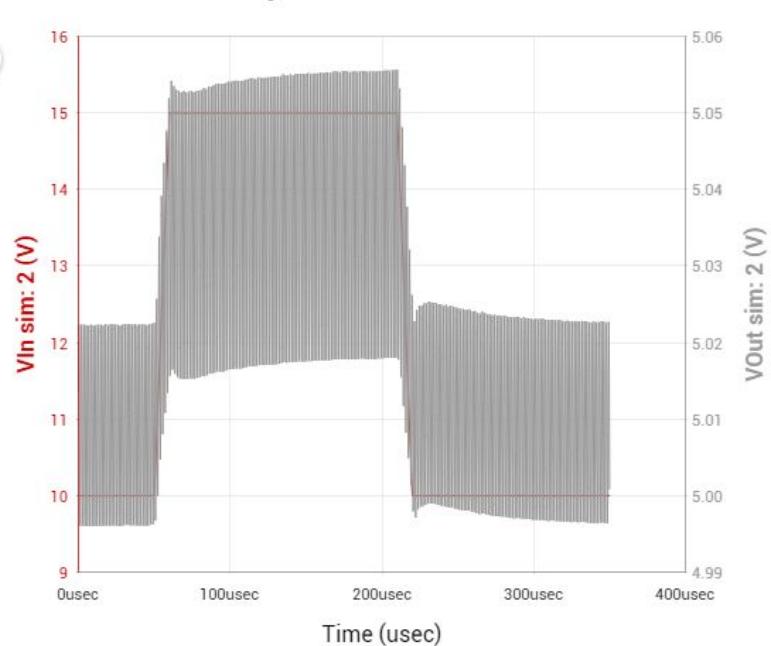
### Design Evaluation:



### Performance Summary

Sim ID	Vout Peak-to-Peak	Vout Average	Inductor Current Peak-To-Peak	Average Freq
1	33.30 mV	5.03 V	1.50 A	616.85 kHz

$$\% \text{ Ripple} = \frac{33.30mV}{5.03V} \times 100 = 0.66\%$$



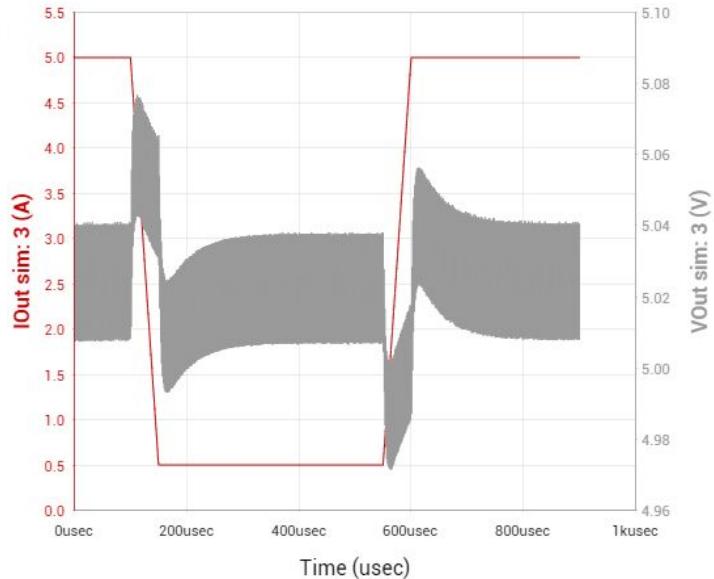
### Performance Summary

Sim ID	Vout Maximum	Vout Minimum
2	5.06 V	5.00 V

Worst case line regulation:

$$= \frac{\Delta V_{out}}{\Delta V_i}$$

$$= \frac{0.06}{5} \times 100 = 1.2\%$$



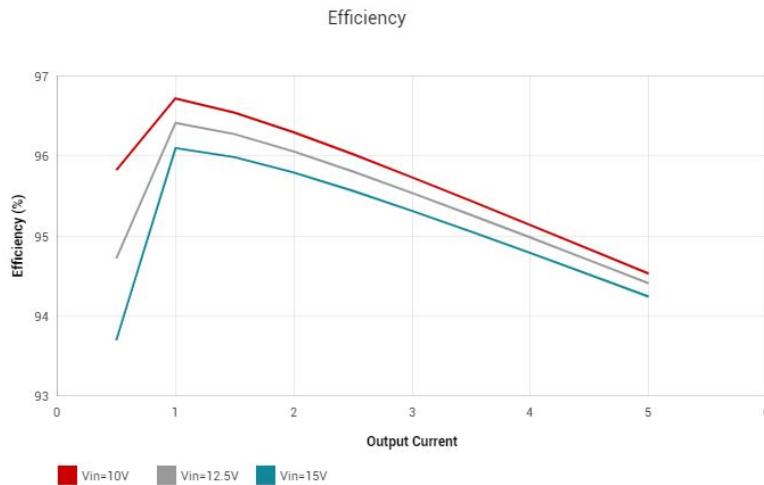
## Performance Summary



Sim ID	Vout Maximum	Vout Minimum	Overshoot Settle Time	Undershoot Settle Time	Overshoot	Undershoot
3	5.08 V	4.97 V	0.15 ms	0.15 ms	0.05 V	0.05 V

Load regulation, looking the settled values from a load transient simulation:

$$\begin{aligned}
 &= \frac{V_{NL} - V_{FL}}{V_{FL}} \times 100 \\
 &= \frac{5.015 - 5.03}{5.03} \times 100 = 0.298\%
 \end{aligned}$$



This design provides great efficiency ( $93.5\% \Rightarrow 97\%$ ) generally and ~94.5% at the required current for the full input voltage range.