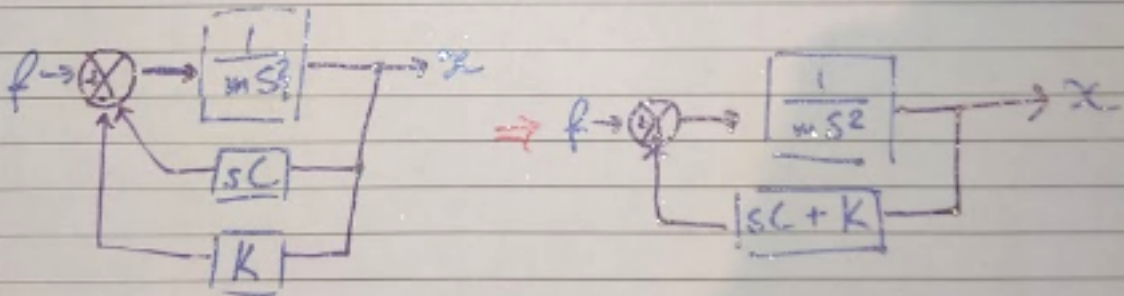
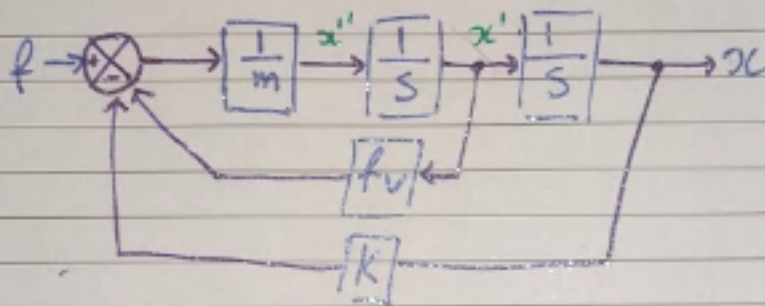


Ecen 321 Test Daniel Eisen 300447549

Q.1. $F = \begin{matrix} ma \\ kx \\ fv\dot{x} \end{matrix}$, $f(t) = \begin{matrix} m\ddot{x} \\ k\dot{x} \\ fv\ddot{x} \end{matrix}$

$$f = m\ddot{x} + fv\dot{x} + kx \Rightarrow \frac{1}{m}[f - fv\dot{x} - kx] = \ddot{x}$$



$$\Rightarrow \frac{\frac{1}{ms^2}}{1 + \frac{sc + k}{ms^2}} = \frac{1}{ms^2 + sc + k} = \frac{x(s)}{F(s)}$$

$$Q2. I) \quad \frac{P}{V} = \frac{1/K}{s(1+sT)} \quad K=0.2 \\ T=0.8$$

$$\frac{R}{R} = \frac{C/K}{s(1+sT)}$$

$$1 + \frac{C/K}{s(1+sT)}$$

$$= \frac{C/K}{s(1+sT) + C/K} \Rightarrow \frac{C/K}{Ts^2 + s + \frac{C}{K}} = \frac{P}{R}$$

$$II) \text{ char: } Ts^2 + s + \frac{C}{K} = 0$$

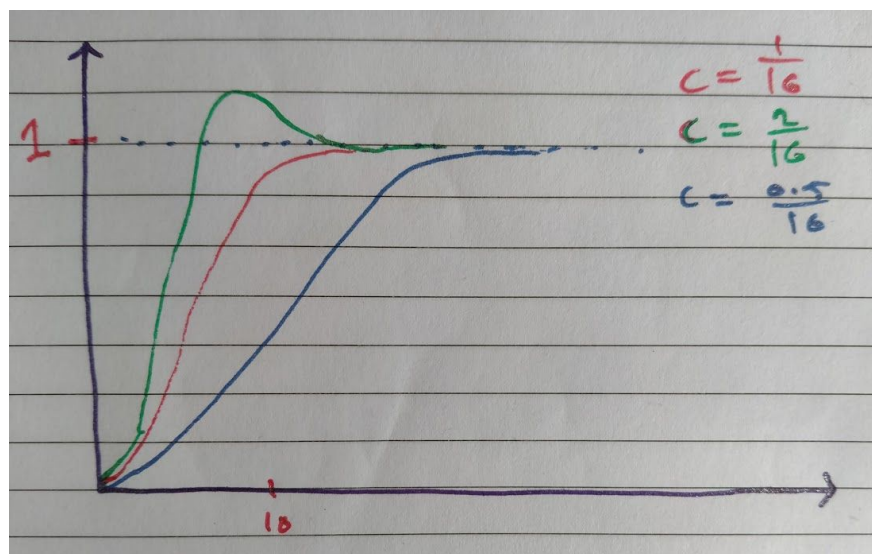
$$\text{critically: } b^2 - 4ac = 0$$

$$1 - 4T\frac{C}{K} = 0$$

$$C = \frac{K}{4T} = \frac{1}{16}$$

$$\therefore \text{ under: } C > \frac{1}{16}$$

$$\text{over: } C < \frac{1}{16}$$



Q3 I) $G(s) = \frac{1}{(s+20)(s^2+5s+20)}$

$p_1 = -20$, $p_{2,3} \Rightarrow$ quadratic equation
 $= \frac{-5 \pm 3.7}{2}$

II) Can approx as second order by discarding the fastest pole and compensate for the change in SS

$\hookrightarrow \frac{1}{20} \cdot \frac{1}{s^2+5s+20}$

III) $\omega_n = \sqrt{20} \approx 4.4721$

$\xi = \frac{5/2}{\sqrt{20}} \approx 0.559$

$T_p = \frac{\pi}{\omega_n \sqrt{1-\xi^2}} = 0.847$

$T_s = \frac{4}{0.559 \cdot 4.472} \approx 1.6$

$\%OS = e^{-\left(\frac{\pi \xi}{\sqrt{1-\xi^2}}\right)} \approx 0.12 \rightarrow 12\%$

Q4 I) Negative feedback: When the output signal is subtracted from the input signal and feedback into system

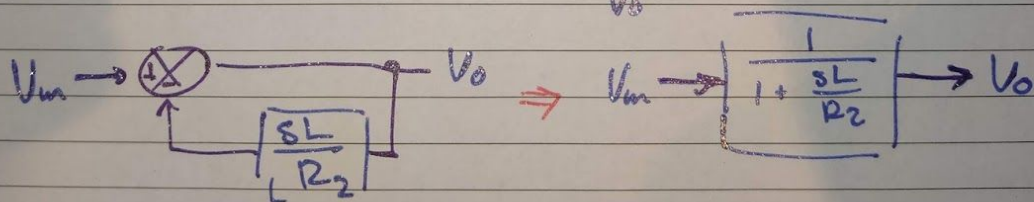
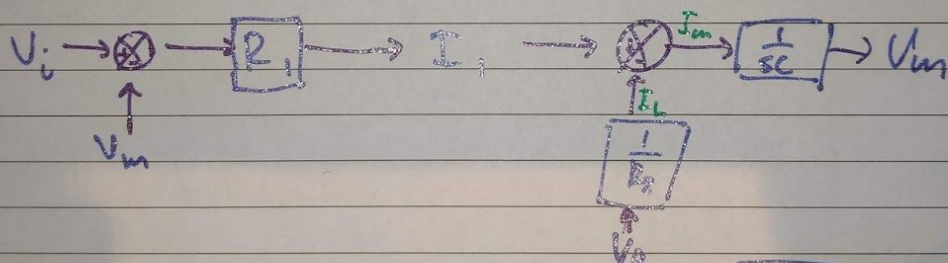
II) Reduces noise, the effects of disturbances & the sensitivity to external change

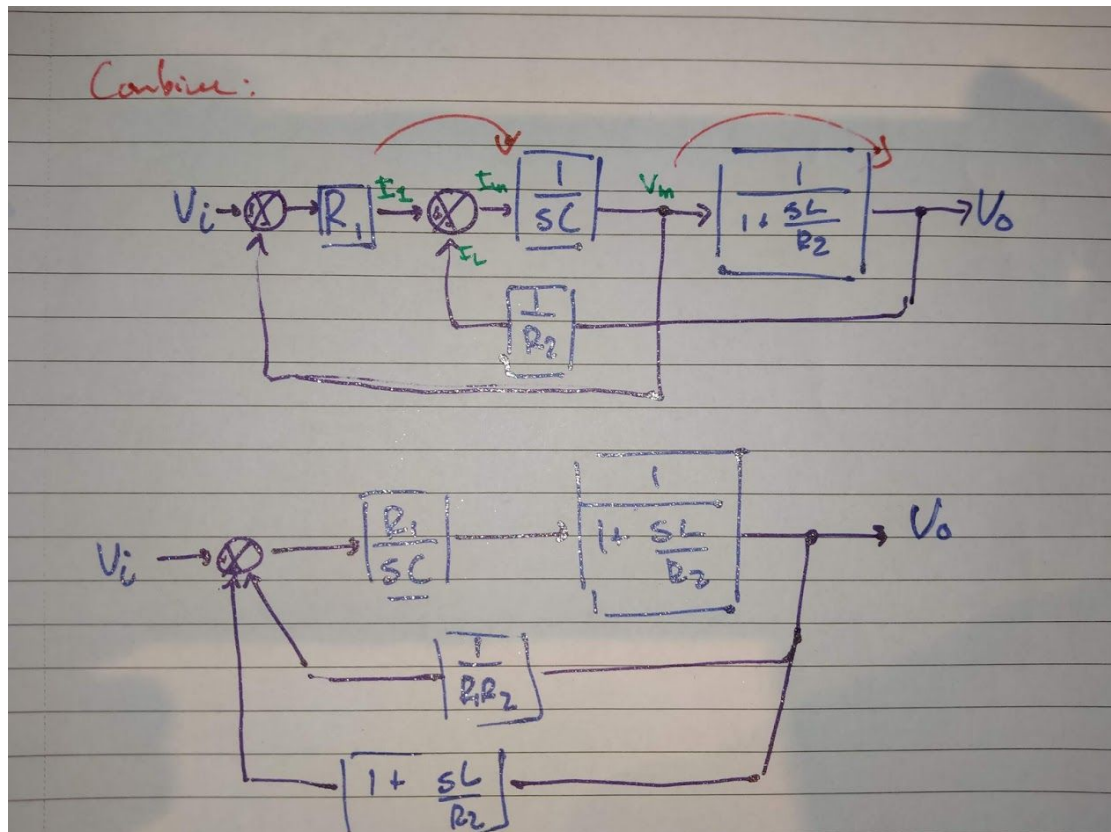
III) In audio, i.e. disturbance effects
Choking, in electronic mechanisms.

Q5. $V_i - V_m = R_1 I_1$ $V_m - V_o = sL I_L$

$I_m = I_1 - I_L$ $I_L = \frac{V_o}{R_2}$

$V_m = \frac{1}{sC} I_m$ $\therefore V_m - \frac{sL}{R_2} V_o = V_o$





Q5, continued:

The block diagram shows a control system with input V_i entering a summing junction. The output of this junction goes through a block $\frac{R_2}{sC + \frac{LCs^2}{R_2}}$ to a second summing junction. The second summing junction also receives feedback from the output V_o through a block $\frac{L}{R_2}s + \frac{1}{R_1 R_2} + 1$. The output of the second summing junction goes through a block $\frac{1}{1 + \frac{sL}{R_2}}$ to produce the output V_o .

Derivation of the transfer function:

$$\Rightarrow \frac{R_2}{\frac{LCs^2}{R_2} + Cs}$$

$$\Rightarrow \times 1 + \left(\frac{L}{R_2}s + \frac{1}{R_1 R_2} + 1 \right) \left(\frac{R_2}{\frac{LCs^2}{R_2} + Cs} \right)$$

$$= \frac{R_1}{\frac{LC}{R_2}s^2 + Cs + \frac{LR_1}{R_2}s + \frac{1}{R_2} + R_1}$$

$$= \frac{R_1}{\frac{LC}{R_2}s^2 + Cs + \frac{LR_1}{R_2}s + \frac{1}{R_2} + R_1}$$

$$= \frac{1}{\underbrace{\frac{LC}{R_1 R_2}}_a s^2 + \underbrace{\left(\frac{C}{R_1} + \frac{L}{R_2}\right)}_b s + \underbrace{\frac{1}{R_1 R_2} + 1}_c}$$

Both C and L do not contribute to steady state gain so altering either can effect damping without changing SSQ.

ie: $b^2 - 4ac : \underline{L=1} \Rightarrow \underline{-32} \therefore \underline{\text{underdamped}}$