

# ECEN301 : Embedded Systems

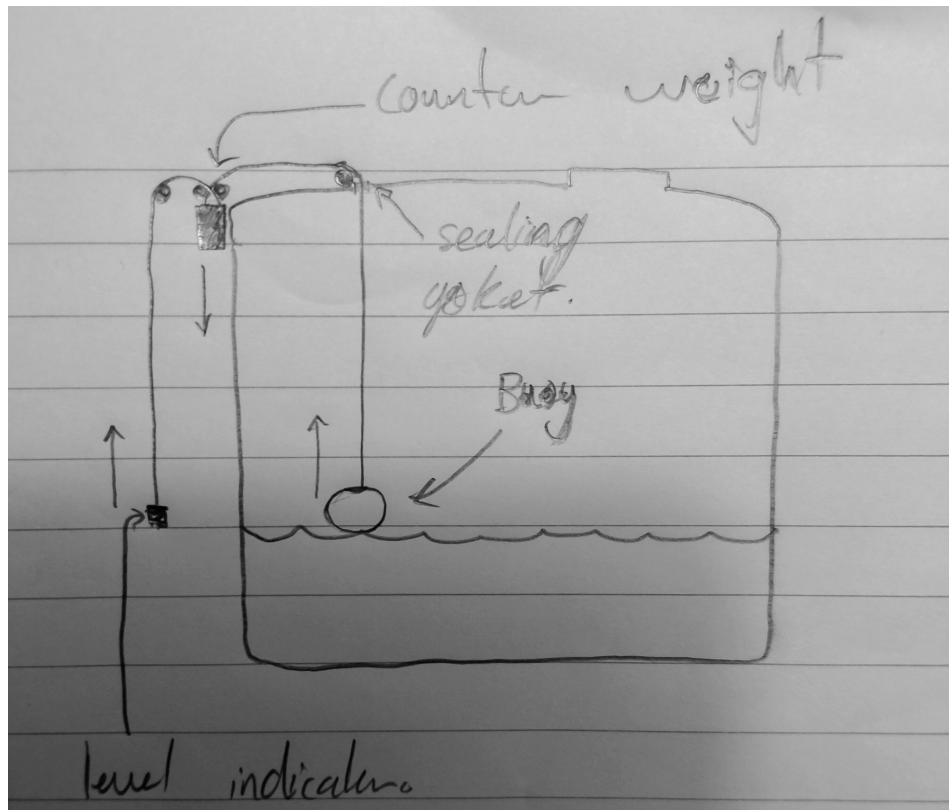
## Assignment 1 Submission

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August 21, 2020

### Question 1

Mk I



- Simple construction, with electrical requirements
- Is a non-reverse indicator. If properly aligned the level indicator will align with the internal water level
- If buoy is sized correctly to the tanks overflow level, they should be no or minimal clipping of mini/max levels.
- Included materials are 4 pulleys, rope, a seal, buoy, level indicator (small stainless steel ball/etc), counter-weight (sand filled plastic container), and mounting hardware. Total material cost should be below \$100 and take a maximum of 2 hours to install.

## Mk II

Mk I succeeds in simplicity and durability, but does not offer much extra. Points that can be improved include:

- Quantifiable output, i.e. volume, days left of consumption.
- Remote monitoring and alerts
- software based extension and future support.

Utilising the MB7369 ultrasonic water level sensor, which is IP-68 water resistant, has a 7.65 meter range, 1cm resolution and 200,000 rating hours of inter-servicing operating time, it can be mounted above the overflow line inside the tank and the cable feed and sealed through a drill hole (or using an existing inspection hole) and provide and can provide either an analog voltage reading, PWM or digital (RS232) signal to a compatible micro-controller.

*cost:* \$40.00

To drive the system, the ESP32 controller can be installed in a weather project box at the base of tank and powered via a DC PSU from the nearby main connection. The sensor has a low current draw of 3.4mA @ 3-5V5 so can be driven from the onboard V-reg. This board provides low power Bluetooth, wifi, and a dual core processor with lower power functionality.

*cost:* \$3-\$6

With this an external display can be driven either mounted at the box or remotely connect indoors (via BLE or wifi). It will display the current level in meters/volume and estimated remaining days calculated from usage.

*cost:* \$15

All extra component cost under \$50 and time and development time estimated at 15-20hr.

The system provide the possible expansion via firmware updates (ESP32 allows this to be set up remotely) to a Mk III installation of a possible mobile app or website based monitoring

## Question 2

$$E = 2.2 \times 10^{11} \text{ N/m}^2, S_{max} = 5.5 \times 10^8 \text{ N/m}^2, G = 2.2 \\ x = 8\text{cm}, t = 0.15\text{cm}, w = 2.5\text{cm}, R = 150\Omega$$

$$E = \frac{S}{\varepsilon} \Rightarrow \varepsilon = \frac{S}{E} = 2.5 \times 10^{-3}$$

$$\varepsilon = \frac{6xF}{wt^2E} \Rightarrow F = \frac{\varepsilon wt^2E}{6X} = 67.03\text{N}$$

$$G = \frac{\Delta R/R}{\varepsilon} \Rightarrow \Delta R = G\varepsilon R = 0.825\Omega$$

## Question 3

$$0.1 \text{ arcmin} = 0.001667^\circ$$

$$360/0.001667 = 215956.8 \Rightarrow \text{round to } 215957$$

$$\log_2(215957) = 17.72, \text{ ie } \mathbf{18bit} \text{ absolute encoder}$$

## Question 4

$$\varepsilon_{emf} = -S\Delta T$$

$$750\mu V = -S(70 - 10) \therefore -S = 12.5\mu V/^{\circ}C$$

$$520\mu V = 12.5(t - 10)$$

$$t = \frac{520}{12.5} + 10 = 51.6^{\circ}C$$

With the rough estimate of sensitivity above of  $12.5\mu V/^{\circ}C$ , this closest resembles a type R, platinum-rhodium thermocouple, which have a nominal sensitivity of around 9 at room temp. As opposed to a type K (chromel and alumel) of 41.

## Question 5

$$\begin{aligned}\varepsilon_{emf} &= -S\Delta T \\ &= 12.5(-35) = -437.5\mu V\end{aligned}$$

## Question 6

i) Taking the pot as a voltage divider:

$$V_{oc} = V_s \left( \frac{R_p x}{R_p x + R_p(1 - x)} \right)$$

With load resistance,  $R_{out}$  becomes  $R_p x // R_L$

$$\begin{aligned}V_L &= V_s \left( \frac{R_p x // R_L}{R_p x // R_L + R_p(1 - x)} \right) \\ &= V_s \left( \frac{\frac{R_p x \cdot R_L}{R_p x + R_L}}{\frac{R_p x \cdot R_L}{R_p x + R_L} + R_p(1 - x)} \right) \\ &= V_s \left( \frac{R_L x}{R_L + R_p x(1 - x)} \right) \\ &= x \cdot V_s \left( \frac{1}{1 + R_p R_L x(1 - x)} \right)\end{aligned}$$

Loading error is defined as:  $N(x) = V_{oc} - V_L$

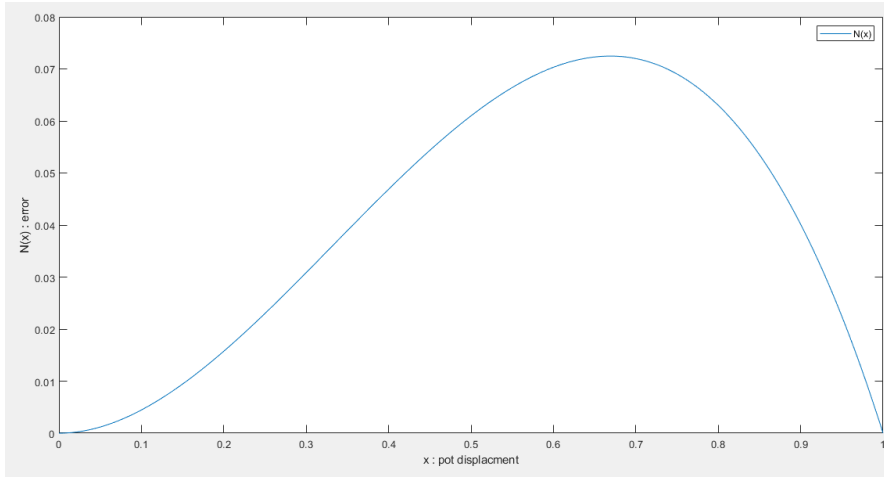
$$N(x) = V_s \left( \frac{R_p x}{R_p x + R_p(1 - x)} - \frac{x}{1 + R_p R_L x(1 - x)} \right)$$

ii) If  $\frac{R_p}{R_L} \ll 1$  then the Loading error can be simplified to  $V_s \cdot (x^2 - x^3) \cdot \frac{R_p}{R_L}$

Differentiate:  $V_s \cdot \frac{R_p}{R_L} \cdot (2x - 3x^2)$

$$(2x - 3x^2) = 0 : x = 2/3$$

$$\begin{aligned}N(x)_{max} &= (4/27)V_s \cdot \frac{R_p}{R_L} \therefore \text{maximum error percentage is } N(x)_{max}/V_s \times 100 = 400/27 \cdot \frac{R_p}{R_L} = \\ 400/27 &= 14.814815 \approx 15 \cdot \frac{R_p}{R_L}\end{aligned}$$



iii)

iv) By knowing the points of maximum error and the characteristics of how the system approaches it, the transducer can be designed in such a way as to the operating region.

v) (a,b) Using max error will ensure it's under requirement across whole displacement, ie fore both, 0.2 and 0.67.

$$0.1 = 15(1k/R_L)$$

$$R_L = 15k/0.1 = 150k$$