



**University
of Dayton**

AEE 553 — Compressible Flow

Department of Mechanical and Aerospace Engineering

Homework 3

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Problem 2

(a) Plot the Mach number of the F-16 during its 20-minute flight.

Givens:

Time series for p_t and p , the total and static pressure, respectively, measured by the F-16's pitot-probe. The flight data given covers a simple trajectory including a take-off, acceleration to max-speed, and deceleration to landing.

Assumptions:

Let region 1 be the area upstream of the bow shock. Let region 2 be the area *immediately behind the shock* but not at the probe's stagnation point. The static pressure measurement taken by the probe is valid for the static pressure *upstream* of the shock. The flow before and after the bow shock is isentropic, calorically perfect air. $\gamma_{air} = 1.4$, $R_{air} = 287 \text{ J/kg} \cdot \text{K}$. The shock can be evaluated as a normal shock in front of the pitot probe. A shock is only present in front of the pitot probe when the F-16 is traveling supersonically, $M > 1$. All flow is isentropically brought to rest at the tip of the pitot-probe.

Solution:

During the subsonic portion of flight, the F-16's Mach number is found using isentropic equations relating p_t , p , and M .

$$\frac{p_{t,1}}{p_1} = \left(1 + \frac{\gamma - 1}{2} M_1^2\right)^{\frac{\gamma}{\gamma - 1}}$$

Rearranging to isolate M :

$$M_1 = \sqrt{\left[\left(\frac{p_{t,1}}{p_1}\right)^{\frac{\gamma - 1}{\gamma}} - 1\right] \frac{2}{\gamma - 1}}$$

During the subsonic portion of flight, we have data for the quantities $p_{t,1}$ and p_1 , and can easily solve for M_1 . However, once the F-16 reaches supersonic velocities, this relation is no longer valid for our measurements. The total pressure measurement becomes the total pressure experienced by the probe *behind the shock*, $p_{t,2}$. We must now find a new relationship using $p_{t,2}$, p_1 , and M_2 . The ratio of total pressure behind a shock to static pressure in front of a shock can be expressed via the multiplication of other ratios we have isentropic/normal shock relations for.

$$\frac{p_{t,2}}{p_1} = \frac{p_{t,2}}{p_2} \frac{p_2}{p_1}$$

The isentropic relationship for total and static pressure has already been shown for the subsonic Mach calculations.

$$\frac{p_{t,2}}{p_2} = \left(1 + \frac{\gamma - 1}{2} M_2^2\right)^{\frac{\gamma}{\gamma-1}}$$

The relationship connecting static pressure across a normal shock is given below:

$$\frac{p_2}{p_1} = \left(\frac{2\gamma}{\gamma+1} M_1^2 - \frac{\gamma-1}{\gamma+1}\right)$$

Combining these two equations yields an expression for $p_{t,2}/p_1$ in terms of γ , M_1 , and M_2 .

$$\frac{p_{t,2}}{p_1} = \left(1 + \frac{\gamma - 1}{2} M_2^2\right)^{\frac{\gamma}{\gamma-1}} \left(\frac{2\gamma}{\gamma+1} M_1^2 - \frac{\gamma-1}{\gamma+1}\right)$$

We do not know M_1 or M_2 , but we do have a normal shock relationship relating the two of them:

$$M_2^2 = \frac{M_1^2 + \frac{2}{\gamma-1}}{\frac{2\gamma}{\gamma-1} M_1^2 - 1}$$

Substituting this relation into our previous defined ratio:

$$\frac{p_{t,2}}{p_1} = \left(1 + \frac{\gamma - 1}{2} \left[\frac{M_1^2 + \frac{2}{\gamma-1}}{\frac{2\gamma}{\gamma-1} M_1^2 - 1}\right]\right)^{\frac{\gamma}{\gamma-1}} \left(\frac{2\gamma}{\gamma+1} M_1^2 - \frac{\gamma-1}{\gamma+1}\right)$$

This equation cannot be solved by hand, so a numerical solver will be used in Python to determine the Mach number based on $p_{t,2}/p_1$ while the F-16 is supersonic. The final question that must be examined before calculating the F-16's Mach number during its flight is how to decide whether the F-16 is subsonic or supersonic without knowing the Mach number. The answer comes by examining the limiting case of exactly sonic velocity, i.e. $M = 1$. The isentropic total-to-static pressure ratio for $M = 1$ is given below, where p^* represents static pressure at sonic conditions.

$$\frac{p_t}{p^*} = \left(1 + \frac{\gamma - 1}{2}\right)^{\frac{\gamma}{\gamma-1}}$$

Inserting our known value of γ yields the critical pressure ratio for sonic flight:

$$\frac{p_t}{p^*} \approx 1.89$$

From this value we can determine when the F-16 reaches sonic velocities. By definition, a normal shock at sonic conditions is an infinitely weak shock and is isentropic. Examining the relationship for $p_{t,2}/p^*$ at sonic conditions:

$$\frac{p_{t,2}}{p_1} = \left(1 + \frac{\gamma - 1}{2} \left[\frac{1 + \frac{2}{\gamma - 1}}{\frac{2\gamma}{\gamma - 1} - 1} \right] \right)^{\frac{\gamma}{\gamma - 1}} \left(\frac{2\gamma}{\gamma + 1} - \frac{\gamma - 1}{\gamma + 1} \right)$$

$$\frac{p_{t,2}}{p_1} = \left(1 + \frac{\gamma - 1}{2} \left[\frac{\cancel{\gamma + 1}}{\cancel{\gamma + 1}} \right] \right)^{\frac{\gamma}{\gamma - 1}} \left(\frac{\cancel{\gamma + 1}}{\cancel{\gamma + 1}} \right)$$

$$\frac{p_{t,2}}{p_1} = \left(1 + \frac{\gamma - 1}{2} \right)^{\frac{\gamma}{\gamma - 1}}$$

$$\frac{p_{t,2}}{p_1} \approx 1.89$$

We have now proven that both the subsonic and supersonic relationships we have found converge onto the same value at the sonic condition. Any time the pressure ratio from the pitot-probe exceeds this critical value, the F-16 is supersonic, and any time it is below, it is subsonic.

Discussion:

Figure 1 shows the time history of the pitot-probe's total to static pressure ratio, highlighting the critical threshold beyond which flight is supersonic.

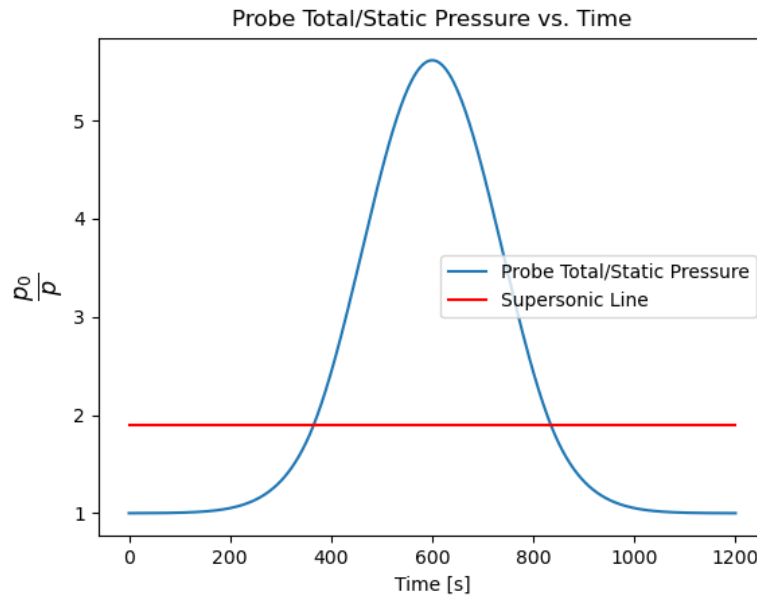


Figure 1: Probe total-to-static pressure ratio and supersonic threshold

Figure 2 shows the F-16's Mach number over the time of its flight using the relationships we have defined.

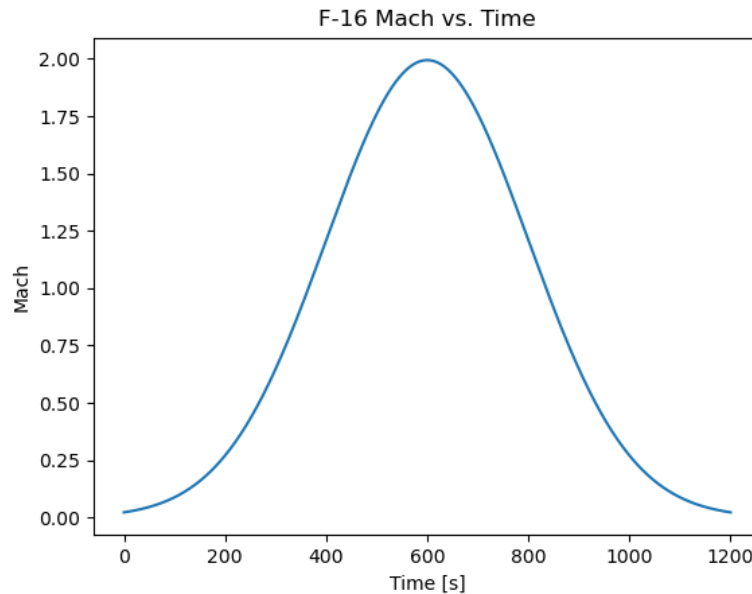


Figure 2: F-16 Mach vs. Time during flight, calculated using isentropic and normal shock relations

Figure 3 shows a comparison of the F-16's Mach number calculated correctly, taking shocks into account, and calculated as if there were no shocks in front of the probe.

Figure 4 shows the Mach number experienced by the pitot probe during the flight.

Figure 5 shows a comparison of the F-16's flight Mach number and that of the pitot probe in-flight. Note that the pitot probe experiences a local minimum Mach number when the F-16 is flying at its largest Mach number. This is indicative of the fact that shock strength increases with incoming Mach number.

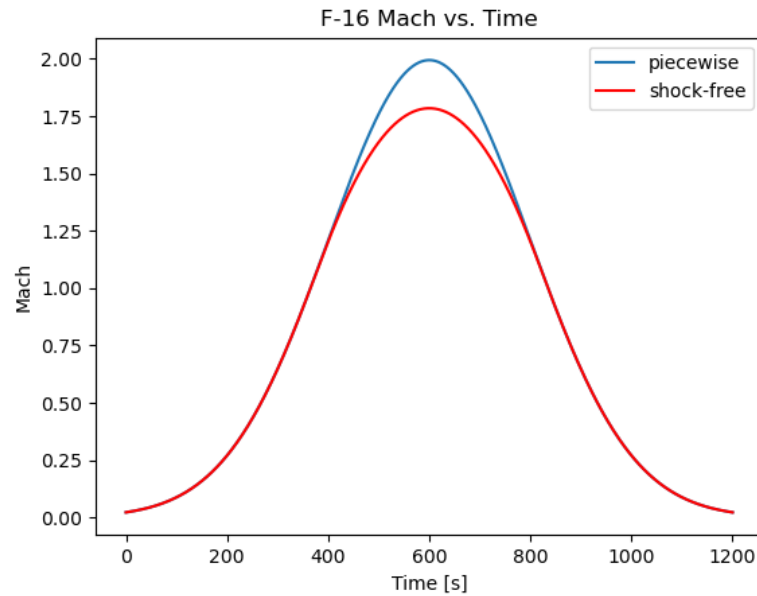


Figure 3: F-16 Mach vs. Time during flight, calculated correctly and as if there were no shocks

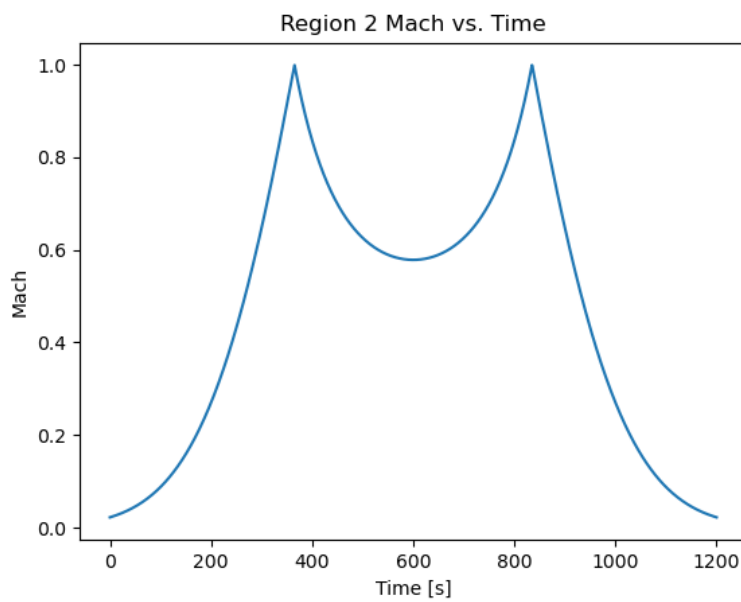


Figure 4: Mach experienced by pitot probe vs. Time during flight

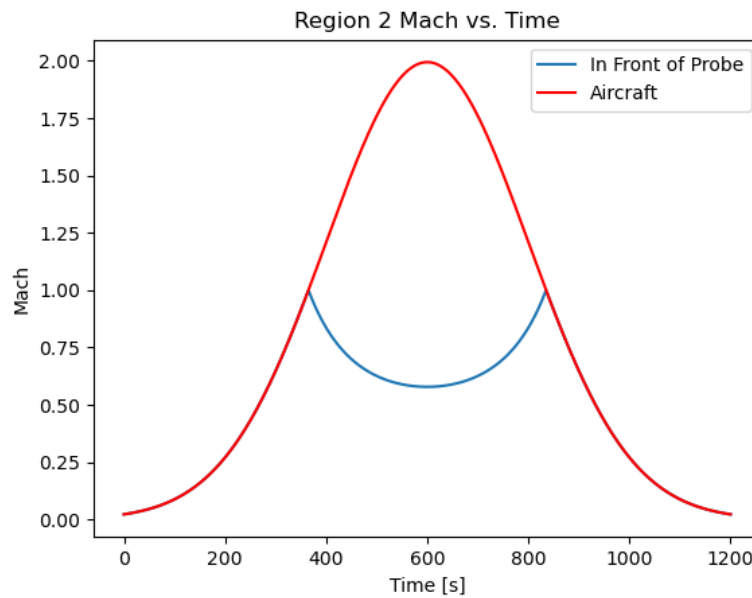


Figure 5: Mach experienced by pitot probe and F-16 vs. Time during flight

(b) Plot the air temperature experienced at the tip of the probe for this 20-minute flight.

Givens:

Time series for p_t and p , the total and static pressure, respectively, measured by the F-16's pitot-probe. The flight data given covers a simple trajectory including a take-off, acceleration to max-speed, and deceleration to landing. There is a constant atmospheric temperature of $T = 298\text{ K}$ at all altitudes in the trajectory.

Assumptions:

Let region 1 be the area upstream of the bow shock. Let region 2 be the area *immediately behind the shock* but not at the probe's stagnation point. The static pressure measurement taken by the probe is valid for the static pressure *upstream* of the shock. The flow before and after the bow shock is isentropic, calorically perfect air. $\gamma_{air} = 1.4$, $R_{air} = 287\text{ J/kg} \cdot \text{K}$. The shock can be evaluated as a normal shock in front of the pitot probe. A shock is only present in front of the pitot probe when the F-16 is traveling supersonically, $M > 1$. All flow is isentropically brought to rest at the tip of the pitot-probe. Total temperature is constant across a shock because shocks are adiabatic.

Solution: