

ARS5 Final Project



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Problem Statement

**Modeling of a Quadcopter System and Backstepping Control
to provide the stability analysis**

Project Goals

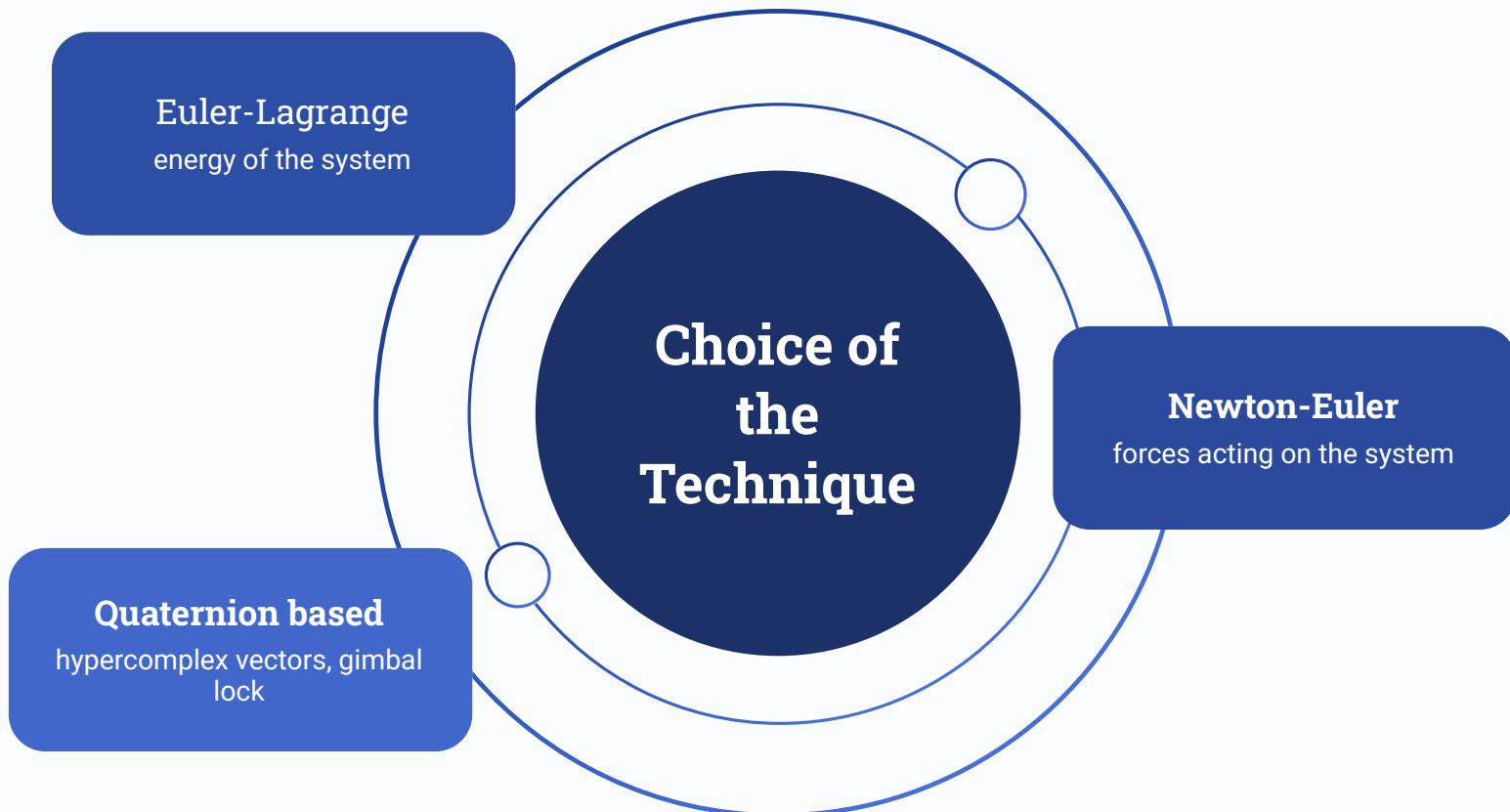
Develop a **complete model** robust to most of the forces that act on the drone

Avoid singularities

Have a stable system after conducting a thorough **stability analysis**

Convergence to fixed targets and **Follow** trajectories

Modeling



Modeling of the Quadcopter

State vector

$$\mathbb{X} = [\xi^T \quad \dot{\xi}^T \quad \mathbf{q}^T \quad \boldsymbol{\Omega}^T]^T$$

Modeling (cont'd)

Translational part

$$\dot{\mathbb{X}}_{pos} = \begin{bmatrix} \dot{\xi} \\ \ddot{\xi} \end{bmatrix} = \left[\mathbf{q} \otimes \frac{F_u}{m} \otimes \mathbf{q}^* + F_{ext} \right]$$

Modeling (cont'd)

Rotational part

$$\dot{\mathbb{X}}_{rot} = \begin{bmatrix} \dot{\mathbf{q}} \\ \dot{\boldsymbol{\Omega}} \end{bmatrix} = \begin{bmatrix} \frac{1}{2}\mathbf{q} \otimes \boldsymbol{\Omega} \\ I^{-1}(\boldsymbol{\tau} - \boldsymbol{\Omega} \times I\boldsymbol{\Omega}) \end{bmatrix}$$

Modeling (cont'd)

Overall base model

$$\dot{\mathbb{X}} = \begin{bmatrix} \dot{\xi} \\ \ddot{\xi} \\ \dot{\mathbf{q}} \\ \dot{\Omega} \end{bmatrix} = \begin{bmatrix} \dot{\xi} \\ \mathbf{q} \otimes \frac{F_u}{m} \otimes \mathbf{q}^* + F_{ext} \\ \frac{1}{2} \mathbf{q} \otimes \Omega \\ I^{-1}(\tau - \Omega \times I\Omega) \end{bmatrix}$$

Backstepping Control

Introduction

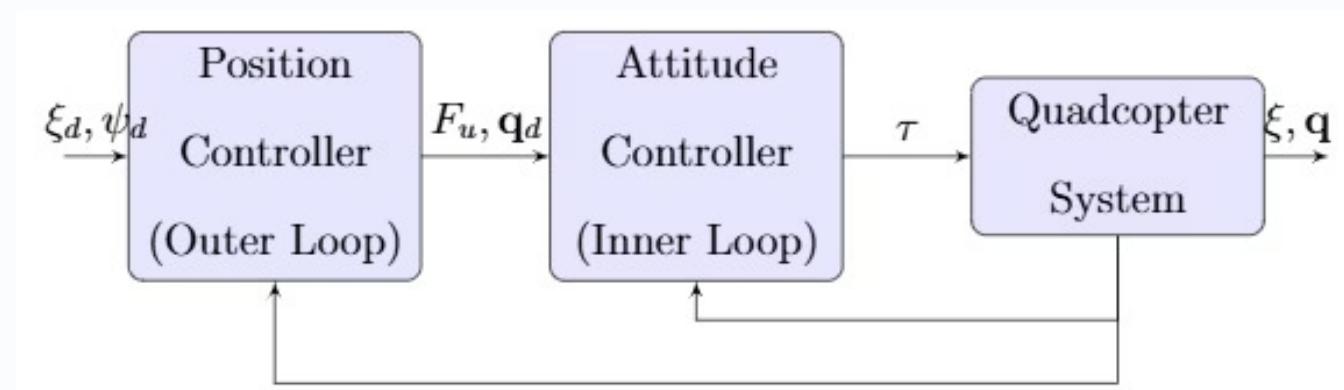
Non-Linear Control Methodology

Effective with 2+ integrator systems

Start with the translational part and follow up with the rotational part

Backstepping Control (cont'd)

Control Flow



Backstepping Control (cont'd)

Translational Part

Tracking error between the agent and the trajectory:

$$\mathbf{e}_{\xi,1} = -[\mathbf{a} * (\xi - \xi_{target}) - \mathbf{d}]$$

We propose:

$$V_1(\mathbf{e}_{\xi,1}) = \frac{\mathbf{e}_{\xi,1}^T \mathbf{e}_{\xi,1}}{2}$$

$$\dot{V}_1(\mathbf{e}_{\xi,1}) = \mathbf{e}_{\xi,1}^T \dot{\mathbf{e}}_{\xi,1} = \mathbf{e}_{\xi,1}^T * [-\mathbf{a}(\dot{\xi} - \dot{\xi}_{target})]$$

$$\dot{\xi}^v = \frac{k_1 \mathbf{e}_{\xi,1}}{a} + \dot{\xi}_{target}$$

$$\mathbf{e}_{\xi,2} = \dot{\xi} - \dot{\xi}^v$$

Our new system

$$\begin{cases} \dot{\mathbf{e}}_{\xi,1} = -\mathbf{a} \cdot \mathbf{e}_{\xi,2} - k_1 \mathbf{e}_{\xi,1} \\ \dot{\mathbf{e}}_{\xi,2} = \mathbf{q} \otimes \frac{F_u}{m} \otimes \mathbf{q}^* + F_{ext} - \left(\frac{k_1 \dot{\mathbf{e}}_{\xi,1}}{a} + \ddot{\xi}_{target} \right) \end{cases}$$

$$V(\mathbf{e}_{\xi,1}, \mathbf{e}_{\xi,2}) = \frac{\mathbf{e}_{\xi,1}^T \mathbf{e}_{\xi,1}}{2} + \frac{\mathbf{e}_{\xi,2}^T \mathbf{e}_{\xi,2}}{2}$$

$$\dot{V}(\mathbf{e}_{\xi,1}, \mathbf{e}_{\xi,2}) = -k_1 \mathbf{e}_{\xi,1}^T \mathbf{e}_{\xi,2} + \mathbf{e}_{\xi,2}^T \cdot [-\mathbf{a} \cdot \mathbf{e}_{\xi,1} + \mathbf{q} \otimes \frac{F_u}{m} \otimes \mathbf{q}^* + F_{ext} - \left(\frac{k_1 \dot{\mathbf{e}}_{\xi,1}}{a} + \ddot{\xi}_{target} \right)]$$

Control input

$$F_u = \mathbf{q}^{-1} \otimes [m \cdot (\mathbf{a} \cdot \mathbf{e}_{\xi,1} - F_{ext} + \left(\frac{k_1 \dot{\mathbf{e}}_{\xi,1}}{a} + \ddot{\xi}_{target} \right) - k_2 \mathbf{e}_{\xi,2})] \otimes \mathbf{q}^{*-1}$$

Backstepping Control (cont'd)

Rotational Part

We propose: $V_1(\mathbf{q}_{\bar{e}}) = \frac{1}{2}\mathbf{q}_e^T \mathbf{q}_e = \frac{1}{2}\mathbf{q}_e^T M(\mathbf{q}_e)\Omega$

$$\begin{aligned}\Omega^v &= -2k_3 M^T \mathbf{q}_e \\ \dot{\Omega}^v &= -2k_3(M^T(\dot{\mathbf{q}}_{\bar{e}})\mathbf{q}_e + M^T\mathbf{q}_e)\end{aligned}$$

we define the error: $\alpha_2 = \Omega - \Omega^v$

we write the new system

$$\begin{cases} \dot{\mathbf{q}}_e = \frac{1}{2}M(\mathbf{q}_{\bar{e}})(\Omega^v + \alpha_2) \\ I\dot{\alpha}_2 = -\Omega \times I\Omega + \tau - I\dot{\Omega}^v \end{cases}$$

We propose

$$\begin{aligned}V(\mathbf{q}_e, \alpha_2) &= \frac{1}{2}\mathbf{q}_e^T \mathbf{q}_e + \frac{1}{2}\alpha_2^T I\alpha_2 = \frac{1}{2}\mathbf{q}_e^T M(\mathbf{q}_{\bar{e}})(\Omega^v + \alpha_2) + \\ &\quad \alpha_2^T(-\Omega \times I\Omega + \tau - I\dot{\Omega}^v)\end{aligned}$$

control input is $\tau = \Omega \times I\Omega + I\dot{\Omega}^v - k_4\alpha_2 - \frac{1}{2}M(\mathbf{q}_{\bar{e}})\mathbf{q}_e^T$

Backstepping Control (cont'd)

New Equivalent System

$$\dot{\eta} = \begin{bmatrix} \dot{\mathbf{e}}_{\xi,1} \\ \dot{\mathbf{e}}_{\xi,2} \\ \dot{\mathbf{q}}_e \\ \dot{\alpha}_2 \end{bmatrix} = \begin{bmatrix} -\mathbf{a} \cdot \mathbf{e}_{\xi,2} - k_1 \mathbf{e}_{\xi,1} \\ \mathbf{q} \otimes \frac{F_u}{m} \otimes \mathbf{q}^* + F_{ext} - \left(\frac{k_1 \dot{\mathbf{e}}_{\xi,1}}{a} + \ddot{\xi}_{target} \right) \\ \frac{1}{2} M(\mathbf{q}_e)(\Omega^v + \alpha_2) \\ I^{-1}(-\Omega \times I\Omega + \tau) - \dot{\Omega}^v \end{bmatrix}$$

Backstepping Control (cont'd)

Final Check on the Stability Analysis

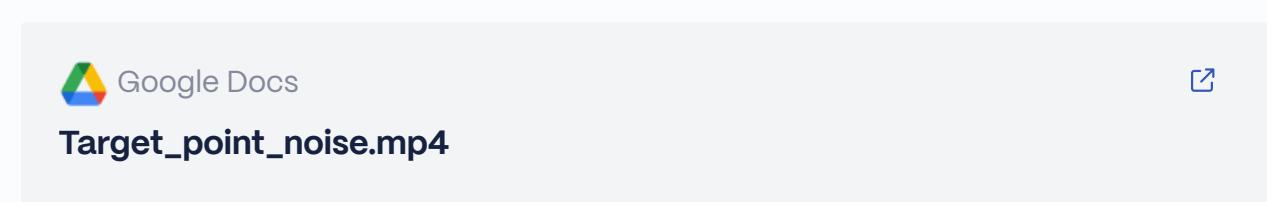
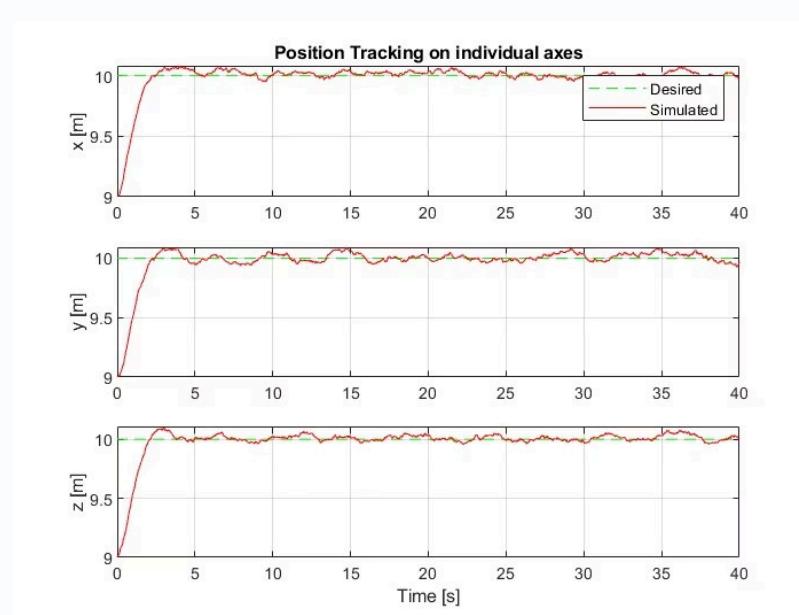
$$\ddot{\xi} \longrightarrow \mathbf{e}_\xi(\xi, m) \longrightarrow \dot{\xi}^v \longrightarrow F_u(u, \mathbf{q}_d)$$

$$\mathbf{q} \longrightarrow \mathbf{q}_e(\mathbf{q}, \mathbf{q}_d) \longrightarrow \Omega^v \longrightarrow \tau$$

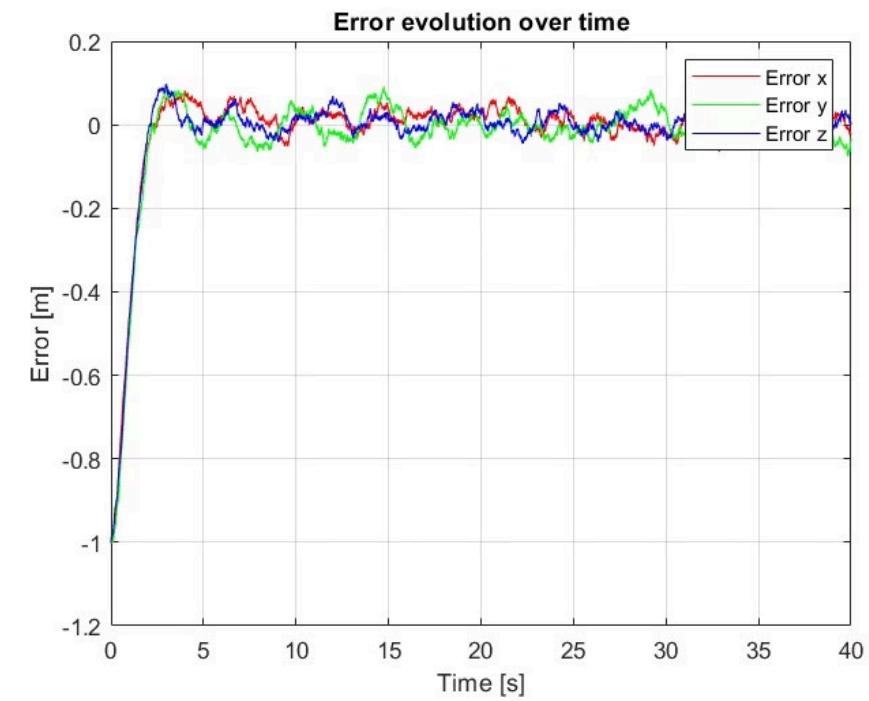
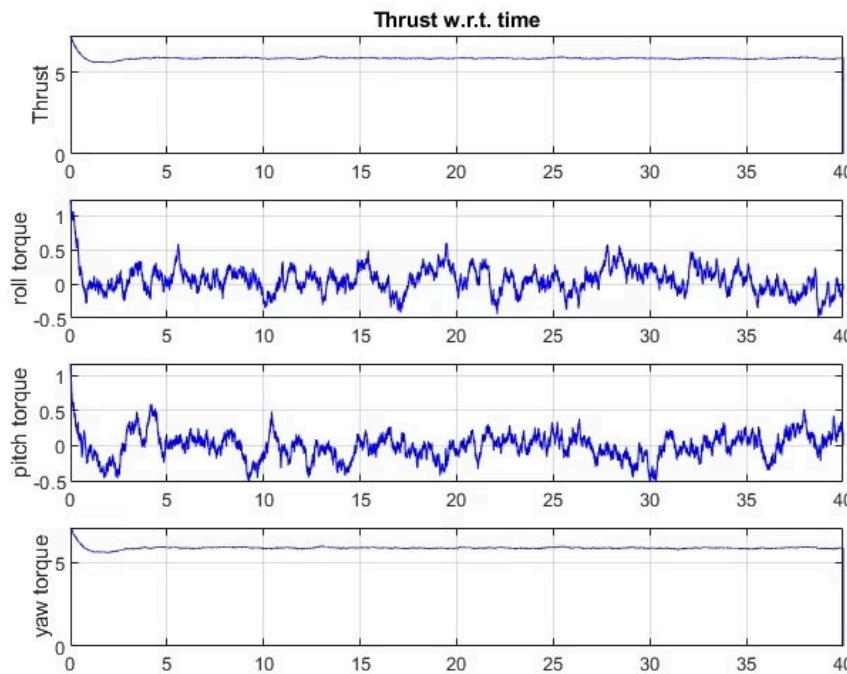
Numerical Simulations

- Constant reference point
- Ascending spiral trajectory
- Lemniscate trajectory in 3D
- Cylinder trajectory

Converging to a fixed desired point



Converging to a fixed desired point (cont'd)

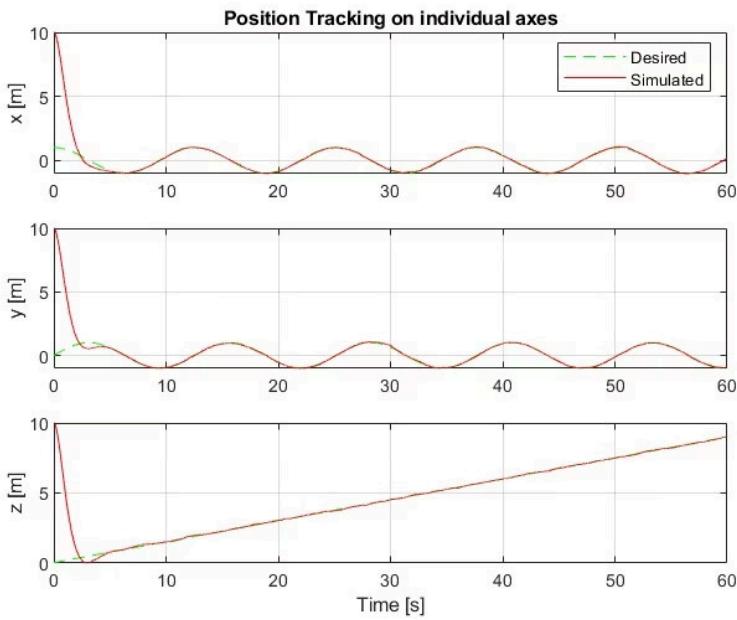


3D Trajectories

Cylindrical Trajectory

$$\mathbf{x}_d(t) = \begin{bmatrix} R \cos(\omega t) \\ R \sin(\omega t) \\ z_0 + v_z t \end{bmatrix}, \quad t \in [0, T]$$

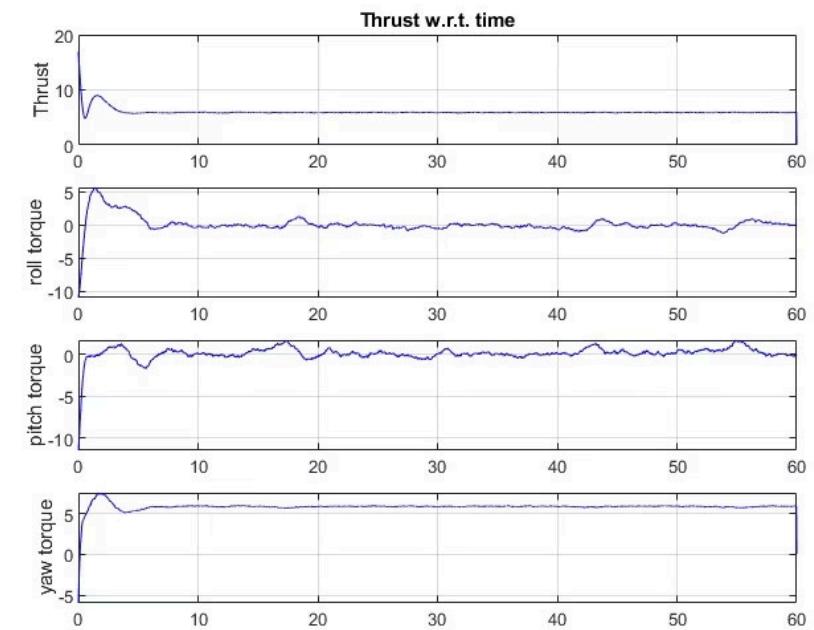
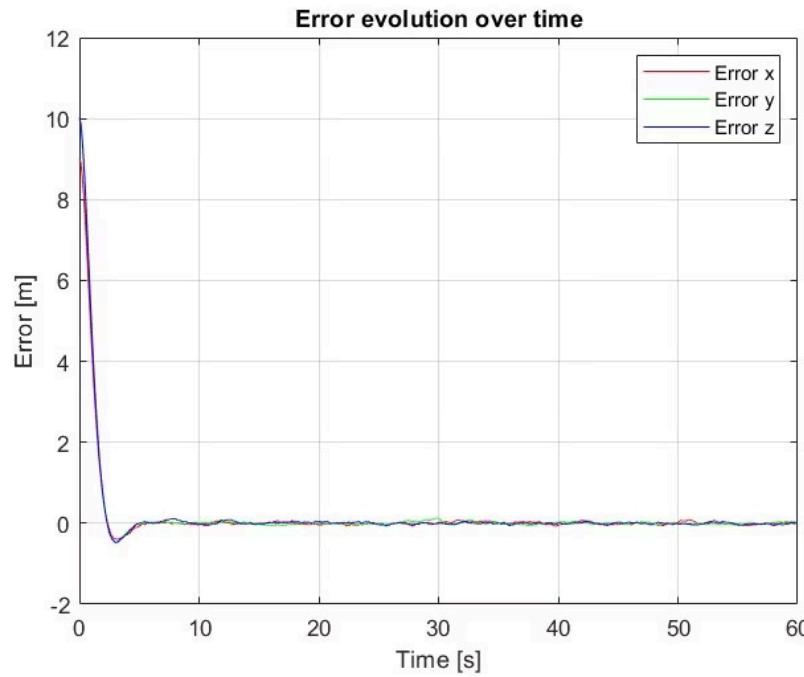
Cylindrical Trajectory (cont'd)



Google Docs
[Quadcopter_Animation.mp4](#)



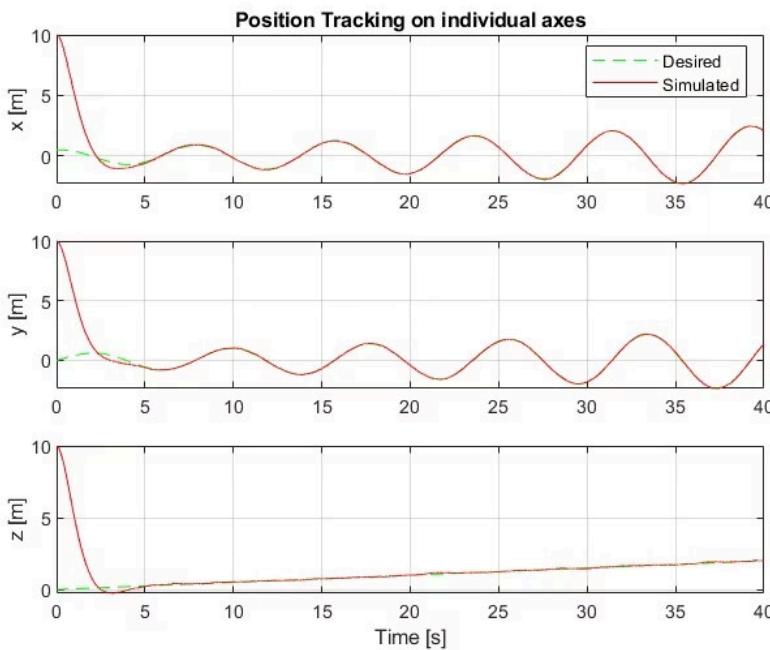
Cylindrical Trajectory (cont'd)



Spiral Trajectory

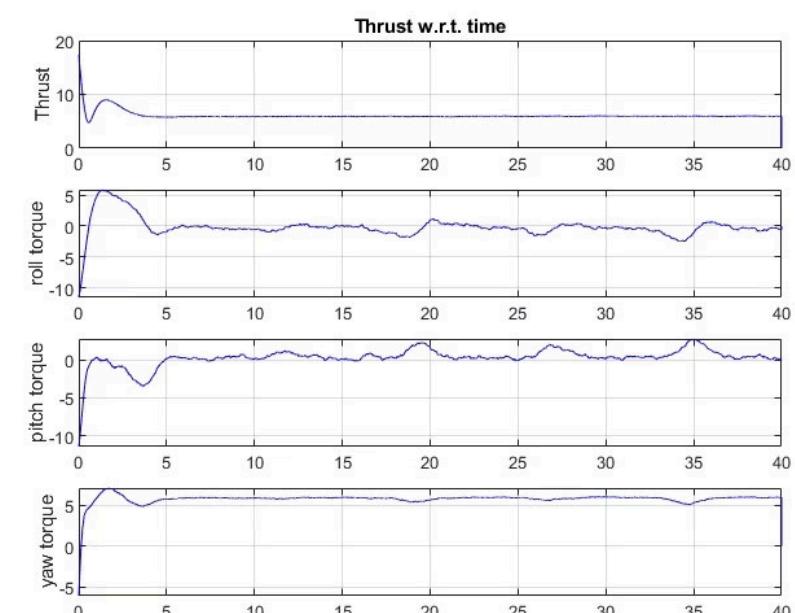
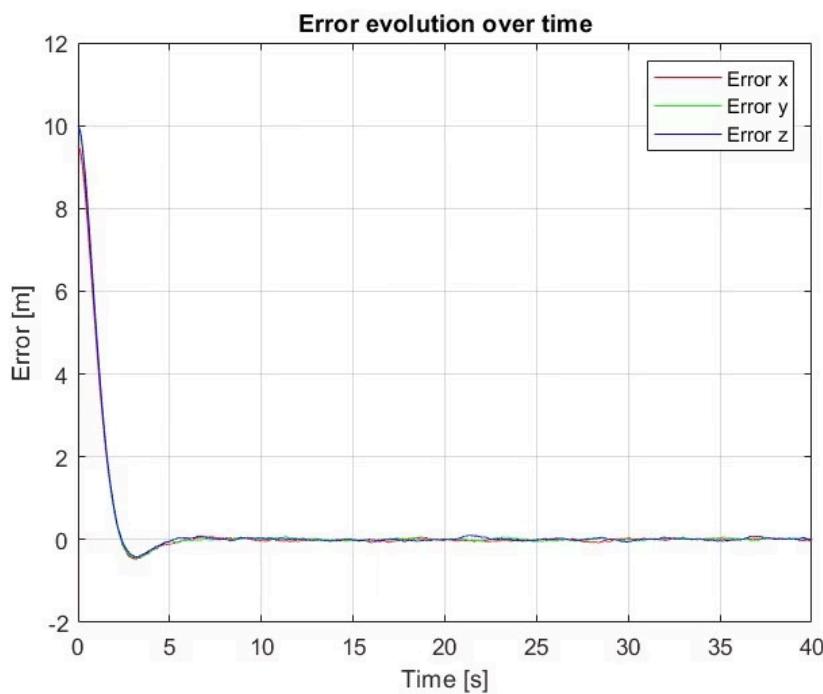
$$\mathbf{x}_d(t) = \begin{bmatrix} (R_0 + v_r t) \cos(\omega t) \\ (R_0 + v_r t) \sin(\omega t) \\ z_0 + v_z t \end{bmatrix}, \quad t \in [0, T]$$

Spiral Trajectory (cont'd)



Google Docs
[Quadcopter_Animation.mp4](#)

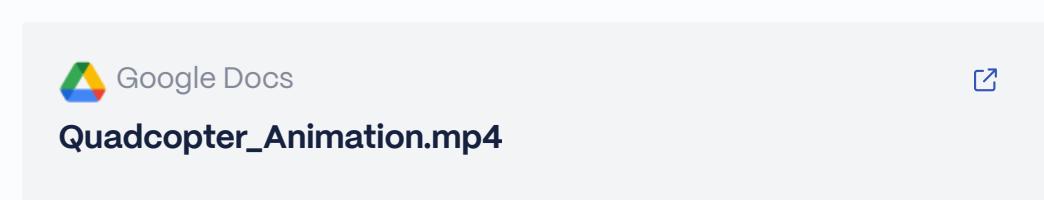
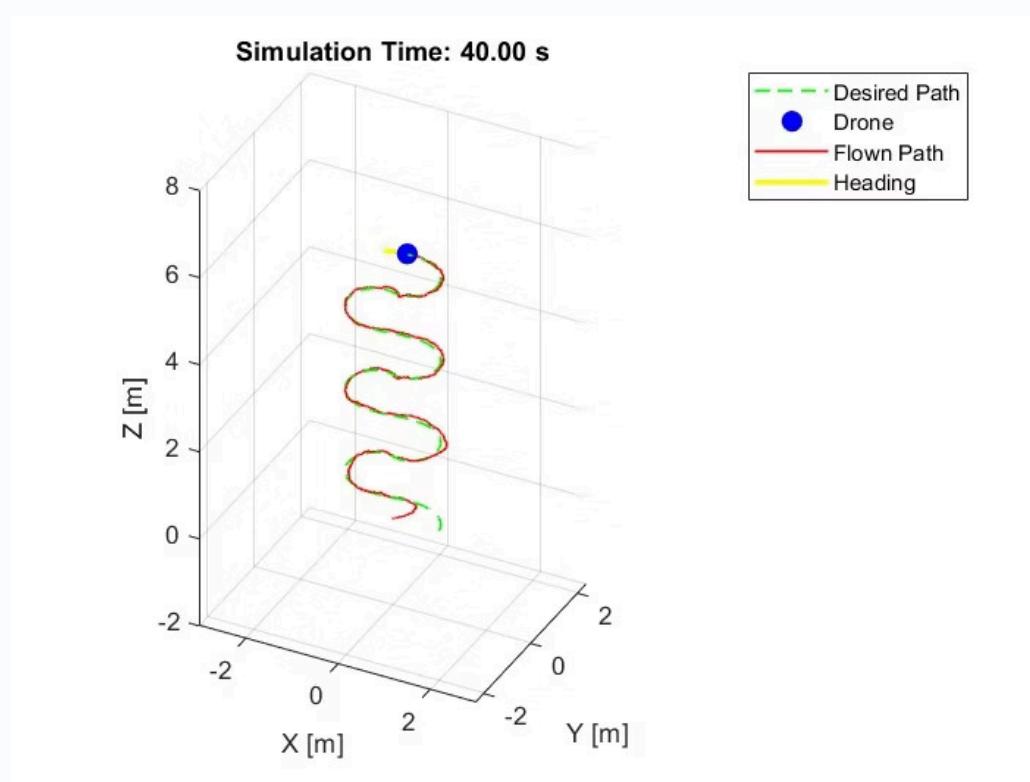
Spiral Trajectory (cont'd)



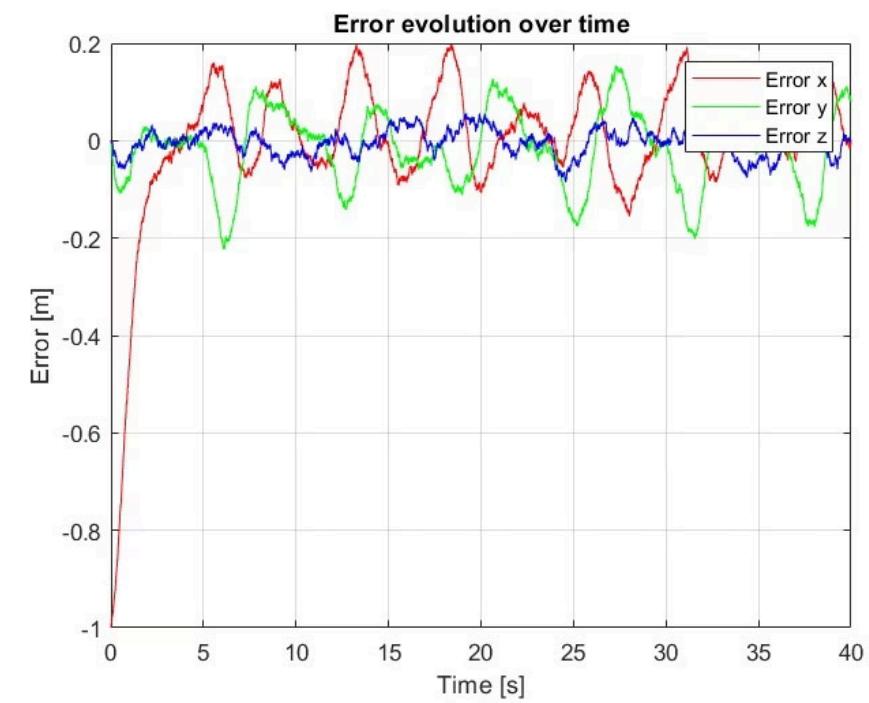
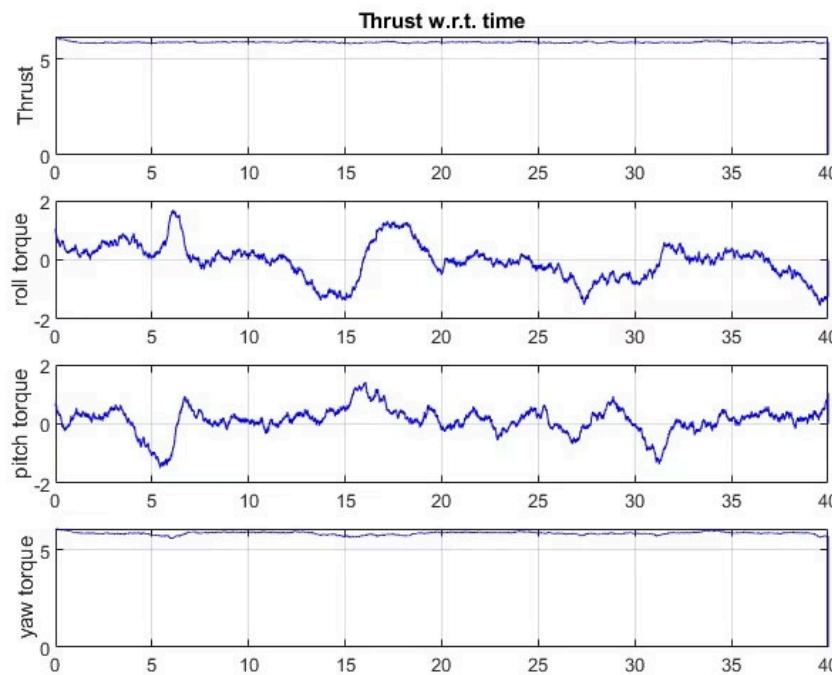
Lemniscate Trajectory

$$\mathbf{x}_d(t) = \begin{bmatrix} A \cos(\omega t) \\ \frac{A \sin^2(\omega t)}{1 + \sin^2(\omega t)} \\ \frac{A \sin(\omega t) \cos(\omega t)}{1 + \sin^2(\omega t)} \\ z_0 + v_z t \end{bmatrix}, \quad t \in [0, T]$$

Lemniscate Trajectory (cont'd)



Lemniscate Trajectory (cont'd)



Multi Robot Coordination

case of 3 robots



Google Docs

[Platooning_Animation.mp4](#)



Discussion

- The results align well with the stability study conducted in the control-theory part.
- The simulation results validate our knowledge about the backstepping control and quadcopter modeling using the quaternion method.

Future Work & Enhancements

- Sensor-Based Control
- Fl-air and ROS implementation
- Hardware choice and integration
- Comparison of backstepping control with other control methods (NL MPC, AI, etc.)

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Contributors

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Issues

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 GitHub

[GitHub – eliascharbelsalameh/Quadcopter_Backstepping_Control](#)

Contribute to eliascharbelsalameh/Quadcopter_Backstepping_Control development by creating an account on GitHub.



Thank You





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