

HW2 - METE

Q1) Increased from $30\text{ cm} \times 10\text{ cm}$ to $32\text{ cm} \times 12\text{ cm}$

$$\text{Original Area } (A_0) = 30 \times 10 = 300 \text{ cm}^2$$

$$\text{Final Area } (A_f) = 32 \times 12 = 384 \text{ cm}^2$$

Percent CW ; $\text{CW}\% = \frac{A_f - A_0}{A_0} \times 100 = 28\%$

From diagrams, for $\text{CW}\% = 28$,

$$\boxed{\text{Yield strength} = 760 \text{ MPa,}}$$

$$\boxed{\text{Ductility} = 11\%}$$

Q2) Strengthening is the relation between dislocation motion and mechanical behavior.

Hardness and strength are related to the ease with which plastic deformation occurs.

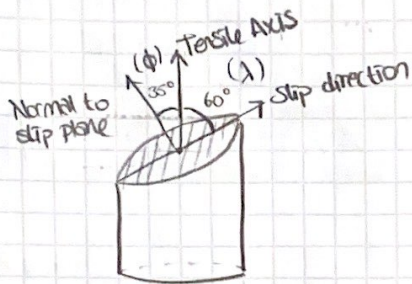
The aim is to reduce dislocation mobility and hence increase the force necessary to cause dislocation motion since the ability of a metal to plastically deform depends on the ability of dislocations to move.

Main strengthening mechanisms:

- ① Grain size reduction: Since atomic disorder at grain boundaries cause a discontinuity in slip planes, grain boundaries are barriers to slip. By reducing grain size, we achieve to increase grain boundary area.
- ② Solid-solution alloying: Adding pinning points that inhibit the motion of dislocation causes the metal to require more stress to continue dislocation motion because of the distortion of lattice and stress generated.
- ③ Precipitation strengthening: Hard precipitates are difficult to shear and precipitates act as pinning sites.

- ④ Odd Work: While simultaneously deforming the metal, we strain harden the metallic material.

Q3)



$$\tau_{\text{crss}} = 6 \text{ MPa}$$

$$\phi = 60^\circ \quad \lambda = 35^\circ \quad \sigma = 11.6 \text{ MPa}$$

$$\tau_R = \sigma \cdot \cos \phi \cdot \cos \lambda$$

$$\tau_R = (11.6) \cdot \overset{0.5}{\cos 60} \cdot \cos 35$$

$$= \boxed{4.75 \text{ MPa}}$$

$4.75 \text{ MPa} < \tau_{\text{crss}} = 6.2 \text{ MPa}$, therefore single crystalline will not yield.

Q4)

Time	Avg diameter
30	$10 \cdot 10^{-6}$
120	$18 \cdot 10^{-6}$

①

$$d^n - d_0^n = K \cdot t$$

$$n \approx 2 \rightarrow d^2 - d_0^2 = K \cdot t$$

$$(10 \mu\text{m})^2 - d_0^2 = 30K$$

$$(18 \mu\text{m})^2 - d_0^2 = 120K$$

$$224 \mu\text{m}^2 = (90 \mu\text{m})K \rightarrow K = \frac{224}{90} \frac{\mu\text{m}^2}{\text{min}}$$

$$100 \mu\text{m}^2 - d_0^2 = (30 \text{ min}) \cdot \left(\frac{224}{90} \frac{\mu\text{m}^2}{\text{min}} \right)$$

$$\boxed{d_0 = 5.0332 \mu\text{m}}$$

(b) $t = 300 \text{ mm}$

$$d^2 - d_0^2 = K \cdot t$$

$$d = \sqrt{K \cdot t + d_0^2}$$

$$d = \sqrt{746667 - 25.3331}$$

$$\boxed{d = 26.8577}$$

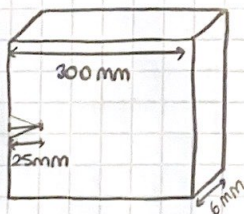
Q5) $K_{Ic} = 101 \text{ MPa}\sqrt{\text{m}}$, $\sigma_y = 890 \text{ MPa}$, $S_{\text{design}} = 510 \text{ MPa}$, $y = 1.0$

(a) Critical crack length, $a_{cc} = \frac{1}{\pi} \left(\frac{K_{Ic}}{y S_{\text{design}}} \right)^2$ (Taken $\pi = 3.14$)

$$a_{cc} = \frac{1}{3.14} \cdot \left(\frac{101 \text{ MPa}\sqrt{\text{m}}}{1.0 \times 510 \text{ MPa}} \right)^2 = 0.01249 \text{ m} = \boxed{12.49 \text{ mm}}$$

(b) $a_{cc} = 12.49 \text{ mm} > 2.7 \text{ mm}$, therefore crack can be detected.

Q6) $K_{Ic} = 85 \text{ MPa}\sqrt{\text{m}}$, $y = 2.1$, $a = 25 \text{ mm}$



(a) $K_{Ic} = y \sigma_c \sqrt{\pi a} \Rightarrow \sigma_c = \frac{K_{Ic}}{y \sqrt{\pi a}} = \frac{85 \text{ MPa}\sqrt{\text{m}}}{2.1 \sqrt{3.14 \cdot 25 \cdot 10^{-3}}} = 144.4657 \text{ MPa}$

$$F = \sigma_c \cdot A = 144.4657 \times 10^6 \times 6 \times 10^{-3} \times 300 \times 10^{-3} = \boxed{260.038 \text{ kN}}$$

(b) $F = \sigma_c \cdot A = (100 \text{ MPa}) \times (300 \times 10^{-3} \times 6 \times 10^{-3}) = \boxed{1.26 \text{ MN}}$

Q7) (Part a is added in the end.)

⑥ Maximum impact energy = 80 J

Minimum impact energy = 5 J

Average = 42.5 J

Ductile-to-brittle transition temperature is approximately -9.75°C .

⑦ Since $-35^{\circ}\text{C} < -9.75^{\circ}\text{C}$, material acts brittle; therefore, it is not suitable for this application. If it would be used, there will be a brittle fracture which would occur without any warnings.

Q8) (Part a is added in the end.)

⑥ Fatigue life N_f for stress amplitude 410 MPa?

Fatigue life 4.95

$\log(N) = 4.95$

$N = 89125 \text{ cycles.}$

⑦ There is no data for 300 MPa; however it is safe to check the material after 5×10^7 cycles.

Q9) $\dot{\epsilon}_s = B \cdot \sigma^n \cdot e^{-\left(\frac{Q}{RT}\right)}$ $T = 540^{\circ}\text{C} = 813 \text{ K}$, $R = 8.315$

Reciprocal temperature $\left(\frac{1}{T}\right) = 1.23 \times 10^{-3} \text{ (K}^{-1}\text{)}$

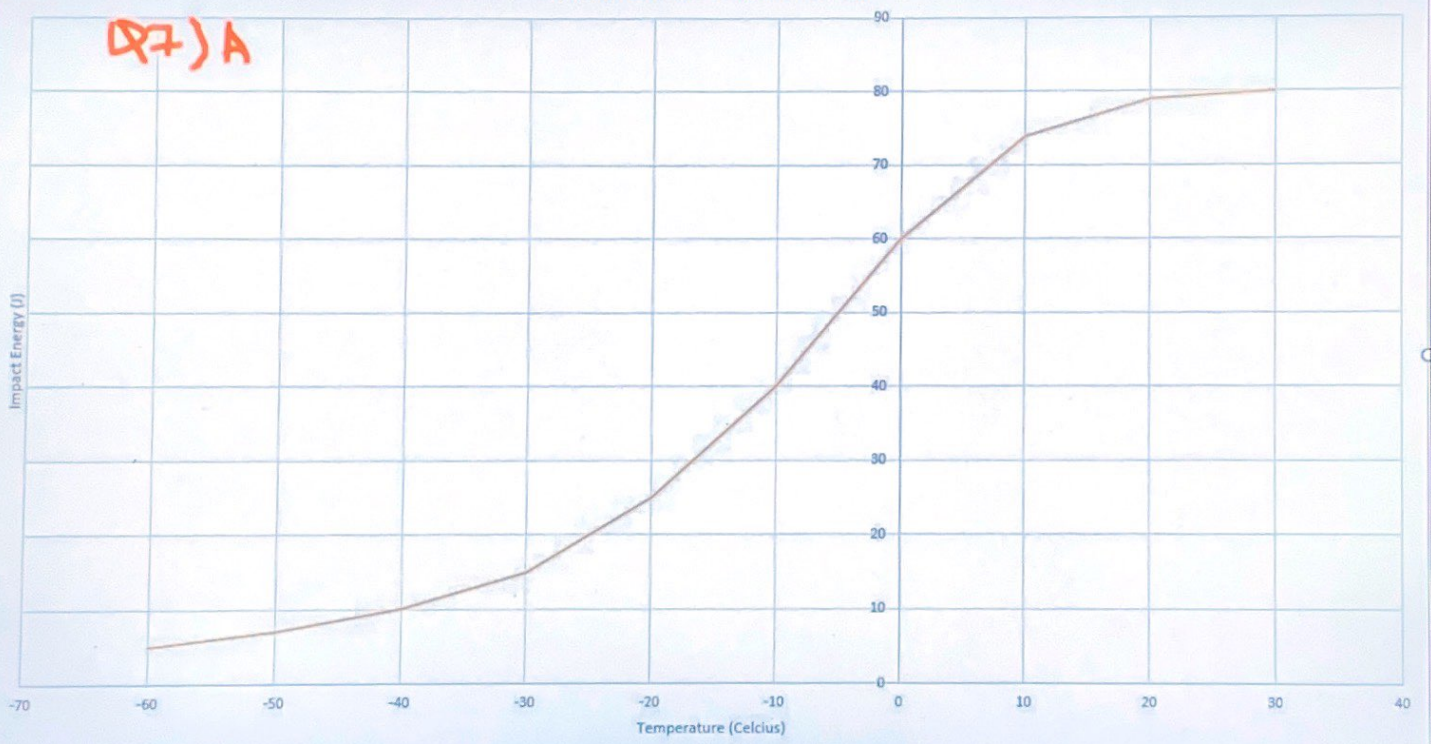
$\sigma = 40 \text{ MPa}$

$\dot{\epsilon}_s = 5 \times 10^{-5} \text{ (hr}^{-1}\text{)}$

$\frac{5 \times 10^{-5}}{3600} \text{ (1/s)} = 1.39 \times 10^{-8} \text{ (1/s)}$

Q7) A

IMPACT ENERGY VS TEMPERATURE



(Q8) A

STRESS VS CYCLES TO FAILURE

