

# **Life cycle impact assessment for a district heating project with seasonal storage**

**A case study analysis for a community project based in Bracht, Rauschenberg,  
Hessen, Germany**

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## **1 Abstract**

A Life Cycle Impact Assessment (LCIA) was conducted for a solar district heating community project in Bracht, Germany, which incorporates solar thermal collectors, a seasonal heat storage unit powered through an included electric heat pump, a supplemental biomass boiler as a backup solution for when there is no heat available from the solar based system, and a transport network to supply residential consumers.

The assessment used standard environmental impact methods to evaluate the system over a 50-year lifetime, based on the energy delivered. Despite supplying the majority of the energy, the solar thermal component with seasonal storage contributed less than 30% to the overall environmental impact. Instead, the biomass backup and electricity sourced from the grid accounted for roughly two-thirds of the total impact, even though they provided only one-third of the energy.

The results are encouraging and show that the Bracht system is environmentally favorable compared to many alternatives. However, substantial potential for improvement through optimization of the system's operating conditions remains. Key opportunities include using renewable electric energy for the heat pump, and reducing heat losses in storage and transport to minimize, or even completely eliminate, the need for supplemental biomass. This is achievable by optimizing settings such as the system's operating temperature.

## **2 Introduction and related work**

Heating is an important topic for energy consumption since it amounts to roughly half of the consumed energy in the EU. Currently, 60% of that energy is generated from fossil fuels [1]. District heating is a setup where one heating generator plant serves many households

connected via pipes. District heating works in two ways: Either to utilise surplus heat from sources such as waste incineration plants for heating purposes in residential areas and service centers [2], or to use a dedicated source of energy, e.g. biomass or solar thermal collectors. There are 6000 existing district heating systems across the EU [1]. Process heating uses a similar setup but is targeted at industrial purposes, which usually require higher heat temperature. Studies like [3] have shown that using a centralized heating component together with heat transport pipes to reach participating consumers has lower environmental impact compared to standalone heating component for each consumers.

Solar thermal collectors (STCs) are devices that absorb solar radiation and convert it into heat. There are different types of solar thermal collectors, including flat plate solar collectors, unglazed water collectors, and evacuated tube solar collectors. They are combined with heat pumps to bridge the gap between solar field produced water temperature and district heating delivery system required temperature [4]. According to [5], there are more than 300 large scale district heating systems globally that are powered with STCs, and more than 1200 STC systems that provide industrial process heat.

Solar thermal collectors are a mature technology. In 2023, the total operational solar thermal capacity reached 560 GWth, which covers roughly 800 km<sup>2</sup> of collector area [5]. STC-provided capacity varies seasonally depending on available sunlight. Sometimes STCs are used only for parts of the year, e.g. to enable turning off a biomass-powered plant in the summer since it would run at extremely low capacity. STCs can be combined with a short term heat storage acting as buffer or a seasonal heat storage tank sometimes referred to as Pit Thermal Energy Storage (PTES) such as an underground hot water basin to store extra heat from the hot season for the cold season. This incurs heat losses. If space restrictions require such a setup (or if land is cheaper), the geographical location of an STC can be remote from consumers and plants via pipelines (e.g., 4 km in Priština [1]). However, there is a trade-off since the remote location required laying the necessary pipes underground.

In scientific literature, a small number of LCIA case studies for district heating systems exist, e.g. for the systems in Milan [6] and Marseille [7]. Life Cycle Impact Assessment, in particular the based on the ReCiPe method, has been used to assess the environmental impact of different STC powered district heating configurations by [8]. The outcome was that larger systems that serve many households have a lower environmental impact per energy unit served. In [9], the authors provide an LCIA study of a STC plant connected to the Geneva district heat network and find that there is no LCI data available for the coupling of large scale solar thermal installations and district heating networks, and provide suggested numbers that could be used to complement district heat production routes.

For the community district heating project in Bracht, the economic viability in comparison to conventional energetic renovation measures has been assessed in a previous study ([10]). However, the environmental impact of the project has not yet been examined in detail. This gap forms the focus of the present study.

### 3 Methodology and research questions

The LCIA was performed using the SimaPro 9.6.0.1 software [11]. The foreground data was collected from various online sources and combined with background data from the Ecoinvent v3 database [12] and the UVEK LCI database version DQRv2:2025 [13]. The environmental impacts were assessed using the mid-point level Environmental Footprint (EF) method [14], and the Ecological Scarcity 2021 (v1.04) method [15] at the single score level with UVEK LCI weighting set.

The research questions were formulated as follows:

1. What is the relevance of the additional electricity required in the setup (amounting to 6% of overall energy consumed) and the supplemental biomass boiler (amounting to 26% of overall energy consumed) with respect to the overall environmental impact? The hypothesis is that the additional electricity and biomass required will amount to a sizable part of the overall environmental impact.
2. How does the STC based system with seasonal heat storage compare to other heating technologies in terms of environmental impact? The comparison will include district heating from other sources that would be available in small communities (such as a heat pump or wood chips), and consumer side heating installations such as oil or gas boilers. The hypothesis is that the STC based system will have a lower environmental impact compared to other district heating setups and to fossil energy based consumer installations.
3. What is the environmental impact contribution of the seasonal heat storage unit in the production, construction, and use stages in the life cycle? A sensitivity analysis will be performed to assess the benefits of the STC based system with a seasonal heat storage component included under several assumed loss coefficients for the storage component and the transport pipes system. The hypothesis is that the seasonal storage component will lower the environmental impact.

The following chapters will cover all the necessary stages of the LCIA: goal and scope definition in Section 4, inventory analysis in Section 5, impact assessment in Section 6, and interpretation in Section 7.

### 4 Goal and scope

The goal and scope definition is a fundamental step in any Life Cycle Impact Assessment (LCIA), as it provides a clear description of the product system under study, its system boundaries, and the definition of a functional unit that reflects the output of the system in a consistent and measurable way.

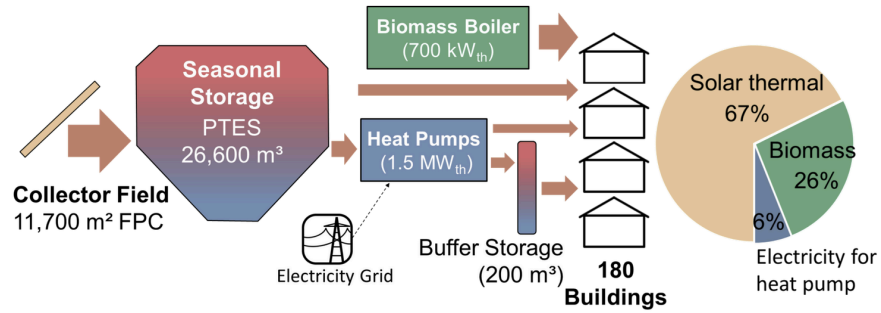


Figure 1: System overview for the Bracht community district heating network. (Source: University of Kassel)

For the present LCIA, the specific goals are to address the research questions outlined in Section 3. The scope of the assessment encompasses a district heating project initiated and operated by a cooperative composed of future household consumers and the local municipal council. As illustrated in Figure 1, the system includes the following key components:

- solar thermal collector (STC) field,
- seasonal storage unit (SSU),
- heat pump (HP) component with heat pump powered by electricity from the grid and a buffer storage unit
- biomass combustion unit serving backup heat when stored heat is unavailable,
- a facility to house the heat pump and the biomass combustion unit,
- heat transport (HT) distribution network that supplies to residential consumers, and
- and receiver units installed in each participating household.

The lifetime of the district heating system is assumed to be 50 years. There are at least 180 consumer households expected, which is roughly 60% of all households that exist in the local community. The plant is currently under construction and on track to be operational for the 2025 winter heating period.

The system diagram shown in Figure 2 describes the product system and its boundaries. The functional unit is defined to be 1 MegaJoule (MJ) of thermal energy provided to the consumer directly at the consumer site during the heating period. Using MJ instead of kilowatt-hours of thermal energy (kWh<sub>th</sub>) ensures consistency with the UVEK processes for other forms of district heating in SimaPro that the comparison will be performed against.



Figure 2: System diagram for the Bracht community district heating network.

## 5 Life Cycle Inventory (LCI)

This section outlines the foundational data used to support system modelling. Extensive project-related information for the Bracht community district heating system is available on the project website [16]. This was used extensively as a key source for detailed LCI data. It provided detailed data on the solar thermal collector field, the seasonal storage unit, and heat preparation systems comprising the heat pump, buffer storage, installation facility, and consumer installations.

The comparison datasets and the heat transport network were modelled based on UVEK LCI data [13], an existing resource for conducting LCIA of energy systems and infrastructure within Switzerland and the broader European context provided by the Swiss Federal Office of Energy (abbreviated in English as SFOE, and in German as UVEK). For electricity input, the modelling assumed the European Network of Transmission System Operators for Electricity (ENTSO-E) production mix, also provided in the UVEK dataset, to ensure the model reflects conditions typical of a plant operating within the European region.

Additional LCI details for all components are provided in Section 9.1. Detailed specifications and parameters of the resulting system model are described in Section 9.2. The remainder of this section outlines the key assumptions regarding component lifetimes, expected electricity demand, and thermal loss coefficients.

### 5.1 Component lifetimes

The planned lifetime for the Bracht plant is 50 years. The assumed individual component lifetimes and the resulting relevant multipliers are shown in Table 1. The assumed individual component lifetimes are in line with the assumptions used in [17].

Table 1

Component	Years	Multiplier	Source
Solar thermal collectors	30	1.67	[18]
Seasonal storage unit	30	1.67	[17]
Heat pumps	20	2.5	[19]
Heat buffer storage	20	2.5	[18]
Heat installation facility	50	1	[20]
Heat exchange stations at consumer	20	2.5	[17]
Heat transport network	50	1	[17]

## 5.2 Electrical power requirements and loss coefficient assumptions

Performance data from [21] provides several estimates of the annual output for the solar thermal collectors used in this project. These estimates vary by geographic location and desired output temperature. The most geographically relevant data point is for Würzburg, with an output of 5.283 kWh per collector per year at a target output temperature of 75 degrees Celsius (°C). Given a total of 855 collectors, the estimated gross thermal energy production is approximately 4.517 MWh per year.

According to the project documentation [22], 2.700 MWh per year are expected to reach end-user households. This implies a total system loss of approximately 40%, accounting for thermal losses in the storage unit and distribution piping.

The energy distribution for heating supply is reported in Figure 1 as follows:

- 67 % from stored solar thermal energy (approximately 2.258 MWh),
- 26 % from biomass sources (approximately 904 MWh), and
- 6 % from the electricity grid (approximately 209 MWh)

Since detailed methods for the loss estimates used in the Bracht assumptions are not provided in the public documentation, the modelling described in this document assumes a 20% loss coefficient as the default for the heat transmission pipe network. The relevant literature and further rationale for the choice are presented in Section 7.3.1. Given this assumption, the implied thermal loss within the seasonal storage unit would be approximately 50% to align with the reported figures from [22]. These assumptions were incorporated into the system model as the default values. More background and a detailed discussion of thermal loss coefficients and their influence on system performance is presented in the sensitivity analysis in Section 7.3.

## 6 Results

The system model, as detailed in Section 9.2, was implemented using SimaPro [11]. This model served as the foundation for generating LCIA results using the Environmental Footprint (EF) method [14] and the Ecological Scarcity 2021 (v1.04) method [15]. The corresponding results derived from these assessments are presented in this section.

To address the first research question regarding the environmental impact of the additional electricity and the supplemental biomass burnt in the wood boiler, the relative influence of the individual components of the solar thermal district heating system on overall environmental impact was evaluated using the Ecological Scarcity 2021 (v1.04) method. The assessment was conducted at the single-score level, applying the UVEK LCI weighting set to define the relative importance of the different damage categories. The results are presented in Figure 3. They show that the biomass (27.3 %) and the electricity (35.8 %) together have a very large impact.



Figure 3: Relative environmental impact for components of Bracht community district heating system (Ecological Scarcity 2021, v1.04, UVEK LCI weighting)

They are responsible for nearly two-thirds of the environmental impact of the overall system. The solar thermal based part of the system with solar thermal field, seasonal storage, and heat pump is responsible for less than 30 % of the overall environmental impact, although they supply two-thirds of the total energy production (see Figure 1). Only one-third of the energy delivered to end consumers originates from the biomass and electricity.

For a more detailed view of the environmental impact by individual damage categories, Figure 4 presents the drilled-down individual results for the most relevant impact categories *Climate change*, *Particulate matter*, *Eutrophication (marine)*, *Land use*, *Resource use (minerals and metals)*, and *Resource use (fossils)*. The figure shows that biomass combustion is the dominant contributor to Land use, Particulate matter, and Marine eutrophication. In contrast, electricity use is the primary driver of impacts in *Fossil resource use* and *Climate change*. The environmental impact in the *Minerals and metals resource use* category is most significantly influenced by heat preparation and the solar thermal collectors. The seasonal storage unit contributes notably to the *Climate change* category.

In summary, electricity and biomass used to operate and supplement the system are the primary contributors to the overall environmental impact. Electricity consumption is unavoidable due to the operation of the heat pump. However, its impact can potentially be mitigated by sourcing electricity from renewable sources instead of the ENTSO-E production mix (as described in Section 5), an option explored in more detail in Section 7.2. Strategies to reduce biomass consumption by improving thermal efficiency, such as lowering heat loss coefficients, are examined in Section 7.3.



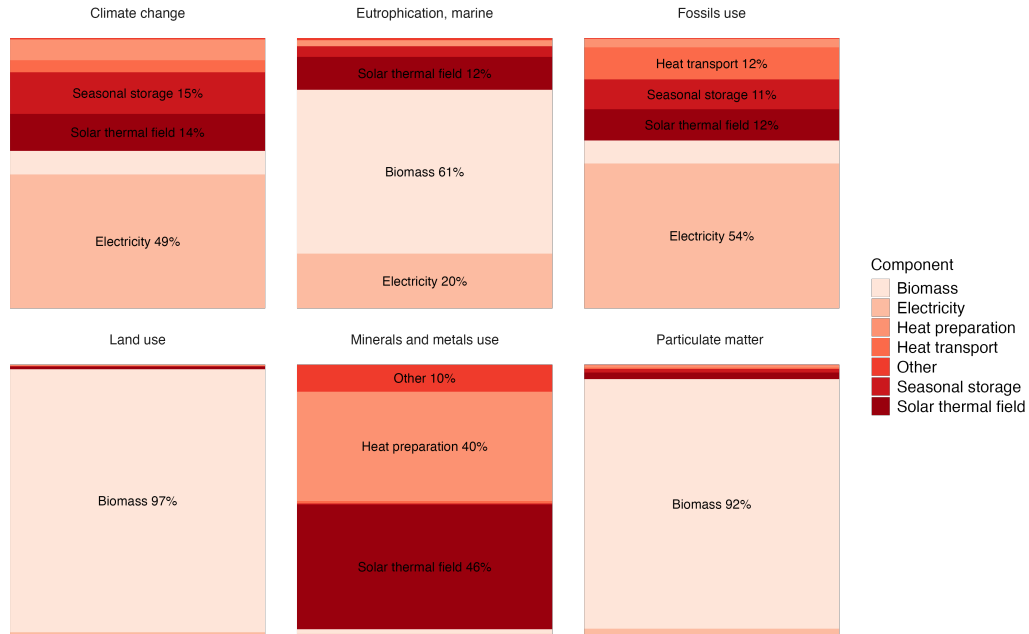


Figure 4: Relative environmental impact of Bracht community district heating network system components (Environmental Footprint Method)

To address the second research question, the environmental impact of heat generated by the solar thermal collector based district heating system with seasonal heat storage was compared to that of other heating technologies. The results, presented in Figure 5, show a comparison of the environmental impacts of STC-based district heating with other district heating (DH) options commonly available in small communities, such as systems powered by wood chips (biomass) or geothermal heat pumps. Additionally, the analysis includes consumer-side heating installations (CI), such as oil and gas boilers. The assessment was conducted using the Ecological Scarcity 2021 (v1.04) method at the single-score level, applying the UVEK LCI weighting set. Results are expressed in environmental impact points (Pt) per kilowatt-hour (kWh) of heat delivered.

The result is that the heat produced by the Bracht plant with 170 Pt per kWh of heat shows the second lowest environmental impact compared to the other heating technologies. The largest contributor is the *Global warming* category, dominantly caused by the electricity required (ENTSO-E production mix as discussed in Section 5) and to a lesser extent by the seasonal storage unit and the solar thermal collectors (cf. Figure 4).

The results indicate that heat produced by the Bracht plant, with an environmental impact of approximately 170 Pt per kilowatt-hour, exhibits the second lowest impact among the heating technologies assessed. The dominant contributor to this impact is the *Global warming* category, primarily driven by electricity consumption, based on the ENTSO-E production

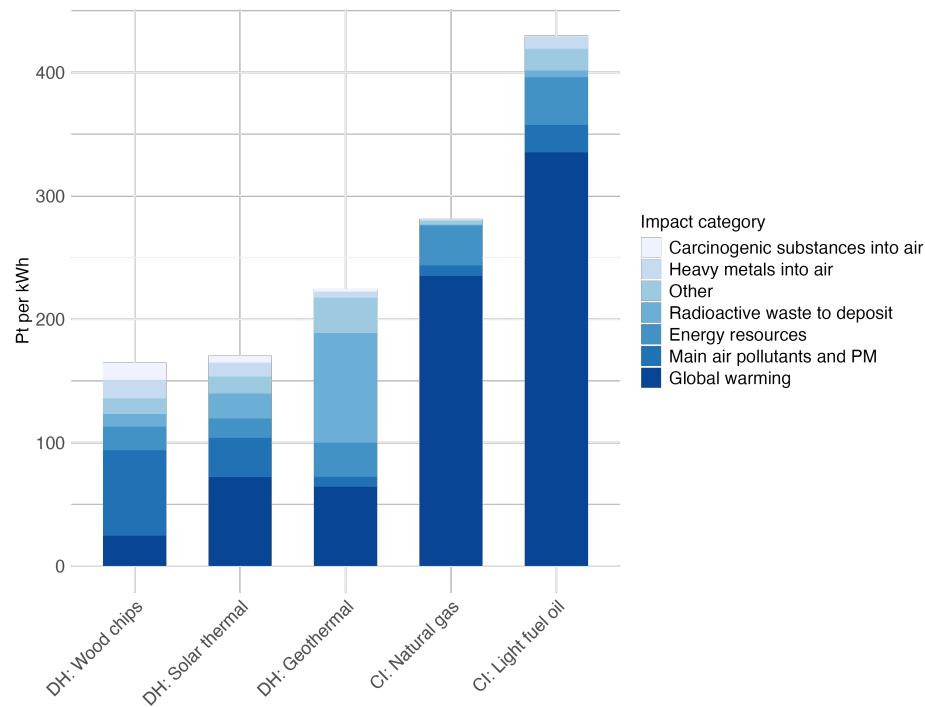


Figure 5: Comparison of environmental impact of Bracht community district heating network to other energy sources for district heating such as wood chips and heat pump, and to consumer installations such as gas and oil burners (Ecological Scarcity 2021 v1.04, UVEK LCI weighting). Results in ascending order: district heating based on wood chips 165 Pt per kWh, as the energy source, Bracht solar thermal based district heating 170 Pt per kWh, district heating based on geothermal heat pump 225 Pt per kWh, gas based consumer installation 281 Pt per kWh, oil based consumer installation 430 Pt per kWh.

mix as detailed in Section 5, and to a lesser extent by the seasonal storage unit and the solar thermal collectors (see Figure 4).

The lowest environmental impact with 165 Pt per kWh of heat is returned for the district heating system based on wood chips as the energy source, even with the impact on main air pollutants and particulate matter (PM) having a significant impact on the overall results for this setup. The district heating system based on a geothermal heat pump as the energy source has the third lowest impact with 225 Pt per kWh of heat, to the largest extent from impact on radioactive waste to deposit. Oil and gas based consumer installations fare worse with 430 Pt and 281 Pt per kWh of heat, dominantly from impact on climate change.

As before, Figure 6 presents the individual results for the most relevant damage categories, comparing them relative to the highest value in each category, which is shown as the longest bar representing 100% relative impact. This analysis confirms the findings from Figure 5, clearly demonstrating that oil and gas boilers have extremely high impacts in the *Climate change* category which is equivalent to Global warming in the Ecological Scarcity method with relative impacts of 100% and 70%, respectively. Additionally, oil and gas boilers exhibit the highest fossil resource use, at 100% and 80%.

A clear trade-off exists because each heating technology performs worst in different impact categories. For example, the district heating network using wood chips shows lower climate change impacts but the highest relative impacts in *Marine eutrophication*, *Land use*, and *Particulate matter* (PM). While PM impact was visible in Figure 5, *Marine eutrophication* and *Land use* impacts were not significant in the single score results. Similarly, solar thermal and geothermal-based district heating systems have the highest relative impacts in Minerals and metals resource use, at 100% and 83%, respectively. These trade-offs imply that selecting a heating technology depends on which environmental impacts are prioritized for a given use case. This highlights the need to weigh and balance different categories manually, or to rely on a single score method if applicable.

## 7 Interpretation and discussion

This chapter discusses the results introduced in Section 6. They revealed that the district heating system based on solar thermal energy and seasonal storage compares favorably to other means of heating. However, in the given modelling, with limitations as documented in Section 7.1, it exhibits higher environmental impact compared to the district heating system based on wood chips as the energy sources. The electricity and the supplemental biomass required were found to be the two top single contributors to the overall results. To understand the saving potential from using lower-emitting (see Section 7.2) or less energy resources (see third research question and Section 7.3), sensitivity analyses for source of electricity and loss coefficients for the heat loss in the seasonal storage unit and the transport pipes will be performed.

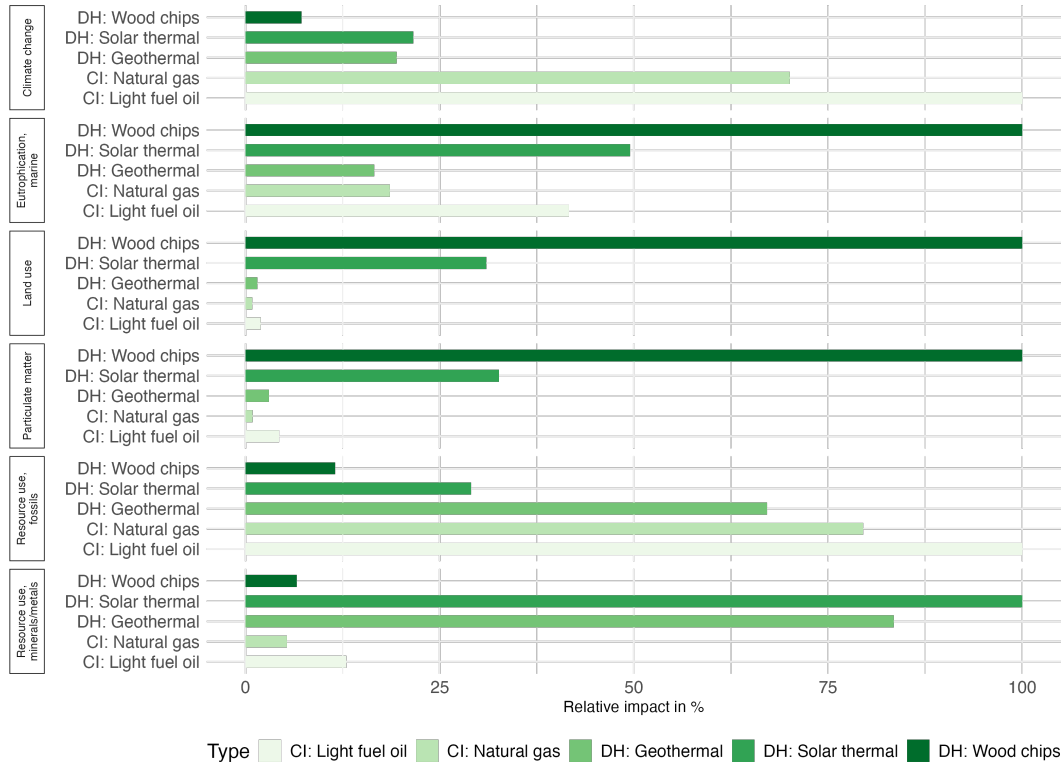


Figure 6: Damage assessment using the Environmental Footprint Method, visualized as relative environmental impacts in comparison.

## 7.1 Modeling limitations

The UVEK data for the other energy sources for district heating (wood chips, heat pump) used an 11 % assumption which means that the solar thermal data with the 20% assumption as mentioned in Section 5.2 is disadvantaged in the comparison in Figure 5. The effect of these assumptions on the results will be investigated in Section 7.3.

Data availability was generally satisfactory with one notable exception for the modelling of the heat pumps used in the system (see Section 9.1.3 for specifications). There are two heat pumps with 630 kW max electrical input power each used in the system, but in the UVEK data, the largest sized heat pump available has a maximum of 50 kW power. The best possible assumption in this situation was that the two large heat pump have the same impact as 25 units of the 50 kW heat pump, but this is likely leading an overestimation of the resource use for minerals and metals. This is acceptable since with 6.1 %, the heat preparation system which includes the heat pump showed only minor impact on the overall results (see Figure 3).

Worth mentioning is that the UVEK data for the transport system district heat has a lifetime assumption of 30 years whereas the Bracht setup assumes 50 years. This is acceptable since with 6.6 %, the heat transport system showed only minor impact on the overall results (see Figure 3).

There was a problem with the weights for the damage category *Water resources, net balance* in the UVEK LCI weighting set that required excluding this category from the analysis.

System deconstruction was modeled for the major infrastructure components, specifically the solar thermal collector field and the seasonal storage unit. The model includes the disposal of plastic materials used for sealing and insulation in the seasonal storage unit, assuming treatment via municipal waste incineration. For the remaining system components only deconstruction processes were included in the model. Final disposal or material recovery for these components was not considered within the scope of this analysis (cf. system diagram in Figure 2).

## 7.2 Sensitivity analysis: Source of electricity

The results as presented in Figure 5 indicate that the dominant environmental impact arises from the electricity demand of the system, which originates from the heat pump. In the default model, the electricity mix was modeled based on the ENTSO-E production mix [13]. This includes a built-in assumption that the electricity production mix will remain constant over the lifetime of the plant. In this section, the effects of the default choice for the modelling as well as potentially achievable savings by using lower-emitting electricity are assessed.

There are two specific aspects of the given use case that need to be considered:

- Electricity consumption primarily occurs during the winter months, when electricity production conditions differ significantly from those in the summer months (e.g., reduced output of photovoltaic systems).
- The plant is assumed to have a lifetime of 50 years, which means it is expected to be decommissioned around 2075. Given the European Union's commitment to achieving net-zero greenhouse gas emissions by 2050, significant changes in the environmental impact of electric energy can be anticipated over the plant's operational period.

To grasp an understanding of the effect of winter conditions on environmental impact of the grid mix, the relevant UVEK-supplied data for operation of storage pumps in winter in several European countries based on energy production technology shares originating from the ENTSO-E Transparency Platform was analysed. Note that these are not directly applicable since the use case is different, but can be used to provide first insights into environmental impact of winter electricity production mix. The relevant data for Germany and Switzerland was used for the analysis. The results show an improvement from 170 Pt per kWh of heat when assuming the ENTSO-E production mix to 166 Pt per kWh of heat for Germany and 145 Pt per kWh of heat for Switzerland based on analysis using the Ecological Scarcity 2021 (v1.04) method. While the exact numbers are not representative, the main insight gathered is that producing winter energy under equal or lower environmental impact than the ENTSO-E production mix is generally feasible.

To assess the impact of future grid decarbonization, it became apparent that no ready-to-use data set is currently available that could be directly applied to the analysis. This is a surprising finding, as such data would be highly relevant for a wide range of assessments, including the one presented in this study. This gap highlights the need for further research and data development to support robust evaluations of future electricity grid scenarios.

- (1) Recherche (Fokus) Vorhersagen Energieperspektiven des BA für Energie (CH) Separate Datensätze machen (Alternative) Europa World Energy Outlook
- (2) Alternative: Statt Ländern die Technologien verwenden (PV nein, Wind, Wasser) Schneller Erneuerbare zusammen gruppieren und andere (Kohle, Kernkraft und Gas) Mehr Interpretation notwendig (da nicht realistisch)

### **7.3 Sensitivity analysis: Loss coefficients**

Heat is harder to transport than electrical power since even good insulation cannot avoid losses of radiating heat. There are two main areas where heat losses occur in the setup: in the pipes, and in the seasonal storage unit. Therefore, the loss coefficients assumed for the pipes and for the storage unit are highly relevant to the modelling. The impact of changes in these loss coefficients assumptions will be assessed in Section 7.3.1 and Section 7.3.2.

### 7.3.1 Pipe heat loss

As summarized in [23], the key parameters affecting heat loss in district heating pipes include the length of the network which depends on the transmission distance relative to demand, the system age, and the operating temperature. The relevant heat loss coefficients reported range between 5 % and 35 %. The Bracht setup involves a relatively long transmission distance of 8800 meters due to its rural context. The planned supply temperature of 85 degrees °C is relatively high and will contribute to increased thermal losses. In contrast, modern district heating systems can operate with lower supply temperatures between 50 and 70 degrees °C to minimize heat loss and improve efficiency as noted by [24].

The rationale behind selecting a default heat loss rate of 20 % for the Bracht setup reflects the combined negative impact of the long transmission distance and high operating temperature on system performance. However, several sources assume lower loss rates. For example, the open source Energy Transition Model [25] suggests a 15 % default loss figure based on real world data for modern district heating networks. The Swiss Federal Office of Energy UVEK assumes an even lower rate of approximately 11 % in its district heating data.

If the Bracht system was optimized to achieve heat loss rates comparable to the UVEK assumption, e.g. by lowering the operating temperature, annual efficiency gains of about 300 MWh could be realized. This would remove one-third of the requirements planned to be supplied via biomass, which would correspond to a 9 % reduction in ecological impact from 170 Pt per kWh to 155 Pt per kWh of heat produced according to the Ecological Scarcity 2021 (v1.04) method at the single score level with UVEK LCI weighting. The most significant reductions can be achieved in the *Main air pollutants and Particulate Matter (PM)* category, primarily due to the reduced combustion of biomass.

### 7.3.2 Seasonal storage unit heat loss

In [26], the authors report a 26% loss of heat production in the storage unit amounted to of heat production. The Energy Transition Model [25] suggests 30% as a sensible default for modelling heat loss in the storage unit. Another study [27] provides a comprehensive review and finds that 30% to 50% heat loss are common for Pit Thermal Energy Storage and that the majority of losses are caused by floating cover.

Given these reference numbers from literature, the 50% loss assumption that was used for the Bracht plant is on the conservative side. For the sensitivity analysis, the assumption made is that it can potentially be lowered to 30% based on two different scenarios: (A) without any changes in the setup but an understanding that the original assumptions were not accurate, and (B) by using twice the cover for the top of seasonal storage unit and therefore better insulation. The sides and the bottom of the seasonal storage unit remain unchanged.

In both scenarios, a significantly higher amount of energy is available from the seasonal storage unit because of the lower heat loss as shown in Table 2. In the original scenario,

out of the 4.517 MWh produced by the solar thermal collectors, an amount of 2.259 MWh remains available from the seasonal storage unit after accounting for assumed losses. When heat losses are reduced, the available energy increases substantially to 3.162 MWh. The difference of 900 MWh is equal in size to the contribution that was expected to be supplied via biomass combustion in the default model. Therefore, the opportunity exists to lower the environmental impact of the system by removing the parts that stem from biomass. These have a significant impact as shown in Section 6.

Table 2

Scenario	Dimension	Value	Assumed loss	Electricity requirements
all	Produced	4.517 MWh	-	
default	Available	2.259 MWh	50%	209 MWh (Factor 0.092)
(A) and (B)	Available	3.162 MWh	30%	293 MWh (Factor 0.092)

However, the higher availability of energy in the seasonal storage unit results in a modified heat supply curve and in heightened electrical energy requirements for the heat pump since it will be used more extensively in the system instead of the biomass boiler. An in-depth analysis of the implications would require additional modelling tools such as [28], which is out of scope for the given work. As a simplification, a rough estimate of the heightened energy requirements was carried based the factor between energy from the seasonal storage unit and energy from electricity from the original assumptions (see Table 2): 209 MWh divided by 2.258 MWh, which returns a 9.2 % electricity requirement factor. Note that this corresponds to a COP of 11 which is indicative for a highly performant system. This was considered plausible, because the initially very high temperature in the seasonal storage unit (85 degrees °C) at begin of the heating periods means that the heat pump will not be required to bridge the temperature gap until the temperature are falling to lower levels. The rough estimate based on the electricity requirement factor as described results in a 293 MWh electricity demand for the heat pump (40 % increase).

Both scenarios were modeled in SimaPro to learn about the implications on environmental impact. The ENTSO-E production mix was assumed. For scenario (*A - update assumptions*), a 15 % reduction from 170 Pt per kWh of heat to 146 Pt per kWh of heat can be achieved. For scenario (*B - double cover*), a 9 % reduction to 155<sup>1</sup> Pt per kWh of heat can be achieved. This confirms the environmental impact savings potential of potential operating conditions improvements.

<sup>1</sup>This is coincidentally the exact same result as already obtained in Section 7.3.1.



## 8 Summary and conclusion

A Life Cycle Impact Assessment was conducted for a solar district heating community project located in Bracht, Rauschenberg, Germany. This project combines solar thermal collectors with a seasonal storage unit to preserve heat produced in summer until the heating period in fall and winter. A heat transport network supplies the thermal energy to 180 residential consumers. The system's energy supply is expected to be 67% from stored solar thermal energy, 26% from biomass, and 6% from the electricity grid. Default modelling assumptions included a 20% heat loss coefficient for the transport network and an implied 50% loss for the seasonal storage unit.

Results indicate that biomass and grid electricity are the primary contributors to the overall environmental impact, accounting for approximately two-thirds of the total, despite supplying only one-third of the energy delivered. The solar thermal collectors contribute less than 15% to the overall environmental impact. Analysis by damage categories shows biomass combustion significantly contributes to land use, particulate matter, and marine eutrophication, while electricity use is the main driver for fossil resource use and climate change.

Comparing the Bracht system to other heating technologies, the STC-based district heating system with seasonal storage shows the second lowest environmental impact at approximately 170 Pt per kilowatt-hour (kWh) of heat, based on analysis using the Ecological Scarcity 2021 (v1.04) method. This is similar to district heating using wood chips (165 Pt/kWh), lower than a geothermal heat pump district heating system (225 Pt/kWh), and significantly lower than gas boilers (281 Pt/kWh) and oil boilers (430 Pt/kWh).

Sensitivity analyses were performed to demonstrate the effects of uncertainties in input data and the potential for reducing environmental impact. The conclusion is that, while the Bracht solar district heating system as planned already compares favorably to many conventional and alternative heating technologies in terms of environmental impact, further improvements to the operating conditions are possible to achieve even lower environmental impact.

Sourcing lower-emitting electricity for the heat pump operation will mitigate the impact driven by the grid mix.

Furthermore, improving heat loss coefficients, particularly reducing the significant heat loss in the seasonal storage unit, could allow the system to meet consumer demand without any combustion of supplemental biomass over the winter heating period. The first step towards achieving this is to use dedicated modelling tools to fully understand the impacts of the different operating conditions on the energy balance to confirm the exploratory analysis carried out in this work.

## 9 Supporting information

This section documents the supporting information related to the life cycle inventory in Section 9.1, the exact data used for process modelling in SimaPro in Section 9.2, and the project organization in Section 9.3.

### 9.1 Life Cycle Inventory

There are several components described in the following sections: solar thermal collector, seasonal storage unit, and heat preparation.

#### 9.1.1 Solar thermal collector (STC)

The relevant data for the solar thermal collector can be found in Table 3.

Table 3

Dimension	Value	Source
Size	11'638 $m^2$ (855 x 13.6 $m^2$ )	[29]
Type	Flat-plate collectors Vitosol 100-F XF13 Viessmann	[29] [30] [21]
Land use	23.500 $m^2$	[29]
Mounting infrastructure material	15 t steel	[16]
Collector weight	50 kg / $m^2$	Own assumption
Production country	China	Own assumption
Transport per container ship	8000 km	Own assumption
Transport per lorry	1000 km	Own assumption

#### 9.1.2 Seasonal storage unit (SSU)

The relevant data for the seasonal storage unit can be found in Table 4. A picture of the floating cover can be found in Figure 7.

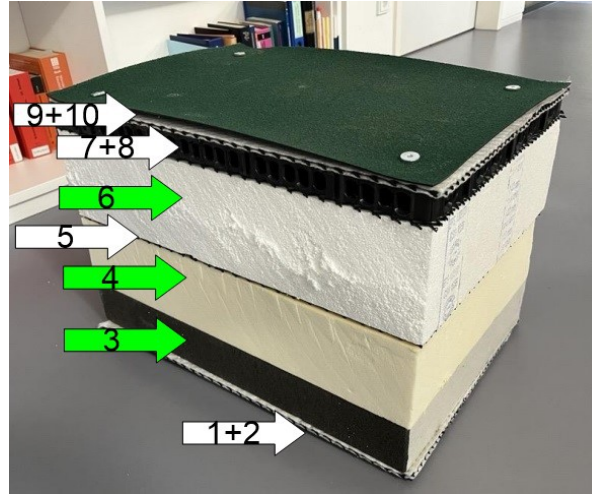


Figure 7: Floating cover profile. Source: Bracht community.

Table 4

Dimension	Value	Source
Volume	$26'600 \text{ m}^3$	Figure 1
Resource: water	$26'600 \text{ m}^3$ filled from local source	[31]
Cover layer 1, 10	Polyethylen (HDPE) sealing membranes 1.5 mm, $1.5 \text{ kg} / \text{m}^2$	[31], estimated weight
Cover layer 2, 9	Fleece ( $0.1 \text{ kg} / \text{m}^2$ ) laminated plastic grid (HDPE, $0.5 \text{ kg} / \text{m}^2$ )	[31], estimated weight
Cover layer 3	Foam glass, $8.33 \text{ kg} / \text{m}^2$	[31]
Cover layer 4	Polyurethane (bauder foam): $3.125 \text{ kg} / \text{m}^2$	[31]
Cover layer 5, 7, 8	Airing gap made of plastic grid, $0.5 \text{ kg} / \text{m}^2$ each	[31], estimated weight
Cover layer 6	Polystyrene (XPS), $3 \text{ kg} / \text{m}^2$	[31]
Floating cover dimensions	$70 \text{ m} \times 70 \text{ m} = 4900 \text{ m}^2$	[32]
Floating cover weight	$2 * (1.5 + 0.1 + 0.5) + 8.33 + 3.125 + 1.5 + 3 = 20.155 \text{ kg} / \text{m}^2$	Calculation
Ground liner	Polyethylen (HDPE), 2.5mm, $2.5 \text{ kg} / \text{m}^2$	[31], estimated weight
Ground liner dimensions	Bottom $20 \text{ m} \times 20 \text{ m}$ , vertical height 15 m, surface area on each of the four sides $5250 \text{ m}^2$	[32]
Ground liner weight	$2.5 \text{ kg} / \text{m}^2$	Assumption
Production country	China	Assumption

Dimension	Value	Source
Transport per container ship	8000 km	Assumption
Transport per lorry	1000 km	Assumption
Required construction process	Excavator 26.600 $m^3$	Figure 1

### 9.1.3 Heat preparation (HP)

The relevant data for the heat preparation unit can be found in Table 5.

Table 5

Dimension	Value	Source
Heat pump	2x Carrier Aquaforce 61XWH-ZE (630 kW max electrical input power)	[29] [33]
Electricity requirements	209 MWh per year	Own calculation, see Section 5.2
Buffer storage	ca. 200 $m^3$ = 200'000 l	Figure 1
Biomass boiler	Mawera boiler with 700 kW thermal power	[29]
Controller	Vitocontrol 200-M	[29] [34]
Heat installation facility	50 $m^2$	Own assumption

## 9.2 SimaPro Data

Table 6 and Table 7 show the parameters and calculated parameters that were defined as helpers for modelling the solar thermal based district heating process in Simapro.

The data for the process *district heat, at consumer, solar thermal, 1MW/MJ/RER U* is kept in an external spreadsheet [accessible here](#).

Table 6

Name	Value	Comment
Plant-size-m2	23500	The total size of the plant in sqm
STC-size-m2	11638	The total size of the STC panels in sqm
STC-weight-per-m2	50	The weight of the STC per sqm
STC-prod-MWh-per-a	2700	Production from the STC per year in MWh

Name	Value	Comment
Lifetime	50	The lifetime of the plant in years
MWhtoMJ	3600	Conversion from MWh to MJ
Mult30To50	1.67	Multiplier for components with 30 years lifetime
Mult20To50	2.5	Multiplier for components with 20 years lifetime
SSU-volume-m3	26600	The volume of the SSU
SSU-top-m2	4900	The size of the SSU at the top (floating cover) in sqm
SSU-side-m2	5250	The size of the SSU at each of the four sides in sqm
SSU-bottom-m2	5400	The size of the SSU at the ground in sqm
Steel-kg	15000	The weight of the required steel for the STC foundation
Freight-ship-dist-km	8000	The transport distance per freight ship in km
Lorry-dist-km	1000	The transport distance per lorry in km

Table 7

Name	Value	Comment
STC-prod-MJ-lifetime	STC-prod-MWh-per-a * Lifetime * MWhtoMJ	The total production from the STC over the plant lifetime in MJ
STC-weight-t-total	(STC-size-m2 * STC-weight-per-m2 * Mult30To50 + Steel-kg) / 1000	The total transport weight of the STC over the plant lifetime in tons
SSU-ground-m2	SSU-bottom-m2 + 4 * SSU-side-m2	The total size of the SSU that is touching the ground on the bottom and sides in sqm

For the comparison, the following SimaPro processes were employed (all of them part of the UVEK dataset):

- *district heat, at consumer, borehole heat pump, 50kW/MJ/CH U*
- *district heat, at consumer, wood chips in industrial furnace, 1MW/MJ/CH U*
- *heat, light fuel oil, at boiler 10kW, average/CH U*
- *heat, natural gas, at boiler condensating modulating, 15kW/CH U*

### 9.3 Project organization

In this section, the time plan and the meeting notes are documented.

### 9.3.1 Time planning

Figure 8 documents the time plan that was followed for this project. The live version can be found [here](#). Access is given upon request.

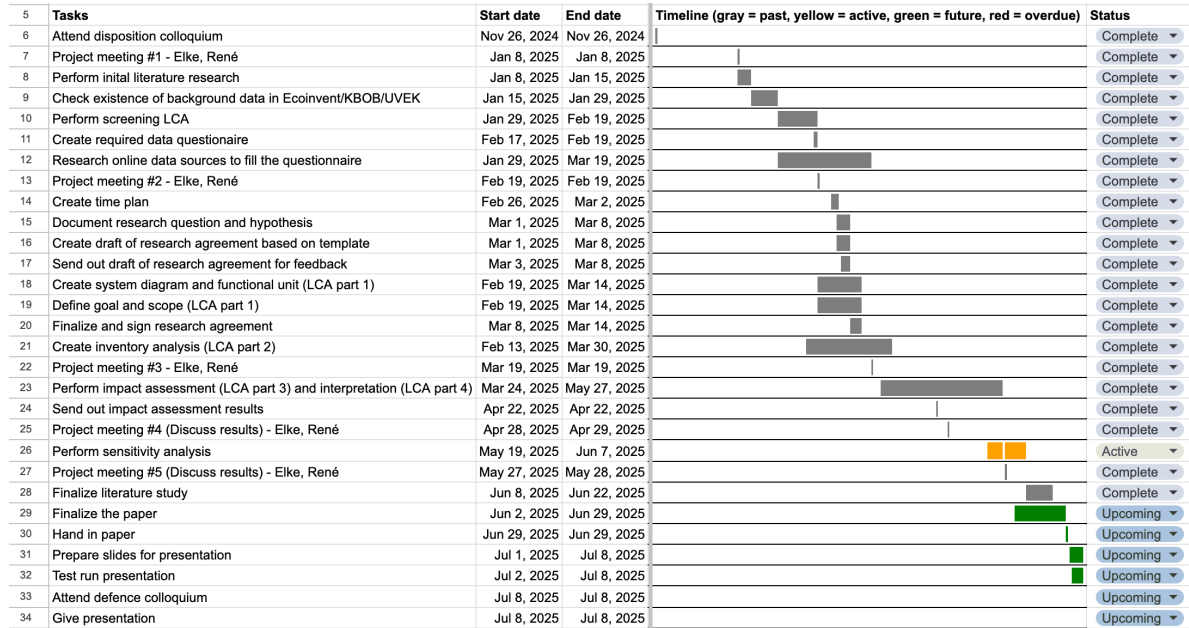


Figure 8: Gantt chart used for time planning.

### 9.3.2 Meeting notes

The notes for the meetings can be found [here](#). Access is given upon request.

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