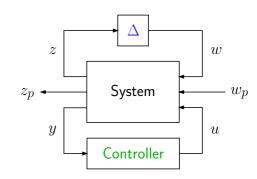
Robust and LPV Control

- Robust controller design
- Parameter Elimination and Dualization
- LPV controller synthesis with multipliers
- An illustrative missile example

Configuration for Robust Controller Synthesis

Design controller guaranteeing:

- robust stability
- robustly desired performance specification on $w_p \to z_p$.



Consider following approach:

- Use robust performance characterization with **multipliers**
- Try to satisfy the multiplier characterization with suitable controller

Just for notational simplicity concentrate on **robust stabilization**. Consider time-varying parametric uncertainty and quadratic stability.



System Descriptions

Uncontrolled LTI part:

$$\dot{x} = Ax + B_1 w + Bu
z = C_1 x + D_1 w + Eu
y = Cx + Fw$$

Controller:

$$\dot{x}_c = A_c x_c + B_c y$$
$$u = C_c x_c + D_c y$$

Controlled LTI part:

$$\dot{\xi} = \mathcal{A}\xi + \mathcal{B}w$$
$$z = \mathcal{C}\xi + \mathcal{D}w$$

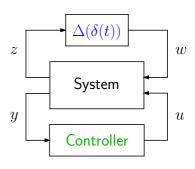
Uncertainty: $w(t) = \Delta(\delta(t))z(t)$.

w: uncertainty input

z: uncertainty output

u: control input

y: measured output



Robust Stability Analysis Inequalities

Assume $\delta(t) \in \delta = \operatorname{co}\{\delta^1, \dots, \delta^N\}$ (polytope) containing zero.

$$\begin{aligned} & \text{Robust stability guaranteed if exist } \mathcal{X} \text{ and } Q, R, S \text{ with} \\ & Q \prec 0, \quad \left(\begin{array}{c} \Delta(\delta^k) \\ I \end{array} \right)^T \left(\begin{array}{c} Q & S \\ S^T & R \end{array} \right) \left(\begin{array}{c} \Delta(\delta^k) \\ I \end{array} \right) \succ 0, \quad k = 1, ..., N \\ & \mathcal{X} \succ 0, \quad \left(\begin{array}{c} I & 0 \\ \frac{\mathcal{X}\mathcal{A} & \mathcal{X}\mathcal{B}}{0} \\ 0 & I \end{array} \right)^T \left(\begin{array}{c} 0 & I & 0 & 0 \\ I & 0 & 0 & 0 \\ \hline 0 & 0 & Q & S \\ 0 & 0 & S^T & R \end{array} \right) \left(\begin{array}{c} I & 0 \\ \frac{\mathcal{X}\mathcal{A} & \mathcal{X}\mathcal{B}}{0} \\ \hline 0 & I \\ \mathcal{C} & \mathcal{D} \end{array} \right) \prec 0. \end{aligned}$$

Apply standard procedure to step from analysis to synthesis.

Robust Synthesis Inequalities

Exists controller guaranteeing robust stability if exist v, Q, R, S:

$$\mathbf{Q} \prec 0, \quad \begin{pmatrix} \Delta(\delta^{k}) \\ I \end{pmatrix}^{T} \begin{pmatrix} \mathbf{Q} & \mathbf{S} \\ \mathbf{S}^{T} & \mathbf{R} \end{pmatrix} \begin{pmatrix} \Delta(\delta^{k}) \\ I \end{pmatrix} \succ 0, \quad k = 1, ..., N$$

$$\mathbf{X}(\mathbf{v}) \succ 0, \quad \begin{pmatrix} I & 0 \\ \mathbf{A}(\mathbf{v}) & \mathbf{B}(\mathbf{v}) \\ 0 & I \\ \mathbf{C}(\mathbf{v}) & \mathbf{D}(\mathbf{v}) \end{pmatrix}^{T} \begin{pmatrix} 0 & I & 0 & 0 \\ I & 0 & 0 & 0 \\ 0 & 0 & \mathbf{Q} & \mathbf{S} \\ 0 & 0 & \mathbf{S}^{T} & \mathbf{R} \end{pmatrix} \begin{pmatrix} I & 0 \\ \mathbf{A}(\mathbf{v}) & \mathbf{B}(\mathbf{v}) \\ 0 & I \\ \mathbf{C}(\mathbf{v}) & \mathbf{D}(\mathbf{v}) \end{pmatrix} \prec 0.$$

Unfortunately **not convex** in all variables v and Q, R, S!

No technique known how to convexify in general!



Dualization Lemma

Suppose that $R \succ 0$ and $Q - S^T R S \prec 0$. Then

$$\left(\begin{array}{c} I \\ W \end{array}\right)^T \left(\begin{array}{c} Q & S \\ S^T & R \end{array}\right) \left(\begin{array}{c} I \\ W \end{array}\right) \prec 0$$

is equivalent to

$$\begin{pmatrix} W^T \\ -I \end{pmatrix}^T \begin{pmatrix} Q & S \\ S^T & R \end{pmatrix}^{-1} \begin{pmatrix} W^T \\ -I \end{pmatrix} \succ 0.$$

Note that
$$\operatorname{im} \left(\begin{array}{c} W^T \\ -I \end{array} \right)$$
 equals orthogonal complement of $\operatorname{im} \left(\begin{array}{c} I \\ W \end{array} \right)$.

In general: Let $P=P^*$ be nonsingular with k negative eigenvalues. If the subspace $\mathcal S$ with dimension k is P-negative then $\mathcal S^\perp$ is P-positive.

Dual Robust Synthesis Inequalities

Exists controller guaranteeing robust stability if exist v, \tilde{Q} , \tilde{R} , \tilde{S} :

$$\tilde{\mathbf{Q}} \succ 0, \quad \begin{pmatrix} -I \\ \Delta(\delta^{k})^{T} \end{pmatrix}^{T} \begin{pmatrix} \tilde{\mathbf{Q}} & \tilde{\mathbf{S}} \\ \tilde{\mathbf{S}}^{T} & \tilde{\mathbf{R}} \end{pmatrix} \begin{pmatrix} -I \\ \Delta(\delta^{k})^{T} \end{pmatrix} \prec 0, \quad k = 1, ..., N$$

$$\mathbf{X}(\mathbf{v}) \succ 0, \quad \begin{pmatrix} \mathbf{A}(\mathbf{v})^{T} & \mathbf{C}(\mathbf{v})^{T} \\ -I & 0 \\ 0 & -I \end{pmatrix}^{T} \begin{pmatrix} 0 & I & 0 & 0 \\ I & 0 & 0 & 0 \\ 0 & 0 & \tilde{\mathbf{Q}} & \tilde{\mathbf{S}} \\ 0 & 0 & \tilde{\mathbf{S}}^{T} & \tilde{\mathbf{R}} \end{pmatrix} \begin{pmatrix} \mathbf{A}(\mathbf{v})^{T} & \mathbf{C}(\mathbf{v})^{T} \\ -I & 0 \\ \overline{\mathbf{B}(\mathbf{v})^{T}} & \mathbf{D}(\mathbf{v})^{T} \\ 0 & -I \end{pmatrix} \succ 0.$$

Note that multipliers are related as
$$\begin{pmatrix} \tilde{Q} & \tilde{S} \\ \tilde{S}^T & \tilde{R} \end{pmatrix} = \begin{pmatrix} Q & S \\ S^T & R \end{pmatrix}^{-1}$$
.

No progress in general. However it helps for state-feedback synthesis

Static State-Feedback Synthesis - Lucky Case!

Recall block substitution:

$$\begin{pmatrix} \mathbf{A}(\mathbf{v}) & \mathbf{B}(\mathbf{v}) \\ \mathbf{C}(\mathbf{v}) & \mathbf{D}(\mathbf{v}) \end{pmatrix} = \begin{pmatrix} A\mathbf{Y} + B\mathbf{M} & B_1 \\ C_1\mathbf{Y} + E\mathbf{M} & D_1 \end{pmatrix}.$$

Last column does not depend on v ...

... dual inequalities are **affine** in all variables ...

... robust state-feedback synthesis possible with LMI's!

Similar results for **robust estimation**! $z \longrightarrow \Delta \longrightarrow w$ Very good exercise. $z_p \longrightarrow z_p \longrightarrow w$

Elimination of Transformed Controller Parameters

Unstructured matrix variables in one LMI can often be eliminated.

For example let us recall the particular structure

$$\begin{pmatrix} \mathbf{A}(\mathbf{v}) & \mathbf{B}(\mathbf{v}) \\ \mathbf{C}(\mathbf{v}) & \mathbf{D}(\mathbf{v}) \end{pmatrix} = \begin{pmatrix} \mathbf{A}\mathbf{Y} & A & B_1 \\ 0 & \mathbf{X}A & \mathbf{X}B_1 \\ \hline C_1\mathbf{Y} & C_1 & D_1 \end{pmatrix} + \\ + \begin{pmatrix} 0 & B \\ I & 0 \\ \hline 0 & E \end{pmatrix} \begin{pmatrix} \mathbf{K} & \mathbf{L} \\ \mathbf{M} & \mathbf{N} \end{pmatrix} \begin{pmatrix} I & 0 & 0 \\ 0 & C & F \end{pmatrix}.$$

Can eliminate
$$\begin{pmatrix} K & L \\ M & N \end{pmatrix}$$
 in synthesis inequalities. How?

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Elimination Lemma

Consider the following quadratic matrix inequality in Z:

$$\begin{pmatrix} I \\ U^T \mathbf{Z} V + W \end{pmatrix}^T \underbrace{\begin{pmatrix} Q & S \\ S^T & R \end{pmatrix}}_{P} \begin{pmatrix} I \\ U^T \mathbf{Z} V + W \end{pmatrix} \prec 0$$

Let U_{\perp} , V_{\perp} be basis matrices of $\ker(U)$, $\ker(V)$.

Suppose that $R \succ 0$ and $Q - S^T R S \prec 0$. Then the quadratic matrix inequality has a solution Z iff

$$V_{\perp}^{T} \begin{pmatrix} I \\ W \end{pmatrix}^{T} P \begin{pmatrix} I \\ W \end{pmatrix} V_{\perp} \prec 0 & & U_{\perp}^{T} \begin{pmatrix} W^{T} \\ -I \end{pmatrix}^{T} P^{-1} \begin{pmatrix} W^{T} \\ -I \end{pmatrix} U_{\perp} \succ 0.$$

Can explicitly construct solution Z if solvability conditions satisfied.

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Application to Quadratic Performance Synthesis

Exists controller that renders A Hurwitz and the QP spec for

$$P_p = \begin{pmatrix} Q_p & S_p \\ S_p^T & R_p \end{pmatrix} \text{ with } R_p \succcurlyeq 0$$

satisfied iff there exists v with

$$\boldsymbol{X}(\boldsymbol{v}) \succ 0, \quad \begin{pmatrix} I & 0 \\ 0 & I \\ \hline \boldsymbol{A}(\boldsymbol{v}) & \boldsymbol{B}(\boldsymbol{v}) \\ \boldsymbol{C}(\boldsymbol{v}) & \boldsymbol{D}(\boldsymbol{v}) \end{pmatrix}^{T} \begin{pmatrix} 0 & 0 & | I & 0 \\ 0 & Q_{p} & 0 & S_{p} \\ \hline I & 0 & 0 & 0 \\ 0 & S_{p}^{T} & 0 & R_{p} \end{pmatrix} \begin{pmatrix} I & 0 \\ 0 & I \\ \hline \boldsymbol{A}(\boldsymbol{v}) & \boldsymbol{B}(\boldsymbol{v}) \\ \boldsymbol{C}(\boldsymbol{v}) & \boldsymbol{D}(\boldsymbol{v}) \end{pmatrix} \prec 0.$$

Suppose P is non-singular and partition $\tilde{P} := P^{-1}$ as P.

Let Φ , Ψ be basis matrices of $\ker \left(\begin{array}{cc} B^T & E^T \end{array} \right)$, $\ker \left(\begin{array}{cc} C & F \end{array} \right)$.

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QP Synthesis Inequalities after Elimination

$$\Psi^{T} \begin{pmatrix} I & 0 \\ 0 & I \\ \hline XA & XB_{1} \\ C_{1} & D_{1} \end{pmatrix}^{T} \begin{pmatrix} 0 & 0 & | I & 0 \\ 0 & Q_{p} & 0 & S_{p} \\ \hline I & 0 & 0 & 0 \\ 0 & S_{p}^{T} & 0 & R_{p} \end{pmatrix} \begin{pmatrix} I & 0 \\ 0 & I \\ \hline XA & XB_{1} \\ C_{1} & D_{1} \end{pmatrix} \Psi \prec 0,$$

$$\Phi^{T} \begin{pmatrix} YA^{T} & YC_{1}^{T} \\ B_{1}^{T} & D_{1}^{T} \\ -I & 0 \\ 0 & -I \end{pmatrix}^{T} \begin{pmatrix} 0 & 0 & | I & 0 \\ 0 & \tilde{Q}_{p} & 0 & \tilde{S}_{p} \\ \hline I & 0 & 0 & 0 \\ 0 & \tilde{S}_{p}^{T} & 0 & \tilde{R}_{p} \end{pmatrix} \begin{pmatrix} YA^{T} & YC_{1}^{T} \\ B_{1}^{T} & D_{1}^{T} \\ -I & 0 \\ 0 & -I \end{pmatrix} \Phi \succ 0.$$

Much fewer variables! Nice system theoretic interpretation!

Alternative Robust Synthesis Inequalities

Synthesis inequalities with non-convex coupling (k = 1, ..., N):

$$\begin{pmatrix} \tilde{Q} & \tilde{S} \\ \tilde{S}^T & \tilde{R} \end{pmatrix} = \begin{pmatrix} Q & S \\ S^T & R \end{pmatrix}^{-1}, \quad \begin{pmatrix} Y & I \\ I & X \end{pmatrix} \succ 0, \quad Q \prec 0, \quad \tilde{R} \succ 0$$

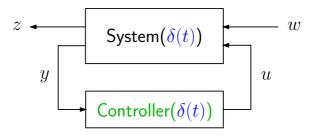
$$[*] \begin{pmatrix} 0 & X & 0 & 0 \\ X & 0 & 0 & 0 \\ \hline 0 & 0 & Q & S \\ 0 & 0 & S^T & R \end{pmatrix} \begin{pmatrix} I & 0 \\ A & B_1 \\ \hline 0 & I \\ C_1 & D_1 \end{pmatrix} \Psi \prec 0, \quad [*] \begin{pmatrix} Q & S \\ S^T & R \end{pmatrix} \begin{pmatrix} \Delta(\delta^k) \\ I \end{pmatrix} \succ 0$$

$$[*] \begin{pmatrix} 0 & Y & 0 & 0 \\ \frac{Y}{0} & 0 & 0 & 0 \\ \hline 0 & 0 & \tilde{Q} & \tilde{S} \\ 0 & 0 & \tilde{S}^T & \tilde{R} \end{pmatrix} \begin{pmatrix} A^T & C_1^T \\ -I & 0 \\ \overline{B}_1^T & D_1^T \\ 0 & -I \end{pmatrix} \Phi \succ 0, \quad [*] \begin{pmatrix} \tilde{Q} & \tilde{S} \\ \tilde{S}^T & \tilde{R} \end{pmatrix} \begin{pmatrix} -I \\ \Delta(\delta^k)^T \end{pmatrix} \prec 0$$

Main Points

- General procedure: Genuine multi-objective synthesis with Youla
- General difficulties in robust controller synthesis
 Illustrated for specific uncertainty/multiplier class
 Show specific information structure and remedy
- Useful Technical Lemmas:
 Linearization, Dualization, Elimination

Gain-Scheduling Control for LPV Systems



Given a parameter-dependent system, design a controller that stabilizes and achieves optimal performance, with the extra advantage (in contrast to a robust controller) that it can take on-line measurements of the parameters as information into account.

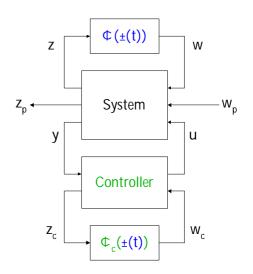
Example application: Gain-scheduling

Configuration for Multiplier LPV Synthesis

Design parameter-dependent controller guaranteeing

- exponential stability
- quadratic performance

If some parameters coincide with state-components procedure leads to nonlinear controller!



Again concentrate on **stability** - no performance channel.

System Descriptions

Uncontrolled LTI part:

$$\dot{x} = Ax + B_1 w + Bu
z = C_1 x + D_1 w + Eu$$

$$y = Cx + Fw$$

w: uncertainty input

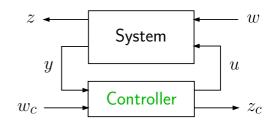
z: uncertainty output

u: control input

y: measured output

Controller LTI part:

$$\dot{x}_c = A_c x_c + B_c \begin{pmatrix} y \\ w_c \end{pmatrix}$$
$$\begin{pmatrix} u \\ z_c \end{pmatrix} = C_c x_c + D_c \begin{pmatrix} y \\ w_c \end{pmatrix}$$



Fundamental Trick to Solve LPV Problem

The interconnection can be seen to result from

$$\begin{pmatrix} \frac{\dot{x}}{z} \\ \frac{z_c}{y} \\ w_c \end{pmatrix} = \begin{pmatrix} A & B_1 & 0 & B_2 & 0 \\ \hline C_1 & D_1 & 0 & D_{12} & 0 \\ 0 & 0 & 0 & 0 & I \\ \hline C_2 & D_{21} & 0 & D_2 & 0 \\ 0 & 0 & I & 0 & 0 \end{pmatrix} \begin{pmatrix} \frac{x}{w} \\ \frac{w_c}{u} \\ z_c \end{pmatrix}$$

controlled with

$$\dot{x}_c = A_c x_c + B_c \begin{pmatrix} y \\ w_c \end{pmatrix}, \quad \begin{pmatrix} u \\ z_c \end{pmatrix} = C_c x_c + D_c \begin{pmatrix} y \\ w_c \end{pmatrix}$$

Can solve the **robust control problem** for this interconnection.

LPV Synthesis: Step I

Synthesis inequalities without non-convex coupling: (k = 1, ..., N):

$$\begin{pmatrix} Y & I \\ I & X \end{pmatrix} \succ 0, \quad Q \prec 0, \quad \tilde{R} \succ 0$$

$$[*] \begin{pmatrix} 0 & X & 0 & 0 \\ X & 0 & 0 & 0 \\ \hline 0 & 0 & Q & S \\ 0 & 0 & S^T & R \end{pmatrix} \begin{pmatrix} I & 0 \\ A & B_1 \\ \hline 0 & I \\ C_1 & D_1 \end{pmatrix} \Psi \prec 0, \quad [*] \begin{pmatrix} Q & S \\ S^T & R \end{pmatrix} \begin{pmatrix} \Delta(\delta^k) \\ I \end{pmatrix} \succ 0$$

$$[*] \begin{pmatrix} 0 & Y & 0 & 0 \\ \frac{Y}{0} & 0 & 0 & 0 \\ \hline 0 & 0 & \tilde{Q} & \tilde{S} \\ 0 & 0 & \tilde{S}^T & \tilde{R} \end{pmatrix} \begin{pmatrix} A^T & C_1^T \\ -I & 0 \\ \overline{B}_1^T & D_1^T \\ 0 & -I \end{pmatrix} \Phi \succ 0, \quad [*] \begin{pmatrix} \tilde{Q} & \tilde{S} \\ \tilde{S}^T & \tilde{R} \end{pmatrix} \begin{pmatrix} -I \\ \Delta(\delta^k)^T \end{pmatrix} \prec 0$$

LPV Synthesis: Step II

Find extension

$$\begin{pmatrix} Q_{e} & S_{e} \\ S_{e}^{T} & R_{e} \end{pmatrix} = \begin{pmatrix} Q & * & S & * \\ * & * & * & * \\ \hline S^{T} & * & R & * \\ * & * & * & * \end{pmatrix} \text{ with inverse } \begin{pmatrix} \tilde{Q} & * & \tilde{S} & * \\ * & * & * & * \\ \hline \tilde{S}^{T} & * & \tilde{R} & * \\ * & * & * & * \end{pmatrix}$$

such that

$$\begin{pmatrix} Q & * \\ * & * \end{pmatrix} \prec 0 \text{ and } \begin{pmatrix} \tilde{R} & * \\ * & * \end{pmatrix} \succ 0.$$

This is always possible.

Size of extension determines size of scheduling function $\Delta_c(.)$.

LPV Synthesis: Step III

Find scheduling function $\Delta_c(\delta)$ such that for all $\delta \in \delta$

$$\left(\begin{array}{c|c}
\Delta(\delta) & 0 \\
0 & \Delta_c(\delta) \\
\hline
I & 0 \\
0 & I
\end{array}\right)^T \left(\begin{array}{c|c}
Q & * & S & * \\
* & * & * & * \\
\hline
S^T & * & R & * \\
* & * & * & *
\end{array}\right) \left(\begin{array}{c|c}
\Delta(\delta) & 0 \\
0 & \Delta_c(\delta) \\
\hline
I & 0 \\
0 & I
\end{array}\right) \succ 0$$

or equivalently

$$\begin{pmatrix}
-I & 0 \\
0 & -I \\
\hline
\Delta(\delta)^T & 0 \\
0 & \Delta_c(\delta)^T
\end{pmatrix}^T \begin{pmatrix}
\tilde{Q} & * & \tilde{S} & * \\
* & * & * & * \\
\hline
\tilde{S}^T & * & \tilde{R} & * \\
* & * & * & *
\end{pmatrix} \begin{pmatrix}
-I & 0 \\
0 & -I \\
\hline
\Delta(\delta)^T & 0 \\
0 & \Delta_c(\delta)^T
\end{pmatrix}
\prec 0.$$

Have explicit formula for $\Delta_c(\delta)$.

LPV Synthesis: Step IV

Design LTI-part of controller

$$\dot{x}_c = A_c x_c + B_c \begin{pmatrix} y \\ w_c \end{pmatrix}, \quad \begin{pmatrix} u \\ z_c \end{pmatrix} = C_c x_c + D_c \begin{pmatrix} y \\ w_c \end{pmatrix}$$

as quadratic performance controller for extended system

$$\begin{pmatrix}
\frac{\dot{x}}{z} \\
z_c \\
y \\
w_c
\end{pmatrix} = \begin{pmatrix}
A & B_1 & 0 & B_2 & 0 \\
\hline
C_1 & D_1 & 0 & D_{12} & 0 \\
0 & 0 & 0 & 0 & I \\
\hline
C_2 & D_{21} & 0 & D_2 & 0 \\
0 & 0 & I & 0 & 0
\end{pmatrix} \begin{pmatrix}
x \\
w \\
w_c \\
u \\
z_c
\end{pmatrix}$$

with performance index $\begin{pmatrix} Q_e & S_e \\ S_e^T & R_e \end{pmatrix}$.

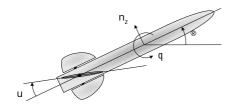
Some Remarks on Sketched Procedure

- Obtained solution of LPV problem with full block scalings.
 Can further enlarge scaling set. Requires behavioral controller [1].
- Comparison to direct implemented version in LMI-toolbox:
 - Allows rational parameter dependence
 - matrices $B(\delta)$, $E(\delta)$, $C(\delta)$, $F(\delta)$ allowed to depend on parameters
 - Care-free scheduling without determination of $\lambda_k(t)$.
- Exists extension to parameter dependent Lyapunov functions.



^[1] C.W. Scherer, LPV control with full block multipliers, Automatica 37 (2001) 361-375.

High-Performance Aircraft System



u: Control input

 α : Measurable parameter

 n_z : Tracked output

Nonlinear system description with aerodynamic effects:

$$\dot{\alpha} = KM \left[\left(a_n \alpha^2 + b_n \alpha + c_n (2 - M/3) \right) \alpha + d_n u \right] + q$$

$$\dot{q} = M^2 \left[\left(a_m \alpha^2 + b_m \alpha - c_m (7 - 8M/3) \right) \alpha + d_m u \right]$$

$$n_z = M^2 \left[\left(a_n \alpha^2 + b_n \alpha + c_n (2 - M/3) \right) \alpha + d_n u \right]$$

Main Idea

Rewrite as linear parameter-varying system

$$\dot{\alpha} = K\delta_1 \left[\left(a_n \delta_2^2 + b_n \delta_2 + c_n (2 - \delta_1/3) \right) \alpha + d_n u \right] + q$$

$$\dot{q} = \delta_1^2 \left[\left(a_m \delta_2^2 + b_m \delta_2 - c_m (7 - 8\delta_1/3) \right) \alpha + d_m u \right]$$

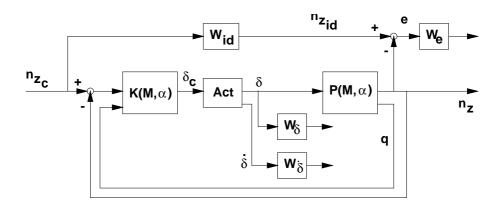
$$n_z = \delta_1^2 \left[\left(a_n \delta_2^2 + b_n \delta_2 + c_n (2 - \delta_1/3) \right) \alpha + d_n u \right]$$

with bounds $2 \le \delta_1(t) \le 4$ and $-20 \le \delta_2(t) \le 20$.

Design good controller scheduled with $\delta_1(t)$, $\delta_2(t)$

 \rightarrow Is good controller for nonlinear system

Interconnection Structure



Model-Matching

Let controlled system approximately act like ideal model $\boldsymbol{W}_{id}.$



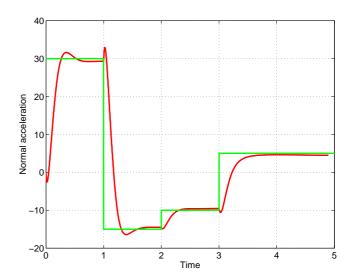
Synthesis with Convex Hull Relaxation

M(t) decreases in 5 seconds from 4 to 2.

Normal acceleration

Reference

Response



Some Book References

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- [5] S. Boyd, L. Vandenberghe, Convex Optimization, Cambridge University Press, Cambridge (2004).
- [6] Manuals for "LMI Control Toolbox" and " μ Analysis and Synthesis Toolbox"
- [7] C.W. Scherer, S. Weiland, DISC Lecture Notes "LMI's in Control".