

# *How does the laser beam travel to the moon ?*

PHY204 - Final Project

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Ecole Polytechnique

- ① Introduction
- ② Theoretical Background
- ③ Numerical Simulation Methods
- ④ Results and Discussion
- ⑤ Conclusion

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# Objective

Investigate how a laser beam propagates from the Earth to the Moon.

- **Goal:** Figure out what parameters are optimal for delivering detectable and useful power to lunar surfaces.
- **Model assumptions:** Clear atmospheric conditions, neglect absorption and scattering, focus only on divergence
- **Challenges:** Extreme distances, beam divergence

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# Theoretical Background

- **Goal:** Understand how a laser beam evolves during propagation.
- **Monochromatic wave:**

$$E(\vec{r}, t) = \mathcal{E}(\vec{r}, t) e^{i(k_0 z - \omega_0 t)}$$

- $\mathcal{E}(\vec{r}, t)$ : slowly varying envelope.
  - $e^{i(k_0 z - \omega_0 t)}$ : rapidly oscillating carrier.
- **Scalar wave equation**

$$\nabla^2 E - \frac{1}{c^2} \frac{\partial^2 E}{\partial t^2} = 0$$

# Theoretical Background

## Assumptions used to simplify the wave equation:

- Envelope varies slowly.
- Beam diverges only slightly —mostly forward-propagating.
- Temporal effects are neglected, we assume a **stationary envelope**.

## Paraxial wave equation

$$\nabla_{\perp}^2 \mathcal{E} + 2ik_0 \frac{\partial \mathcal{E}}{\partial z} = 0$$

- $\nabla_{\perp}^2 \mathcal{E}$ : transverse curvature of the beam.
- $2ik_0 \partial \mathcal{E} / \partial z$ : describes evolution along the propagation axis.

# Gaussian Beam Characteristics (1/2)

## Analytical solution to the paraxial wave equation

$$\mathcal{E}(r, z) = \mathcal{E}_0 \frac{w_0}{w(z)} \exp\left(-\frac{r^2}{w^2(z)}\right) \exp\left(i\frac{k_0 r^2}{2R(z)} - i\zeta(z)\right)$$

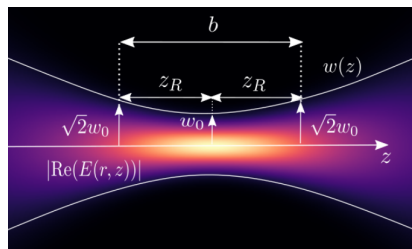
- Models a beam that is:
  - Narrowest at its **waist** ( $w_0$ )
  - Symmetrical in the transverse plane
  - Spreads due to diffraction as it propagates



# Gaussian Beam Characteristics (2/2)

## Key physical parameters:

- $w_0$  – Beam waist  
$$w(z) = w_0 \sqrt{1 + \left(\frac{z}{z_R}\right)^2}$$
- $z_R = \frac{\pi w_0^2}{\lambda}$  – Rayleigh range
- $R(z) = z \left[1 + \left(\frac{z_R}{z}\right)^2\right]$   
Radius of curvature of the phase front
- $\zeta(z) = \tan^{-1} \left(\frac{z}{z_R}\right)$   
Gouy phase shift

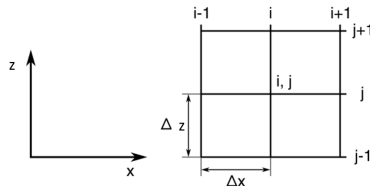


Gaussian Beam.

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# Discretization and moving window

- Divide the computational window in  $\Delta x$  and  $\Delta z$  steps.



*Space discretization.*

- Diffraction over large distances :
  - computational memory waste on empty space
  - reflections at the boundary if the box is too small

## Discretization and moving window

- Change of variable for a fixed size simulation box :  
Transverse component : tracks the beam as it spreads

$$\xi = \frac{x}{w_0} \Rightarrow \frac{\partial}{\partial x} = \frac{1}{w_0} \frac{\partial}{\partial \xi}$$

Longitudinal component : stretches the propagation steps

$$\zeta(z) = \arctan \left( \frac{z}{z_R} \right) \Leftrightarrow z(\zeta) = z_R \tan \zeta$$

- Transformed equation :

$$\frac{\partial C}{\partial \zeta} = \frac{i}{4} \nabla_{\xi}^2 C + i(1 - \xi^2) C$$

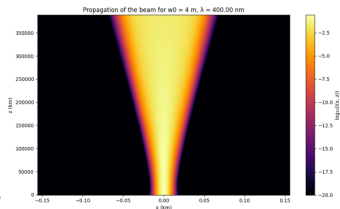
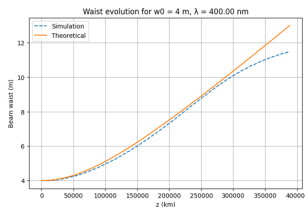
→ artificial potential term : soft restoring force

# Split step FFT

- Outline of the algorithm :

$$\begin{aligned}
 C(\xi, \zeta + \Delta\zeta) &= \mathcal{F}^{-1} \left[ e^{-\frac{i}{4} k_{\xi}^2 \frac{\Delta\zeta}{2}} \mathcal{F}[C(\xi, \zeta)] \right] \quad (1/2 \text{ diffraction}) \\
 &\times e^{i(1-\xi^2)\Delta\zeta} \quad (\text{Full potential step}) \\
 &\times \mathcal{F}^{-1} \left[ e^{-\frac{i}{4} k_{\xi}^2 \frac{\Delta\zeta}{2}} \mathcal{F}[\cdot] \right] \quad (\text{Half-step diffraction})
 \end{aligned}$$

- Preliminary results :



# Crank–Nicolson Matrix Formulation

This scheme can be expressed compactly in matrix form as:

$$AU^{n+1} = BU^n,$$

where  $U^n$  contains discretized field values at step  $n$ , and matrices  $A$  and  $B$  are tridiagonal with elements derived from centered differences. Neumann boundary conditions are enforced at the edges.

## Matrix $A$

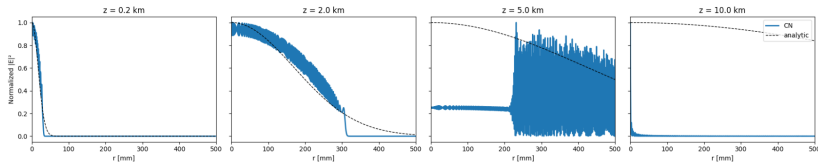
$$\begin{bmatrix} 1+4\sigma & -4\sigma & 0 & \cdots & 0 & 0 \\ -\sigma(1-\frac{1}{2}) & 1+2\sigma & -\sigma(1+\frac{1}{2}) & \cdots & 0 & 0 \\ 0 & -\sigma(1-\frac{1}{3}) & 1+2\sigma & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & -\sigma(1-\frac{1}{2j}) & 1+2\sigma & -\sigma(1+\frac{1}{2j}) \\ 0 & 0 & \cdots & 0 & -4\sigma & 1+4\sigma \end{bmatrix}$$

## Matrix $B$

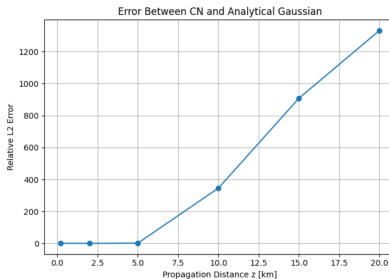
$$\begin{bmatrix} 1-4\sigma & 4\sigma & 0 & \cdots & 0 & 0 \\ \sigma(1-\frac{1}{2}) & 1-2\sigma & \sigma(1+\frac{1}{2}) & \cdots & 0 & 0 \\ 0 & \sigma(1-\frac{1}{3}) & 1-2\sigma & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & \sigma(1-\frac{1}{2j}) & 1-2\sigma & \sigma(1+\frac{1}{2j}) \\ 0 & 0 & \cdots & 0 & 4\sigma & 1-4\sigma \end{bmatrix}$$

# Crank–Nicolson in Physical Space

CN vs Analytical at Selected Distances



*Comparison of CN simulation vs analytic beam profiles at selected distances.*



*Evolution of error of CN method in a physical space model.*

# Crank–Nicolson in Computational Space

- **Coordinate transformation :**

- Transverse normalization :  $\xi = r/w(z)$
- Propagation variable :  $\zeta = \arctan(z/z_R)$

- **Absorption at edges :**

- Absorption mask  $\alpha(\xi) = \exp(-(\xi/\xi_{max})^8)$  applied near boundaries
- Eliminates artificial reflections

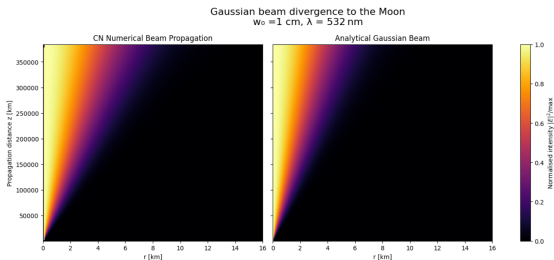
- **Centering :**

- $i(1 - \xi^2)$  is the potential term
- Keeps the beam guided and centered

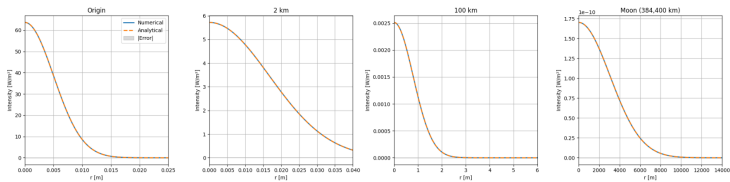


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# Validation of the model



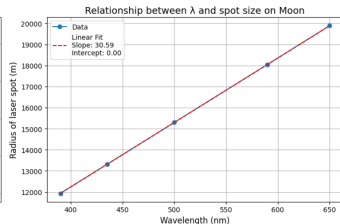
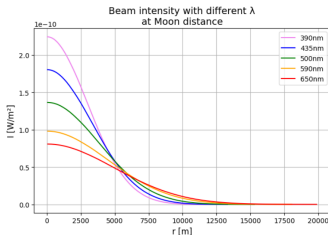
*Left: CN simulation. Right: analytical solution.*



*Radial intensity profiles at selected distances (origin, 2 km, 100 km, Moon).*

# Parameter Effects (1/2)

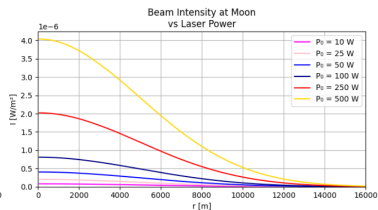
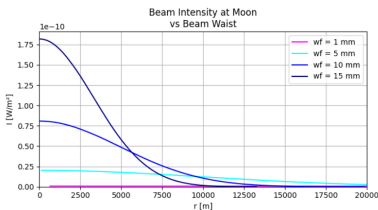
- **Wavelength:** shorter  $\lambda$  result in tighter focusing and less spreading.



*Effects of wavelength on intensity profile and final spot size on the Moon*

## Parameter Effects (2/2)

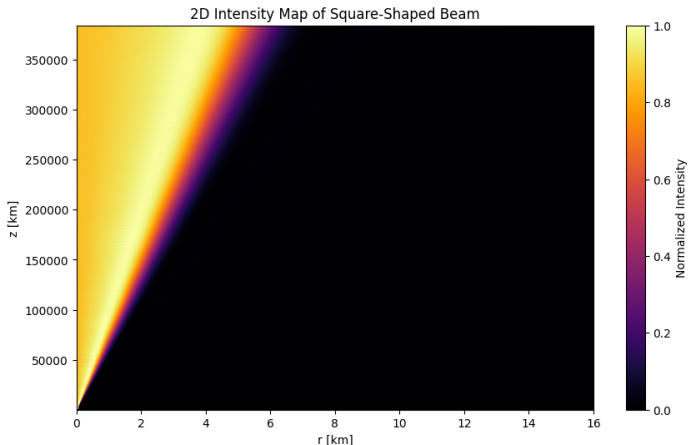
- **Beam waist:** led to stronger confinement of the beam.
- **Power:** scaled linearly the intensity. No effect on beam shape nor on divergence.



Left: effect of beam width on intensity profile at Moon. Right: effect of beam power on intensity profile at Moon

# Square Beam Profile

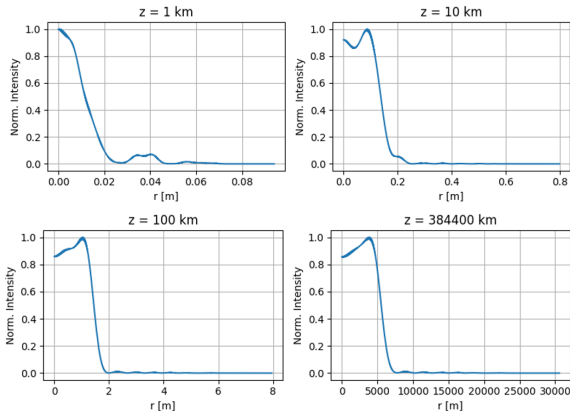
- Sharp edges cause severe diffraction causing "lobes"
- Poor confinement, low efficiency.



*Square shaped beam propagation to the Moon*

# Square Beam Profile

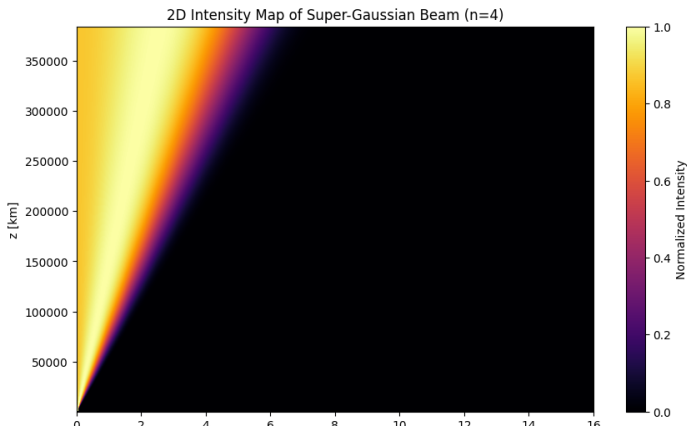
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*Square shaped beam profile propagation to the Moon*

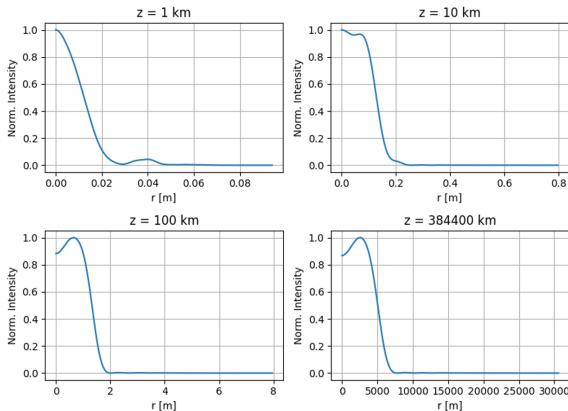
# Super-Gaussian Beams

- Order- $n$  beams: flatter center, sharper edges.
- Orders  $n = 4$  provide optimal spot size at Moon.
- Higher  $n$  increases divergence due to strong edge diffraction.



# Super-Gaussian Beams

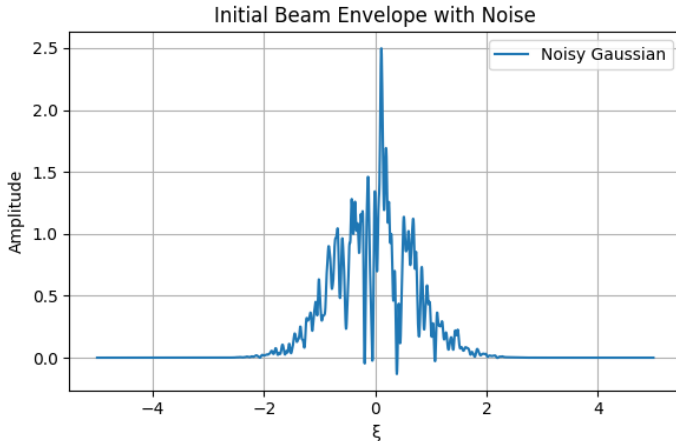
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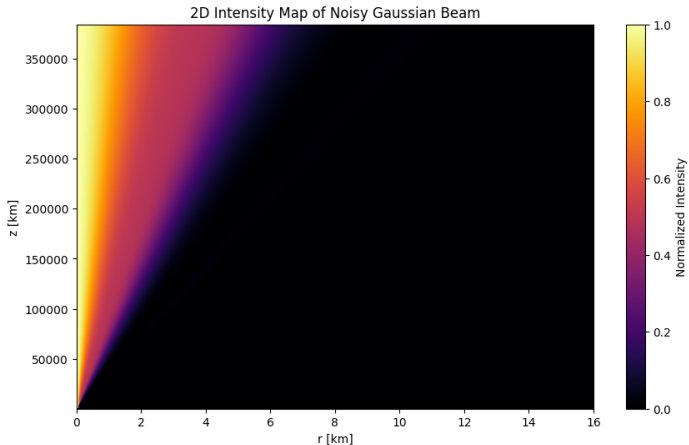
# Noisy Gaussian Propagation

- Initial noise is smoothed by diffraction.
- Approximates real-world atmospheric imperfections.



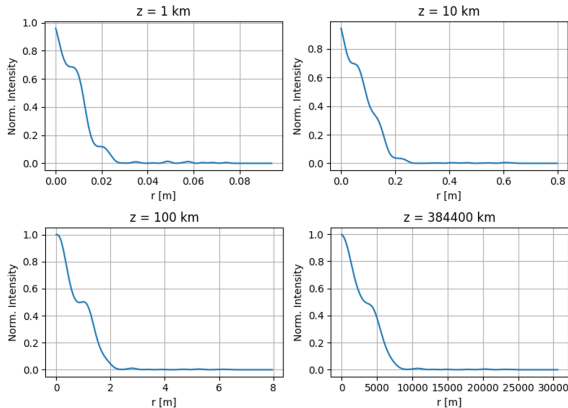
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*Noisy Gaussian beam profile propagation to the Moon*

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# Key Takeaways

- Simulating lunar laser propagation requires adaptive grids.
- Crank-Nicolson in computational space is robust and accurate.
- Key parameters:
  - Super-Gaussian beam (order  $n = 4$ )
  - Shorter wavelength ( $\lambda = 400\text{nm}$ )
  - Larger beam waist (up to 0.5m)
  - Varying power depending on application

# Thank You!

