<sub>1</sub> Eqs

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<sup>3</sup> July 14, 2021

# 4 1 Paper

Eq1

$$CH_4 + 2O_2 \to CO_2 + 2H_2O$$
 (1)

Eq2

$$\begin{split} F_i^{cake} &\geq F_i^{in} \cdot \eta_i^{\mathbf{j}} - \mathbf{M} \cdot (1 - y^j) \\ &\mathbf{i} \in \{P, N\} \\ &j \in \{\text{filtermedia}\} \end{split} \tag{2}$$

Eq3

$$\sum y^{j} = 1 \tag{3}$$

Eq4

$$F_i^{\text{liquid effluen}t} = F_i^{in} - F_i^{\text{cake}} \tag{4}$$

$$F_k^{cake} = F_k^{in}; \ \mathbf{k} \in \{TS, C, K\} \tag{5} \label{eq:5}$$

$$F_{Wa}^{cake} = \left(F_{TS}^{cake} + \sum_{i} F_{i}^{cake}\right) \cdot \frac{C_{Wa}^{cake}}{1 - C_{Wa}^{cake}} \tag{6}$$

Eq7

$$F_{Wa}^{\text{liquid effluent}} = F_{Wa}^{in} - F_{Wa}^{cake} \tag{7}$$

Eq8

$$F\left(\frac{ft^3}{\min}\right) = \frac{F_{in}}{\rho_{digestate}} \tag{8}$$

Eq9

$$n_{\text{filters}} \ge \frac{F_{total}^{filter}}{F_{\text{max}}^{filter}} \tag{9}$$

Eq10

$$F_{design}^{filter}\left(\frac{ft^3}{\min}\right) = \min\left(F_{\max}^{filter}, F_{total}^{filter}\right)$$
 (10)

Eq11

$$FC_{filtration}(\$) = 4.7436 \cdot F_{design}^{filter} + 807.6923 \tag{11}$$

Eq12

$$ChemC_{filtration}\left(\frac{EUR}{year}\right) = \frac{F_{P}^{in} \cdot 3600 \cdot h \cdot d}{\frac{kg_{P}}{kg_{filter\ media}}} \cdot Price_{filter\ media}$$
(12)

Labour cost 
$$\left(\frac{EUR}{year}\right) = \left(61.33 \cdot F_P^{recovered} \cdot 3.6 \cdot h^{(-0.82)}\right) \cdot \left(F_P^{recovered} \cdot 3.6 \cdot h \cdot d\right) \cdot \left(\frac{Salary}{\cdot h \cdot d}\right) \cdot n_{OP}$$

$$\tag{13}$$

Operatingcost 
$$\left(\frac{EUR}{year}\right) = \frac{\text{ChemC} + 1.5 \cdot \text{Labourcost} + 0.3 \cdot FixedCost \cdot f_i \cdot f_j}{(1 - Utilities)}$$
 (14)

Eq15

$$Cost_{cake}\left(\frac{EUR}{year}\right) = \left(F_P^{recovered} \cdot \operatorname{Price}_P + F_N^{recovered} \cdot \operatorname{Price}_N + F_K^{recovered} \cdot \operatorname{Price}_K\right) \cdot 3600 \cdot h \cdot d$$

$$\tag{15}$$

Eq16

Benefits<sub>Filtration</sub> 
$$\left(\frac{EUR}{year}\right) = Cost_{cake} - \text{Operatingcost}$$
 (16)

Eq17

$$F_j^{\text{coagtank}} \ge \frac{F_P^{\text{in}}}{MW_P} \cdot MeP_{ratio} \cdot \frac{MW_j}{C_{Me}} - M \cdot (1 - y^j); \ j \in \{coagulantagents\}$$
 (17)

Eq18

$$\sum \mathbf{y}^j = 1 \tag{18}$$

Eq19

$$F_{j}^{\rm coagtank} = F_{j}^{\rm floctank} = F_{j}^{\rm sedimentator} = F_{j}^{\rm centrifuge} = F_{j}^{\rm cake}; \ j \in \{coagulants\} \eqno(19)$$

Eq20

$$F_i^{in} = F_i^{\text{coagtank}} = F_i^{\text{floctank}} = F_i^{\text{sedimentator}}; \ \mathbf{i} \in \{P, N\}$$

$$F_{i}^{cake} = F_{i}^{centrifuge} = F_{i}^{\text{sedimentator}} \cdot \eta_{i}^{j} \tag{21} \label{eq:21}$$

$$F_i^{\rm sink1} = F_i^{\rm sedimentator} - F_i^{\rm cntrifuge} \tag{22}$$

Eq23

$$F_k^{in} = F_k^{\rm coagtank} = F_k^{\rm floctank} = F_k^{\rm sedimentator} = F_k^{\rm centrifuge} = F_k^{\rm cake}; \ k \in \{TS, C, K\} \eqno(23)$$

Eq24

$$F_{Wa}^{in} = F_{Wa}^{\text{coagtank}} = F_{Wa}^{\text{floctank}} = F_{Wa}^{\text{sedimentator}}$$
 (24)

Eq25

$$\mathbf{F}_{\mathrm{Wa}}^{centrifuge} = \left(\mathbf{F}_{TS}^{centrifuge} + \sum_{i} \mathbf{F}_{i}^{centrifuge} + \sum_{j} \mathbf{F}_{j}^{centrifuge}\right) \cdot \frac{C_{Wa}^{\mathrm{sedimentator}}}{1 - C_{Wa}^{centrifuge}} \tag{25}$$

Eq26

$$F_{Wa}^{sink1} = F_{Wa}^{sedimentator} - F_{Wa}^{centrifuge}$$
 (26)

Eq27

$$\mathbf{F}_{\mathrm{Wa}}^{cake} = \left(\mathbf{F}_{TS}^{cake} + \sum_{i} \mathbf{F}_{i}^{cake} + \sum_{j} \mathbf{F}_{j}^{cake}\right) \cdot \frac{C_{Wa}^{centrifuge}}{1 - C_{Wa}^{centrifuge}} \tag{27}$$

Eq28

$$F_{Wa}^{sink2} = F_{Wa}^{centrifuge} - F_{Wa}^{cake}$$
 (28)

$$V_{\text{Coagtank}}\left(m^{3}\right) = HRT_{\text{Coagtank}} \cdot \frac{F_{digestate}^{in}}{\rho_{digestate}} \tag{29}$$

$$D_{\text{Coagtank}}(m) = \left(\frac{6 \cdot V_{\text{Coagtank}}}{7 \cdot \pi}\right)^{1/3}$$
(30)

Eq31

$$L_{\text{Coagtank}}(m) = 4 \cdot D_{\text{Coagtank}}$$
 (31)

Eq32

$$e_{\text{Coagtank}}(m) = 0.0023 + 0.003 \cdot D_{\text{Coagtank}}$$
(32)

Eq33

$$W_{\text{Coagtank}}(kg) = \rho_{SS316} \cdot \left[ \pi \cdot \left( \left( \frac{D_{\text{Coagtank}}}{2} + e_{\text{Coagtank}} \right)^2 - \left( \frac{D_{\text{Prectank}}}{2} \right)^2 \right) \cdot L_{\text{Coagtank}} + \frac{4}{3} \cdot \pi \cdot \left( \left( \frac{D_{\text{Coagtank}}}{2} + e_{\text{Coagtank}} \right)^3 - \left( \frac{D_{\text{Coagtank}}}{2} \right)^3 \right) \right]$$
(33)

Eq34

$$Cost_{Vessel} = 6839.8 \cdot V_{Coagtank} (m^3)^{0.65}$$
(34)

Eq35

$$P_{agitator}(HP) = V_{Coagtank}(USgallon) \cdot \frac{\kappa_{agitator}}{1000}$$
 (35)

$$Cost_{\text{agitator}1985}(\$) = e^{a+b \cdot \ln(P_{agitator}(HP)) + c \cdot [\ln(P_{agitator}(HP))]^2}$$
(36)

$$Cost_{Coagtank} = Cost_{Vessel} + Cost_{agitator2016}$$
(37)

Eq38

$$A_{clarifier} = \frac{A_{specific} \cdot F_{digestate}^{in} \left(\frac{m^3}{day}\right)}{1000}$$
(38)

Eq39

$$D_{clarifier} = \left(\frac{4 \cdot A_{clarifier}}{\pi}\right)^{1/2} \tag{39}$$

Eq40

$$n_{clarifiers} \ge \frac{D_{total}^{clarifier}}{D_{max}^{clarifier}} \tag{40}$$

Eq41

$$D_{design}^{clarifier} = \min(D_{\max}^{clarifier}, D_{total}^{clarifier}) \tag{41}$$

Eq42

$$D_{design}^{clarifier} = \frac{D_{\max}^{clarifier}}{1 + e^{\left(-F_{digestate}^{in} + 0.342\right) \cdot 2.718}} \tag{42}$$

Eq43

$$Cost_{\text{clarifier}1979} = \left(13060 \cdot D_{design}^{clarifier} - 58763\right) \cdot n_{clarifiers} \tag{43}$$

$$D_{Centrifuge}(in) = 0.3308 \cdot \frac{F_{digestate}^{in}}{1000} \cdot 3600 + 9.5092$$
 (44)

$$n_{centrifuges} \ge \frac{D_{total}^{centrifuge}}{D_{\max}^{centrifuge}}$$
(45)

Eq46

$$D_{design}^{\text{centrifuge}} = \min \left( D_{\max}^{centrifuge}, D_{total}^{centrifuge} \right) \tag{46}$$

Eq47

$$D_{design}^{\text{centrifuge}} = \frac{D_{\text{max}}^{centrifuge}}{1 + e^{\left(-F_{digestate}^{in} + 35.369\right) \cdot 0.0395}}$$
(47)

Eq48

$$Cost_{\text{centrifuge2004}} (\$) = \left(10272 \cdot D_{design}^{\text{centrifuge}} - 24512\right) \cdot n_{centrifuges}$$
 (48)

Eq49

$$FC_{coagulation}\left(\frac{EUR}{year}\right) = \left(Cost_{Coagtank} + Cost_{Floctank} + Cost_{centrifuge2016}\right) \cdot f_i \cdot f_j + Cost_{clarifier2016}$$
(49)

Eq50

$$\operatorname{ChemC}_{coagulation}\left(\frac{EUR}{year}\right) = \left(F_{Fe_{2}(SO_{4})_{3}}^{in} \cdot \operatorname{Price}_{Fe_{2}(SO_{4})_{3}} + F_{Al_{2}(SO_{4})_{3}}^{in} \cdot \operatorname{Price}_{Al_{2}(SO_{4})_{3}} + F_{FeCl_{3}}^{in} \cdot \operatorname{Price}_{FeCl_{3}} + F_{AlCl_{3}(SO_{4})_{3}}^{in} \right)$$

$$(50)$$

$$F_{j}^{in} = F_{TS}^{in} \cdot \frac{\varphi_{j}}{C_{j}} j \in \{\text{precipitationagents}\}$$
 (51)

$$F_j^{in} = F_j^{\text{prectank}} = F_j^{\text{centrifuge}} = F_j^{\text{cake}}$$
 (52)

Eq53

$$F_i^{in} = F_i^{\text{prectank}} = F_i^{\text{centrifuge}} \mathbf{i} \in \{ \mathbf{P}, \mathbf{N} \}$$
 (53)

Eq54

$$F_i^{cake} = F_i^{\text{centrifuge}} \cdot \eta_i \tag{54}$$

Eq55

$$F_i^{\rm liquideffluent} = F_i^{\rm centrifuge} - F_i^{cake} \tag{55}$$

Eq56

$$F_k^{in} = F_k^{\text{prectank}} = F_k^{\text{centrifuge}} = F_k^{\text{cake}} \mathbf{k} \in \{TS, C, K\}$$
 (56)

Eq57

$$F_{Wa}^{in} = F_{Wa}^{\text{prectank}} = F_{Wa}^{\text{centrifuge}} \tag{57}$$

Eq58

$$\mathbf{F}_{\mathrm{Wa}}^{cake} = \left(\mathbf{F}_{TS}^{cake} + \sum_{i} \mathbf{F}_{i}^{cake} + \sum_{j} \mathbf{F}_{j}^{cake}\right) \cdot \frac{C_{Wa}^{centrifuge}}{1 - C_{Wa}^{centrifuge}} \tag{58}$$

$$F_{Wa}^{liquideffluent} = F_{Wa}^{centrifuge} - F_{Wa}^{cake}$$
(59)

$$V_{\text{Prectank}}\left(m^{3}\right) = HRT_{\text{Prectank}} \cdot \left(\frac{F_{digestate}^{in}}{\rho_{digestate}} + \frac{F_{FeCl_{3}}^{in}}{\rho_{FeCl_{3}}}\right)$$
(60)

Eq61

$$FC_{centrifugation} \left( \frac{EUR}{year} \right) = \left( Cost_{centrifuge2016} + Cost_{Prectank} \right) \cdot f_i \cdot f_j \tag{61}$$

Eq62

$$\operatorname{ChemC}_{centrifugation}\left(\frac{EUR}{year}\right) = \left(F_{CaCO_3}^{in} \cdot \operatorname{Price}_{CaCO_3} + F_{FeCl_3}^{in} \cdot \operatorname{Price}_{FeCl_3}\right) \cdot 3600 \cdot h \cdot d \tag{62}$$

Eq63

$$Mg^{2+} + NH_4^+ + H_nPO_4^{3-n} + 6H_2O \Leftrightarrow MgNH_4PO_4 \cdot 6H_2O + nH^+$$
 (63)

Eq64

$$K^{+} + Mg^{2+} + H_{n}PO_{4}^{3-n} + 6H_{2}O \Leftrightarrow KMgPO_{4} \cdot 6H_{2}O + nH^{+}$$
 (64)

Eq64bis

$$\frac{-dC}{dt} = k \left( C - C_{eq} \right) \tag{65}$$

Eq65

$$\ln(C - C_{eq}) = -kt + \ln(C_0 - C_{eq}) \tag{66}$$

$$IAP_{eq} = (Mg^{2+})(NH_4^+)(PO_4^{3-}) = 7.08 \cdot 10^{-14}$$
 (67)

$$u_{\rm mf} = \frac{\text{Re}_{\rm lmf} \cdot \mu_{digestate}}{\rho_{digestate} - d_p} \tag{68}$$

Eq68

$$Re_{lmf} = \sqrt{33.72 + 0.0404 Ar_l (1 - \alpha_{mf})^3} - 33.7$$
 (69)

Eq69

$$Ar_{l} = \rho_{digestate} \left(\rho_{struvite} - \rho_{digestate}\right) g \frac{d_{p}^{3}}{\mu_{digestate}^{2}}$$

$$(70)$$

Eq70

$$u_t = \left(\frac{1.78 \cdot 10^{-2} \cdot \eta^2}{\rho_{digestate} \cdot \mu_{digestate}}\right)^{1/3} d_p \tag{71}$$

Eq71

$$\eta = g \left( \rho_{struvite} - \rho_{digestate} \right) \tag{72}$$

Eq72

$$u_{mf} < u_0 < u_t \tag{73}$$

Eq73

$$u_0 = 5 \cdot u_{mf} \tag{74}$$

$$A_{FBR} = \frac{F_{digestate}^{in}}{u_0} \tag{75}$$

$$D_{FBR} = \sqrt{\frac{4A_{FBR}}{\pi}} \tag{76}$$

**Eq76** 

$$t = \frac{\ln(C_0 - C_{eq}) - \ln(C - C_{eq})}{k}$$
 (77)

Eq77

$$L_{bed} = \frac{u_0}{t} \tag{78}$$

Eq78

$$L_{FBR} = 1.15 \cdot L_{bed} \tag{79}$$

Eq79

$$D_{\text{hydrocyclone}}\left(\text{in}\right) = F_{digestate}^{in} \left(\frac{\text{USgallon}}{\text{min}}\right) \cdot \frac{20}{1000}$$
(80)

Eq80

$$n_{\text{hydrocyclon}e} \ge \frac{D_{total}^{\text{hydrocyclon}e}}{D_{\text{max}}^{\text{hydrocyclon}e}}$$
(81)

Eq81

$$D_{design}^{\rm hydrocyclone} = \min(D_{total}^{\rm hydrocyclone}, D_{\rm max}^{\rm hydrocyclone}) \tag{82}$$

$$Cost_{\text{hydrocyclone}2014} = n_{\text{hydrocyclone}} \cdot \left(2953.2 \cdot D_{design}^{\text{hydrocyclone}} - 34131\right) \tag{83}$$

$$Cost_{dryer2007}(\$) = 1.15 \cdot \left(6477.1 \cdot \frac{F_{water}^{in}}{e_{capacity}} + 102394\right)$$
 (84)

Eq84

$$FC_{struvite}\left(\frac{EUR}{year}\right) = \left(\sum Cost_{\text{equipment}}\right) \cdot f_i \cdot f_j \tag{85}$$

Eq85

$$Cost_{struvite} \left( \frac{EUR}{year} \right) = \left( F_{struvite}^{recovered} \cdot \text{Price}_{struvite} \right) \cdot 3600 \cdot h \cdot d \tag{86}$$

Eq86

Operatingcost 
$$\left(\frac{EUR}{year}\right) = 20521 \cdot F_{design} \left(\frac{ft^3}{\min}\right) - 33488 \cdot a_{Filter}$$
 (87)

Eq87

$$a_{\text{Filter}} = \frac{1}{1 + e^{(-F_{design} + 0.049) \cdot 361}}$$
(88)

Eq88

$$Operatingcost\left(\frac{EUR}{year}\right) = 1019589.91 \cdot F_{digestate}^{in}\left(\frac{kg}{s}\right) - 368838.56 \cdot a_{Coag}$$
(89)

Eq89

$$a_{\text{Coag}} = \frac{1}{1 + e^{\left(-F_{digestate}^{in} + 0.068\right) \cdot 863}}$$
(90)

Operatingcost 
$$\left(\frac{EUR}{year}\right) = 458498.29 \cdot F_{digestate}^{in} + 24924.67 \cdot a_{Centrifugation}$$
 (91)

$$a_{\text{Centrifugation}} = \frac{1}{1 + e^{\left(-F_{digestate}^{in} + 0.068\right) \cdot 863}}$$
(92)

Eq92

OperatingCost<sub>FBR</sub> 
$$\left(\frac{EUR}{year}\right) = 245008 \cdot F_{digestate}^{in} + 1 \cdot 10^6 \cdot a_{FBR}$$
 (93)

Eq93

$$a_{FBR} = \frac{1}{1 + e^{\left(-F_{digestate}^{in} + 0.06785\right) \cdot 862.9679}}$$
(94)

Eq94

$$Operatingcost_{CSTR} \left( \frac{EUR}{year} \right) = 277051 \cdot F_{digestate}^{in} + 1 \cdot 10^6 \cdot a_{CSTR}$$
 (95)

Eq95

$$a_{CSTR} = \frac{1}{1 + e^{\left(-F_{digestate}^{in} + 0.06785\right) \cdot 862.9679}}$$
(96)

Eq96

$$\operatorname{Price}\left(\frac{EUR}{year}\right) = \left(F_P^{\text{recovered}} \cdot \operatorname{Price}_P + F_N^{\text{recovered}} \cdot \operatorname{Price}_N + F_K^{\text{recovered}} \cdot \operatorname{Price}_K\right) \cdot \frac{1}{F_{total}^{\text{recovered}}} \cdot 3600 \cdot h \cdot d$$

$$(97)$$

Eq97

$$Z = \left[ \left( \sum_{i \in turbinebody} \mathbf{W}_{(\text{Turbine})} + W_{(GasTurb)} - \sum_{j \in compressors} W_{(compressors)} \right) \cdot 3600 \cdot h \cdot d \cdot C_{\text{Electricity}} \right]$$

 $+ Benefits_{Filtration} + Benefits_{Centrif} + Benefits_{Coagulation} + Benefits_{FBR} + Benefits_{CSTR}$ 

(98)

### 5 2 Nomenclature

 $\mathbf{k} \in \{TS, C, K\}$ 

#### 6 2.1 Sets

$$\mathbf{i} \in \{P, N\}$$
 
$$j \in \{\text{filtermedia}\}$$

 $a' \in \{CH_4, CO_2, NH_3, H_2S, O_2 and / or N_2\}$ 

 $a \in \{\mathrm{H_2O,CH_4,CO_2,NH_3,H_2S,O_2and/orN_2}\}$ 

 $d \in \{C, Norg, Nam, P, K, H2O and / or Rest\}$ 

 $e \in \{CH_4, NH_3 and / or H_2 S\}$ 

$$h \in \{CH_4, CO_2, O_2, N_2\}, \{O_2, N_2\} \text{ or } \{CO_2, O_2, N_2\}$$

### 8 2.2 Parameters

 $A_{\rm specific}$ 

 $_{9}~:$  specific clarifier area (m2 / (ton·day))

A(i)

 $_{10}\;$  : Antoine A coefficient for vapor pressure of component i

B(i)

11	: Antoine B coefficient for vapor pressure of component i
	$\mathrm{C}(\mathrm{i})$
12	: Antoine C coefficient for vapor pressure of component i
	$\mathrm{Cp}_{sat}$
13	: specific heat capacity of flue gas.
	d
14	: work days per year
	$\mathrm{d}_p$
15	: particle diameter (m)
	k
16	: kinetic constant (s-1)
	$\mathrm{IAP}_{\mathrm{eq}}$
17	: equilibrium ion activity product
	h
18	: work hours per day $\mathrm{HRT}_{\mathrm{unit}} .$ hydraulic retention time of unit (s)
	$\mathrm{MW}_{\mathrm{component}}$
19	: molecular weight of component (kg/kmol)
	$ m MeP_{ratio}$
20	: metal/phosphorus molar ratio in coagulation process $Price_{component} :$ price of the component

21	$(\mathfrak{C}/\mathrm{kg})$
	g
22	: gravity acceleration (m2/s) $$\rm k$$
	Α.
23	: polytropic coefficient (1.4)
	$\kappa_{ m agitator}$
24	: agitators specific power consumed ( HP / 1000 US gallon) $\varphi_{\rm j}$ : precipitation agent j per total solids mass ratio
25	
	$\eta_c$
26	: Compressor's efficiency (0.85)
	$\eta_s$
27	: Isentropic efficiency (0.9)
	$\eta_{ m i}^{ m j}$
28	: i component separation yield using in the process the element j
	$\mathrm{P}_{atm}$
29	: atmospheric pressure (1 bar)
	$\mathrm{T}_{atm}$
30	: atmospheric temperature (25 $^{\rm o}{\rm C})$
	R
31	: ideal gas constant (8.314 J/mol·K)
	$\mathrm{Cp}_{H_2O}$

 $_{32}$  : specific heat capa

## **2.3 Variables**

55	210 (6116.6165	
34	a <sub>technology</sub> : parameter which takes the va	lue 0 when
		$F_{design}^{ m technology}$
35	is 0 and 1 if	ted a dea
		$F_{design}^{ m technology}$
36	is not equal to 0	$lpha_{mf}$
37	: parameter dependent of the phases num	
		$Ar_l$
38	: Arquimedes number for liquid	٨
39	: area of unit (m2)	${ m A}_{unit}$
	В	$enefits_{technology}$
40	: benefits or losses obtained with technol	ogy
		C - N
41	: carbon to nitrogen molar ratio	$C_{eq}$
42	: equilibrium concentration (kmol/m3)	A
		$C_0$
43	: initial concentration (kmol/m3)	$\mathrm{Cost}_{unit}$
		<i>3.000</i>
		17

44	: cost of unit
	$C_{component}^{unit}$
45	: concentration of component in the unit inlet stream (kgcomponent/kgtotal)
	$\mathrm{ChemC}_{\mathrm{technology}}$
46	: cost of chemicals for technology
	$D_{ m unit}$
47	: diameter of unit
	$e_{ m unit}$
48	: thickness of unit
	$Ec_{j}\left( T ight)$
49	: equilibrium constant of component j at temperature T.
	$F_{component}^{unit}$
50	: mass flow of component in the unit inlet stream (kg/s) $F_{\rm max}^{unit}$ : maximum mass inlet flow admitted
51	by a single unit (kg/s) $F_{\text{design}}^{unit}$ : mass inlet flow used in the design of unit (kg/s)
	$\mathrm{FC}_{\mathrm{technology}}$
52	: fixed cost of technology
	$F^{ m recovered}_{total}$
53	: recovered matter total mass flow (kg/s)

 $\mathcal{F}_{(unit,unit1)}$ 

54	:	mass flow from stream from unit to unit1 (kg/s)
		$fc_{(J,unit,unit1)}$
55	:	mass flow of component J from unit to unit 1 (kg/s)
		$H_{b,(unit,unit1)}$
56	:	enthalpy of the stream at the state b from the stream from unit to unit 1 (kJ/kg) $$
		$H_{\rm steam(isoentropy)}$
57	:	enthalpy of the stream at the if the expansion is is entropic (kJ/kg).
		$l_{j-i}$
58	:	molar fraction of component j in the liquid phase of equilibrium system i.
		$K_{index}$
59	:	Potassium index of fertilizer. $L_{\rm unit}$
60	:	length of unit
		$N_{am}$
61	:	nitrogen contained in ammonia. $N_{org} \label{eq:Norg}$
62	:	nitrogen contained in organic matter. $n_{\rm unit} :$ number of units used in the process
		$n_{(unit,unit1)}$

63	: total mol flow from stream from unit to unit 1 (kmol/s).	
	$N_{index}$	
64	: nitrogen index of fertilizer.	
	$P_{in/compressor}$	
65	: inlet pressure to compressor (bar).	
	$P_{out/compressor}$	
66	: outlet pressure of compressor (bar).	
	$P_j * (T)$	
67	: saturation pressure of pure component j at temperature T (bar).	
	$P_v$	
68	: vapor pressure (bar)	
	$P_{index}$	
69	: phosphorous index of fertilizer.	
	$p_{turbi}$	
70	: inlet pressure to body i in the turbine (bar)	
	$P_{unit}$	
71	: power of unit	
	$Q_{(unit)}$	
72	: heat exchanged in unit (kW).	
	$R_{C-N/k}$	

73	carbon to nitrogen ratio in k.	
	$R_{C-N/fertilizer}$	
74	carbon to nitrogen ratio in fertilizer.	
	$R_{V/F-i}$	
75	rate of evaporation in equilibrium system i.	
	Rest	
76	: rest of the elements contained in the biomass.	
	$\mathrm{Re}_{\mathrm{lmf}}$	
77	Reynolds number for liquid in minimum fluidization co	onditions
	$s_{b(unit,unit1)}$	
78	: entropy the stream at the state $b$ for the stream from $b$	unit to uni1 kJ/kg.K
	$T_{turbimin}$	
79	: saturating temperature at exit of body i ( ${}^{\circ}$ C)	
	$T_{(unit,unit1)}$	
80	: temperature of the stream from unit to unit 1 ( ${}^{o}$ C)	
	$T_{bubble/i}$	
81	: bubble point temperature of equilibrium system i ( ${}^{0}$ C)	
	$T_{m/i}$	

82	: average temperature in equilibrium system i ( ${}^{0}$ C).
	$T_{in/compressor}$
83	: in let temperature to compressor (°C).
	$T_{out/compressor}$
84	: outlet temperature of compressor ( ${}^{o}$ C).
	t
85	: time (s)
	$u_t$
86	: terminal velocity (m/s)
	$u_0$
87	: fluid velocity (m/s)
	$u_{ m mf}$
88	: minimum fluidization velocity $(m/s)$
	$v_{j-i}$
89	: molar fraction of component j in the vapor phase of equilibrium system i.
	$V_{ m biogas,k}$
90	: biogas volume produced per unit of volatile solids (VS) (m3biogás/kgVS/k) associated to k.
91	$V_{unit}$ : volume of unit
	$W_{ m unit}$
92	: weight of unit
	$w_{DM/k}$

: dry mass fraction of k (kgDM/k/kg). : dry mass fraction of volatile solids out of the dry mass of k (kgVS/k/kgDM/k). : dry mass fraction of C in k (kgC/k/kgDM/k). : dry mass fraction of Nam in k (kgNam/k/kgDM/k). : dry mass fraction of Norg in k (kgNorg/k/kgDM/k). : dry mass fraction of P in k (kgP/k/kgDM/k). : dry mass fraction of K in k (kgK/k/kgDM/k). : dry mass fraction of the rest of the elements contained in k (kgK/k/kgMS/k).

 $W_{(unit)}$ 

98 : power produced or consumed in unit (kW).

 $x_{a/biogas}$ 

99 : mass fraction of component a in the biogas

 $y^j$ 

100 : binary variable to evaluate the element j

 $y_{biogas}$ 

: specific saturated moisture of biogas

 $Y_{a'biogas-dry}$ 

102 : molar fraction of component a in the dry biogas.

 $\Delta H_{reaction(Bioreactor)}$ 

: Heat of the anaerobic digestion's reaction (kW).

 $\Delta H_{comb}\left(k\right)$ 

: heat of combustion of component k (kW).

$$\Delta H_{comb}\left(e\right)$$

105 : heat of combustion of component e (kW).

$$\Delta H_{comb} \left( Digestate - dry \right)$$

106 : heat of combustion of dry digestate (kW)

$$\Delta H_f(h)_{T(unit,unit1)}$$

: heat of formation of component h at temperature T(unit,unit1) (kW)

Z

108 : objective function  $\rho_{component}$ : component density (kg/m3)

 $\mu_{component}$ 

 $_{109}$ : viscosity of component  $(kg/(m\cdot s))$ 

## 3 Supplementary Material

$$MW_{dry-biogas} = \sum_{a'} Y_{a'/biogas-dry} MW_{a'}$$
(99)

$$0.7 \le YCH4 \le 0.5$$
  
 $0.3 \le YCO2 \le 0.5$   
 $0.02 \le YN2 \le 0.06$   
 $0.005 \le YO2 \le 0.16$   
 $YH2S \le 0.002$   
 $9 \cdot 10^{-5} \le YNH3 \le 1 \cdot 10^{-4}$ 

Eq3

$$y_{\text{biogas}} = \frac{MW_{\text{H}_2\text{O}}}{MW_{\text{biogas-dry}}} \frac{Pv(T)}{P - Pv(T)}$$
(101)

Eq4

$$F_{\text{biogas}} = \rho_{\text{biogas}} \sum_{\text{waste}} w'_{\text{SV/waste\_i}} w_{\text{MS/waste\_i}} F_{\text{waste\_i}} \cdot V_{\text{biogas/waste\_i}}$$
(102)

Eq5

$$fc(H_2O)_{biogas} = y_{biogas} \cdot \sum_{a'} fc(a')_{biogas}$$
 (103)

Eq6

$$fc_{(a',Bioreactor,Compres1)}/MW_{a'} = \frac{Y_{a'/biogas-dry}}{MW_{biogas-dry}} (F_{(Bioreactor,Compres1)} - fc_{(H_2O,Bioreactor,Compres1)}) \end{magnetical}$$

$$MW_{\rm biogas} \sum_{\rm a} \frac{x_{\rm a/biogas}}{MW_{\rm a}} = \sum_{\rm a} x_{\rm a/biogas}$$
(105)

$$0.20 \leq Vbiogas, waste \leq 0.50$$
 
$$0.10 \leq wMS, Waste \leq 0.20$$
 
$$0.50 \leq wVSB, Waste \leq 0.80$$
 (106)

Eq9

$$w'_{C/k} = R_{C-N/k} \left( w'_{Norg/k} + w'_{Nam/k} \right)$$

$$(107)$$

Eq10

$$\begin{split} 6 & \leq R_{C-N/Waste} \leq 20 \\ 0.005 & \leq wN/Waste \leq 0.047 \\ 0.005 & \leq wNorg/Waste \leq 0.036 \\ 0.008 & \leq wP/Waste \leq 0.013 \\ 0.033 & \leq wK/Waste \leq 0.1 \end{split}$$
 (108)

Eq11

$$w_{C/Waste} + w_{Norg/Waste} + w_{Nam/Waste} + w_{P/Waste} + w_{K/Waste} + w_{Rest/Waste} = 1$$
 (109)

Eq12

$$fc(C)_{digestate} = w'_{C/Waste} \cdot w_{MS/Waste} \cdot F_{Waste} - fc(CH_4) \frac{MW_C}{MW_{CH_4}} - fc(CO_2) \frac{MW_C}{MW_{CO_2}}$$
(110)

$$fc(Norg)_{digestate} = w'_{No/Waste} \cdot w_{MS/Waste} \cdot F_{Waste} - fc(N_2) \frac{MW_N}{MW_{N_2}}$$
(111)

$$fc(N)_{digestate} = w'_{N/Waste} \cdot w_{MS/Waste} \cdot F_{Waste} - fc(NH_3) \frac{MW_N}{MW_{NH_3}}$$
(112)

Eq15

$$fc(P)_{digestate} = w'_{P/Waste} \cdot w_{MS/Waste} \cdot F_{Waste}$$
 (113)

Eq16

$$fc(K)_{digestate} = w'_{K/Waste} \cdot w_{MS/Waste} \cdot F_{Waste}$$
 (114)

Eq17

$$fc(Rest)_{digestate} = w'_{rest/Waste} \cdot w_{MS/Waste} \cdot F_{Waste} + fc(CH_4)_{biogas} \frac{4 \cdot MW_H}{MW_{CH_4}} - fc(CO_2)_{biogas} \frac{2 \cdot MW_O}{MW_{CO_2}} - fc(NH_3)_{biogas} \frac{3 \cdot MW_H}{MW_{NH_3}} - fc(H_2S)_{biogas} - fc(O_2)_{biogas}$$

$$(115)$$

Eq18

$$fc(H_2O)_{digestate} = (1 - w_{MS/Waste}) \cdot F_{Waste} - fc(H_2O)_{biogas}$$
(116)

Eq19

$$\begin{aligned} &Q_{\rm digestor} = \Delta H_{\rm reaction} - Fcp(T_{\rm digestor} - T_{\rm in}) \\ &\Delta H_{\rm reaction} = \sum_{\rm prod} \Delta H_{\rm combus} - \sum_{\rm reactants} \Delta H_{\rm combus} \end{aligned} \tag{117}$$

$$T_{out/compressor} = T_{in/compressor} + T_{in/compressor} \left( \left( \frac{P_{out/compressor}}{P_{in/compressor}} \right)^{\frac{z-1}{z}} - 1 \right) \frac{1}{\eta_c}$$
 (118)

$$W_{(Compressor)} = (F) \cdot \frac{R \cdot z \cdot (T_{in/compressor})}{((MW) \cdot (z-1))} \frac{1}{\eta_c} \left( \left( \frac{P_{out/compressor}}{P_{in/compressor}} \right)^{\frac{z-1}{z}} - 1 \right)$$
(119)

Eq22

$$Q_{(Furnace)} = \sum_{h} \Delta H_f(h)|_{T(Furnace, GasTurb)} \bigg|_{(Furnace, GasTur)} - \sum_{h} \Delta H_f(h)|_{T(Compres2, Furnace)} \bigg|_{(Compres2, Furnace)}$$

$$(120)$$

Eq23

$$\eta_{s} = \frac{H_{\text{steam}-(\text{Turb1},\text{HX5})} - H_{\text{steam}-(\text{HX4},\text{Turb1})}}{H_{steam-(isoentropy)} - H_{\text{steam}-(\text{HX4},\text{Turb1})}}$$
(121)

Eq24

$$H_{steam-(isoentropy)} = f\left(p_{\text{(Turb1,HX5)}}, T^*_{\text{(Turb1,HX5)}}\right)$$
(122)

Eq25

$$s_{\text{steam},(HX4,Turb1)} = f(p_{(HX4,Turb1)}, T_{(HX4,Turb1)}) = f(p_{(Turb1,HX5)}, T^*_{(Turb1,HX5)})$$
 (123)

Eq26

$$p_{\text{turb2}} \cdot 760 = e^{\left(A(H_2O) - \frac{B(H_2O)}{\left(C(H_2O)T_{\text{turb1min}}\right)}\right)}$$
(124)

$$T_{\text{(Turb1,HX5)}} > T_{\text{turb1min}} \tag{125}$$

$$W_{(Turbine1)} = fc_{(H2O,HX4,Turb1)} \cdot \left(H_{steam,(HX4,Turb1)} - H_{steam(Turb1,HX5)}\right)$$
(126)

Eq29

$$Q_{(HX5)} = fc_{(H2O,Turb1,HX5)} \cdot \left(H_{steam,(HX5,Turb2)} - H_{steam,(Turb1,HX5)}\right)$$
(127)

Eq30

$$Q_{(HX5)} = -F(Spl1, HX5) \cdot \int_{T_{(Spl1, HX5)}}^{T_{(HX5, Mix1)}} Cp_{salt} dT$$

$$(128)$$

Eq31

$$Q_{(HX5)} = -F(HX4, HX5) \cdot \int_{T_{(HX4, HX5)}}^{T_{(HX5, Mix1)}} Cp_{salt} dT$$
 (129)

Eq32

$$fc_{(H_{2O},HX5,Turb2)} = fc_{(H_{2O},Turb2,HX7)} + fc_{(H_{2O},Turb2,Turb3)}$$
 (130)

Eq33

$$\mathbf{Q}_{(\mathrm{HX6})} = \mathbf{fc}_{(H2O,\mathrm{Turb3},\mathrm{HX6})} \cdot \left( \mathbf{H}_{liq,(HX6,HX7)} - \mathbf{H}_{steam(Turb3,HX6)} \right) \tag{131}$$

$$T_{(HX7,HX8)} \le T_{turb2min} \tag{132}$$