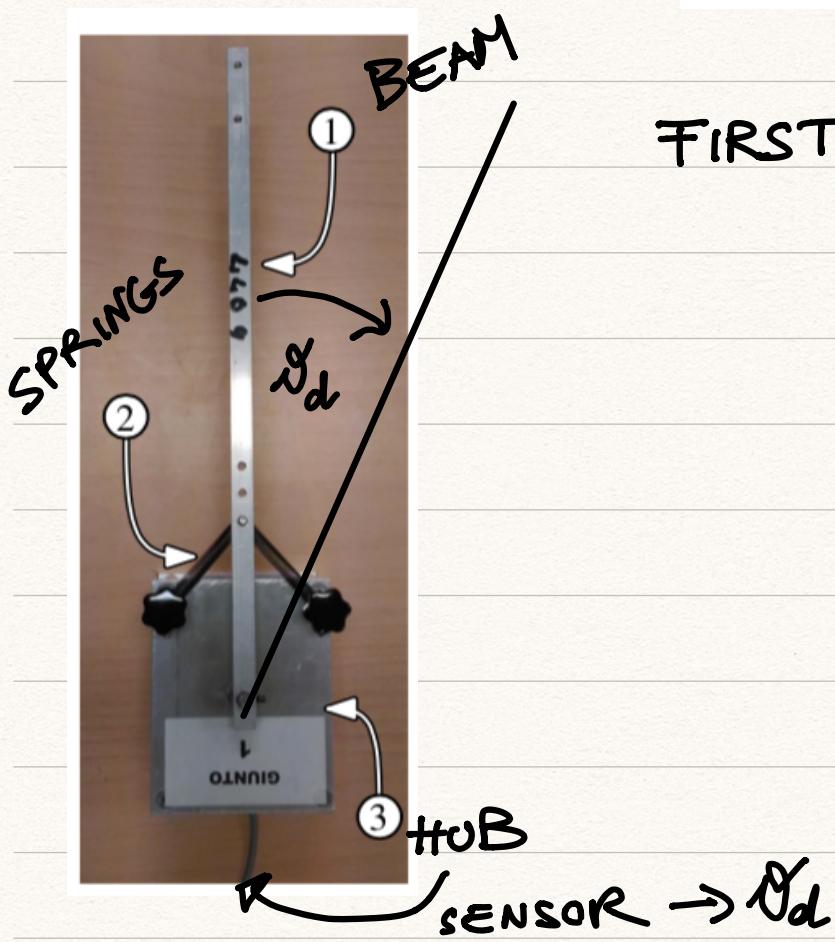
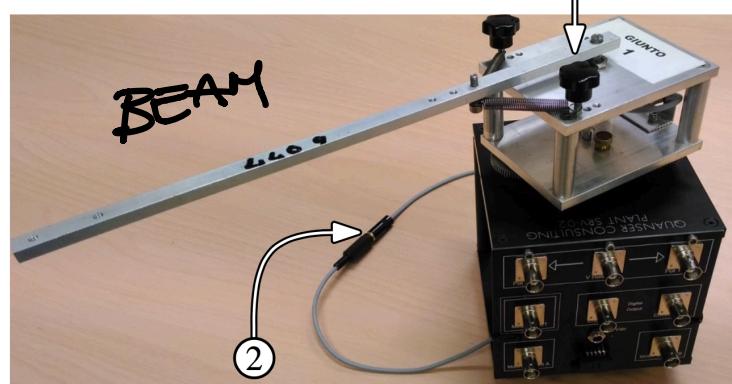


"NEW" SYSTEM

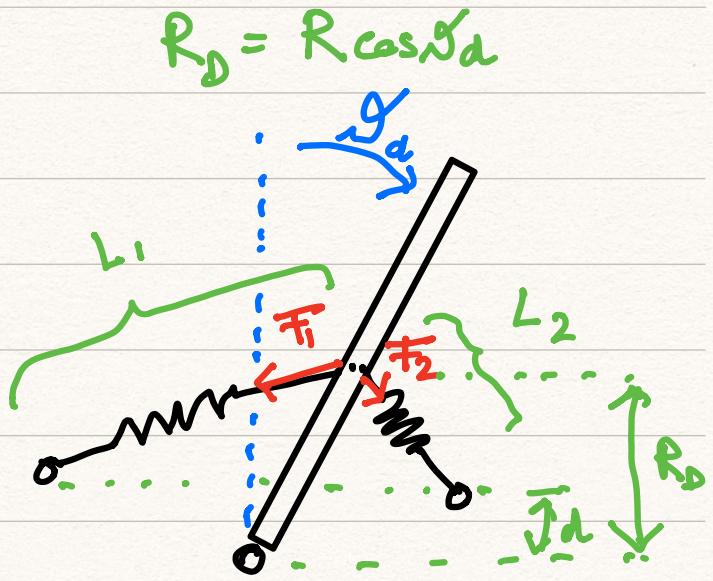
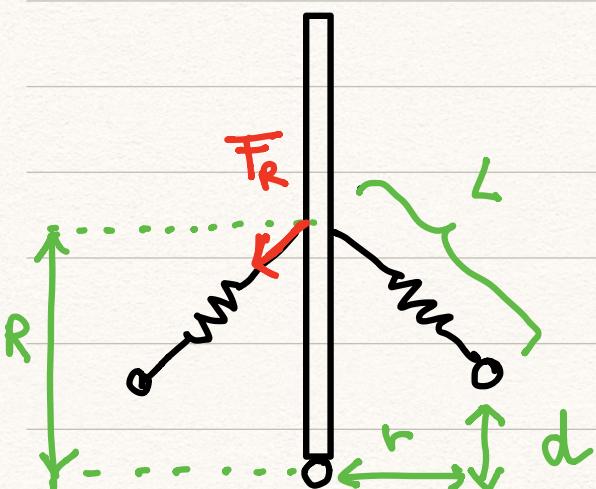
MOTOR + RESONANT LOAD



HUB +
FLEX JOINT



FIRST : FOCUS ON THE PHYSICS OF THE NEW LOAD



$$R_d = R \cos \theta_d$$

A LITTLE GEOMETRY:

$$\left\{ \begin{array}{l} L_{1,x} = r + R \sin \delta_d \\ L_{2,x} = r - R \sin \delta_d \\ L_{i,y} = R \cos \delta_d - d \quad i = 1, 2 \end{array} \right.$$

FORCES : ELASTIC CONSTANT \times DISPLACEMENT

$$F_i = k_s (L_i - L) + F_R$$

WE NEED : TORQUES (TRANSMITTED TO MOTOR'S SHAFT)

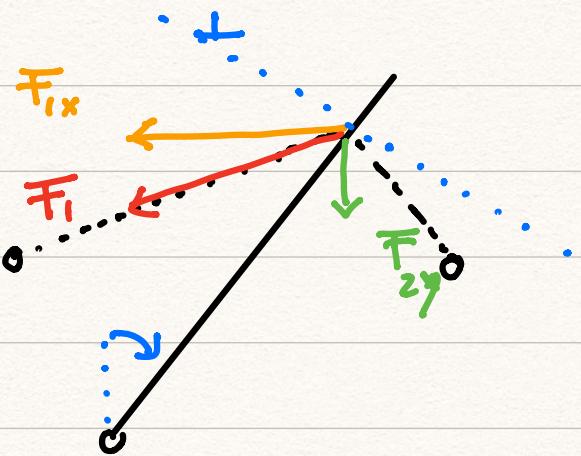
How : - We WRITE $F_{i,x}$, $F_{i,y}$;

- PROJECT each component onto \perp to BEAM ;

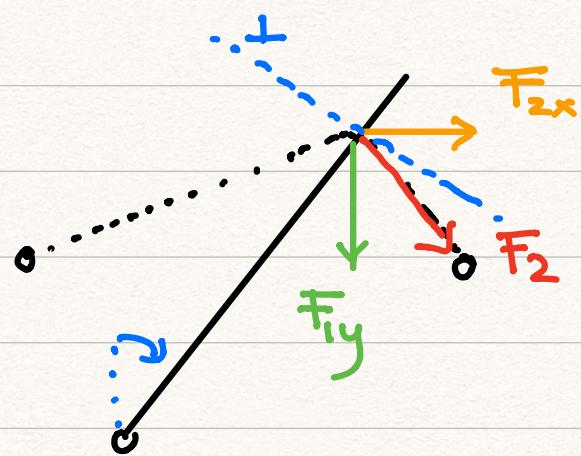
- COMPUTE $\tau = \sum_i F_i^\perp \cdot R$

$$F_{i,x} = F_i \frac{L_{ix}}{L_i}; \quad F_{i,y} = F_i \frac{L_{iy}}{L_i}$$

Let's see ...



F_1 DECOMPOSITION
& \perp COMPONENTS



F_2 DECOMPOSITION
& \perp COMPONENTS

$$\Rightarrow \tau_e = (F_{2,x} - F_{1,x}) R \cos(\delta_d) + (F_{3,y} + F_{2,y}) R \sin(\delta_d)$$

IF δ_d SMALL : LINEARIZE AROUND ϕ (REST)

$$\tau_e \approx -K \delta_d$$

IF HUB MOVES :

$$\delta_d = \delta_h - \delta_b$$

w.r.t. SAME REFERENCE

$$= \frac{2R}{L^3} \left[(L^2 d - Rr^2) F_R + (r^2 RL) K_s \right]$$

(Pb) : F_R , K_s are unknown

↳ WE NEED ESTIMATES !

- ASSUME HUB STILL ("LOCKED" TO TABLE),
NO EXTERNAL FORCES

$$\underbrace{J_b \ddot{\theta}_d}_{\text{INER Acceleration}} + \underbrace{B_b \dot{\theta}_d}_{\text{FRICTION}} + \underbrace{K \theta_d}_{\text{ELASTIC}} = 0$$

- REDEFINE $\omega_n = \sqrt{\frac{k}{J_b}}$; $\xi = \frac{B_b}{2\sqrt{J_b k}}$

NOTE: KNOWING ω_n, ξ
EQUIVALENT TO k, B_b

$$\Rightarrow \ddot{\theta}_d + 2\xi\omega_n \dot{\theta}_d + \omega_n^2 \theta_d = 0$$

↳ STANDARD FORM FOR II ORDER SYSTEM

↳ IN OUR CASE : $\xi < 1$ UNDERDAMPED

↳ GIVEN INITIAL CONDITIONS $\dot{\theta}_d(0)$, $\ddot{\theta}_d(0)$

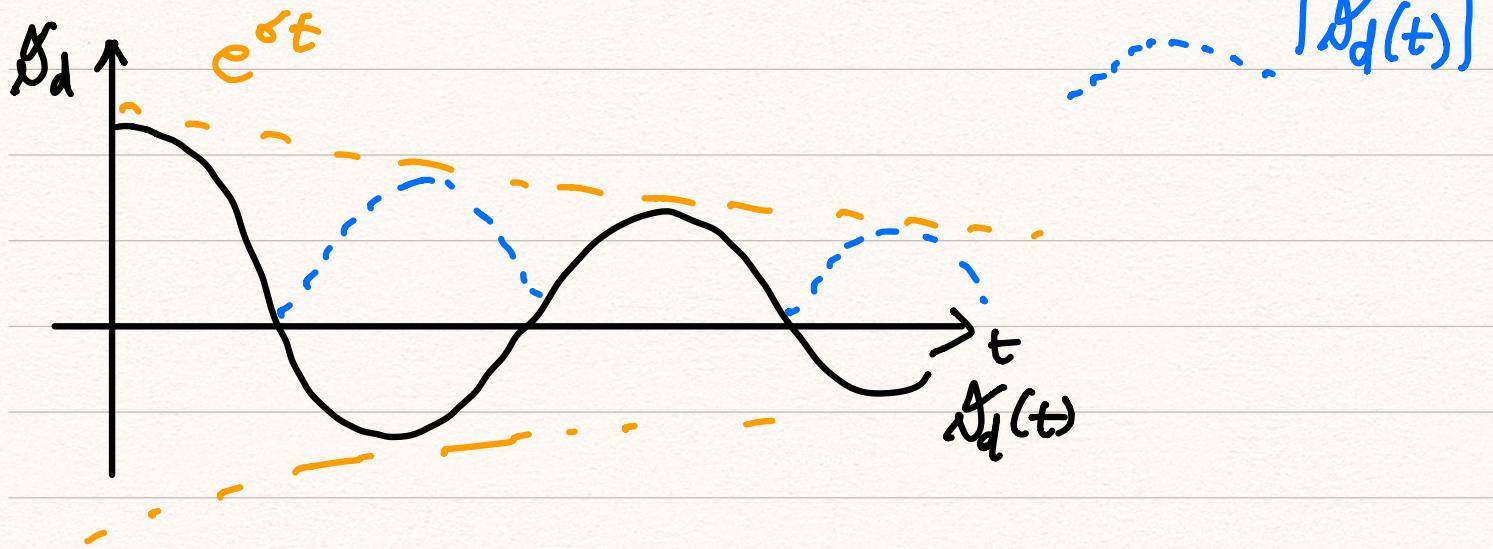
$$\theta_d(t) = \alpha e^{\delta t} \cos(\omega t + \phi)$$

• AS USUAL : $\delta = -\xi\omega_n$; $\omega = \omega_n \sqrt{1-\xi^2}$

• ALSO

$$\alpha = \sqrt{\dot{\theta}_d^2(0) + \left(\frac{\dot{\theta}_d(0) - \delta \theta_d(0)}{\omega} \right)^2}; \quad \phi = \tan^{-1} \left(\frac{\delta \theta_d(0) - \dot{\theta}_d(0)}{\omega \dot{\theta}_d(0)} \right)$$

- TYPICAL RESPONSE :



- LET'S FOCUS ON THE MAX OF $|\delta_d(t)|$

$$|\delta_d(t_k)| = \alpha e^{\sigma t_k}, \quad \text{for } t_k \text{ s.t. } \dot{\delta}(t_k) = 0$$

$$\Rightarrow t_k = \frac{k\pi - \phi}{\omega}$$

$$\bullet \text{ NOTICE : } \frac{|\delta_d(t_k)|}{|\delta_d(0)|} = e^{\sigma(t_k - t_0)} = e^{\frac{-\xi}{\sqrt{1-\xi^2}} k\pi}$$

- TAKING LOGARITHMS :

$$\log |\delta_d(t_k)| - \log |\delta_d(t_0)| = - \gamma k$$

where $\gamma = \frac{\xi\pi}{\sqrt{1-\xi^2}}$

linear γ IN k

EXPERIMENT :

- Run Test on still hub ;

Measure $\delta_d(t_k)$

- Do a linear Least square fitting on the $\log(|\delta_d(t_k)|)$

SETUP :

$$y \underset{\text{MEAS}}{\approx} -a \underset{\text{FREE VAR}}{\circlearrowleft} k + b = \varphi_k^T \theta$$

STACK UP

Define :

$$\Phi = \begin{bmatrix} \varphi_0^T \\ \varphi_1^T \\ \vdots \\ \varphi_M^T \end{bmatrix}; \quad y = \begin{bmatrix} \log|\delta_d(t_0)| \\ \vdots \\ \log|\delta_d(t_n)| \end{bmatrix}$$

$$\Rightarrow \text{LEAST SQUARE : } V(\theta) = \sum_k (\log|\delta_d(t_k)| - \varphi_k^T \theta)$$

$$= [y - \Phi \theta]^T [y - \Phi \theta]$$

$$\hat{\theta}_{LS} = \begin{bmatrix} \hat{a} \\ \hat{b} \end{bmatrix} = (\Phi^T \Phi)^{-1} \Phi^T y$$

← USUAL
FORMAT

- FROM $\hat{a} \equiv \hat{\gamma} \rightarrow \hat{\xi} = \frac{\hat{a}}{\sqrt{\pi^2 + \hat{a}^2}}$

- FOR ω_n ? FIRST ESTIMATE $(\omega \approx \frac{\pi}{t_{k+1} - t_k})$

$$\Rightarrow \hat{\omega} = \frac{1}{N} \sum_k \frac{\pi}{t_{k+1} - t_k}$$

then compute :

$$\hat{\omega}_n = \frac{\hat{\omega}}{\sqrt{1 - \hat{\xi}^2}}$$

- FINALLY, FROM $\hat{\xi}, \hat{\omega}_n \rightarrow \hat{k}, \hat{\beta}_{eq}$

$\#$