

# Verification Problems for FEM matlab program

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## Contents

**Formulae used:**

$$error\% = \left| \frac{w_{analytical} - w_{FEM}}{w_{analytical}} \right| \times 100 \quad (1)$$

$$D = \frac{Eh^3}{12(1 - \nu^2)} \quad (2)$$

# 1 Triangular Plate With Point Load (VM34)

## Description :

A triangular plate with point load ( $P$ ) on one corner is tested and its opposite edge is build-in.

## Reference :

C.O.Harris , Introduction to Stress Analysis, The Macmillan Co., pg:114, Pr:61.  
Solution Retrieved from Ansys verification problem (VM34).

## Material and Geometric data :

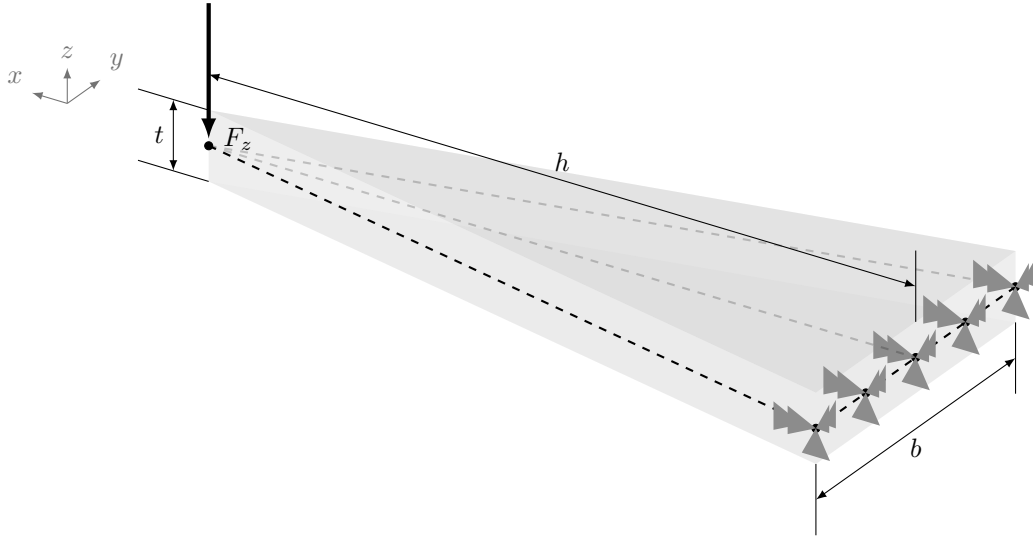


Figure 1: VM34

Table 1: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	3E7 <i>psi</i>	Height ( $h$ )	20 <i>in</i>	Point Load ( $F_z$ )	10 <i>lbs</i>
Poisson's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	3 <i>in</i>		
		Thickness( $t$ )	0.5 <i>in</i>		

## Mesh and boundary condition :

Table 2: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary			
Geo - Entity	$w$	$\theta_x$	$\theta_y$	Geo - Entity	$F_z$	$M_x$	$M_y$
line {3}	Fixed	Fixed	Fixed	Point {2}	-10 <i>lbs</i>		

## Analytically solution :

The target analytically solution is given as -0.042677 *in* at the corner where the loading is applied.

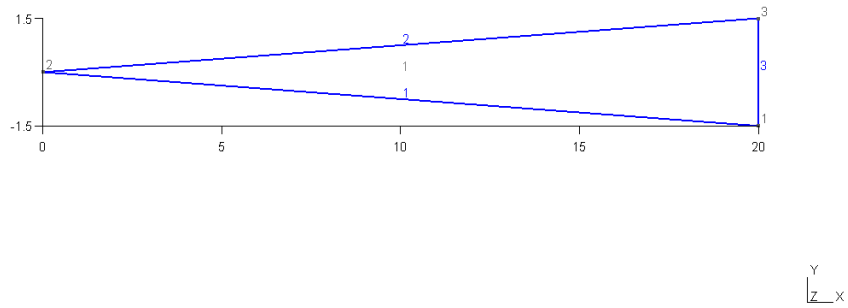


Figure 2: Geomentry of the problem

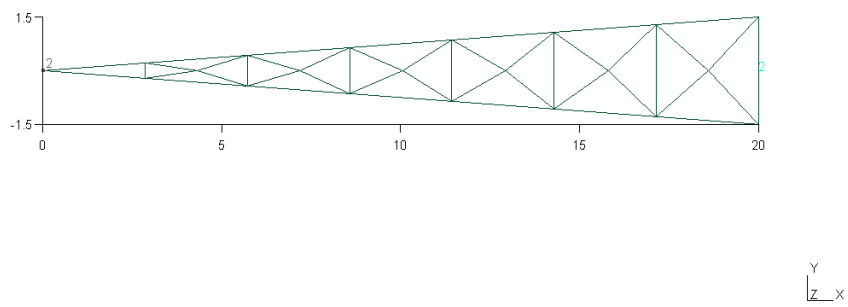


Figure 3: Discritization

**Result and error analysis :**

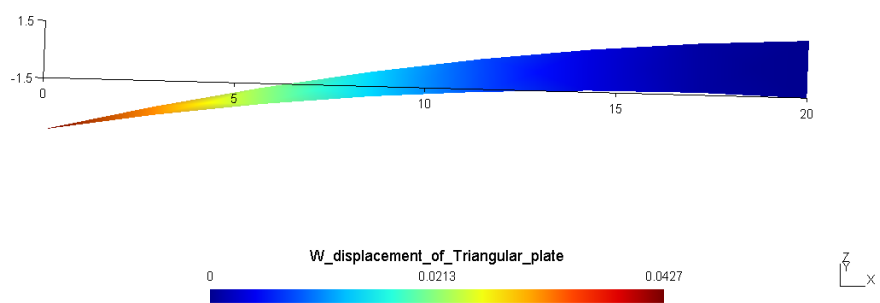


Figure 4: FEM solution plot

The maximum displacement of the domain is our solution . w displacement at point 2 is  $-0.0426677in$ .

So the Error percentage is 0.00234%.

## 2 Simply Supported Circular plate with point load (TIM68)

### Description :

Simply Supported Circular plate with point load at the center.

### Reference :

S.Timoshenko , S . Woinowsky , Theory of Plates and Shells , pg:68, Article : 19 .

### Material and Geometric data :

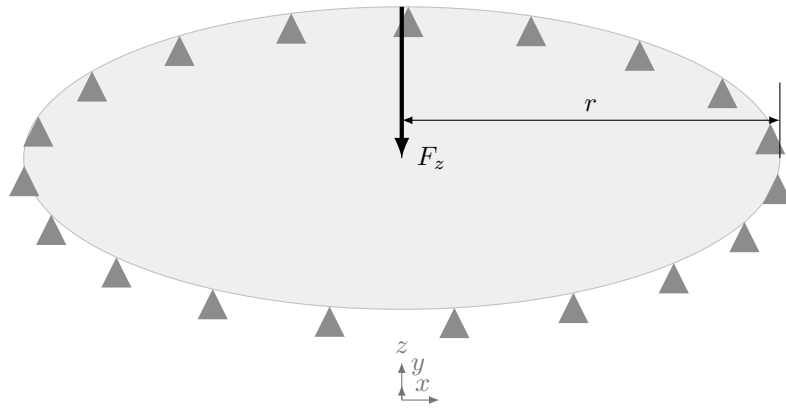


Figure 5: TIM68

Table 3: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	5E11 $Pa$	Radius ( $r$ )	1 $m$	Point Load ( $F_z$ )	1000 $N$
Poisson's Ratio ( $\nu$ )	0.3	Thickness( $t$ )	0.01 $m$		

### Mesh and boundary condition :

Table 4: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary			
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$F_z$	$M_x$	$M_y$
line {1,2,3,4}	Fixed	Free	Free	Point {1}	-1000 $N$		

### Analytically solution :

The target analytically solution given as

$$w_{at\_center} = \frac{F_z}{16\pi D} \left[ \frac{(3 + \nu)r^2}{1 + \nu} \right] \quad (3)$$

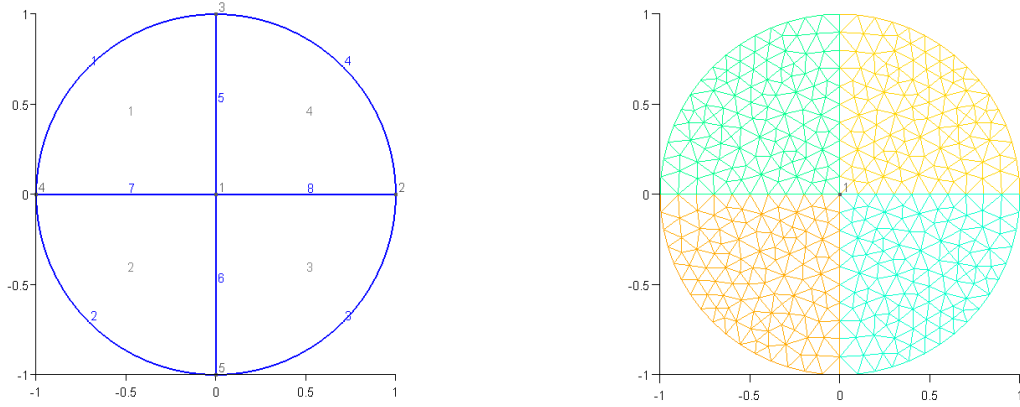


Figure 6: Geomentry and Mesh of TIM68

#### Result and error analysis :

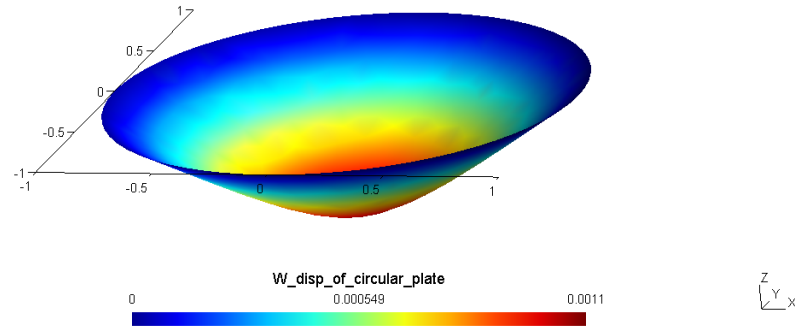


Figure 7: FEM solution plot

The maximum displacement of the domain is our solution . w displacement at center is  $-0.0010983in$ .  
So the Error percentage is 0.42103%.

### 3 Build-in Circular plate with point load (TIM69)

#### Description :

Simply Supported Circular plate with point load at the center.

#### Reference :

S.Timoshenko , S . Woinowsky , Theory of Plates and Shells , pg:69, Article : 19 .

#### Material and Geometric data :

Table 5: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	5E11 Pa	Radius ( $r$ )	1 m	Point Load ( $F_z$ )	-1000 N
Poisson's Ratio ( $\nu$ )	0.3	Thickness( $t$ )	0.01 m		

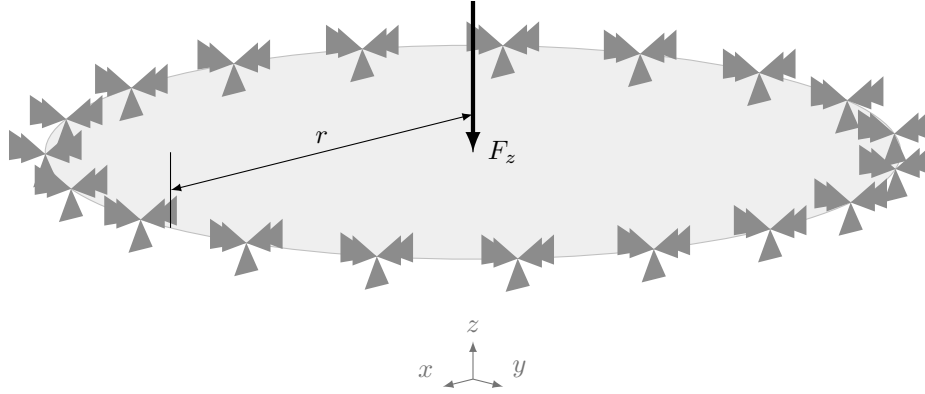


Figure 8: TIM69

**Mesh and boundary condition :**

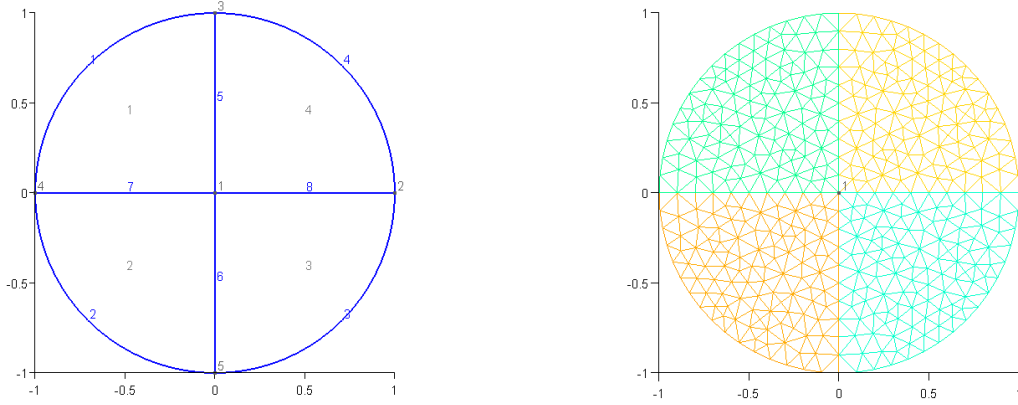


Figure 9: Geomentry and Mesh of TIM68

Table 6: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary			
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$F_z$	$M_x$	$M_y$
line {1,2,3,4}	Fixed	Fixed	Fixed	Point {1}	-1000	$N$	

**Analytically solution :**

The target analytically solution given as

$$w = \frac{F_z}{16\pi D} [r^2 - a^2] + \frac{F_z r^2}{8\pi D} \left[ \log \frac{a}{r} \right] \quad (4)$$

The displacement at center is obtained by substituting  $a \approx 0$ . The analytical solution is  $-0.000434$  m.

**Result and error analysis :**

The maximum displacement of the domain is our solution . w displacement at center is  $-0.000429in$ . So the Error percentage is 1.26%.

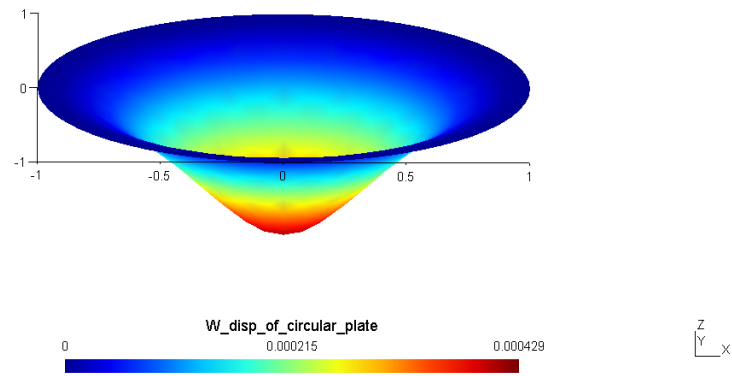


Figure 10: FEM solution plot

## 4 Natural Frequency of Square plate (VMP09)

### Description :

Natural frequency of a square plate is analyzed and compared.

### Reference :

NAFEMS Manual. Solution Retrieved from Ansys verification problem (VMP09-T12).

### Material and Geometric data :

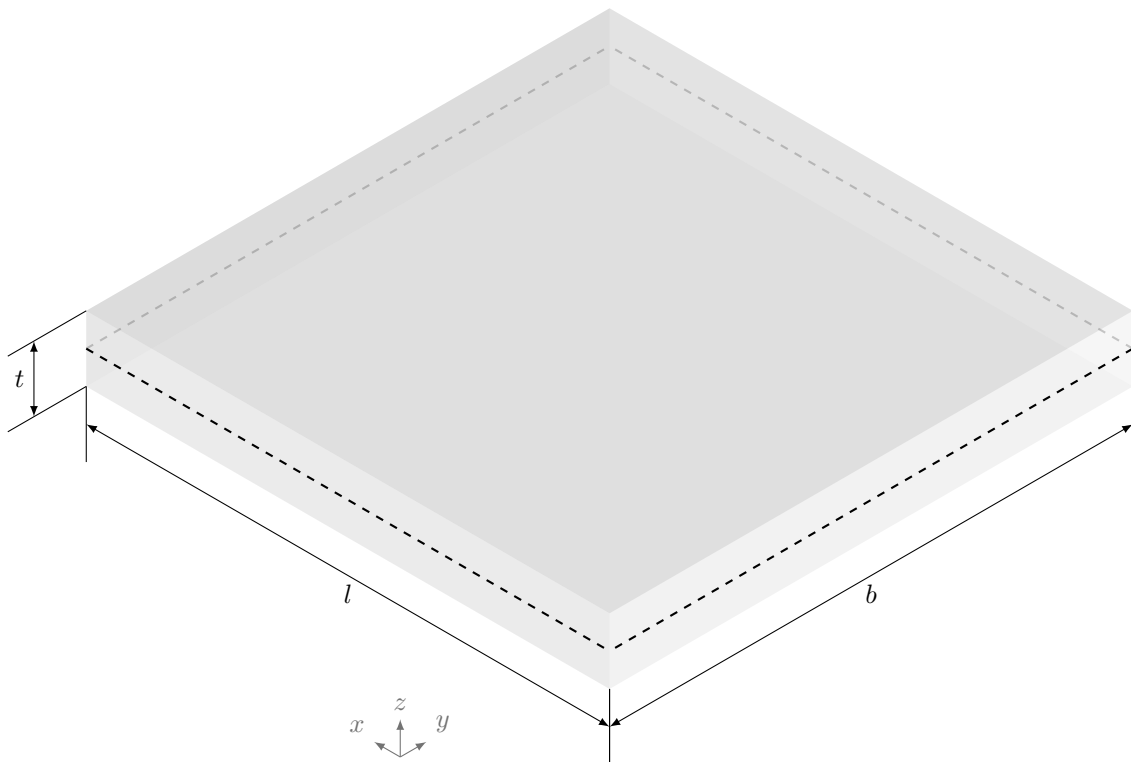


Figure 11: VMP09

Table 7: Input Data

Material Property		Geometric Data		Loading Data
Young's Modulus ( $E$ )	2E11 $pa$	Length ( $l$ )	10 $m$	Nil
Poission's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	10 $m$	
Density ( $\rho$ )	8000 $Kg/m^3$	Thickness( $t$ )	0.05 $m$	

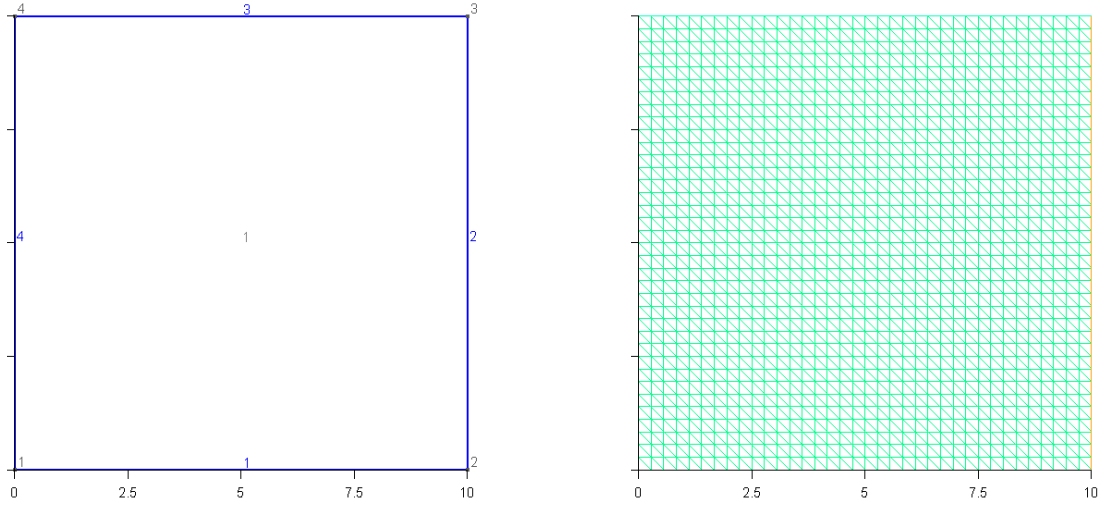


Figure 12: Geomentry and Mesh of TIM68

Table 8: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary			
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$F_z$	$M_x$	$M_y$
line {1,2,3,4}	Free	Free	Free	Nil			

**Mesh and boundary condition :**

**Analytically solution :**

Retrieved Natural frequencies from reference manuals are

Mode 4 = 1.622  $Hz$

Mode 5 = 2.360  $Hz$

Mode 6 = 2.922  $Hz$

Mode 7 = 4.233  $Hz$

Mode 8 = 4.233  $Hz$

Mode 9 = 7.416  $Hz$

**Result and error analysis :**

The Natural modes obtained are plotted in the below figures.

For each natural frequency the error percentage is

Mode 4 = 0.0018 %

Mode 5 = 0.0042 %

Mode 6 = 0.061 %

Mode 7 = 0.911 %

Mode 8 = 0.902 %



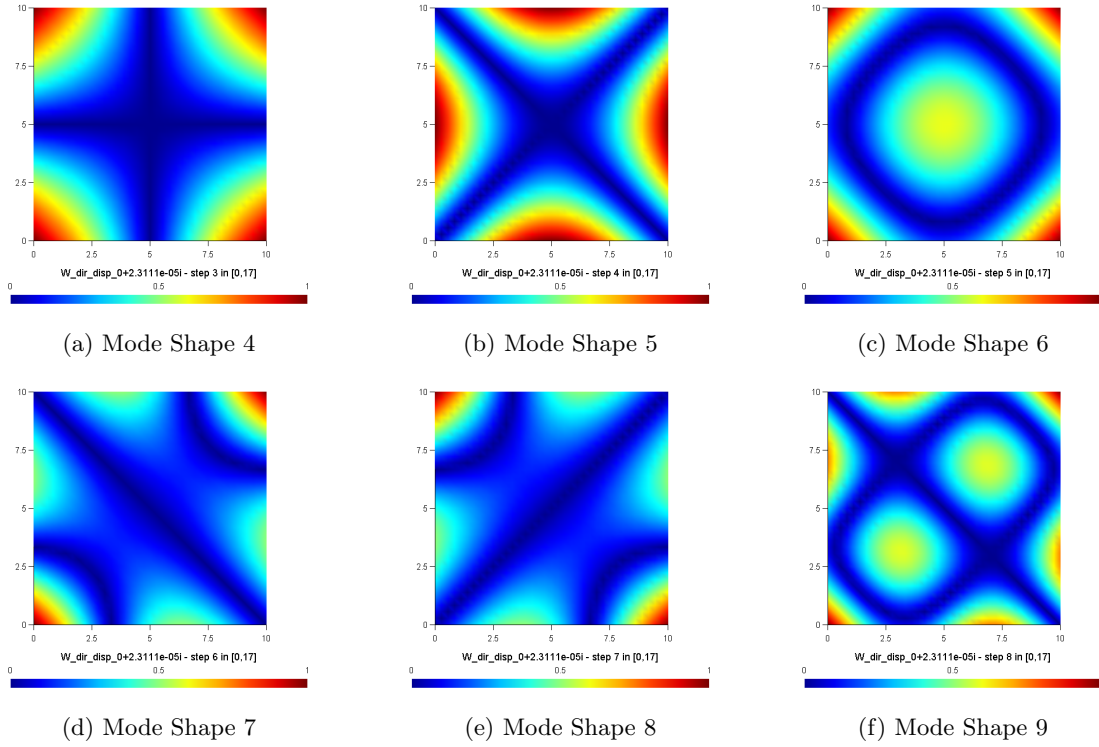


Figure 13: Natural Modes of a Square Plate

Mode 9 = 0.645 %

## 5 Square plate with distributed load(TIM116)

### Description :

A simply Supported square plate with distributed load ( $q$ ).

### Reference :

S.Timoshenko , S . Woinowsky , Theory of Plates and Shells , pg:116, Article : 30 .

### Material and Geometric data :

Table 9: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	2E11 $pa$	Length ( $a$ )	10 $m$	Distributed Load ( $q$ )	1000 $N/m^2$
Poission's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	10 $m$		
		Thickness( $t$ )	0.1 $m$		

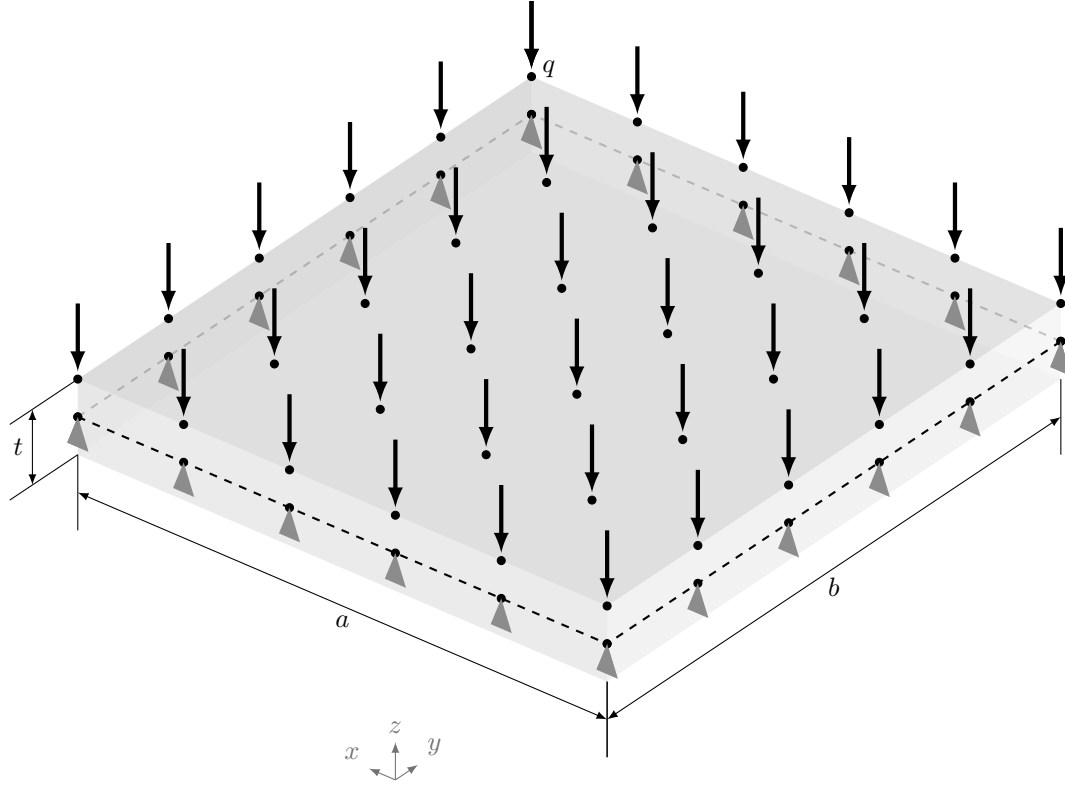


Figure 14: TIM116

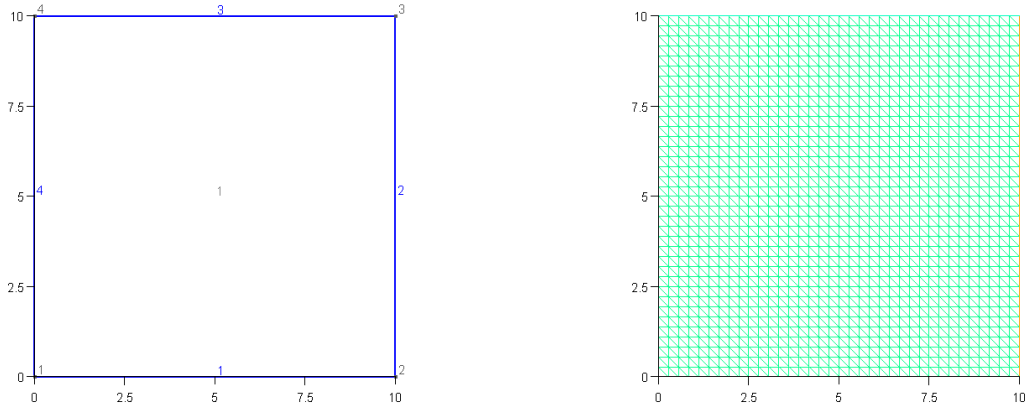


Figure 15: Geomentry and Mesh of TIM116

Table 10: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary			
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$F_z$	$M_x$	$M_y$
line {1,2,3,4}	Fixed	Free	Free	Area {1}	$1000 \text{ N/m}^2$		

**Mesh and boundary condition :**

**Analytically solution :**

The  $w_{max}$  which is the  $w$  displacement at the middle of the plate is given by

$$w_{max} = 0.00406 \frac{qb^4}{D} \quad (5)$$

The analytically solution of the problem is calculated as  $w_{max} = -0.0022167m$

**Result and error analysis :**

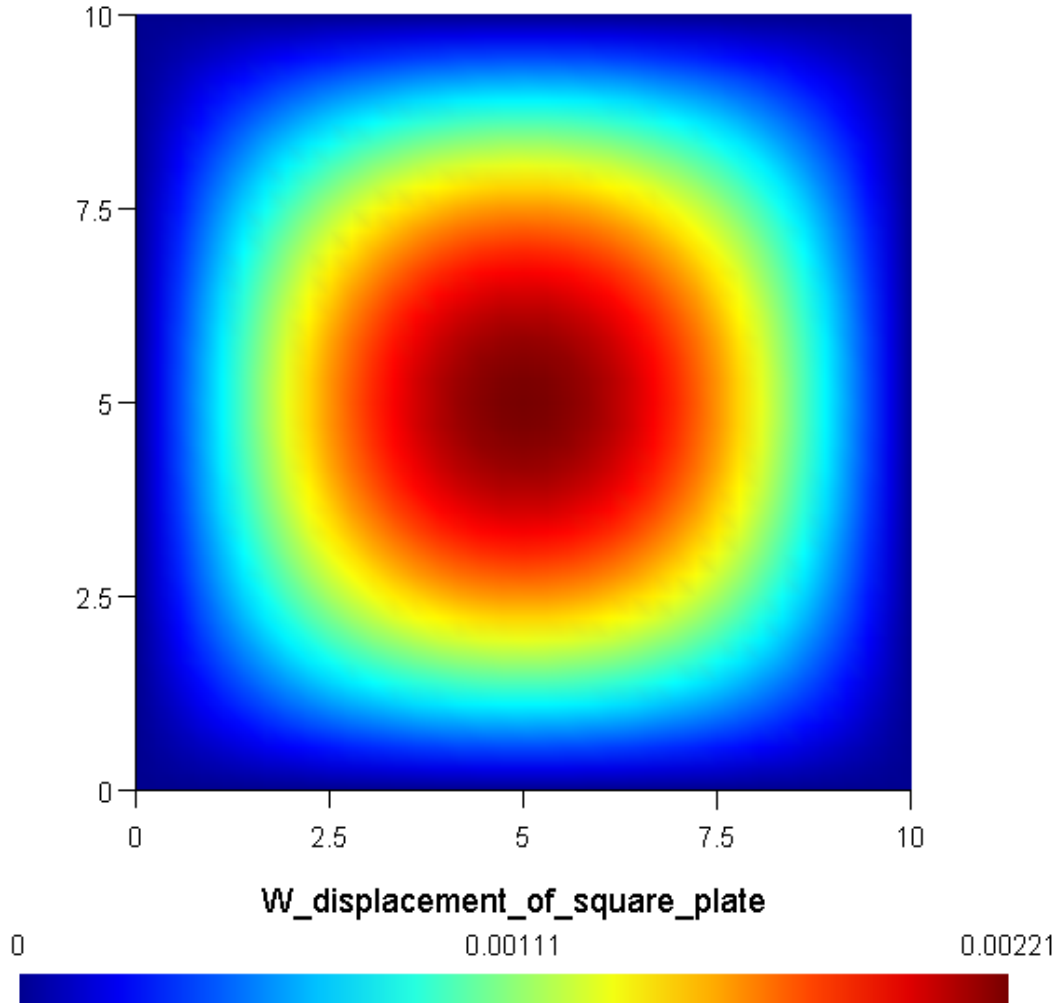


Figure 16: FEM solution plot

The maximum displacement of the domain is our solution . w displacement at middle is  $-0.0022144m$ .

$$error\% = \left| \frac{w_{analytical} - w_{FEM}}{w_{analytical}} \right| \times 100 \quad (6)$$

So the Error percentage is 0.1%.

## 6 Square plate with combined load(TIM381)

**Description :**

A simply Supported square plate with distributed load (q).

**Reference :**

S.Timoshenko , S . Woinowsky , Theory of Plates and Shells , pg:381, Article : 30 .

**Material and Geometric data :**

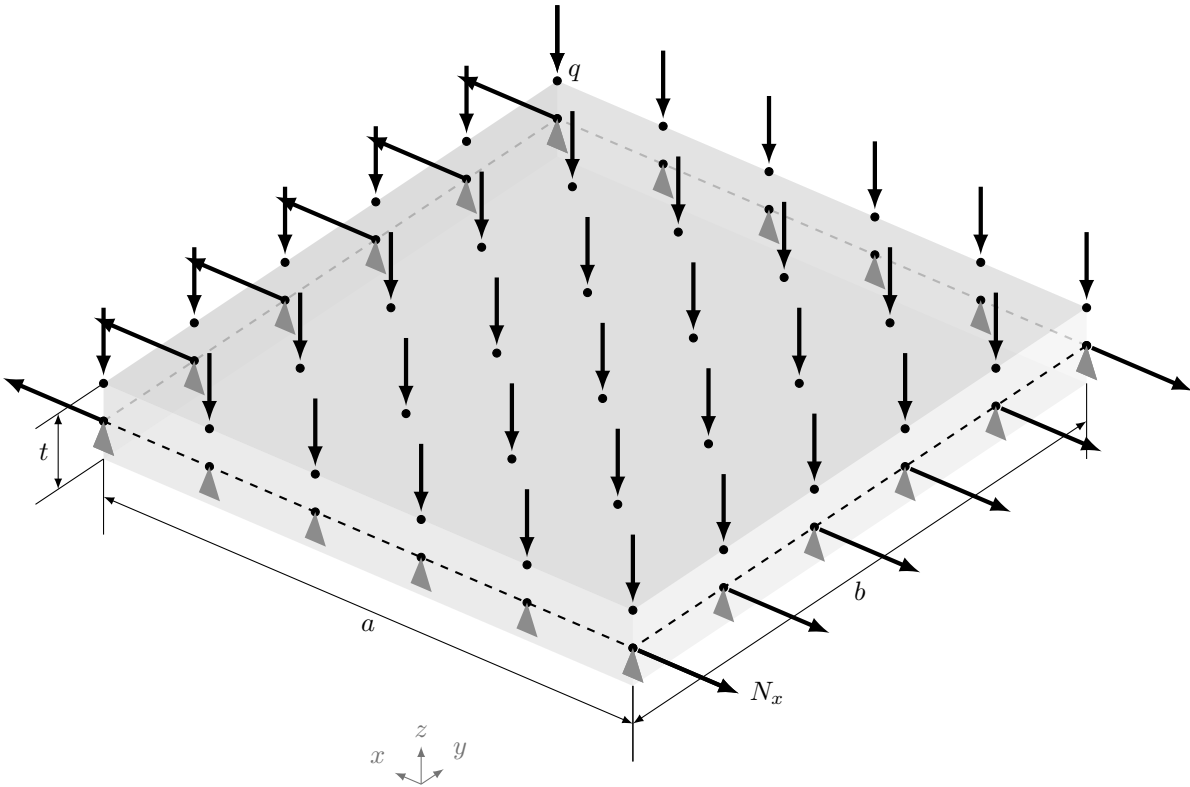


Figure 17: TIM381

Table 11: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	2E11 $pa$	Length ( $a$ )	10 $m$	Axial Tension( $N_x$ )	2E7 $N/m$
Poission's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	10 $m$	Distributed Load ( $q$ )	1000 $N/m^2$
		Thickness( $t$ )	0.1 $m$		

**Mesh and boundary condition :**

Table 12: FEM and Boundary condition data

Direchlet Boundary				Neumann Boundary		
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$F_z$	$M_x$ $M_y$
line {1,2,3,4}	Fixed	Free	Free	Area {1}	1000 $N/m^2$	
				Geo -Entity	Fx	
				line{1,3}	2E7 $N/m$	

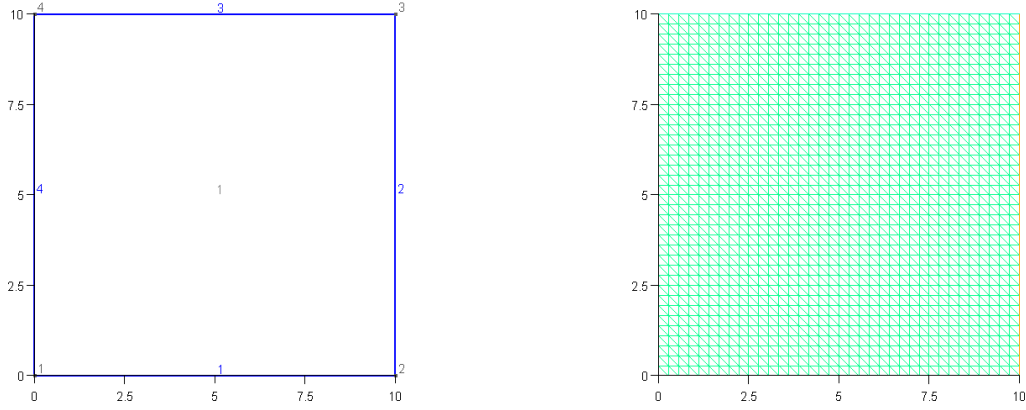


Figure 18: Geometry and Mesh of TIM381

### Analytically solution :

The  $w_{max}$  which is the  $w$  displacement at the middle of the plate is given by

$$w_{max} = \alpha \frac{qb^4}{Et^3} \quad (7)$$

Where  $\alpha$  can be taken from the graph given in the figure : ?? . For this problem alpha is taken as  $\alpha \approx 0.0113$ .

The parameter  $\gamma$  is given by

$$\gamma = \frac{N_x b^2}{4\pi^2 D} \quad (8)$$

The analytically solution of the problem is calculated as  $w_{max} = 0.000565m$

### Result and error analysis :

The maximum displacement of the domain is our solution .  $w$  displacement at middle is  $0.000566m$ .

So the Error percentage is 0.17%.

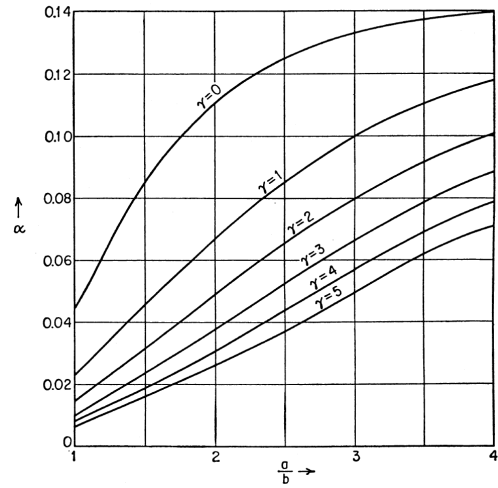


Figure 19: Graph to find  $\alpha$  .

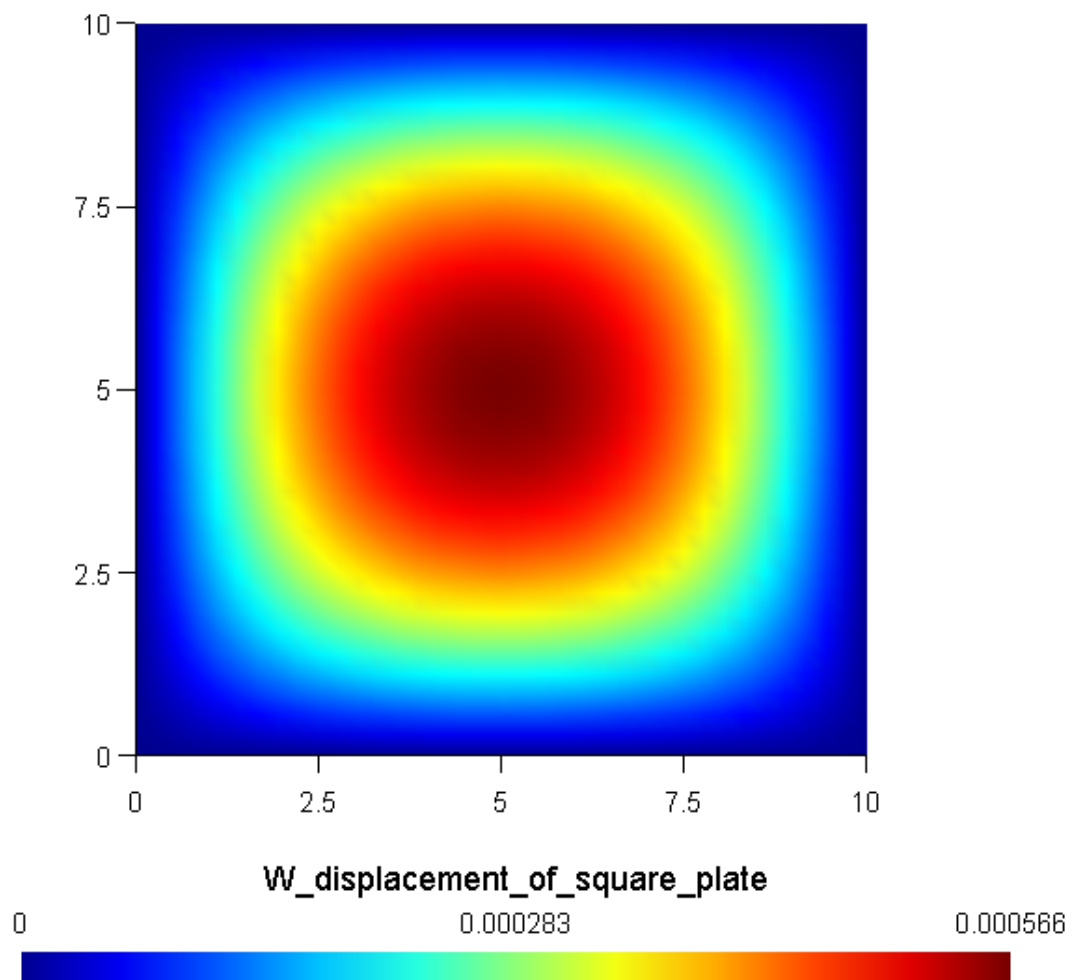


Figure 20: FEM solution plot

## 7 Natural Frequency of Rectangular strip with axial load (NAS277)

### Description :

Modal analysis of a rectangular strip with axial stress ( $N_2$ ) on short edge.

### Reference :

Arthur W.Leissa ,Vibration of Plates,NASA SP-160, pg:277, Ch:10.2.

### Material and Geometric data :

### Mesh and boundary condition :

### Analytically solution :

The analytical solution of the this problem is given by

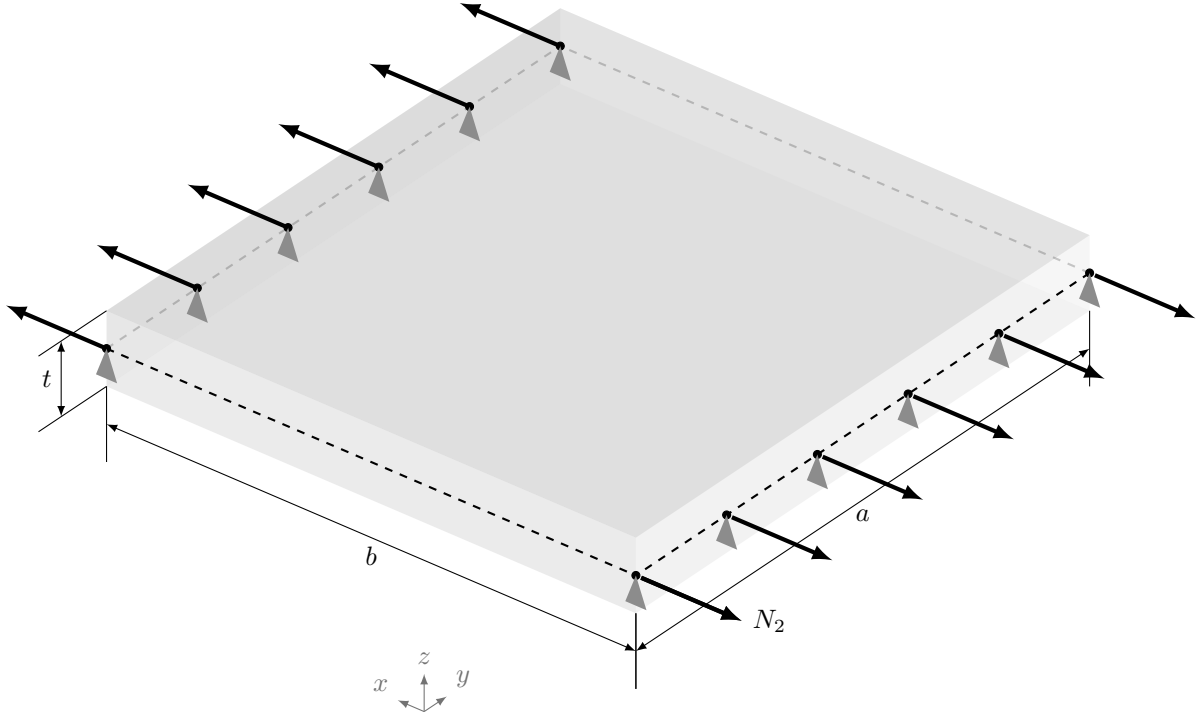


Figure 21: NAS277

Table 13: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	1E11 $pa$	Length ( $a$ )	1 $m$	$N_2$	3E11 $N/m^2$
Poisson's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	40 $m$		
Density ( $\rho$ )	7810 $Kg/m^3$	Thickness( $t$ )	1 $m$		

Table 14: FEM and Boundary condition data

Direchlet Boundary				Loading Conditions	
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$N_2$
line {1,3}	Fixed	Free	Free	line {1,3}	3E11 $N/m^2$

$$\omega_{mn} = \sqrt{\frac{1}{\rho} \left( D \left[ \left( \frac{m\pi}{a} \right)^2 + \left( \frac{n\pi}{b} \right)^2 \right] + N_1 \left( \frac{m\pi}{a} \right)^2 + N_2 \left( \frac{n\pi}{b} \right)^2 \right)} \quad (9)$$

Natural frequencies are

mode 1 : 77.479  $Hz$

mode 2 : N.A

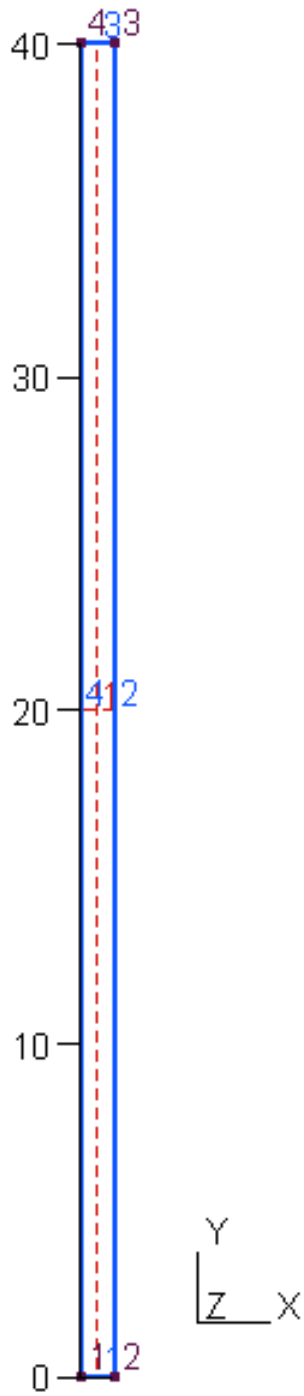
mode 3 : 155.00  $Hz$

mode 4 : N.A

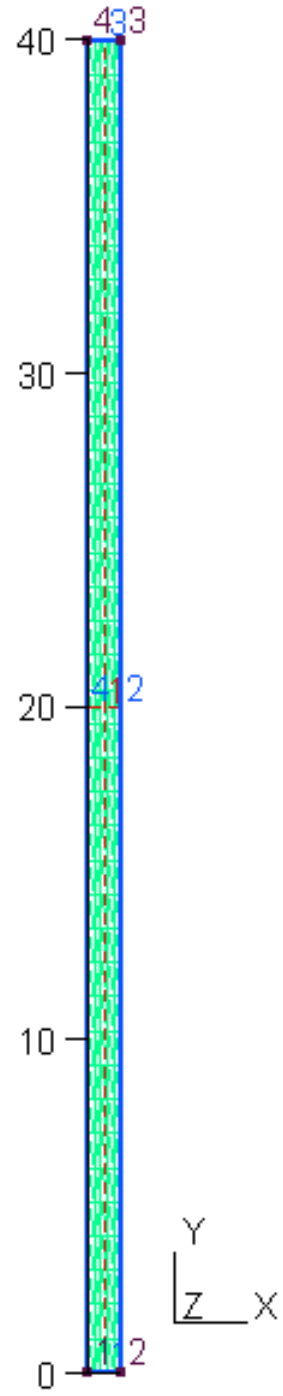
mode 5 : 232.61  $Hz$

mode 6 : N.A

note : modes 2,4 and 6 are twisting modes, which are not given by the formula.



(a) Geomentry of the problem



(b) Discritization

### Result and error analysis :

The natural frequencies of the plates are provided below.

mode 1 : 77.458  $Hz$

mode 2 : 95.610  $Hz$

mode 3 : 154.98  $Hz$

mode 4 : 191.46  $Hz$

mode 5 : 232.63  $Hz$

mode 6 : 287.38  $Hz$



So the Error percentage for each mode is :

mode 1 : 0.026 %

mode 3 : 0.012 %

mode 5 : 0.013 %

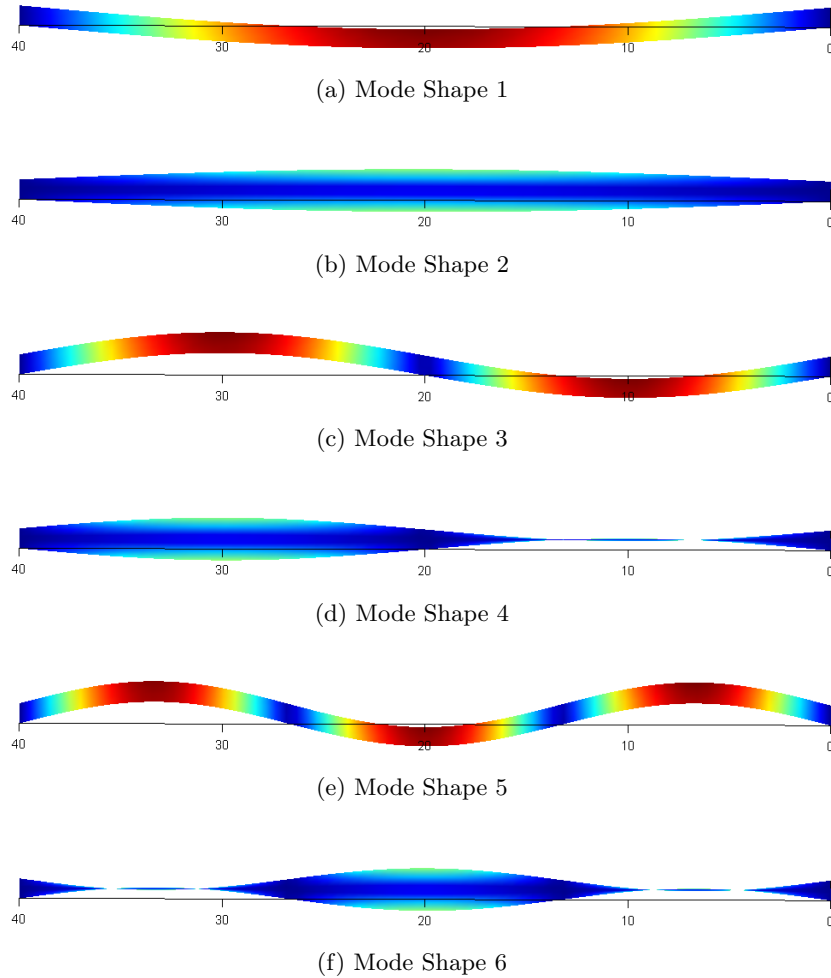


Figure 23: Natural Modes of a rectangular strip

## 8 Error analysis of strip with various thickness (NAS277)

### Description :

It is the continuation of previous problem but the error of the solution is compared for different thicknesses.

### Material and Geometric data :

### Mesh and boundary condition :

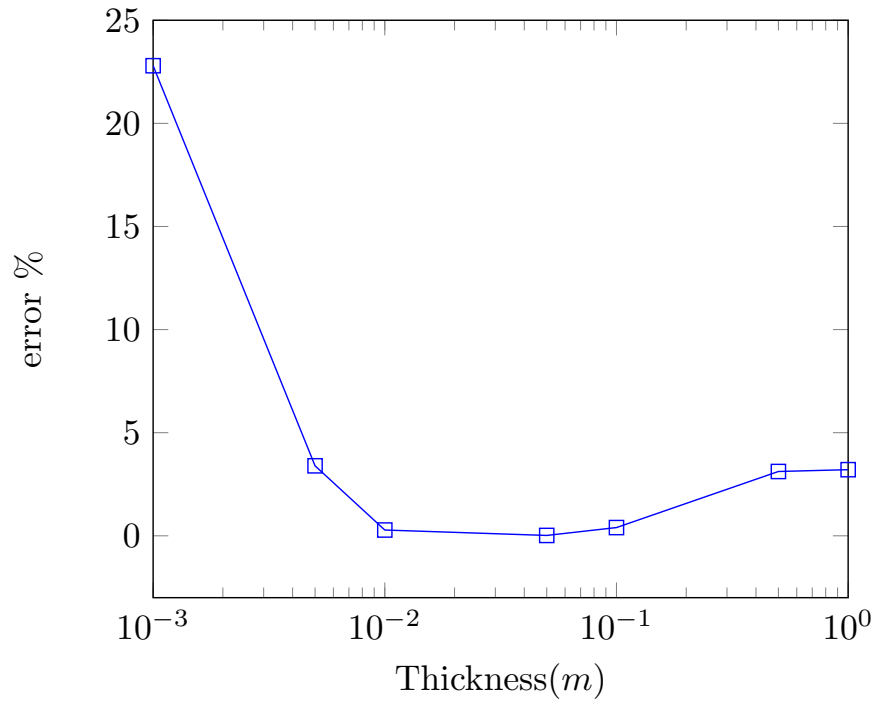
### Result and error analysis :

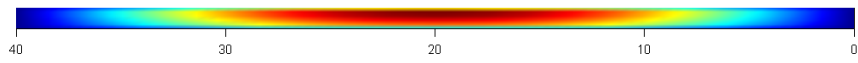
Table 15: Input Data

Material Property		Geometric Data		Loading Data	
Young's Modulus ( $E$ )	1E11 $pa$	Length ( $a$ )	1 $m$	$N_2$	$\frac{T}{t}$ $N/m^2$
Poission's Ratio ( $\nu$ )	0.3	Breath ( $b$ )	40 $m$	Tension $T$	3E4 $N/m$
Density ( $\rho$ )	7810 $Kg/m^3$	Thickness( $t$ )	{0.001,0.005,...,0.5,1} $m$		

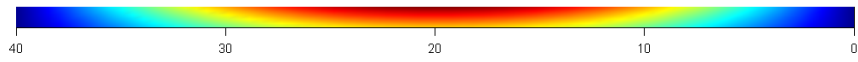
Table 16: FEM and Boundary condition data

Direchlet Boundary				Loading Conditions	
Geo -Entity	$w$	$\theta_x$	$\theta_y$	Geo -Entity	$N_2$
line {1,3}	Fixed	Free	Free	line {1,3}	$\frac{T}{t}$ $N/m^2$

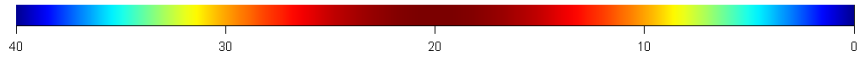




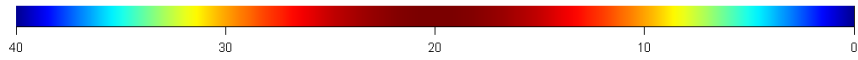
(a) Mode Shape 1 for thickness = 0.001 ( $m$ )



(b) Mode Shape 1 for thickness = 0.01 ( $m$ )



(c) Mode Shape 1 for thickness = 0.1 ( $m$ )



(d) Mode Shape 1 for thickness = 1 ( $m$ )

Figure 24: Natural Modes of a rectangular strip