

24.1 A 24-to-30GHz Watt-Level Broadband Linear Doherty Power Amplifier with Multi-Primary Distributed-Active-Transformer Power-Combining Supporting 5G NR FR2 64-QAM with >19dBm Average P_{out} and >19% Average PAE

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The continuous worldwide demand for multi-Gb/s data-rate has driven the rapid development and standardization of 5G New Radio (NR) specifications in the mm-wave bands [1-3]. As a result, there is a surge of interest in high-performance yet compact mm-wave 5G front-end chipsets to enable large-aperture phased arrays. In User Equipment (UE) devices, the limited form factor restricts the number of antenna array elements, e.g., 2x2, which dramatically increases the output power (P_{out}) requirement per element [1,4]. For base stations, although some applications require only moderate element P_{out} and high antenna gain, high P_{out} capabilities allow array-divisions/sub-arrays for concurrent multi-stream mm-wave links.

However, generating high P_{out} at mm-wave necessitates high-efficiency power amplifiers (PAs) and judicious power combining in low-breakdown silicon processes. A few silicon high-power (>26dBm P_{out}) mm-wave PAs have been reported but with limited linearity and average efficiency (PAE_{avg}) due to the unbalanced impedance across ports and/or limited passive efficiency [4-8]. In parallel, high-speed spectrally efficient modulation schemes, e.g., high-order QAM, OFDM, and carrier-aggregation (CA), will be widely used in 5G, leading to high peak-to-average power ratio (PAPR) waveforms [1-4,9-11]. This makes both PA peak and back-off efficiency values highly critical. To support 5G multi-Gb/s high-PAPR signals, outphasing PAs require substantial baseband computation and DPD overhead [9]. Although Doherty PAs potentially support large modulation bandwidths with low baseband overhead, existing mm-wave Doherty PAs in silicon exhibit limited efficiency and P_{out} mainly due to lossy and complex on-chip Doherty output networks [2,3]. Hence, mm-wave silicon PA solutions with high power, high linearity, and high peak/back-off efficiency still remain elusive. To address these challenges, we introduce a fully integrated watt-level broadband linear Doherty PA with multi-primary distributed-active-transformer (DAT) power-combining to efficiently support multi-Gb/s 5G NR signals.

Figure 24.1.1 shows the design of the proposed broadband power-combined multi-primary DAT Doherty output network. The equivalent network and the transmission matrix show that a transformer can be designed as an inductive impedance inverter after the capacitive loadings resonate out the remaining inductances ($L_{12}M/L_s$ and $L_{12}M/L_p$), resulting in an impedance inverter with the characteristic impedance of $Z_0 = 1/Y_0 = \omega L_{12}$. Schematic simulations verify that this one-transformer network indeed achieves ideal Doherty active load modulation. We propose a multi-primary distributed active transformer to achieve simultaneous series/parallel multi-way power combining. It achieves series power combining between Primary #1 and #2 as well as between Primary #3 and #4; meanwhile, it achieves parallel power combining between Primary #1 and #3 as well as between Primary #2 and #4. Furthermore, to enable multi-primary DAT power combining in both main/auxiliary paths and broaden the carrier bandwidth, an impedance scaling network, composed of two impedance inverters, i.e., one transformer-based and one capacitor-based, is inserted in the auxiliary (Aux) path. In practice, the two negative capacitors ($-C_i$) are absorbed in the two shunt physical capacitors (C_{s1} and C_{s2}). Finally, the one-transformer Doherty output network is extended to the proposed multi-primary DAT configuration at both main/auxiliary paths, achieving high-efficiency power combining and desired Doherty active load modulation simultaneously. Four differential main PAs (Main 1 to 4) and four differential auxiliary PAs (Aux 1 to 4) are respectively combined in a DAT fashion with series/parallel power combining. The layout of a multi-primary transformer is shown in Fig. 24.1.1, where the multi-primary coils are implemented using two top metals and the secondary coil uses the second top metal. It also simplifies DC supply feeding and layout integration with PA cells.

Figure 24.1.2 shows 3D EM simulation results of the proposed broadband power-combining multi-primary DAT Doherty output network including custom MOM capacitors (the layout is shown in Fig. 24.1.3). Simulation results ($f_c=28$ GHz)

verify that the proposed network achieves highly desired Doherty active load modulation, in that all the single-ended complex loads for all 8 main/auxiliary differential PAs are well balanced and symmetric across all power levels. This achieves the multi-way power combining and desired Doherty active load modulation with >81% total passive efficiency (<1dB loss) at 28GHz. Simulations also show that the proposed DAT Doherty network supports broadband symmetrical operations for all 16 main/auxiliary ports over 24 to 34GHz at both 0dB (peak P_{out}) and 6dB back-off. More than 80% total passive efficiency (<1dB loss) is maintained at 0dB and 6dB back-off over the entire Doherty load modulation over 23.8 to 29.2GHz.

The proposed broadband power-combined multi-primary DAT Doherty PA is prototyped in a standard 0.13 μ m SiGe BiCMOS process (Fig. 24.1.3). The PA and driver stages employ common-emitter amplifiers with sizes of 2x6x8 μ m and 2x2x12 μ m, respectively. Neutralization capacitors are used at the PA (55fF) and driver (32fF) for gain and stability improvement. RC pairs at the inputs of the PA and driver further enhance stability. Figure 24.1.7 shows the die micrograph. The PA occupies 4.19mm² total chip size and the core area is only 1.35mm².

The chip is wirebonded to an Aluminum PCB and probed for measurement. Figure 24.1.4 shows the small-signal S-parameters and large signal continuous-wave (CW) measurement results. The peak S_{21} is 23.2dB at 24GHz with a 3dB bandwidth from 22.0 to 28.5GHz. The input matching is <-10dB from 23.2 to 34.0GHz. The PA CW tests demonstrate Doherty back-off efficiency enhancement over the 23 to 31GHz P_{sat} 1dB bandwidth. At 24GHz, the PA achieves 37.8% peak PAE (PAE_{max}) with 28.2dBm P_{sat} and 37.8% PAE at 26.6dBm P_{1dB} and 27.8% PAE at 6dB back-off from P_{sat} . At 28GHz, the PA achieves 30.4% PAE_{max} with 28.3dBm P_{sat} and 30.2% PAE at 26.8dBm P_{1dB} and 21.2% PAE at 6dB back-off from P_{sat} .

Figure 24.1.5 shows modulation tests using single-carrier 64-QAM signals and FR2 5G NR signals. For 200MSym/s (1.2Gb/s) single-carrier 64-QAM signal, the PA achieves 21.3/20.9dBm average P_{out} (PA_{avg}) and 24.6/18.4% average PAE (PAE_{avg}) with -25.4/-25.0dB rms EVM at 24/28GHz. For 200MHz 1-CC FR2 5G NR 64-QAM signal (9.64dB PAPR), the PA achieves 19.1/18.1dBm P_{avg} and 19.0/13.8% PAE_{avg} with -25.2/-25.1dB rms EVM at 24/28GHz. For 200MHz 2-CC FR2 5G NR 64-QAM signal (11.84dB PAPR), the PA achieves 17.9/17.5dBm P_{avg} and 16.2/12.9% PAE_{avg} with -25.6/-25.5dB rms EVM at 24/28GHz. Moreover, for 800MHz 2-CC FR2 5G NR 16-QAM signal (11.78dB PAPR), the PA achieves 18.2/18.7dBm P_{avg} and 17.4/16.6% PAE_{avg} with -19.3/-19.4dB rms EVM at 24/28GHz.

In summary, the proposed watt-level broadband linear Doherty power amplifier with multi-primary DAT power-combining achieves high P_{out} and high peak/back-off efficiency simultaneously. The prototype PA demonstrates the highest P_{out} among reported 28GHz Doherty/outphasing silicon PAs in [12] and the highest PAE at peak/back-off among mm-wave high-power silicon PAs in both CW and modulation operations in [12].

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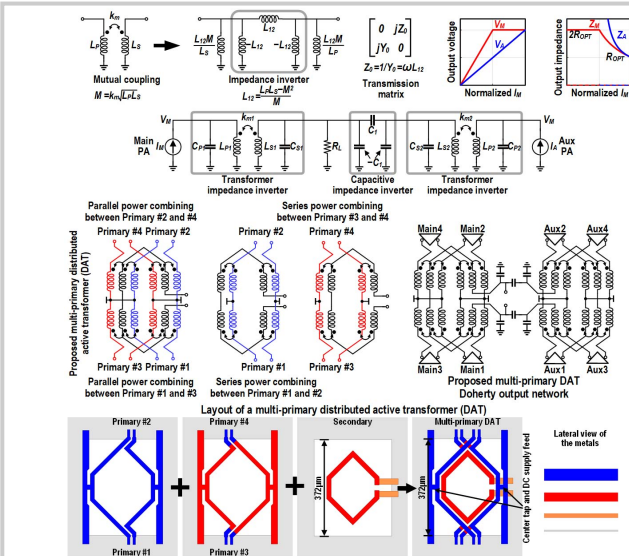


Figure 24.1.1: Design of the multi-primary DAT Doherty output network.

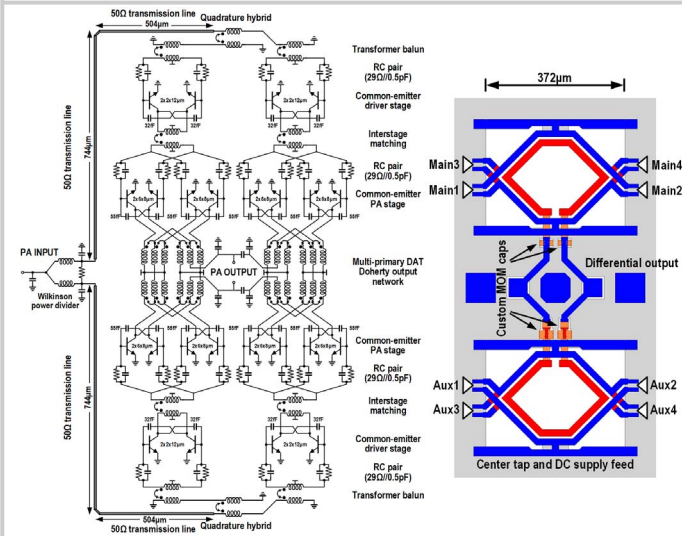


Figure 24.1.3: Top schematic of the prototype PA and layout of the multi-primary DAT Doherty output network.

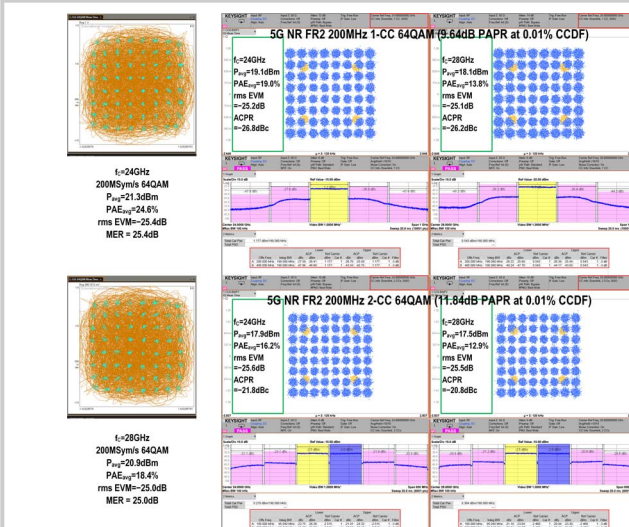


Figure 24.1.5: Modulation measurement results with single-carrier 64-QAM and FR2 5G NR signals.

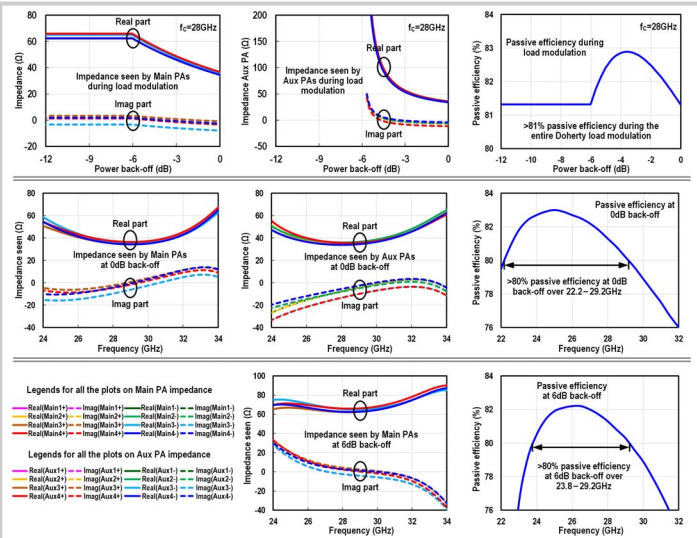


Figure 24.1.2: 3D EM simulation results of the multi-primary DAT Doherty output network.

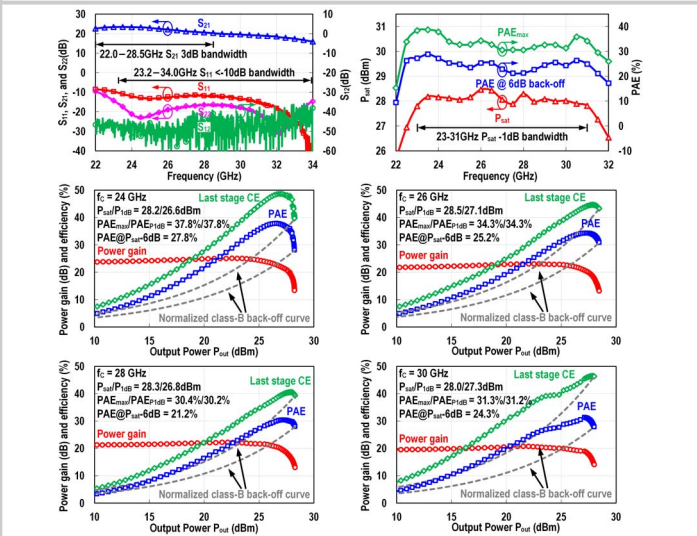


Figure 24.1.4: Small-signal S-parameters and large-signal CW measurement results.

Comparison with recently reported mm-Wave PAs in silicon

	This work	[4] Dasgupta, RFIC '19	[5] Nguyen, ISSCC '19	[7] Bhat, TMTT '15	[8] Datta, ISSCC '15	[2] Wang, ISSCC '19	[3] Hu, ISSCC '17	[9] Rabat, ISSCC '18	[11] Li, ISSCC '18	[10] Shalib, ISSCC '17
Technology	0.13μm SiGe	28nm CMOS	45nm SOI CMOS	45nm SOI CMOS	0.13μm SiGe	45nm SOI CMOS	0.13μm SiGe	0.13μm SiGe	0.13μm SiGe	40nm CMOS
Architecture	Multi-Primary DAT Doherty	Cascaded Asymmetric DAT	4-stacked Dynamic Load Modulated	Digital 8-way Modulated	Mixed-Signal Doherty	Multiband Analog Doherty	Trivial Balun Outphasing	Continuous Class F-1	Dual-Resonance Transformer	
Supply (V)	2.0	2.2	2.0	4.8	5	2.0	1.5	4	1.9	1.1
Freq. (GHz)	24	28	39	60	42.5	46	27	28	28.5	27
Gain (dB)	23.6	20.5	38.0	24.7	19.4	13	19.1	18.2	14.0	20
P _{out} (dBm)	28.2	28.3	36.0	30.1	27.2	28.9	23.3	16.8	23	15.1
P _{1dB} (dBm)	26.6	26.8	21.5	26.5	24.0*	N.A.	22.4	15.2	N.A.	13.7
PAE _{max}	37.8%	30.4%	26.6%	20.8%	10.7%	18.4%	40.1%	20.3%	41.4%*	33.7%*
PAE _{1dB}	37.8%	30.2%	13.6%	15.4%	7.5%	N.A.	39.4%	19.5%	N.A.	31.1%*
PAE@6dB back-off	27.8%	21.2%	10%	7.0%*	4.5%	11%	33.1%	13.9%	34.7%*	15.1%
Modulation scheme	64-QAM	64-QAM	64-QAM	N.A.	ASK	64-QAM	64-QAM	64-QAM OFDM	64-QAM	64-QAM OFDM
Data rate (Gb/s)	1.2	6.2	0.6	6.0	N.A.	N.A.	6	6	0.48	9
EVM(dB)	-25.4	-25.0	-28.5*	23.4	N.A.	N.A.	-25.3	-26.6	-30.5	-26.8
DPD	NO	NO	Yes	NO	N.A.	NO	NO	Yes	NO	NO
P _{avg} (dBm)	21.3	20.9	19.0	23.0	N.A.	15.9	7.2	14.3	10.7	6.7
PAE _{avg} (%)	24.6%	18.4%	8.3%*	5.2% PAE	N.A.	N.A.	29.1% PAE	25.3% PAE*	21.4%	11%
Area (mm ²)	4.19 (1.35†)	2.96 (0.945†)	6.6†	4.16	13.7	2.87 (0.52†)	1.76	0.56	0.29†	0.23†

*graphically estimated †last stage CE †1-stage PA core area

Figure 24.1.6: Comparison table with recently reported mm-wave PAs in silicon.

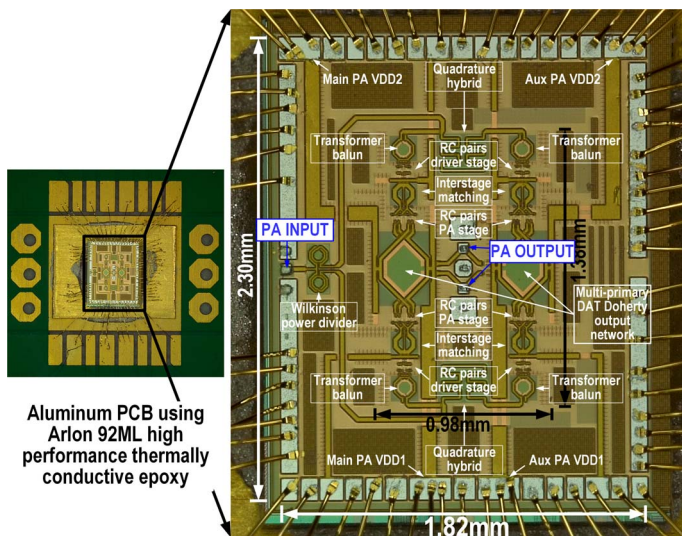


Figure 24.1.7: Die micrograph.

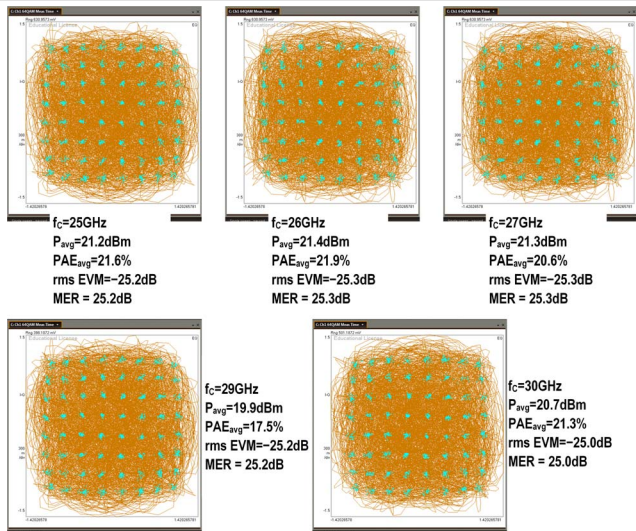


Figure 24.1.S2: Modulation measurement results with 200MSym/s single-carrier 64-QAM signals.

Additional References:

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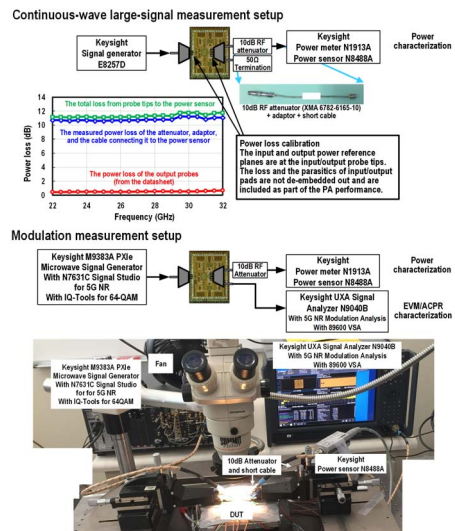


Figure 24.1.S1: Large-signal CW measurement and modulation measurement setups.

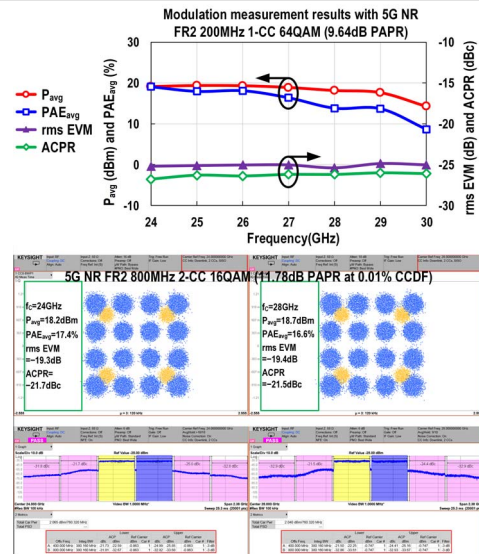


Figure 24.1.S3: Modulation measurement results with 5G NR FR2 signals.