									1000		MEN.							jir.							3 1			1	Ļ	1			
		0.					T					3	ams	cin	7 7	Ted	hoigh	10	13	a	TO	ent	4.2	2.35	1								3
		رم											F		+		V	-		*													
		3 =														1.1														12			- W
NE		2 de		0			412			40		^			0		-4	9			r	(4	S		1	+		/1			v		->
4		15	-	e	1		200	-		n	-1	U			۲			V					3		72.0	100		u)			
			36'3								14 12															r	1.0			5	16 12 6		
																														221	16 65		
		3	37 5	16 17	7-3	14 17	12	1-5	23.5	13 43	15'4	12	18	22.7	13	3 8	21.0	17 6	18 3	13'7	15 6.0	21.	2 13	55	216	17 5/3		T	11+3				
		4	23.3	5 5	5.7	19'5	15	45	- 1	T 3.6	17:5	13	30	18.8	14	3.5	28.5	16 13	6 9	1517	14 7	26.	5 16	8.8		7 10-1		T	19.1	-		-	
*																														27.0	17 10 3		
																															16 11-9		
			000																												16 8 h		
		7											100																				
		8	15 '5	/5 3	3.6				28.5	18 8.9	21 16	16	2 5	31,4	14	19.7	261	16 5	3 4	(4) 3	10 %.	2/	/ //	10 8		F	14.6	. 13	1.3	20.10	16 10.5		
	(9	18 '2																												16 87		
	¥ 1	0																													15 8 1		
	1	11																													14 6.9		
																															20 29.1		
																															10 0-4		
																															17 10 8		
0	1																																
																															17 16-5		1
																															13 55		
1	1	17	11 '0	14	1.5	27.0	16	70	22.4	15 57				2716	16	9.4	15 0	13 2	1 2	6'4	17 8	7	ηı	5-3	27.3	18 14 B	23'1	14	25 h	34'4	16 207		
ì		18	22'0	15	4.6	1310	14	2.7	2116	14 4-5		TI	22	2115	14	5.0	4182	18 21	0 3	35.0	17 11	20	1 16	57	250	17 12 8	32.0	16	13 4	33.7	18 146		
																															16 72		
																															F 13 0		
		21	21.40	1	2/	20.0	15	1. 1.			9210	15	5.3	,	7	1, 9	20.2	2	9 3	35 13	F 16 15	1 2).	0 /11	3.6	2/1, 7	15 93	2773	16	96	25 .2	17 90		
																																	9
	2	22		7' 1	1.2	2413	10	8-9	206	17 7-3	21 2	17	b G	201	F	24 S24	14.7	15			11.	24	7 , 1	10.4	3 .0	13 216	41.0	746	.6-2		16 8.9	3 -	
1 1	2																														77 13 3	1	
	J 2										267																			B	T 6-2		
	2	25	32'5	18 /	4.5	24.0	15	43	22.7	14 55	20'6	16	5.0	39'0	16	57	13 '7	11 3	0 3	34.4	17 12	40.	2-16	16.2		F	23'8	14	46	86.5	16 7.7		
(6)																												18	260	38.0	16 173		
																															18 20.3		
Y		24	9517	1/-	11-	26.0	11	מ ת	ריפם	1/0	24'8	16	9.1	3/1.2	F	He h			12	7.9	F 16 10	, 37.	0 20	93.0	27.6	16 5	28.9	17	4.7	-		-	1
		26	\$D /	10	5	2415	10	7/	1017	10	91.6	17	0.7	15.0	15	1 3	15:0	13	0	11.13	14	2				77	2 21-12	F	7-1	10.7	F 20.0		
		29	26.8	1-1	1.6	30 5	10	1.4	10.3	10 13	26 0	1	717	0000	15	5.4	2012	F	1	4 5	F		4		1,1	F	20 3	F	110	2/10	19 30.9	* L	
		30	30 17	17: 1	11-1	19.2-	14	3.1	3216	17 12 ··	30.3	17 F	10-7	24'7	F	5 2	DU L	11 10	1	-	F	(1. d)	9	7 10	44'6	/=	A	F			17 12.9		
		31	24'2	16	99	18.0	15	1418	37 4	18 250	3 3	17 F	15.6	43.5	17	22.7		F			F 141										17 9:0		
		32	2317	15	6.5	6.8	9	0.5	27'7	17 13	33'1	16	12.6	19.7	15	4:1	49'/	14 311	12 4	10.3											17 8.7		1
		33	7 .8	7:	1.0	21'5	15.	6.0	17.0	14 25	18 2	16	5.0	26:3	16	6.8	28.8	16 10	2 2	10.5	16 19	431	5 17	202	37.5	18 143	29.2	17	11:6	33:0	18 148		72 X 4
																															18 156		3
		35	28 16	F	1. 0	28.5	F	1118	-		2318	110	6.5	911	12	1:0	301	16 11	-2 /	1.0	13 %	1 1	Tr	4-3	23.8	14 61	25'3	16	106	28.7	18 11.7		
																															17 51		
		36	20'7	15	60	11 2	E	10	20.3	15 5	11.1	1.1	111	140	11	2 3	90.7	110	17	-0 3 1	14 /10	10	0 14		1013	11	3/ 8	F	0	S D	F		7
		37	26.1	14	6.8	35'3	17	170	19.7	13 4		F		77.0	16	44	28./	F	3		T 15	24	3 1/5	64	74.5	16 7 :	20.0	17	9.1	24'2	15 4.4		
	1																														15 6.5		3
																															17 7.7		
		40	31.0	17	82	27.8	17	11:5	21'6	15 60	20'3	14	3 17	27'2	16	10-1	18 18	15 h	-9 2	15.0	16 5	30.	7 15	10.5	36.1	17 158	29.7	17	10.0	19.6	17. 46	-	4
				L								/-			11.0																16 54		-
	-	62	24:0	Me	2.0	112.1.	17	20.3	39.10	F8 211	7	7	4.7	19:7	15	3-6	27:5			#	12 1					16 Q	1913	13	39	38.2	17 12.4	1	

		13	400			39.4	17	16.5	15'3	15	3.7	21'3	15	5.3	26.7	17	7.9	26 10	18 13	3 9 2	919	16 13.	0 2	1.1	16 6.9	25.3	1/2	7:6		T 10	. 9 :	30'3	17	2.6			43
	1		21 '3	12	0.0								-				4 .								F				33.8	E	E		F				44
	L	15	24.0	15	61	25.5	16	6.7	-			28'6	17	8.3	33'1	17	16.0	30.5	19 11	3	6.0	F 17 11:	5 3	7.0	18 19 B	30 2	17	13.7	33.5	J8 , 13	7	433	18 =	24.9			45
	L	16	*	T	6.4	25.7	17	10.8	30.7	16	15 1	26'7	15	5.5	4713	17 2	14.5	29.8	15	29 20	7'4	17 13	3 /	7'2	15 37	31.8	19	11-4	25.4	16 8	7 :	30.2	18.	108			46
H	4	7	30:3	17	8.4,	27'7	17	7.6	28.0	15	8:1	36.3	18	19.0	20'7	15	49	22.1	15 3	2 2	3.5	7.	7 2	3'4	17 68	39-7	19	18.9	25.0	16 8	2		F				47
	4	46	21 .0	14	4.1	27'4	17	9.5	321	18	16. 6		77	7.4	28.7	17 /	13.5	23.5	5	1.4 2	5.8	16 9.	4 2	5.6	17 82		77	17.2	32.5	18 15	.3	29.7	17,	4.5			48
	4	19	24'6	17	8.6	251	1 5	8.9	27.3	14	72	-	T	3-/	9.6	12	1.4	16.8	15 3	3 8 1	5.4.	16 3	5 3	20.2	17 10.2	24-6	15	4.3	50.3	14 5	2	23.2	14	6.5			49
<u>U</u>							_										*					F			17 13-5	4		Deal Co.	4	9							50
- 10	9	1	37.1	17	14.7	30'5	17	11-0	30.0	17	11/				14.7	13	24			3	115	17 12	0		7 21	21.7	15	47	2513	16 10	.0	20:4	15	6.1			51
				F		9																	75								-11						52
			32.0	15														- 0				_			13 3-1	4	-			- 4		-					53
		4															*						100		12 07					F							54
		5							1								1. 14		50						14 3 8			- 75									55
		3	85.8	17																			- 1											80	Hi		56
		7	,, _	,,					1												X		- 1			A. C.									-		5/
		8																							15 2.6	1			1					- 1	27		50
	-77	0		T						31										- 381			5.34		16 51		+		1				T 1.			- A	60
		1							1														-		14 20			-57			,		1	i		The state of the s	61
	411		19.3	15					4							C .									15 32	1 110			W					i			62
		3	77 5	70																			1 1		13 4.7				1								63
			32.2	16																100					16 59				A					3			64
		5															-1/								14 17								1-0				65
			3613	17	16.8	27:5	16	97	28.8	16	90	16.0	14	4.1	24.4	16	4.9	14	2	1 3	2 3	F 17 12.	4 2	2.3	16 5.7	17.8	14	3 2	29.9	18 10	.5	16.3	14	3 5			66
	6								4									107							17 89				Van de	E							67
	Ь	8	19.6	15	4.3	26.0	1.6	74	14.5	14	3 8	1913	15	5.3	7'0	9	0.4	20'6	14 5	55 2	015	15 h	3 /8	5 '5	15 32	12.0	13	2.5	22:1	17 6	5	3217	17 1	109			68
	· 6																								15 33												69
	7	U	30'0	15	9-2	213	15	525		T	3-8	24.2	15	6-8	18 13	16	6.2	20.7	15 5	5 3 2	7 '4	17 7.	3		•	22 2	16 F	4.2	18.8	15 5	2	24'5	17	4.7			70
	7	1			-	16.0	J																		15 36											-	71
100	7																								16 7/												. 72
																									15 54												73
			18.3	14	4.4			,	11 . 8	12	1 4	1910	15	5-1	10'0	10	1:1	00.	F 2	9 1	8.0	12 2	0 /9	7 13 1	15 3.4	28.3	16 F	87	3217	10 F	.0	26.0	14	67			74
10		5				31.7										-									16 11:11												7/
5							-								N										14 4.4 15 5.4	V	L					-					72
1																									14 5.6												78
		9	X 0 /	73	0.4	28 . 8	F 16	9.3	18:0	15	3-5	35.2	F	16.0	20.2	15	8.9	73/	П 1	2.9 2	8.3	17 7	0 2	1 '2 .	13 4.6	21 2	15	5 3	21:3	14 1	9	25.8	16 1	10 8			79
	8	0	1010	12	1.4	30:7	18	15.0	13.3	16	3.0	12 1	14	0.5	15 '0	14.	24	22 17	160	6.6 1	7.5	14 2	8 2	5 6	16 53	21.9	15	4.5	8 19	10 1		24'6	17	6.7			-80
		1 2		ידי	4.2	27.2	16	9-8	25.2	16	6.2	11.2	12	1-4	27'7	17	10.3	24.2	15	5.7	1	71 5.	7 2	4'3	15 5.6	22.4	18	51	3918	15 21	5	22.5	17	6.2			81
		12																							14 3.0								UET E	-			84
	8	13	35.5	16	14.5	38.5	18	16-2	33.7	17	15.6	16 8	13	2.4	, i	T	65	17.5	14 3	3-6 2	6'5	17.6	4 1	7.0	14 45	10 .8	1/	1-4	25'9	16 8	.3	23.1	17	7.7			83
~	8	4																19.5											28'8								84
								-										~		1			J					N.					1				***
										8									- 10	. ,			,	e e				4			1						
										92	(90)								4		So.								a de la companya de l								1
					~						9	THE PARTY OF					- 2			3								100		16						1	Mary -