	1 3	1.		10-	7												5	am	ph	inc	17	ec	lue	igu	e	. C	3a	P	to	ent	7.	1.3	5.												٧,				
01 -	land			<	K			,				pun									_				1																							1-1	
NE	2	-	#	=	+		ļ.,	*				~	\			#	¥ ¥			-	2		E		PA			3	Q				R			5	5			T				U					. 3
	2	14-	7 11	B. 1	5.10	13	'S	105	-11-	30 1	2.8	8	3	85	11:3	3 8		3.85	17	8	105	7:6	-5	7.0		-	11	8	75 -	7 45	1/			an	12-2	(1)	R	0.1	10.5	₹				*	-	4	-	7	> S
	2	18.0	0 0	13 1	0 05	/5	0.0	11B	14	50 1	6'0	10	\$ 10	80	13.8	10	05 6	2.00	8	7	8	3.7	5 1	7.3	123	990	.16	1 10	BI	1:15	19.	7 10.	BILL	90	15.0	9	יאו ם	90	10.5	8	4:0	5 /.	3 .8	7	5	60			
	4	// 3	0 10	5 1	6:00	10	15	8	4	00 1	14.0	77	7	30	15.6	T6	_ 8	80	7	5T	7	2.6	0 1	8.8	1/5	12.90	-				14	5. 9	S 9.	45	1202	11 1	3 1/1	90	0 7	0	3:1	0 1	3.2	101	3 7	90			
	5	12:0	2 10	> R ,	0 44	- 13	.0	14.0	1	15 6	6.5	95	5 11	-35	16.2	10	5 7	-30	12:	5 9	75	7:1	5 1	7.50	IB.	8 70	16:	5 10	28 1	3:455	16:	7 111	3 11	.00	13:5	115	5 /4	95 2	9.5	IIB	2		7.3	75	5	25			
	6	6.0	9 8	Q. <i>I</i> .	1.0	19	0	100	7:5	25 2	2.8	11.13	20	70	16.2	111	3 8	35	12	0	115	10.0	5/2	R-2T	8	640	9:	775	7	3:80	// .:	5 8	3.	15	9.8	79	١.	165	6:2	115	16.5	15 11		115	8.	30			
	7	1/0.0	110	- 12	2.10	104	, 8	110	()	40 /	3:3	1.8	- 9	85	17.4	10	S 13	1.85	9,	7T	10_	3.9.	5 10	(13)	15	4 25	14 .	5 10	10 8	1:95				-	9.8	11	4.	50 2	0.5	IIB	19.0	5 11	1.7	100	.4.	00			45
	8	17.8	111	3 11	15	_			-	2	3.1	1113	20	40	221	11.	5 29	-45			12	7	15	5-7	0	0.30	18:	0 12	BIT	7:70	14'1	10	5 8	15 1	1.9	105	7.	80 1	8.3	IIB	9.9	5 16	7	118	0.	30			
	9	17.8	78	, ,	- 55	14	.4	IIB	10.1	A 9	9-7	19 13	15:	30	249	12	32,	1.85	18	7	IOB.	11:4	0 /3	5	IS. I	10 65	10:	7 8	2	2.90	18.5	10	. 12	75 1	12:0	105	3 7.	60 1	6.7	11 B	14.7	5 17	2,5	115	10.	20			
	10	9:4	101	3 15	.30	17	3	II B	10 0	10 1	0.0	115	2.5	80	217	12	B 23	75	16	7 9	2 6	8.3	0 11	.5	3	4.95	14.3	9.	S	.40	<i>/5 '</i> 3	111	3 10.	65 1	4.1	8	4:5	50	9.8	10,5	4.2	5	٥	" "	10.	95			
	t/	17:5 13:2	101	3 7	3.5	11.	1.	105	5.	70 3	0 2	IIR	10	75	10.0	101	13 11	. 15	9 12) /	05	5.15	2 /	14 1	13.1	8.65	12.0	9.	S 5	10	11.6	95	5	15 2	5:0	11/3	29	15-1	1.37	8	4.0	0 14	1.8	95	7.	20			
	12	13:2	11 [3 15	:60	16	5.1	OB	9.6	10 /	1.8	115	L	ot:	16.0	101	3 11	115	1217	TY	03	4.25					11.0	8	4	.20	16:8	100	3 11.	30 2	0.0	115	8	35 18	6	11 3	10-5	5 15	. a	105	10.0	5-			
	13	18:0	11 8	10	00	21	2	//B	18 1	5 1	7'3	IIR	9.	110	12.2	100	6	.55	10 1	9 10	2	8 2	5 5	5 8		2.35	16'	2 703	5 9	15	11 .6	9	5	10 2	1.7	II B	15.9	5 2	2.0	10B	15:3	07	.77	1 0	5	15			
	14	12:5	1/5	12	95	-				15	514	MB	11.	30	13-2	91	2 10	50	/5 0	2 10	05	90	4	5 7		1 55	5.3	7	2	25	14.5	1/ 13	13 1	0 1	6:2	115	13.2	5			-	24	.0	II B	20.9	30			
	15	215	105	3	20	16.	8 8	23	8.9	5 21	1.8	IIR	19.	15		/(1. 10	.30	10%	2 8		6:66	12	8 10	- 1	4.80	411	7	1	30	16:4	115	14:0	00 22	2 /	113	19:2	5 14	0	113	15:80	23	.7	11/3	20.2	45			
	16	11:0	1/5	8	30	14.	8 /	OB	9 9	5 /	5:2	8	J. 1	-0	14.7	110	-	5.4	14.00	2 4			//	10/1	5 7	7:40	17.8	10	B15	.50	16.2	11 3	12.5	0 1	3.5	115	8.3	0 -				15	.6	95	7.4	10		12	
	17	16:0	IIS	20	05	16.	1	213	17.6	0 11	4.3	10 5	5	KO KO	12.0	מנו	. /	20	14	5 /0	الم	8 40	10	7 ()	S	7.15	5:0	6	2:	25	17.6	95	10.5	5 11	7.2	9	3.0	5 /4	.2	II B	8:20	15	.7	128	8.9	5-			
	18	1911			-	15	7 /	05	7.6	5 21	1.0	110	15	5.5	ס: כו	1115	1/	0.5	11.10	, ,	, R	2 4	123	-		5:95	6.2	9	0.	80	16.3	1113	11:19	5 /	6:2	12B	15.6	5			-	2)	.0	1113	12:1	4			-
	19	22:0	11 B	20	00	13:	7 9	s.	7.9	5 15	10	105	10.	30	11.5	105	13	10	14:7	_ //	D 1	3:75	15	7 9	SIG	35	9.9	1/3	5 6.	55	9.2	95	6.0	0 1	3:3	95	5:7	0 15	0 1	25	11:20) //	7	105	5-14	5-			
	20	22:0 14:6	95	8	15	17:0	3 //		23.8	0 111	17	INR	Q:-	00 /	8.6	IND	, , ,	of	10 +9	/va		0 "	13	7 11	S /1	80	14.2	103	5 7.	80 1	7.2	128	10.2	0 17	7:7	IIB	13 8	5 14	7 1	05	9.35	17	9	12 B	15.4	5-			
	21	14·6 23·2	IIB	17	15	14:3	2 9	5	5.9	7		70 70	u .					DOOR PHILIP		1 8	-		180	D CO	W 11	100	/ JE O	1/3 4	5 (7)	0111	n 1/1	$T \sim C_{\rm b}$	T	35 B 8		11 1		100 a 44	F 1										
	22	15:7	115	12.	60	14.5	719) "	4:70	21	.8	1113	16:	4	-2	115	40	4	10.0	- //	DI	163	1/8	4 10.	5 13	.80	11.7	//S	5.	25 10	7'3	128	17.0	0 22	7	1313	23.6	0 19	7 12	2131	7:60	//	3 10	08	7.9	0			
	23	15:7	- 7	. 4	35	11.0	5 8	3	3.5	2 15	'5	IIR	9.3	5 ,	4.7	IAR	15	27-	1311	11.	15 1.	2.05	14	8 14	S 10	90	13:4]]	8.	40	9.7	95	6.6	0 8	77 70	7	5.40	0 21	2 1	13	11.10	17 .	7 1	IB	11.7	5			
	24	6:2	7	2.	50			-	-	19	0	IDB	14.2	5 9	6.1	133	47	35	10.4	7	5	10	10	4 10	5 9	.70	14.8	10	7.	30 1	1:7	105	7.4	5 11	.7	95	4.80	18	71	05	6.85	13	8 /	B	9 74	-			
	25	230	ILB	24.	85	1-			-111/2	23	·8	11 12	20.2	0 1	9.1	IAR	9	20	0.0	9		- 645	12	- 04	- 2	40		1	4.	15 /	4 17	95	5.75	> 11	:7 /	0	6.95	13	2 11	os .	5:15	18:	3 1	2R.	9.30	,			
	26	20.2	108	1/0.	75	221	7 - 11	B	a. 57	10	0	9	5.0	5 ,-	2	an	10	2 -	// 19	10	2		1			20 1	40	7 ~	, 8,	10 1	1.4	105	8:63	5 11	8 8	3	4.00	11:	7 10	os -	7.00	15:	1 8	ns	9:01	-			
	27	26.6	113	27.	25	9.1	7 9	494	515	15	0	, IIS	10.6	0 1	2.2	15 R	19.4	ani	- 0	10	15 1		10	~ (3.5)	-	1	0:0	7	3.	15		2	7	9	.9 9	7	4.00	/3:	2 10	s ·	7.05	15%	5 10	OB.	9.10				
	28	18.1	MB	16	101	13:7	7 9	5	7 35	22	٠2	1/3	18:15	15 2	5.5	12.A	2311	05			-	-		- 100	e (1)	43	13.0		6.3	00 /	3 .0	45	6.25	1/2	2 '	7	5.75	19.	OT 7	7 .	510	19.	2 11	OB I	2.40				
:	29	17:5	IIB	-16:	5	13.9	10	SI	0.35	20	1	II B	14.0	5 1	7:7	inc	0.	02 5-	10.0	10	<i>p</i>		0		3		14 0	100	6.	10				100				16:	3 /0	15 6	85	15.5	5 K	15	9.90	1 1			
	30	17:5 9:7	9 s	5	55	13.9	11	S	8.70	16	0 /	OB	10-4	5 13	5-2	105	8	15	12 '8	10	DI	95	131	1 00	i- 1:	90 1	3:1	7	6.3	30	7:5	10	3.80	12	7 9	7	5.75	16.	1 10	13 8	.40	20-0	0 11	SIS	5.10				
	31	9:7 20:7	103	18.	25	10.2	10	S	1.83	14	4	105	7.9	5 14	1.2 T	9	10.5	00	7 2	19	9	.00	74	90	-4	15	14.7	123	9.3	0 16	.9	10	5.75	8	0 8	}	2.55	15.	1 10	\$ 2	3.5	17/	59		4.55	-			
	32					_	_	_	-	151	1 1	IR	17.70	9 91	.9.	INR	91 7	00 /	11 +1	0	,	70	10			70	A: /	100	4	2 /0	18	75	6.35	5	7.6		1.50	14:	5 10	5 7	:05	14.9	3 11	B	9.10	1 7			
	33	19.1	95	9.9	5	21:8	10	BI	9:45	19.	7 /	1B	14.31	2 2 1	11.	10.12	** /	0 /	7 .30	7 4	-	1.5				20 1	4:3	10 3	0:1	0 16	2.6	93	8.75	9 .	5 7		2 65	12:	0 10	5	.95	15.1	+ 10	5	415	-			
	34	/5·4T 13·5T	9	12.1	5	No to a gamenta		THE THE PROPERTY OF		17:0	6 1	1B	0.81	0	5-	10	50	A 0	100	7 5		1-0	70		-0	00		.7	5:3	0 13	13	8	5.95	9	5 10)	5.05	14.7	7 8 5	5 7	.00	-	-	21 1					
	35	13.5T	8	8.1	01	2.8	10	5 -	7.75	17 .	2 1	IR	9 9	5 13	, h	11B	10 0	10 1	0.5	100	~		10:0		χ.	(0.5)	0	P	3.11	0 1	4.3	1013	8.40	9:1	8 0		3.85	12:5	3 95	S 5	40	20.3	3 ///	3 20	0.10				,
	36	18:0	11B	16 7	0	-			-	17:	1 /	18	14.51	2 12	,3	IAC	7/2	by C	117	0	1	75	100	- O	3 /	7 0 1	, _	75	2.0	3 /4	.8	1013	12:10	10 .	7 8		1 55	12.8	95	5 7	35	16:4	10	5 9	.95				1
	3/	9:3	10 S.	80	0 1	7.2	10	SA	.00	20.0	9 1	IR	9 31	2 17	i i	AR.	10	4 0) . ti	-		20-	1715	1		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		70	10:11.	2 8	OT	8	2.80	15	0 10		6.00	13-3	91	6	30	19.2	10	B 10	7. 25	-			3
	58	7.7	9.	80	01	6.0	99	5 1	.30	1515	5 9	S	7.450	a	. 2	2	1 0	1 - A			,)n -		9 4				3 7	1/	1/	105	5:50	19.0	3 99	5 0	1.00	8-3	9	3	15	20.5	100	3 10	.80			J	3
	37	11.5	75	6.8	011	1:0	105	5 7	25	1319	n 9	9	9:50	12	.0	3.0	, 5	-	112			0.0	1.0	P	0.5	,0 10		1 0 1	12.45	8	'/	7	3:55	11.2	7	-	1:50	13.0	77	5	30	7.0	101	3 9	.50				3
	40 /	3.2	105	71	5/1	6.4	10%	3 11	80	17:0) //	S	1.0	1 7	.1	2	2.2	10	15	4		1.65	110	10	3 .	10	~		1-00	1.1	2 9	'S	5.50	7.8	7	2	:55	16:2	95	6	45	15.3	11	9	. 65				3
	+(-	-	10	9,0	0	1	an	0 11			0 00												0-1	0		7.	2:40	1/3	3 9	S.	7.50	9:5	10	5	.90	19.2	HOP	2 9.	1.5	0.7	00	- 4	100				4
14	12	2 .4	9	51	5 10	ילינ	7.8	. 10	270	13.0	7 /1	5	5.95	13	51	8	4.5	0					1.0	Vac	1	5 12			- 6	10	8 7	:	2.70	10:4	. 10	5 5	.00	13:7	103	8	05	13.2	105	5 4	.35				4

																				12																		3					
	43	118	8 9		3 55	5 11	.0	9	3.	90				+-	16:2	10	5.3	0 19	6 11	5 10	45-1	9.0	25	1. 04	912	a	2.0	1 13 6	2 MC	8 53	0.1	0	lion	0 11	7 1	2 2	1.0					1	
	44	~	101	- 18 8 4	- mari	-100	1 20 2 3 4 4 5 1 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1	nd had as the same	ne ij mare e kil	alongs .	12:	5 11	B -	35	11.2	8	24	0 13	8 10) B 7	60	11:2	95	5 45	131	II B	10.30	9	11 8	3 15	12.5	10	4 30	14.	2 9	13 9.1	45 10	Ŕ·1	1112	11.50			
	45	7.	7 8		1.75	5					13:4	. 9	4	500	7.6	9	2.6	5 13	5 9	S 5	25	8.6	9	3.30	13.7	113	10.20	123	3 10.5	8.30	10 .7	TR	3.9	5 13.	779	9.	40 2	1.1	115	17.05			
1	46	10	d 7	2	8 30	13	/	40	4.	60	19.1	10	5 5	55	9.8	8	3.3	5 10	7 9	S 3.	70	9.4	8	2.40	12.5	913	7.98	11 0	09	4.85	13.0	165	8.9	-	7		- 1	318	93	7.15			
	47	17	6 11	13 1	0.10	14	2	7	5	70	7.2	8	/	95	11.5	10	510	12.	0 11	5 5.	60	11.4	9	3.90	15.5	IIB	3.95	5 15.0	+ 93	7.55	8.7	9	2.98	- 10 5	57 8	45.8	15 1	3:47	8	7.30			-
	48	9.	8 9		2.55	7.	7 /	0	2:	70	18.3	1/1	B 15	:40	146	9E	5.5	5 16.	3 10	5 6.	70	7.7	9	2.55	14.3	9	4.40	13.7	4 105	7.30	11.7	10	5.90	2 12 .	27 8	19	15-15	5.6	105	9 35			
M .	49	10	4 9	\$ 3	3:75	/3.	4 9	75	5.	70	15.0	10	B 9	80	13.8	95	4:10	6	47	7 4.	15	7.57	6	2.70	6.5	8	1.83	5 161	0 1/B	11.60	18:3	2 10 1	18:00	17.	2 11	B 15	70	8:4T	17	3 85			4
	50	13'	1 10	S	6.90	10 .	47	8_	7.	15	12.8	9	3	-53	1513	95	8.3	5 1/4	7 11	S 8.	60	9.0	7	2.90	11:10	9	3.90	9.	9	3.80	11 1	9	3.81	13.	2 91	2 0	20 0	7.10	8	2 34			Ç
	51	101	1 8	S	4.65	11	57	8	7.	25	h-managed by			· · ·	14.0	105	7.10	12.	79	6	10	11.7	95	5.90	110	8	4-55	- 9.1	77	6.35	18:2	8	3 100	17.	0 100	5	25 1	1.3	95	2 20			
8	52	10.1	6 10	s (6.70	16.	3 /	13	9	50	16:4	111	3 14	.40	18.7	113	98	5 10:	3 9	2.	70 /	12.5	8	1.95			-1 00	18 10	105	10.50	12.3	105	5.40	10.	1 10	6 3	35 11	1.0	INC	5 83			
	53	14'	3 9	S	7.75	11.	9/		2.4	30	17.8	#1	5 9	00	15:7	108	8.63	5 13.	8 10	B 10.	10 1	0.07	9	405	12.2	95	4.85	- 22,0	7 /313	22.75	8:3	95	5.35	- 6	07	9.4	20 16	(e)	1117	11.65			
	54	9.0	0 7	2	.65	13.	5 7	1	3	05		,			7.1	9	2.20	14.	7 10	S 5.	30 1	3:3	lis	5.50	1011	9	2.85	15.0	1 105	6.20	12.5	99	1,190	18.	11 101	3 10.0	0 11	9	90	11.65			5
	55	14.1	4 10	S	7.05	9.	8 8	3	3	15	12.7	9	5 5	3.5	8.8	7	2.90	14:	8 95	5 6	00 1	6.2	//	7.75	11.7	9	3.50	15.9	7 9	8.30	12.0	95	510	9 4	+ 10x	2 10 0	- 9	-5	9	2 95			5
	56	5 '3	7	1	. 65	16.	8 10	B	10	45	9.0	9	S 4	.90	17.0	9.13	8 15	11.	0 7	2	95 1	513	9 B	7:10	13.8	115	11.20	11 11	73	2.60	11 8	10.5	5.50	7,0	3 9	3.0	0 9	.3	9	3.30			5
	57	18.8	3 10	3 10	75	22.	5 9	B	12.1	00	12.3	105	5 7	.10	15.7	103	6 65	: 11 1	+ 9	6	25 1	1-0	95	6.75	11:10	85	5.65	17.	5 9 B	9.75	19.11	InR	15.30	111:	39	1, 7	5 9	.7	8	3.15			5
	58	18.8	2 //	3 13	85	20	8 18	B	3/4-7	a i	18.5	111	3 10	.65	10.8	18	5 65	14:	2 10	S 6.0	10 1	1.2	8	2 65	9.7	95	6.15	15.0	10R	9.70	9.9	9 5	1, 90	14	978	L	5 11		9 <	5.15			Š
	59	13.8	3 95	5 5	. 25	7 .	3 7		1.9	10	9.7	8	2	. 65	10.5	95	4.96	14.5	5 /0	S 7.	20 9	3.0	9	3:10	11.0	10	5.25				12-0	7	3.10	10.	59	1.1.	0 8	.9	8	3.11			5
	60	6.5	5 8	2	.20	22-	\ /	013	18.2	5 8	3.3	11 6	3 24	165	18.5	95	4.70	17:2	91	3 8	75	9.5	8	2 40	5.5	7	1.25	11'0	76	8.40	19.1.	95	11.50	10.1	1 0	4.6	0 12	1 +),	9	1, 10			6
1	61	19.0	1/1	3 14	.10	13:	5 10	18	6.9	0 1	4.8	95	6	15	13.8	85	8.85	1911		100	- 8	3.8	8	2 45	9.7	8	425	11:	3 9 5	6.55	19.0	93	10.10	17.9	7 115	3.0	0 17	7.07	8	10.20			6
	62	15:0	1/	S 8	00	13.1	4 11	B	9.4	51	0.7	9 6	3 6	55	14.5	105	7.90	16:3	3 8	2.0	55 9	7.2	8	3:30	131/1	9	6.65	11.9	/05	7.65	9.6	7	1.30	13.2	3 9	ש בו ע	5 19	13	9	1.20			6
	63	9.2	8	3	10	17.0	0 11.	13	13-1	51	7.2	10	5	30	22.8	10B	17.50	12 13	3.95	3 619	15 1	3.0	9	5.05	5.27	4	1.05	15.1	10 5	6.95	16.7	Ins	7.35	12.0	0 8	2 . /.	5 11	1.0	Q	1.30			6
	1 64	-	_	-		19.1	7 10	013	13.4	15 1	6.6	90	3 7.	75	10.5	105	4-25	16.2	10	3 81	15 10	8.6	9	3.85	10.0	8	1.95	11.0	9 9 5	7.65	9-11	h	9.115	- 15.0	3 9	1. 9	5 11	·Q (D 95	4.70			60
	65				7	8.1	11	1	4:13	5/	5.5	105	9.	20	12.6	85	4.95	11 ·L	19	40	5 8	.8	10	3-60	7.5	8	2.60	7.0	8	2.25	8.5	2	3.30	15.1	9	7.1	5 12	1-6	90	E.1.5			6
	66	7.7	8 5	5 4	.50	13-1	9	S	80	5/	6.3	115	3 14.	20	16.7	11 B	9.60	10 .11	+ 10	3.1	0 8	310											3.65										66
	67	10.0	9	4	.30	5.5	5 8		1-2	5 8	87	95	4.	75	13.3	10.5	6.30	800	8	2.7	00 1	0.0	75	4.40	17'3	95	9.00	9.7	105	5.90	9.7	85	1.40	111:0	100	24	0 19	1.10	2	11.115			6
-	68	16:0	100	3 9	05	19.8	3 11	B	198.	5/6	2:2	8	3.	55	14.2	9	5 65	1/3.5	5 118	10.3	0 13	3.5	15	7.25	12.0	105	8:90	12.7	9	7.00	10-6	98	5.05	15.6	8	1.0	5 12	18	INA	7 15			69
	69	21.0	11 0	3 12	70	14.0	9	S	71	0 1	0.8	8	3.	90	13.0	85	520	11 .8	85	5-4	10 16	2.8.	os a	4.20	15.6	95	7.15	12.2	9	5.00	1152	1013	8.85	7.0	1 6	1.3	0 12	,8	9.5	1,30			6
	70	14.7	109	5 6.	70	15:8	3 10	20	10.9	011	1.7	10	4.	90	8.7	8	3 70			1991	8	21	7	2.25	12:3	S	3.95	17:4	115	9.00	10-3	8	4.60	6.7	7 7	9.0	0 7	.6	9	3.40			70
	71	7.8	8	3	65	13.0	9		44	5 !	7:37	7.	3 .	40	2.7	9	6 75	10.8	91	3 6.5	0 1	212	8	3.95	8 2	8	3.30	9.0	7	2.35	8.8	9	3.65	10.1	7	9.1	4-8	9.	8	3.80			71
	72	11 '9	-7	2	85	5.0	26)	1.7	0 10	6.2	10	11.	45	13.5	95	5.65				13	7.8 1	113	3.00	11:5	105	6.80	-			10.9	08	15 60	11 3	3 7	9.3.	5 1	-6	la	1.70			77
	73	15.6	91	3 8	80	6 3	3 8		1.9	0 1	1:07	16	3	25	4.0	6	0.95	12.2	. 9	4.5	010	5 9	S	2.80	12.4	8	5.65	11.0	105	8.20	16.7	105	7.90	12.0	9	3 8	5 1/1	0	3	3.75			73
	74		-			14.6	91	B	8:4	5 1	3.0	95	7.	60	10.1	9	4.65	13 .7	10 5	6.4	10 8	15	7	3-25	15.7	95	8.20	10-8	8	3.65	7'3	7	2.50	15.3	10	10 11	2 114	.7	115	800			74
	75	10 5	8	3.	80	15:2	8		6.5	0 10	4.9	9	5	15	8.5	IIB	14.25	16.4	10	3:3	5 /7	7.0	013 1	3-30	12.3	95	6.40	8.8	9	3.45	17.3	10.5	9.95	110,0	95	7.0	0 15	6	IR :	3.40	2		75
	16	14.5	7 =	6.	35	132	8		4:40	0 16	9'4	118	10.	30	2.3	115	6.60	8.4	8	22	5		- Harri	-	13.0	95	7.00	7.8	8	1-65	12.5	9	3.65	13.5	108	10.7	5 16	10 1	115	0.50	-off		76
	//	16.8	95	7.	25	10.8	10	S	5.75	5 11	4:4	95	100	45 1	0.7	10	430				lo	16 1	7 :	2.25	7.8	10	2.75	9.9	6	1.65	7.8	7	1.35	10.3	9	411	- 15	.51	108	8-35	11		
	78	14.8	83	4	05	3.8	6		2 35	7	13	7	2.	40 1	2.1	95	5.70	12.5	95	3.0.	5 10	8	3 5	2.00	15.9	108	11.20	7.1	7	1.35	8 .75	7	3.00	15.7	100	9.11	17	81	OR.	8.40			77
	77	14.4	7	3.	115	10.0	9	1	3.45	13	5.2	105	6	0	9.0	9	3.20	18.8	8	5-2	5 15	5.4 /	0B 1	1.60	9.3	9	4.90	13.2	79	8.05	17.9	IIR	13.50	12.5	85	50	5- 1113	· /1 C	13	5.90			79
	80	11.4	42	6.	50	// • //	9		3.90)				*	1.0	105	4.00	9.1	8	3 4	5 12	57 48	0 1	1.80	16.5	105	10-40	9.7	T9	4.95	18.0	115	10 35	1413	913	7:41	0 13	2 9	135	4.35	1		8
	101	11.2	10	4.	75	311	115	5 1	3.80	13	3.3	9	4 5	54	8.3	7	1.75	12.4	85	510	0 11	9 8	P 1	1.30	12.7	9	6.75	15.7	1013	10.50	15-0	95	875	17.8	INR	9 7	2 11	.3 1	15	7.45			81
	02	11.5	102	8	22	12.3	113	S	6.05	18	8.8	1113	13.1	51	5.6	115	6 10	7.0	6	15	07	2 9	1 2	.10	12.7	10B	7.40	12:4	9	4.20	4.1	E	1.65				elon.						82
	8.5	14,5	95	6.0	05	7.6	115	S	4.75	12	5.3	105	7.6	10 1	1.2	95	3.70	10.8	105	7.3	0 -			-	3.5	10	7.65	16.2	105	11.45	9:5	9	3.55	17 -0	1113	8.7.	5.19	0 /	05 -	7 95			8
	84	15:1	105	4	45	13.5	111	8_	6.65	10	3.	8	311	55 1	5.0	115	5.80	16.7	B	10:25	5 14	4 9	5 1	.60	13.4	10B_	7:10	12.8	79	5.30	137	10B	10:35	17.8	95	11:41	5 18	.71	2B /	5.10		, un	84
																					1																		0.35d1,	J_ J_Y.			
										1				1			100				1																4						
			8																											1							R						3