



Analytic Inverse Kinematics

(Date : 2020/08/31)

V 1.1

[KOR]

Rainbow-Robotics

www.rainbow-robotics.com

Rainbow Robotics Inc. owns copyright and intellectual property rights on all contents and designs of this manual. Therefore, the use, replication, and distribution of Rainbow Robotics Inc. properties and materials without prior written permission is strictly prohibited and corresponds to Rainbow Robotics' infringement of intellectual property rights.

User is solely responsible for any misuse or alteration of the patent rights of this equipment. The information contained in this manual is reliable.

The information provided in this manual is the property of Rainbow Robotics Inc. and may not be reproduced in whole or in part without of Rainbow Robotics Inc.'s consent. The information contained in this manual is subject to change without notice.

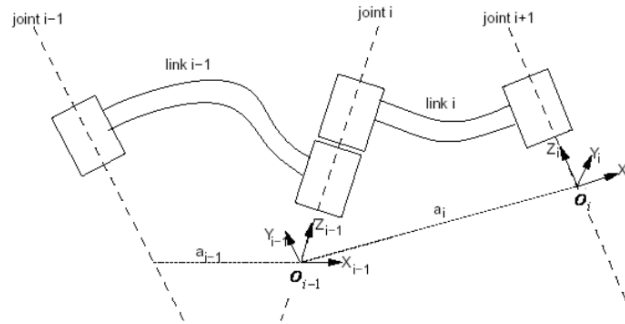
For more information on revising the manual, please visit the website (www.rainbow-robotics.com).

© Rainbow Robotics Inc. All rights reserved

Analytic Inverse Kinematics

Inverse kinematics described in this technical paper uses an analytic method and is calculated based on standard DH parameters.

Standard D-H Parameter

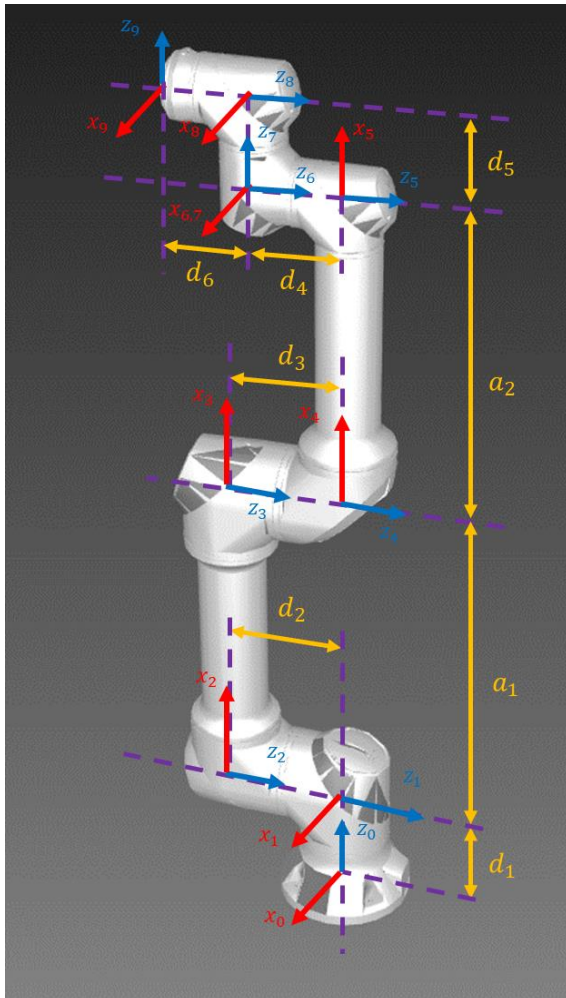


- A rotation θ_i about z_{i-1} axis;
- A translation d_i along the z_{i-1} axis;
- A translation a_i along the x_{i-1} axis;
- A rotation α_i about x_{i-1} axis;

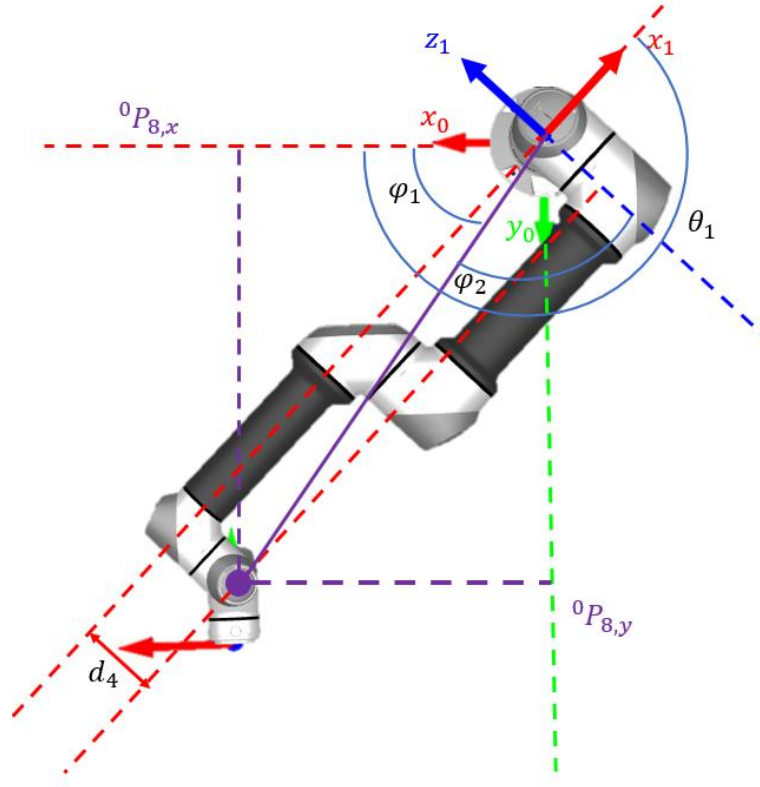
$${}^{i-1}T_i = \begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i C\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0T_n = {}^0T_1 {}^1T_2 {}^2T_3 \dots {}^{n-1}T_n$$

	d1	d2	d3	d4	d5	d6	a1	a2	
RB5-850	169.2	148.4	148.4	110.7	110.7	96.7	425.0	392.0	
RB3-1200	169.2	148.4	148.4	110.7	110.7	96.7	566.9	522.4	
RB10-1300	197.0	187.5	148.4	117.15	117.15	115.3	612.7	570.15	



Standard(Spong)				
link i	θ_i	d_i	a_i	α_i
L1	θ_1	d_1	0	-90
L2	$\theta_2 - 90$	$-d_2$	0	0
L3	0	0	a_1	0
L4	θ_3	d_3	0	0
L5	0	0	a_2	0
L6	$\theta_4 + 90$	$-d_4$	0	0
L7	0	0	0	90
L8	θ_5	d_5	0	-90
L9	θ_6	$-d_6$	0	90



$${}^0P_8 = {}^0P_9 + d_4 \hat{Y}$$

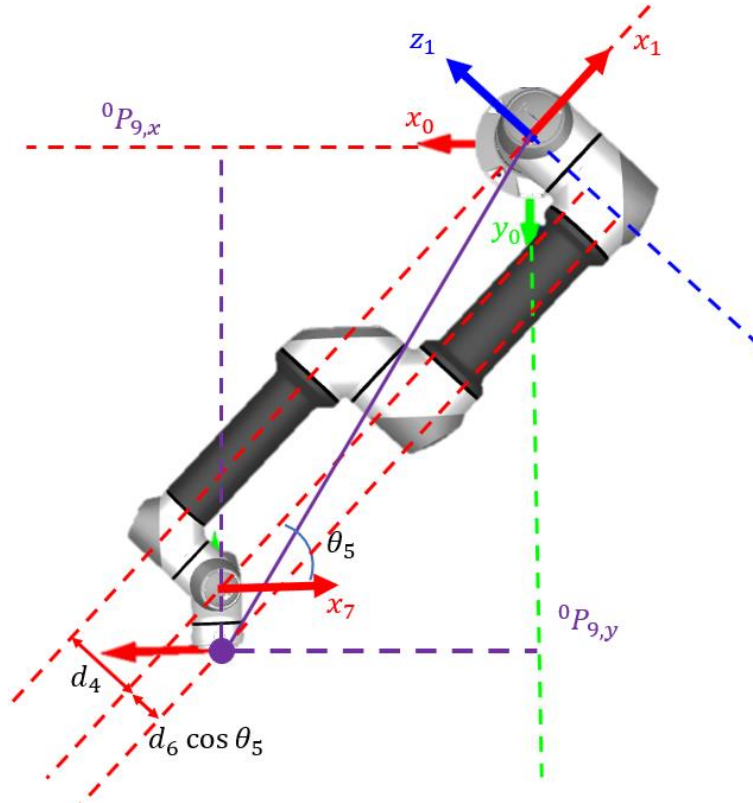
$$\theta_1 = \varphi_1 + \varphi_2 + \frac{\pi}{2}$$

$$\varphi_1 = \text{atan2}({}^0P_{8,y}, {}^0P_{8,x})$$

$$\cos \varphi_2 = \frac{d_4}{|{}^0P_{8,xy}|} = \frac{d_4}{\sqrt{{}^0P_{8,x}^2 + {}^0P_{8,y}^2}}$$

$$\varphi_2 = \pm \arccos \left(\frac{d_4}{\sqrt{{}^0P_{8,x}^2 + {}^0P_{8,y}^2}} \right)$$

$$\theta_1 = \text{atan2}({}^0P_{8,y}, {}^0P_{8,x} \pm \arccos \left(\frac{d_4}{\sqrt{{}^0P_{8,x}^2 + {}^0P_{8,y}^2}} \right) + \frac{\pi}{2}$$



$$d_4 + d_6 \cos \theta_5 = -{}^1P_{9,z}$$

$${}^1P_9 = {}^0R_1^T {}^0P_9$$

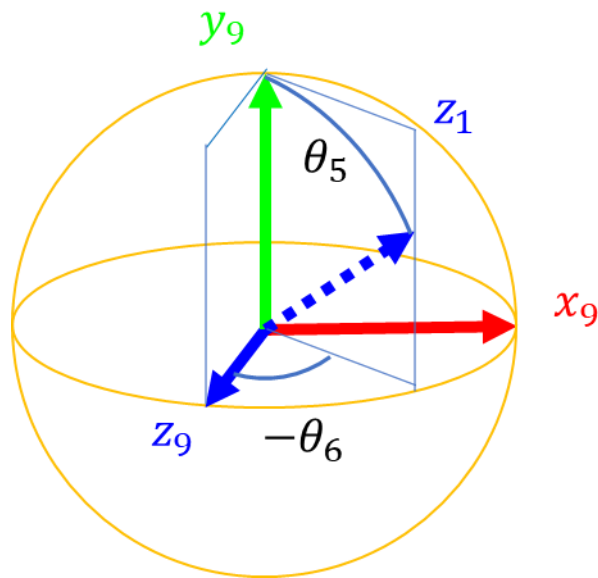
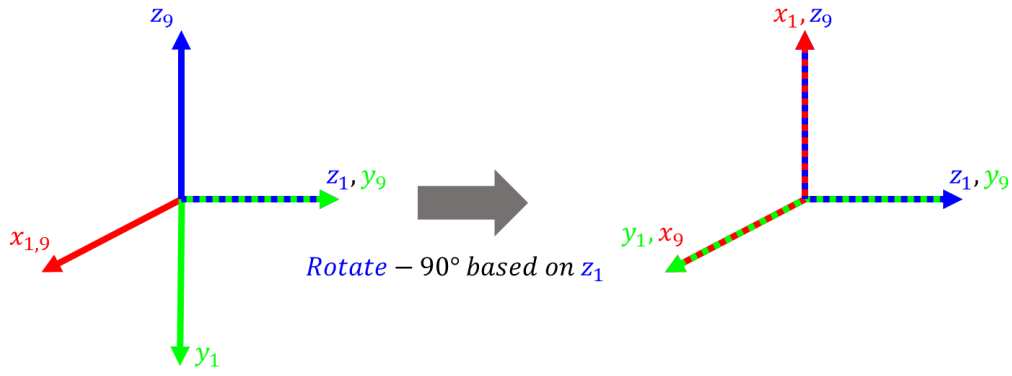
$$= \begin{bmatrix} c_1 & s_1 & 0 \\ 0 & 0 & -1 \\ -s_1 & c_1 & 0 \end{bmatrix} \begin{bmatrix} {}^0P_{9,x} \\ {}^0P_{9,y} \\ {}^0P_{9,z} \end{bmatrix}$$

$$= \begin{bmatrix} c_1 {}^0P_{9,x} + s_1 {}^0P_{9,y} \\ -{}^0P_{9,z} \\ -s_1 {}^0P_{9,x} + c_1 {}^0P_{9,y} \end{bmatrix}$$

$$d_4 + d_6 \cos \theta_5 = -(-s_1 {}^0P_{9,x} + c_1 {}^0P_{9,y})$$

$$\cos \theta_5 = \frac{s_1 {}^0P_{9,x} - c_1 {}^0P_{9,y} - d_4}{d_6}$$

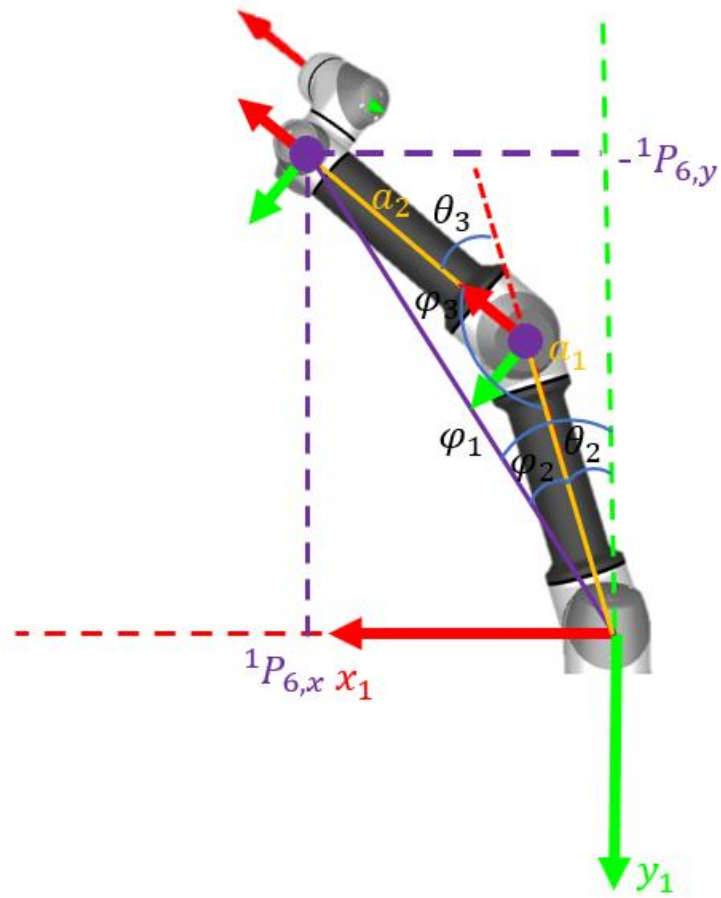
$$\theta_5 = \pm \arccos \left(\frac{s_1 {}^0P_{9,x} - c_1 {}^0P_{9,y} - d_4}{d_6} \right)$$



$${}^1\hat{Z}_9 = \begin{bmatrix} -\sin \theta_5 \sin \left(-\theta_6 + \frac{\pi}{2} \right) \\ \cos \theta_5 \\ \sin \theta_5 \cos \left(-\theta_6 + \frac{\pi}{2} \right) \end{bmatrix}$$

$$= \begin{bmatrix} \sin \theta_5 \sin \left(\theta_6 - \frac{\pi}{2} \right) \\ \cos \theta_5 \\ \sin \theta_5 \cos \left(\theta_6 - \frac{\pi}{2} \right) \end{bmatrix}$$

$$\begin{aligned}
{}^9R_1 &= {}^1R_9^T = \left[{}^0R_1^{-1} {}^0R_9 \right]^T = \left[{}^0R_1^T {}^0R_9 \right]^T \\
&= \left[\begin{array}{ccc} c_1 & s_1 & 0 \\ 0 & 0 & -1 \\ -s_1 & c_1 & 0 \end{array} \right] \left[\begin{array}{ccc} \hat{X}_x & \hat{Y}_x & \hat{Z}_x \\ \hat{X}_y & \hat{Y}_y & \hat{Z}_y \\ \hat{X}_z & \hat{Y}_z & \hat{Z}_z \end{array} \right]^T \\
&= \left[\begin{array}{ccc} c_1\hat{X}_x + s_1\hat{X}_y & -\hat{X}_z & -s_1\hat{X}_x + c_1\hat{X}_y \\ c_1\hat{Y}_x + s_1\hat{Y}_y & -\hat{Y}_z & -s_1\hat{Y}_x + c_1\hat{Y}_y \\ c_1\hat{Z}_x + s_1\hat{Z}_y & -\hat{Z}_z & -s_1\hat{Z}_x + c_1\hat{Z}_y \end{array} \right]^T \\
&= \left[\begin{array}{ccc} c_1\hat{X}_x + s_1\hat{X}_y & -\hat{X} & -s_1\hat{X}_x + c_1\hat{X}_y \\ c_1\hat{Y}_x + s_1\hat{Y}_y & -\hat{Y} & -s_1\hat{Y}_x + c_1\hat{Y}_y \\ c_1\hat{Z}_x + s_1\hat{Z}_y & -\hat{Z} & -s_1\hat{Z}_x + c_1\hat{Z}_y \end{array} \right] \\
{}^1\hat{Z}_9 &= \left[\begin{array}{c} -s_1\hat{X}_x + c_1\hat{X}_y \\ -s_1\hat{Y}_x + c_1\hat{Y}_y \\ -s_1\hat{Z}_x + c_1\hat{Z}_y \end{array} \right] = \left[\begin{array}{c} \sin \theta_5 \sin \left(\theta_6 - \frac{\pi}{2} \right) \\ \cos \theta_5 \\ \sin \theta_5 \cos \left(\theta_6 - \frac{\pi}{2} \right) \end{array} \right] \\
\sin \left(\theta_6 - \frac{\pi}{2} \right) &= \frac{s_1\hat{X}_x - c_1\hat{X}_y}{\sin \theta_5} \\
\cos \left(\theta_6 - \frac{\pi}{2} \right) &= \frac{-s_1\hat{Z}_x + c_1\hat{Z}_y}{\sin \theta_5} \\
\theta_6 - \frac{\pi}{2} &= \text{atan2} \left(\frac{s_1\hat{X}_x - c_1\hat{X}_y}{\sin \theta_5}, \frac{-s_1\hat{Z}_x + c_1\hat{Z}_y}{\sin \theta_5} \right) \\
\theta_6 &= \text{atan2} \left(\frac{s_1\hat{X}_x - c_1\hat{X}_y}{\sin \theta_5}, \frac{-s_1\hat{Z}_x + c_1\hat{Z}_y}{\sin \theta_5} \right) + \frac{\pi}{2}
\end{aligned}$$



$$\cos \varphi_3 = \frac{a_1^2 + a_2^2 - |^1P_{6,xy}|^2}{2a_1a_2}$$

$$\cos \theta_3 = \cos(\pi - \varphi_3) = -\cos \varphi_3 = -\frac{a_1^2 + a_2^2 - |^1P_{6,xy}|^2}{2a_1a_2}$$

$$\theta_3 = \pm \arccos\left(-\frac{a_1^2 + a_2^2 - |^1P_{6,xy}|^2}{2a_1a_2}\right)$$

$$\varphi_1 = \varphi_2 + \theta_2 = \operatorname{atan2}(^1P_{6,x}, -^1P_{6,y})$$

$$\frac{\sin \varphi_2}{a_2} = \frac{\sin \varphi_3}{|^1P_{6,xy}|}$$

$$\varphi_2 = \operatorname{asin}\left(\frac{a_2 \sin(\pi - \theta_3)}{|^1P_{6,xy}|}\right) = \operatorname{asin}\left(\frac{a_2 \sin \theta_3}{|^1P_{6,xy}|}\right)$$

$$\theta_2 = \varphi_1 - \varphi_2 = \operatorname{atan2}(^1P_{6,x}, -^1P_{6,y}) - \operatorname{asin}\left(\frac{a_2 \sin \theta_3}{|^1P_{6,xy}|}\right)$$

Because coordinate system 5 and coordinate system 6 differ by 90 degrees,

$${}^5R_6 = \begin{bmatrix} \cos\left(\theta_4 + \frac{\pi}{2}\right) & -\sin\left(\theta_4 + \frac{\pi}{2}\right) & 0 \\ \sin\left(\theta_4 + \frac{\pi}{2}\right) & \cos\left(\theta_4 + \frac{\pi}{2}\right) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\theta_4 + \frac{\pi}{2} = \text{atan2}({}^5\hat{X}_{6,y}, {}^5\hat{X}_{6,x})$$

$$\theta_4 = \text{atan2}({}^5\hat{X}_{6,y}, {}^5\hat{X}_{6,x}) - \frac{\pi}{2}$$

```
% -----
% Rainbow Robotics
% Analytic Inverse Kinematics Example Code (based on Octave)
% All Right Reserved.
% -----

clc; clear all; close all;
% -----
D2R = pi/180.;
R2D = 180./pi;
% -----
disp('-----');
disp('Input Cartesian Value (mm & deg)');
disp('-----');
% Rainbow Robotics use ZYX euler notation
% Z -> Y' -> X''
input_x = -156.76
input_y = -155.15
input_z = 814.96
input_rx = -43.47
input_ry = 80.56
input_rz = -60.88
% -----
x = input_x;
y = input_y;
z = input_z;
rx = input_rx*D2R;
ry = input_ry*D2R;
rz = input_rz*D2R;
% -----
% Link Length parameter (RB5 - 850)
d1 = 169.2;
d2 = 148.4;
d3 = 148.4;
d4 = 110.7;
d5 = 110.7;
d6 = 96.7;

a1 = 425.0;
a2 = 392.0;
% -----

Rz = [cos(rz) -sin(rz) 0;
      sin(rz) cos(rz) 0;
      0 0 1];
```

```

Ry = [cos(ry) 0 sin(ry);
      0 1 0;
      -sin(ry) 0 cos(ry)];

Rx = [1 0 0;
      0 cos(rx) -sin(rx);
      0 sin(rx) cos(rx)];

R = Rz * Ry * Rx;
% -----

Y06 = R(:, 2);
P06 = [x;y;z];

P05 = P06 + d6*Y06;

th1 = atan2(P05(2), P05(1)) - acos(d4/sqrt(P05(2)^2 + P05(1)^2))+0.5*pi;
th5 = +acos((sin(th1)*P06(1)-cos(th1)*P06(2)-d4)/d6);
th6 = atan2(-(sin(th1)*R(1,1)+cos(th1)*R(2,1))/sin(th5),
            (sin(th1)*R(1,3)+cos(th1)*R(2,3))/sin(th5))+0.5*pi;

A01 = [cos(th1) -cos(-pi*0.5)*sin(th1) sin(-pi*0.5)*sin(th1) 0;
      sin(th1) cos(-pi*0.5)*cos(th1) -sin(-pi*0.5)*cos(th1) 0;
      0 sin(-pi*0.5) cos(-pi*0.5) d1;
      0 0 0 1];

A67 = [cos(0) -cos(pi*0.5)*sin(0) sin(pi*0.5)*sin(0) 0;
      sin(0) cos(pi*0.5)*cos(0) -sin(pi*0.5)*cos(0) 0;
      0 sin(pi*0.5) cos(pi*0.5) 0;
      0 0 0 1];

A78 = [cos(th5) -cos(-pi*0.5)*sin(th5) sin(-pi*0.5)*sin(th5) 0;
      sin(th5) cos(-pi*0.5)*cos(th5) -sin(-pi*0.5)*cos(th5) 0;
      0 sin(-pi*0.5) cos(-pi*0.5) d5;
      0 0 0 1];

A89 = [cos(th6) -cos(pi*0.5)*sin(th6) sin(pi*0.5)*sin(th6) 0;
      sin(th6) cos(pi*0.5)*cos(th6) -sin(pi*0.5)*cos(th6) 0;
      0 sin(pi*0.5) cos(pi*0.5) -d6;
      0 0 0 1];

A17 = inv(A01)*[R P06;0 0 0 1]*inv(A89)*inv(A78)*inv(A67);

P14 = [A17(1,4);
      A17(2,4);
      A17(3,4)];

th3 = +acos((P14(1)^2+P14(2)^2-a1^2-a2^2)/(2*a1*a2));
th2 = atan2(P14(1), -P14(2))-asin(a2*sin(th3)/sqrt(P14(1)^2+P14(2)^2));

A12 = [cos(th2-pi*0.5) -cos(0)*sin(th2-pi*0.5) sin(0)*sin(th2-pi*0.5) 0;
      sin(th2-pi*0.5) cos(0)*cos(th2-pi*0.5) -sin(0)*cos(th2-pi*0.5) 0;
      0 sin(0) cos(0) -d2;
      0 0 0 1];

A23 = [cos(0) -cos(0)*sin(0) sin(0)*sin(0) a1*cos(0);
      sin(0) cos(0)*cos(0) -sin(0)*cos(0) a1*sin(0);

```

```

0 sin(0) cos(0) 0;
0 0 0 1];

A34 = [cos(th3) -cos(0)*sin(th3) sin(0)*sin(th3) 0;
sin(th3) cos(0)*cos(th3) -sin(0)*cos(th3) 0;
0 sin(0) cos(0) d3;
0 0 0 1];

A45 = [cos(0) -cos(0)*sin(0) sin(0)*sin(0) a2*cos(0);
sin(0) cos(0)*cos(0) -sin(0)*cos(0) a2*sin(0);
0 sin(0) cos(0) 0;
0 0 0 1];

A56_cal = inv(A45)*inv(A34)*inv(A23)*inv(A12)*inv(A01)*[R_P06;0 0 0 1]*inv(A89)*inv(A78)*inv(A67);

th4 = atan2(A56_cal(2,1), A56_cal(1,1))-0.5*pi;
% -----
disp('-----');
disp('Inverse Kinematics Result (deg)');
disp('-----');
th1 = th1 * R2D
th2 = th2 * R2D
th3 = th3 * R2D
th4 = th4 * R2D
th5 = th5 * R2D
th6 = th6 * R2D

```

WE
TOUCH
THE **CORE** .

- Rainbow Robotics Research Center -