

**ECE 522  
Induction Machines  
Fall Semester 2019  
Midterm  
Problems I, II, and III**

***EXAMINATION RULES***

- 1 You are on your honor to do your own work on this examination. That is, you will neither give nor receive aid on this examination, except from the course instructor. If you violate this confidence, you will receive the grade of zero for this examination.
- 2 Please summarize your work at the end of each problem. Thank you!
3. Show all of your work! Make it neat. No partial credit will be given if I can not easily follow your work.
4. Submit your completed examination 48 hours after you receive it.
5. Please use "ECE 522 Exam 1" as the subject for the email that you use to return your work.
6. Attach a separate file for each problem. Please name them:  
    LastName\_FirstName\_P1.what ever extension is appropriate  
    LastName\_FirstName\_P2.what ever extension is appropriate  
    LastName\_FirstName\_P3.what ever extension is appropriate

pu := 1

$j := \sqrt{-1}$

The induction machine to be used in the first three problems is operating in steady state and can be described by the following parameters:

$$r_s := 0.03 \cdot \text{pu}$$

$$L_{Ls} := 0.1 \cdot \text{pu}$$

$$L_m := 2.0 \cdot \text{pu}$$

$$L_{Lr} := 0.1 \cdot \text{pu}$$

$$r_r := 0.03 \cdot \text{pu}$$

## Problem I

### Part A:

- 1) **Determine**  $\text{slip}_{\text{rated}}$  and  $\omega_{r\_rated}$   
and  $\Lambda_{dr\_rated} = |\Lambda_{dqrA1}|$

Rated is defined to mean the operating condition such that:

$$|V_{dqs}| = 1.0 \cdot \text{pu} \quad \text{and} \quad T_{EM} = 1.0 \cdot \text{pu} \quad \text{and} \quad \omega_{es} = 1.0 \cdot \text{pu}$$

- 2) **Create a vector diagram that includes:**  
(use  $V_{dqs}$  as the reference)

$$\Lambda_{dqsA2} \quad \Lambda_{dqrA2} \quad I_{dqrA2} \quad I_{dqsA2} \quad V_{dqsA2}$$

(The subscript A2 denotes Part A subpart 2.)

- 3) **Create a vector diagram that includes:**  
(put  $\Lambda_{dqr}$  at 0 degrees,  
such that  $\Lambda_{qr} = 0$ )

$$\Lambda_{dqsA3} \quad \Lambda_{dqrA3} \quad I_{dqrA3} \quad I_{dqsA3} \quad V_{dqsA3}$$

(The subscript A3 denotes Part A subpart 3.)

Indirect field oriented control is used to control the induction machine for Parts B and C.  
Put  $\lambda_{dr}$  at 0 degrees in Parts B and C.

**Part B: Set the command torque to zero:**

$$T_{EMB} := 0.0 \cdot \text{pu}$$

**Calculate and create a vector diagram that includes:**

$$\Lambda_{dqsBx} \quad \Lambda_{dqrBx} \quad I_{dqrBx} \quad I_{dqsBx} \quad V_{dqsBx}$$

x equal 1, 2, and 3

**For:**    1)     $\omega_{rB1} := 0.0$                       and                       $\Lambda_{drB1} = \Lambda_{dr\_rated}$

2)     $\omega_{rB2} = \omega_{r\_rated}$                       and                       $\Lambda_{drB2} = \Lambda_{dr\_rated}$

3)     $\omega_{rB3} = 2 \cdot \omega_{r\_rated}$                       and                       $\Lambda_{drB3} = \frac{\Lambda_{dr\_rated}}{2}$

**Part C:**

**Calculate and create a vector diagram that includes:**

$$\Lambda_{dqsCx} \quad \Lambda_{dqrCx} \quad I_{dqrCx} \quad I_{dqsCx} \quad V_{dqsCx}$$

x equal 1, 2, and 3

**For:**    1)     $T_{EMC1} := 1.0 \cdot \text{pu}$                        $\omega_{rC1} := 0.0$                       and                       $\Lambda_{drC1} = \Lambda_{dr\_rated}$

2)     $T_{EMC2} := 1.0 \cdot \text{pu}$                        $\omega_{rC2} = \omega_{r\_rated}$                       and                       $\Lambda_{drC2} = \Lambda_{dr\_rated}$

3)     $T_{EMC3} := 0.5 \cdot \text{pu}$                        $\omega_{rC3} = 2 \cdot \omega_{r\_rated}$                       and                       $\Lambda_{drC3} = \frac{\Lambda_{dr\_rated}}{2}$

Put  $\lambda_{dr\_cmd}$  at 0 degrees in Problems II and III.

You might find it easier to put Problems II and III in separate files from each other and Problem I.

**Problem II: Repeat Parts B and C of Problem I for the situation where the parameter  $L_r/r_r$  in the "slip calculator" is in error by +25%.**

Comment on the effect on steady state performance of such "detuning" of the controller.

**Problem III: Repeat Parts B and C of Problem I for the situation where the parameter  $L_r/r_r$  in the "slip calculator" is in error by -25%.**

Comment on the effect on steady state performance of such "detuning" of the controller.