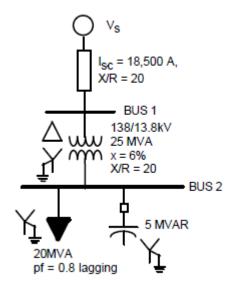
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ECE 524 - EXAM 1 (Midterm)

```
In [74]:
             # Import Libraries
           2
              import numpy as np
           3 import matplotlib.pyplot as plt
           4 import eepower as eep
             from eepower import p,n,u,m,k,M
           5
              from scipy.optimize import fsolve
           6
           7
           8
              # Define Loaded Voltage Source Function
           9
              def loadedsource(Vload,Zload,Zline,Zsource=None,Zload2=None):
          10
                  loadedsource Function
          11
          12
          13
                  Evaluates the terminal voltage of a voltage source given
                  a specified load impedance and line impedance. Can also
          14
                  find the internal voltage of a generation source given the
          15
                  internal source impedance.
          16
          17
          18
                  Parameters
          19
                  -----
          20
                  Vload:
                               complex
          21
                               The desired voltage across the load impedance.
                  Zload:
          22
                               complex
          23
                               The load impedance in ohms.
                  Zline:
          24
                               complex
          25
                               The line impedance in ohms.
                               complex, optional
          26
                  Zsource:
          27
                               The source internal impedance in ohms,
          28
                               default=None.
          29
                  Zload2:
                               complex, optional
                               A secondary load impedance to be included in
          30
          31
                               parallel, default=None.
          32
          33
                  Returns
          34
                  _____
          35
                  Vt:
                               complex
                               The terminal voltage of the source.
          36
          37
                  Iload:
                               complex
          38
                               The load current in amps.
          39
                               complex, optional
                  Ea:
          40
                               The internal source voltage.
          41
          42
                  # Evaluate Load Current
          43
                  if Zload2 != None:
                      Zload = eep.parallelz(Zload,Zload2)
          44
          45
                  Iload = Vload/Zload
          46
                  # Evaluate Voltage Drop Down Line
          47
                  Vdrop_line = Iload * Zline
          48
                  Vt = Vload + Vdrop line
                  # If Given, Evaluate Source Vdrop
          49
          50
                  if Zsource != None:
          51
                      Vdrop source = Iload * Zsource
          52
                      Ea = Vt + Vdrop_source
          53
                      return(Vt,Iload,Ea)
          54
                  # Return The Terminal Voltage
          55
                  return(Vt,Iload)
```

Problem 1:

Consider the system shown below. The power ratings given are three phase ratings, and voltages listed are line to line.



A) Create a system equivalent for capacitor switching studies. Explain your reasoning in developing the model. Describe how you would validate this model to ensure accuracy. Build this model in your transient program. Perform a steady-state analysis and adjust the source voltage so the voltage at the capacitor bus is 1.0pu with the capacitor in the system. Verify this with your transient simulation program.

- Calculations to demonstrate the process related to this simplification in the code section following these responses.
- I have so chosen to simplify the system by combining the transformer and source impedances into one lumped impedance. The load should still be maintained as a discrete element.
- As might have been guessed, the source voltage must be greater than the bus voltage.
- · Simulation included as Prob1 PA

B) Describe (with sketches as needed) what happens when the breaker for the capacitor bank is opened. Back this up with simulation results.

- Opening the capacitor bank's breaker will cause transient to begin. The transient will cause a
 high-frequency ringing on the system that will slowly damp over time. The capacitor helps
 maintain voltage stability and reliability on the bus, so removing the cap will inevitebly reduce
 these characteristics.
- · Simulation included as Prob1 PB
- C) Estimate the worst case current on energization of the capacitor bank. Does the 60Hz term need to be considered in this calculation (why or why not)? Again, confirm this with simulation results. Compare simulation results with and without the load and the resistances of the source and transformer included and comment on the impact on the response.
 - To estimate this worst case current, I'm neglecting all inductance between the source and capacitance. I'm also assuming that the capacitor starts at 0 volts, and we're using the peak voltage.

- In this case, I'm using the 60Hz voltage, only out of convenience, it does play a significant role, as it's voltage sets the voltage that the capacitor is trying to reach. I am neglecting this fact for my approximation, as such, it should be noted that my approximation is quite crude.
- Simulation Included as Prob1_PC

D) Determine the worst voltage seen by the load due to this worst case capacitor switching transient from part (C) through simulation.

• From simulation, the resulting worst-case voltage is approximately 55kV, Line-Neutral.

E) Propose options to reduce this transient.

- Break the cap-bank into smaller sub-banks which can be switched independently.
- Introduce a small resistance or inductance between the bus and the cap bank to reduce transient action. Note that the inductance would need to be tuned as an appropriate filter.

```
In [42]:
           1 # Define Givens
            2 | Vs = 138*k
           3 ISC = 18500
           4 \text{ XoR} = 20
           5 \times m = 138/13.8
           6 xfm_rat = 25*M
           7
              xfm x = 6/100
           8 \times \text{fm xor} = 20
           9 load = 20*M
          10 load_pf = 0.8 #lagging
          11 \mid cbank = 5*M
          12 # Define PU Bases
          13 | Sbase = xfm_rat
          14 | Vb1 = 138*k
          15 \mid Vb2 = 13.8*k
          16 Zb = eep.zpu(Sbase,VLL=Vb2)
          17
          18 | # Evaluate Source Impedance
          19 SCMVA = ISC*Vs
          20 | Zsrc = eep.zsource(SCMVA,Vs,XoR,Sbase=Sbase)
          21 | print("SRC Z:\t",np.round(Zsrc,6),"pu-\Omega\tR:",round(Zsrc.real*Zb,4),"\Omega\tL:",r
          22 # Evaluate Transformer Impedance
          23 r,x = eep.zdecompose(xfm x,xfm xor)
          24 \mid Zxfm = r+1j*x
          25 | print("XFM Z:\t",np.round(Zxfm,6),"pu-\Omega\tR:",round(Zxfm.real*Zb,4),"\Omega\tL:",r
              # Break the Load into Resistance/Reactance
          27 | #### NOTE #### Load is divided by three to account for 3-phs value being pro
          28 r,x = eep.powerimpedance(load/3,Vb2,load_pf)
          29 |Zload = r+1j*x
          30 print("LOAD Z:\t",np.round(Zload/Zb,6),"pu-Ω\t\tR:",round(Zload.real*Zb,4),"
          31 | print() # Insert Gap
          32
          33 | # Evaluate Capacitance Value
          34 | Cval = eep.farads(cbank, Vb2)
          35 | print("Capacitor Value:",Cval/u,"μF")
          36 print()
          37
          38 # Find the source voltage to sustain 1.0pu-V on the cap bank
          39 Vsln,Ild = loadedsource(1.0,Zload/Zb,Zsrc+Zxfm,Zload2=eep.phasorz(C=Cval)/Zb
          40 | Vsll = eep.phaseline(VLN = Vsln)
          41 | eep.cprint(Vsll,"pu-V","Required Source Voltage:")
          42 | eep.cprint(Vsl1*Vb2/np.sqrt(2),"V","Required Source Voltage:")
          43
          44 | # Estimate the Worst-Case Charging Current
          45 | Iworst = Vsln*Vb2 / (Zsrc.real*Zb + Zxfm.real*Zb)
          46 | eep.cprint(Iworst/k,"kA","Worst-Case Charging Current:")
          SRC Z:
                   (0.000489+0.00978j) pu-\Omega
                                                    R: 0.0037 Ω
                                                                     L: 0.1979 mH
          XFM Z:
                                                    R: 0.0228 Ω
                                                                     L: 1.2124 mH
                   (0.002996+0.059925j) pu-\Omega
          LOAD Z: (4.6875+6.25j) pu-\Omega
                                                    R: 272.0055 \Omega L: 157.8618 mH
          Capacitor Value: 69.64351987147981 μF
```

Required Source Voltage: 1.721 ∠ 0.0° pu-V Required Source Voltage: 16791.294 ∠ 0.0° V Worst-Case Charging Current: 516.398 ∠ 0.328° kA

Problem 2:

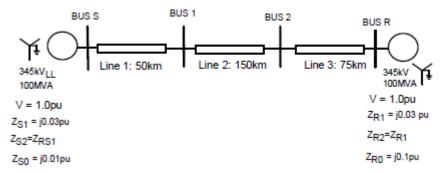
- A) Explain what causees overvoltage conditions in transient recovery voltage. What is the voltage we are concerned about? Describe with diagrams as needed. Explain.
 - Transient Recovery Voltages are caused by inductive properties of the power system. When a breaker opens, the current is interrupted, but inductors can't instantly allow current flow to cease. As a result, the inductors raise enormous ammounts of voltage as a way to compensate. It is this "recovery" voltage that is known as a TRV. This TRV amplitude and its accompanying rate of rise are both factors that need to be considered for the effectiveness and safety of electrical breakers. In particular, the voltage across the breaker contacts is the one that we're most concerned about. If this voltage exceeds the breaker's capacity, it will restrike until the transient has subsided. This restrike is extremely damaging to breaker contacts, and can be threatening to the safety of any nearby personel. As such, it is of great concern.
- B) Once you know the worst case transient recovery voltage amplitude, how will you use that information? Does natural frequency matter? Why?
 - Such information can be used to rate circuit breakers and equipment to withstand the TRV.
 - Natural frequency does matter. It can be very useful in applying TRV mitigation techniques such as filtering. If the natural frequency is considerably greater than the 60Hz frequency or any significant harmonics, it can be used to apply a filter that appears as a dead-short at the natural frequency. This would allow for effective current disipation during TRV conditions.
- C) Describe corrective actions that can be used to reduce the impact if the transient recovery voltage transient is unacceptable. Briefly describe how these corrective actions work.
 - As mentioned previously, applying filters tuned to the natural frequency can be a highly
 effective mitigation technique as they will allow current disipation into a safe route.
 - Additionally, since TRV is caused primarily by inductance in a circuit path. Applying capacitors
 in varying ways may also be beneficial by providing a current route for the TRV.
 - As a final mention, switching in resistors at the same time as the breaker being opened may be of particular use by providing a disipation path.
- D) Does the angle between the voltage and breaker current prior to transient impact the TRV transient response? In what way?
 - The angle does play a particular role in transient response as it dictates the addative point
 where transient voltage is applied to the 60Hz component. If the current and voltage are in
 phase, the overall voltage (60Hz comp. and TRV comp.) will serve to be greater as it will be a
 summation of their impacts.

Problem 3:

You are given a 345 kV transmission system that consists of 3 transmission line segments, with intermediate buses separating them (see figure below). Each of the transmission line segments has the following characteristics (calculated at 60Hz).

$$\begin{array}{lll} R_0 := 0.3112 \frac{ohm}{mi} & R_1 := 0.0381 \frac{ohm}{mi} & R_2 := 0.0381 \frac{ohm}{mi} \\ \\ Z_{e0} := 654.86ohm & Z_{e1} := 256.35ohm & Z_{e2} := 256.35ohm \\ \\ \nu_0 := 1.2254 \cdot 10^5 \cdot \frac{mi}{s} & \nu_1 := 1.8213 \cdot 10^5 \cdot \frac{mi}{s} & \nu_2 := 1.8213 \cdot 10^5 \cdot \frac{mi}{s} \end{array}$$

- A) The mode 1 and mode 2 terms are identical. Explain what this tells you about the transmission line. What underlying assumptions have been made and what limitatons should be considered for applying this model.
 - Identifying mode 1 as being equal to mode 2 informs me that the three concuctors are equally transposed, meaning that they have swapped positions enough that no one line shows features that significantly differentiate it from the others.
 - The underlying assumptions to support this are that the lines themselves will carry the same characteristics over their entire length such that they do not vary reistive, capacitive, or inductive properties for their entire length. The supporting pole structure should remain consistent along the entire length of the line.
- B) Calculate the ABC domain R', L' and C' matrices per mile.
 - · Calculations Shown in Code Cell below.
- C) What do the modes 0, 1 and 2 represent? Where do the signals they represent travel?
 - Mode 0 represents what is commonly known as the "ground mode", its related signals travel through the ground return.
 - Modes 1 and 2 represent "line modes" as their signals travel through the transmission lines themselves.
- D) A single line diagram for the system is shown below. Implement a model of this system, each line has the characteristics above. Use the appropriate travelling wave model. Describe how you would validate your model before starting transient studies, and suggest a time step for transient simulation. Use coupled RL (sequence data input) for the source impedances.



 Model validation would come from a process of cross-validating the model in a phasor-domain simulator (something like PowerWorld) to a electromagnetic transients program (ATP/ATPDraw). Validating that the steady-state performance is equal or nearly equivalent between the two modeling platforms would illustrate model validity.

- Given the signal propogation velocity (*v*) being at a maximum of 1.8213e5 (mi/s), it might be sensible to desire collecting distance traveled to the 10th of a mile, at a sampling rate of 20 samples/cycle. This means that a multiple of 200 must be combined with the propigation velocity. A resulting 3.6526e7 samples/second results in a delta-T of 2.74529e-8. Rounding this result down for sake of simplicity provides a value of 2.7e-8.
- Model included as Prob3_PD
- E) Suppose a three phase fault occurs 60% of the way from Bus 1 to Bus 2 (set both sources to be at 1.0 pu at an angle of 0 degrees). Do a simple analysis for each step and then simulate.
 - 1. How long will it take the transient to reach Bus 1? How long will it take to reach Bus 2?
 - Numerical results calculated in cell below.
 - 2. What is the voltage reflection coefficent seen by the voltage when it reaches Bus 1? Based on that, what would expect the voltage to look like at that bus?
 - Based on the fact that all lines share the same Zc, it is safe to say that the reflection coefficent (for voltage) at BUS 1 will be 0 (as demonstrated in formula below).
 - 3. How would your answer to (2) change if the line between buses BUS S and BUS 1 were open?
 - If the line between BUS S and BUS 1 was open, the resultant coefficient would be 1 as noted from the SEL presentation. Thus the voltage should see a full step change ramping upwards.
 - 4. Calculate the initial surge current at the fault location.
 - · Numerical results calculated in cell below.
 - 5. How long will it take the initial surge current to reach BUS 1 and BUS 2? For case (3) currents look like at BUS 1 and BUS 2 look like when those surges arrive?
 - It will take the current approximately the same ammount of time to reach BUS 1/2.
 - For case (3) the currents will see a -1 coefficient impact, so they will reduce by that ammount.

```
In [96]:
              # Part B
           1
           2
           3
              # Define Ti and Rp
           4
              Ti = np.asmatrix(np.array( [[1,np.sqrt(2),0],
           5
                                            [1,-1/np.sqrt(2),np.sqrt(3/2)],
                                            [1,-1/np.sqrt(2),-np.sqrt(3/2)]])) * 1/np.sqrt(3
           6
           7
              Rp = np.asmatrix(np.array([[0,0,1],
           8
                                           [1,0,0],
           9
                                           [0,1,0]]))
              def modaltoabc(array):
          10
          11
                  matrix = np.asmatrix(array)
          12
                   return(Ti*matrix*Ti**-1)
          13
              def modalcl(zo,vo):
          14
                  def equations(data):
          15
                       C,L = data
                       Z = np.sqrt(L/C)-zo
          16
          17
                       V = 1/np.sqrt(L*C)-vo
          18
                       return(Z,V)
          19
                  C,L = fsolve(equations, (10*n,5*m))
          20
                   return(C,L)
              # Define and Evaluate Modal Components
          21
              R0, R1, R2 = 0.3112, 0.0381, 0.0381
          22
          23
              C0,L0 = modalcl(654.86,1.2254*10**5)
              C1,L1 = modalcl(256.35,1.8213*10**5)
          24
          25
              C2,L2 = modalcl(256.35,1.8213*10**5)
          26
              Rmod = np.array([[R0,0,0],
          27
                            [0,R1,0],
          28
                            [0,0,R2]])
          29
              Cmod = np.array([[C0,0,0],
          30
                            [0,C1,0],
          31
                            [0,0,C2]])
          32
              Lmod = np.array([[L0,0,0],
          33
                               [0, L1, 0],
          34
                               [0,0,L2]])
              for i,arr in enumerate([Rmod,Cmod,Lmod]):
          35
                   nm = [["R",1,"Ω/mi"],["C",n,"nF/mi"],["L",m,"mH/mi"]]
          36
          37
                   print("Modal Form ("+nm[i][0]+"mod):\n",arr/nm[i][1],nm[i][2])
                   print("ABC-Domain ("+nm[i][0]+"'):\n",modaltoabc(arr)/nm[i][1],nm[i][2])
          38
          Modal Form (Rmod):
           [[ 0.3112 0.
                              0.
           [ 0.
                     0.0381
                             0.
                              0.0381]] \Omega/mi
           [ 0.
                     0.
          ABC-Domain (R'):
           [[ 0.12913333  0.09103333  0.09103333]
           [ 0.09103333  0.12913333  0.09103333]
           [ 0.09103333 0.09103333 0.12913333]] \Omega/mi
          Modal Form (Cmod):
                                                     ]
           [[ 12.46159579
                                          0.
              0.
                          21.41830953
                                        21.41830953]] nF/mi
              0.
                           0.
          ABC-Domain (C'):
           [[ 18.43273829 -2.98557125 -2.98557125]
           [ -2.98557125
                          18.43273829
                                        -2.98557125]
           [ -2.98557125
                          -2.98557125 18.43273829]] nF/mi
          Modal Form (Lmod):
                                                  ]
           [[ 5.34405092 0.
                                       0.
```

```
1.40751112]] mH/mi
           [ 0.
                         0.
          ABC-Domain (L'):
           [ 1.31217993  2.71969105  1.31217993]
           [ 1.31217993    1.31217993    2.71969105]] mH/mi
In [106]:
            1
              # Part D
            2
            3 # 1)
            4
              dist = 150 #km
            5 | dist *= 0.621371 #mi
            6 \quad v0 = 1.2254e5
            7 v12 = 1.8213e5 #mi/sec
            8 floc_1 = dist * 0.6
            9 floc_2 = dist * 0.4
           10 print("1) Time to travel from fault to Bus 1:",floc_1/(v12*u),"µsec")
              print(" Time to travel from fault to Bus 2:",floc_2/(v12*u),"μsec")
           11
           12
           13 # 2)
           14 | zc12 = 256.35
           15 Zc = zc12
           16 \mid Zt = zc12
           17 V \operatorname{coef} = (Zt-Zc)/(Zt+Zc)
           18 print("2) Voltage Reflection Coefficent:", Vcoef)
           19
           20 # 4)
           21 vfault = 345*k
           22 | ifault = vfault/zc12
           23 | print("4) Initial Surge Current:",round(ifault,2),"A")
          1) Time to travel from fault to Bus 1: 307.05205073299294~\mu sec
             Time to travel from fault to Bus 2: 204.70136715532863 µsec
          2) Voltage Reflection Coefficent: 0.0
          4) Initial Surge Current: 1345.82 A
  In [ ]:
  In [ ]:
```

1.40751112 0.

[0.