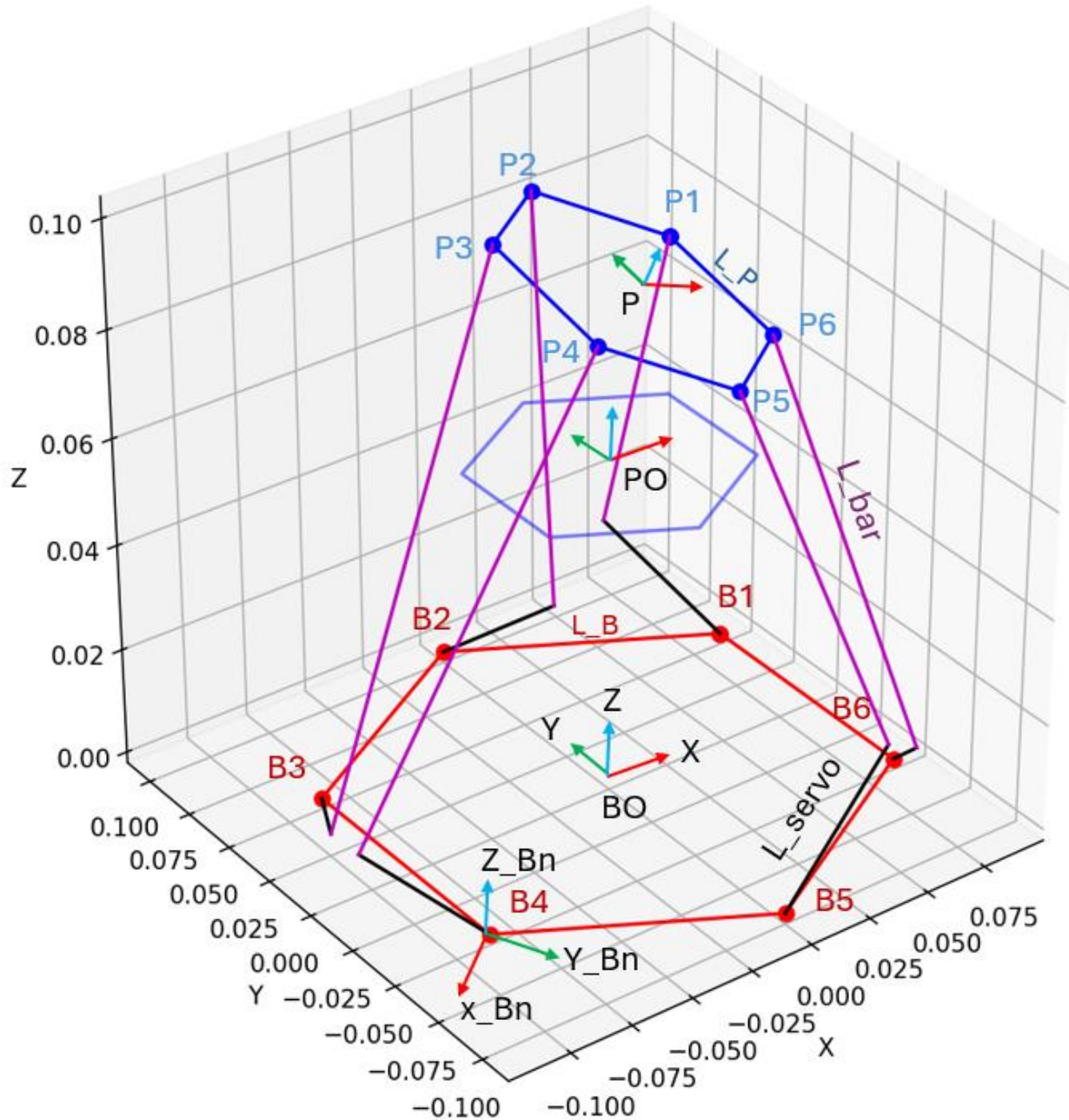


## Method

1. Find the distance between base joint  $B_n$  and platform joint  $P_n$  for all joint pairs based on the final desired platform orientation
2. Find the servo angle that achieves the distance between  $B_n$  and  $P_n$  while satisfying all required constraints



# Key Concepts

Position Vector (e.g., position of Bn rel. BO)

$${}^{Bn}P_{BO} = [X_{Bn}, Y_{Bn}, Z_{Bn}]^T, \\ \text{for } n \in \{1 \dots 6\}$$

Rotation Matrix (e.g., rotation of Bn rel. BO)

$${}^{Bn}_{BO}R = Rot(roll_{Bn}, pitch_{Bn}, yaw_{Bn}), \text{ for } n \in \{1 \dots 6\}$$

$$R = R_z(\alpha) R_y(\beta) R_x(\gamma) = \begin{bmatrix} \cos \alpha & \overset{\text{yaw}}{-\sin \alpha} & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \overset{\text{pitch}}{\cos \beta} & 0 & \sin \beta \\ 0 & 1 & 0 \\ -\sin \beta & 0 & \cos \beta \end{bmatrix} \begin{bmatrix} \overset{\text{roll}}{1} & 0 & 0 \\ 0 & \cos \gamma & -\sin \gamma \\ 0 & \sin \gamma & \cos \gamma \end{bmatrix} \\ = \begin{bmatrix} \cos \alpha \cos \beta & \cos \alpha \sin \beta \sin \gamma - \sin \alpha \cos \gamma & \cos \alpha \sin \beta \cos \gamma + \sin \alpha \sin \gamma \\ \sin \alpha \cos \beta & \sin \alpha \sin \beta \sin \gamma + \cos \alpha \cos \gamma & \sin \alpha \sin \beta \cos \gamma - \cos \alpha \sin \gamma \\ -\sin \beta & \cos \beta \sin \gamma & \cos \beta \cos \gamma \end{bmatrix}$$

Homogeneous Transformation Matrix (e.g., translation and rotation of Bn rel. BO)

$${}^{Bn}_{BO}T = \begin{bmatrix} {}^{Bn}_{BO}R & {}^{Bn}P_{BO} \\ 000 & 1 \end{bmatrix}$$



# Calculations

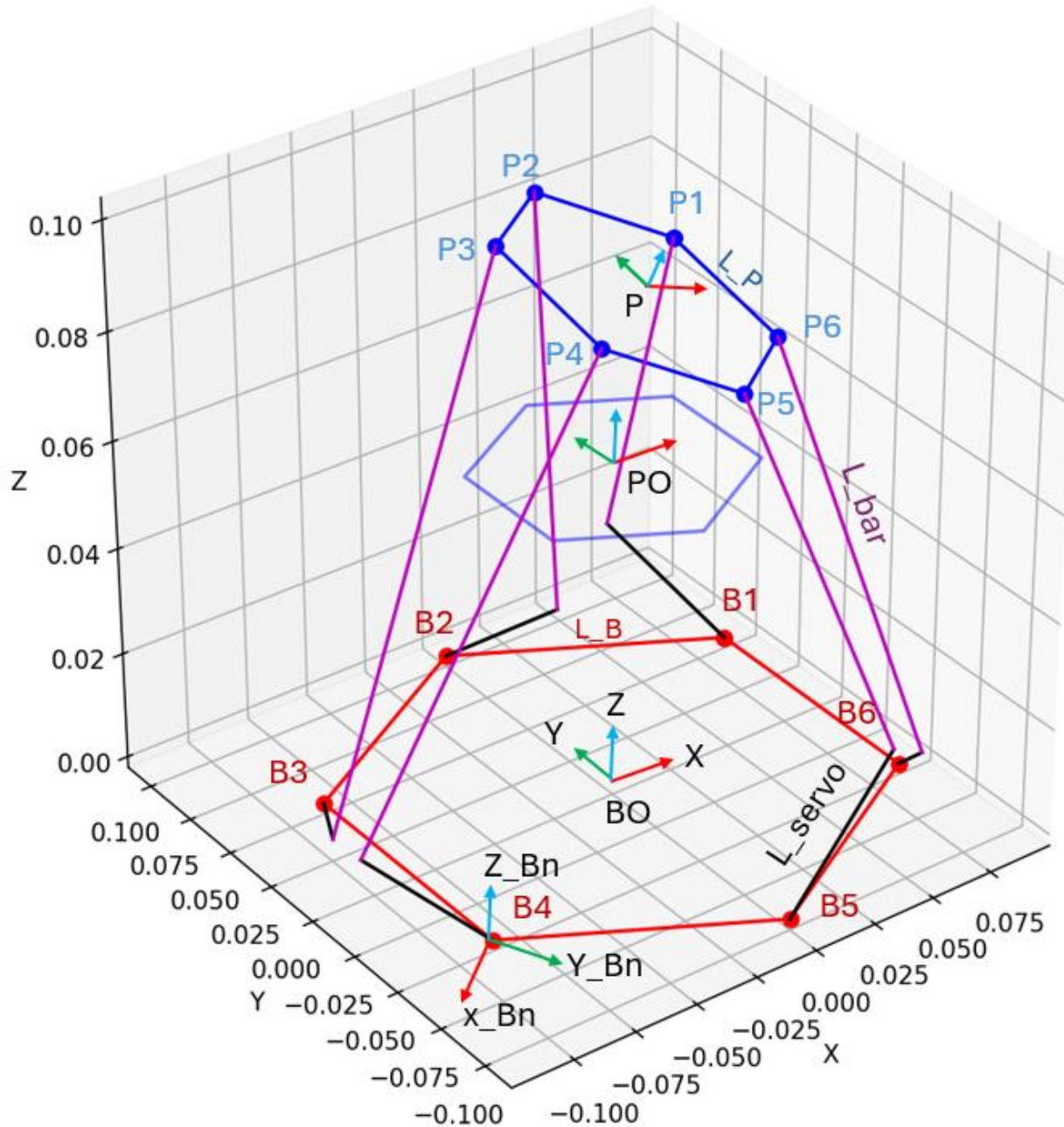
1. Find the distance between base joint  $B_n$  and platform joint  $P_n$  for all joint pairs based on the final desired platform orientation  $P$

$${}^P O P_P = [X_P, Y_P, Z_P]^T$$

$${}^P O_P R = Rot(roll_P, pitch_P, yaw_P)$$

To find the distance, we first describe the platform joints relative to base origin  $BO$ , since having all points in a single coordinate system makes calculation easier.

$${}^P P_{Pn} \rightarrow {}^{BO} P_{Pn}$$



# Key parameters

Position and rotation of base joints ( $B_n$ ) relative to the base origin ( $BO$ )

$${}^{B_n}P_{BO} = [X_{B_n}, Y_{B_n}, Z_{B_n}]^T, \quad \text{for } n \in \{1 \dots 6\}$$

$${}^{B_n}_{BO}R = Rot(roll_{B_n}, pitch_{B_n}, yaw_{B_n}), \text{ for } n \in \{1 \dots 6\}$$

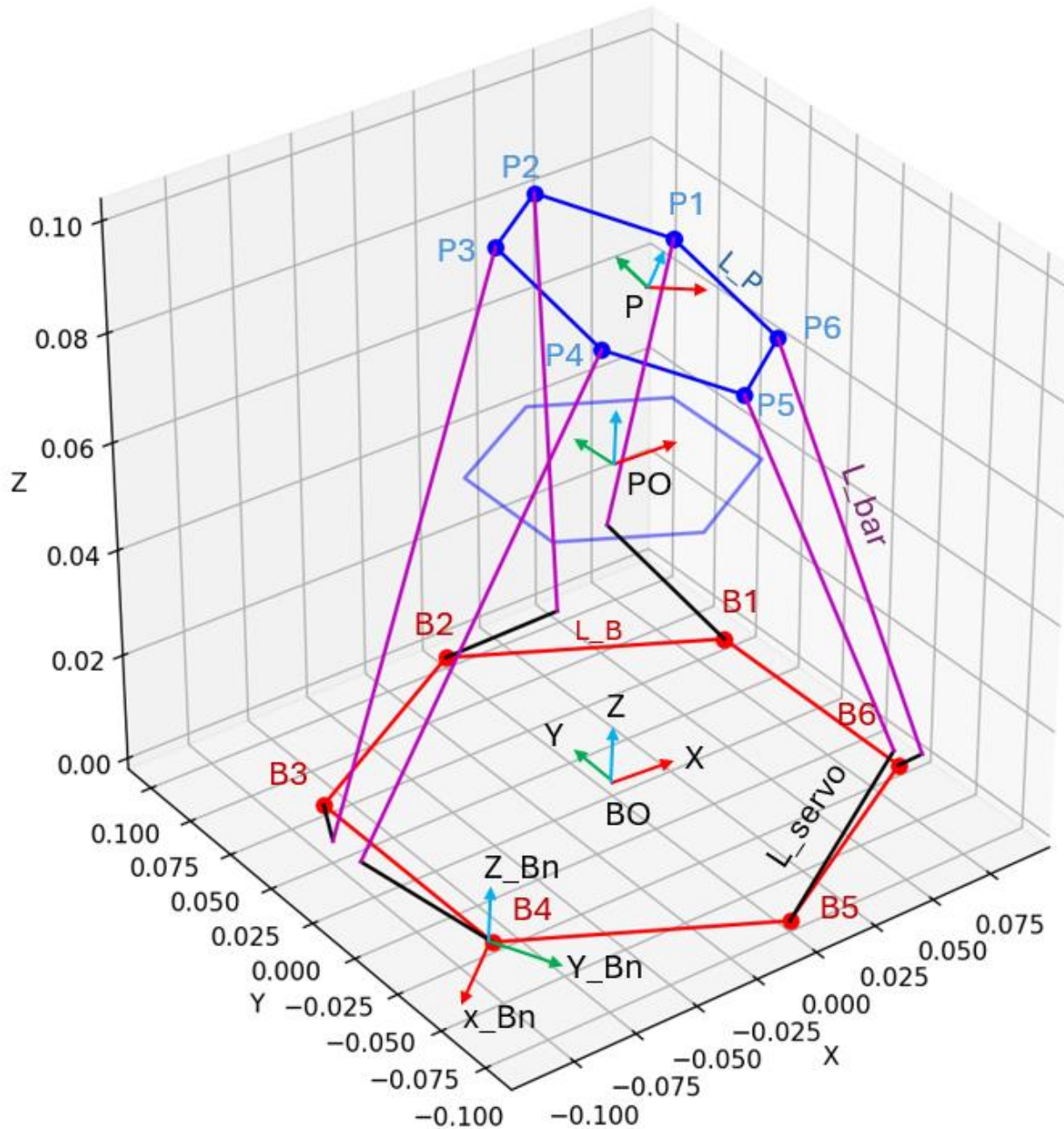
Position and rotation of platform joints ( $B_n$ ) relative to the base origin ( $BO$ )

$${}^{BO}P_{PO} = [X_{PO}, Y_{PO}, Z_{PO}]^T = [0, 0, Z_{PO}]^T$$

$${}^{BO}_{PO}R = Rot(roll_{PO}, pitch_{PO}, yaw_{PO})$$

Position and rotation of platform joints ( $B_n$ ) relative to the base origin ( $BO$ )

$${}^{BO}P_{P_n} = [x_{P_n}, y_{P_n}, z_{P_n}]^T, \quad \text{for } n = \{1 \dots 6\}$$



# Calculations

To find the distance, we first describe the platform joints relative to base origin BO, since having all points in a single coordinate system makes calculation easier.

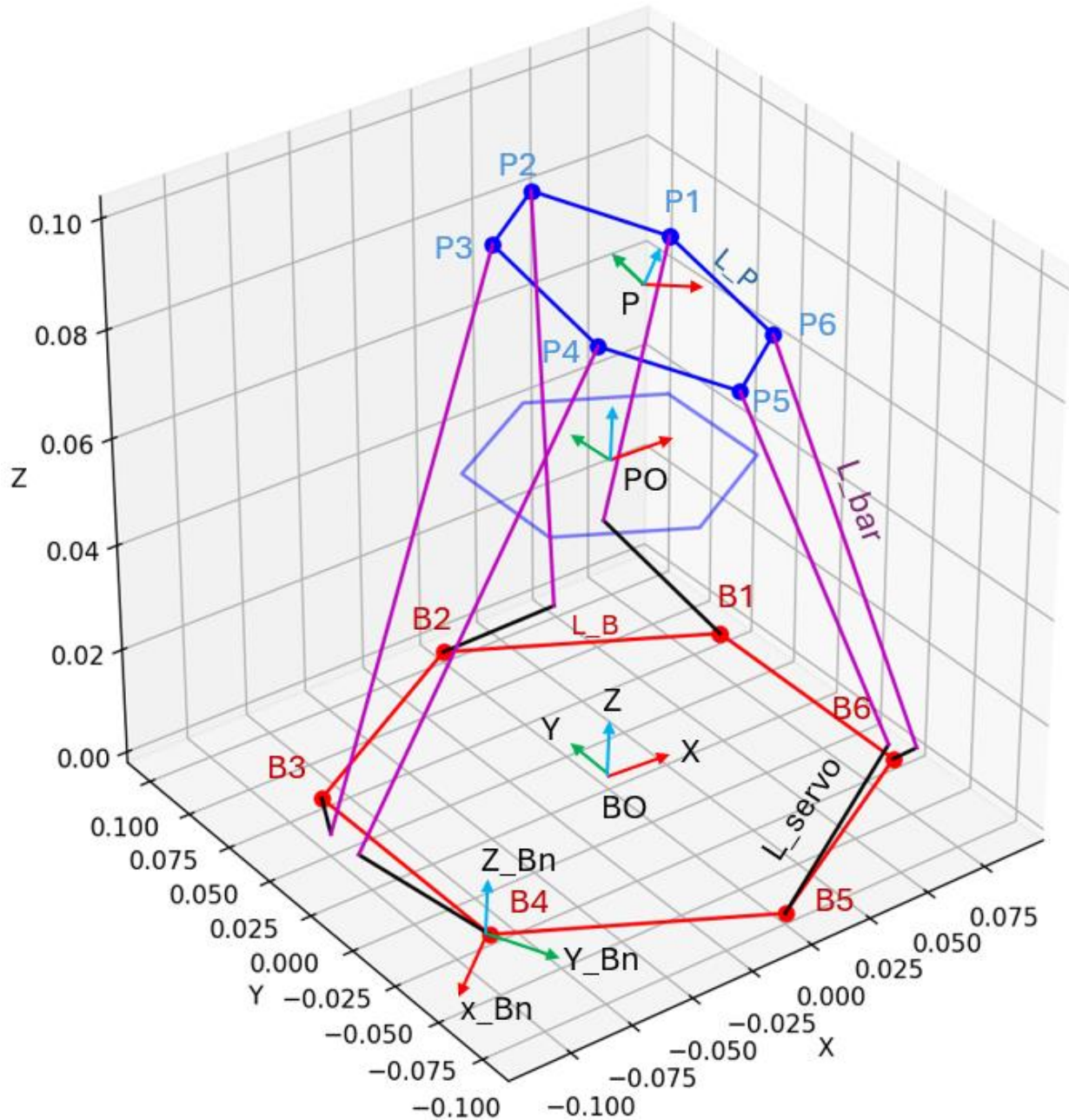
$${}^P P_{Pn} \rightarrow {}^{BO} P_{Pn}$$

This can be achieved by multiplying  ${}^P P_{Pn}$  with a homogeneous transformation matrix  ${}^{BO}_P T$ .

$${}^{BO} P_{Pn} = {}^{BO}_P T \cdot {}^P P_{Pn}$$

Using the property of homogeneous transformation matrix,  ${}^{BO}_P T$  can be further decomposed to,

$${}^{BO}_P T = {}^{BO}_{PO} T \cdot {}^{PO}_P T$$





# Calculations

Using the property of homogeneous transformation matrix,  ${}^{B_0}_PT$  can be further decomposed to,

$${}^{B_0}_PT = {}^{B_0}_{P_0}T \cdot {}^{P_0}_PT$$

Where,

$${}^{P_0}_PT = \begin{bmatrix} {}^{P_0}_PR & {}^{P_0}P_P \\ 000 & 1 \end{bmatrix}, {}^{B_0}_{P_0}T = \begin{bmatrix} {}^{B_0}_{P_0}R & {}^{B_0}P_{P_0} \\ 000 & 1 \end{bmatrix}$$

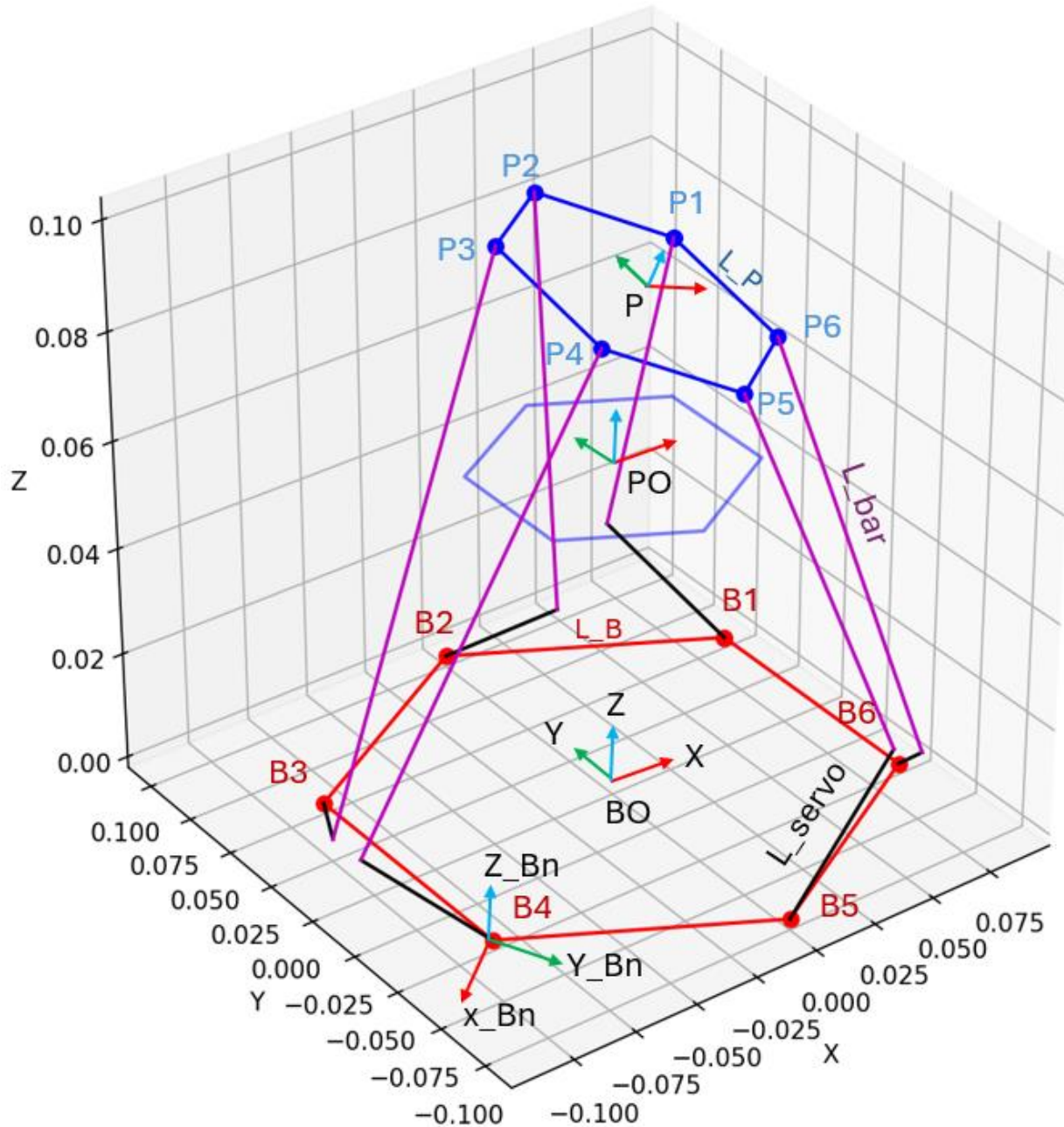
and,

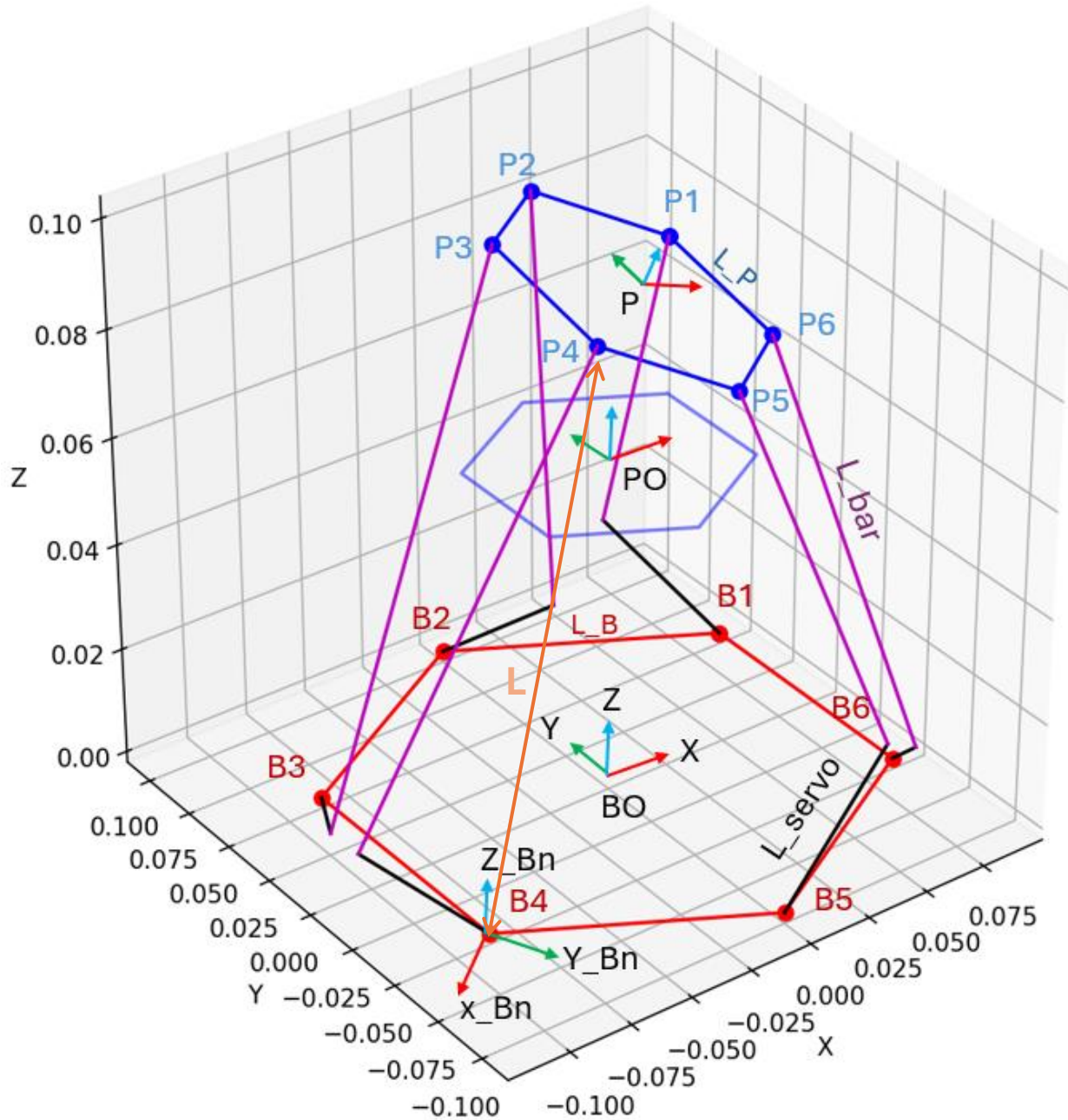
$${}^{P_0}P_P = [X_P, Y_P, Z_P]^T = \text{Func.Input}$$

$${}^{P_0}_PR = \text{Rot}(\text{roll}_P, \text{pitch}_P, \text{yaw}_P) = \text{Func.Input}$$

$${}^{B_0}P_{P_0} = [X_{P_0}, Y_{P_0}, Z_{P_0}]^T = [0, 0, Z_{P_0}]^T$$

$${}^{B_0}_{P_0}R = \text{Rot}(\text{roll}_{P_0}, \text{pitch}_{P_0}, \text{yaw}_{P_0}) = \text{Rot}(0,0,0)$$





## Calculations

Once  ${}^{BO}_PT$  is found, we can find platform position  $P_{Pn}$  described in the coordinate system of the base origin BO.

$${}^{BO}P_{Pn} = {}^{BO}_PT \cdot {}^P P_{Pn}, \quad \text{for } n \in \{1 \dots 6\}$$

The position of base joints  $B_n$  relative to the base origin BO is predefined (i.e., dependent on design itself).

$${}^{BO}P_{Bn} = [X_{Bn}, Y_{Bn}, Z_{Bn}]^T, \quad \text{for } n \in \{1 \dots 6\}$$



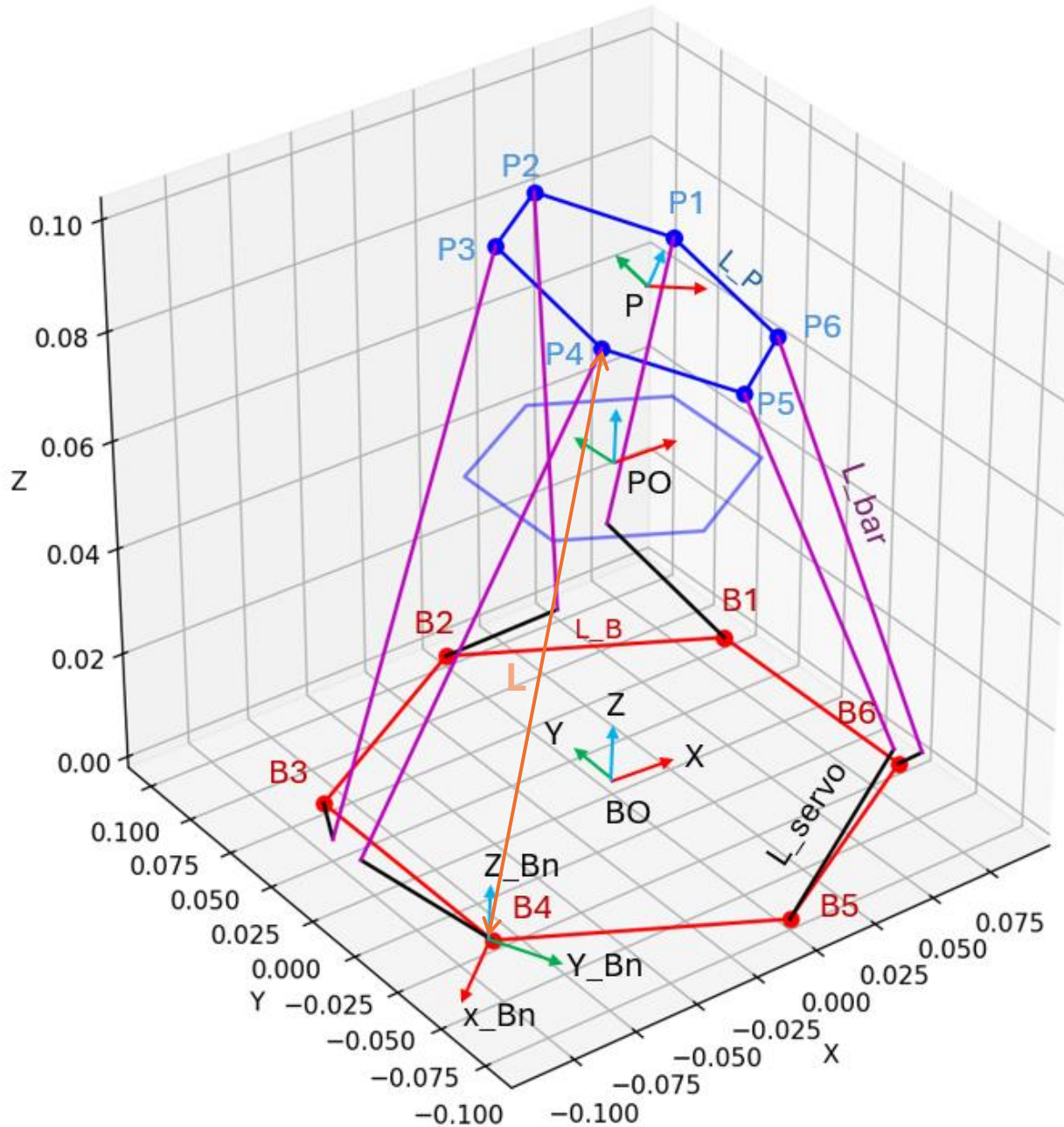
# Calculations

2. Find the servo angle that achieves the distance between  $B_n$  and  $P_n$  while satisfying all required constraints

For linear actuators, the derived lengths between the platform joints  $P_n$  and the base joints  $B_n$  can be used.

$$L_n = |{}^{B0}P_{P_n} - {}^{B0}P_{B_n}| = \text{norm}({}^{B0}P_{P_n} - {}^{B0}P_{B_n})$$

However, for a Stewart Platform with servo motors, the offset due to the servo rotation must be considered.



# Calculations

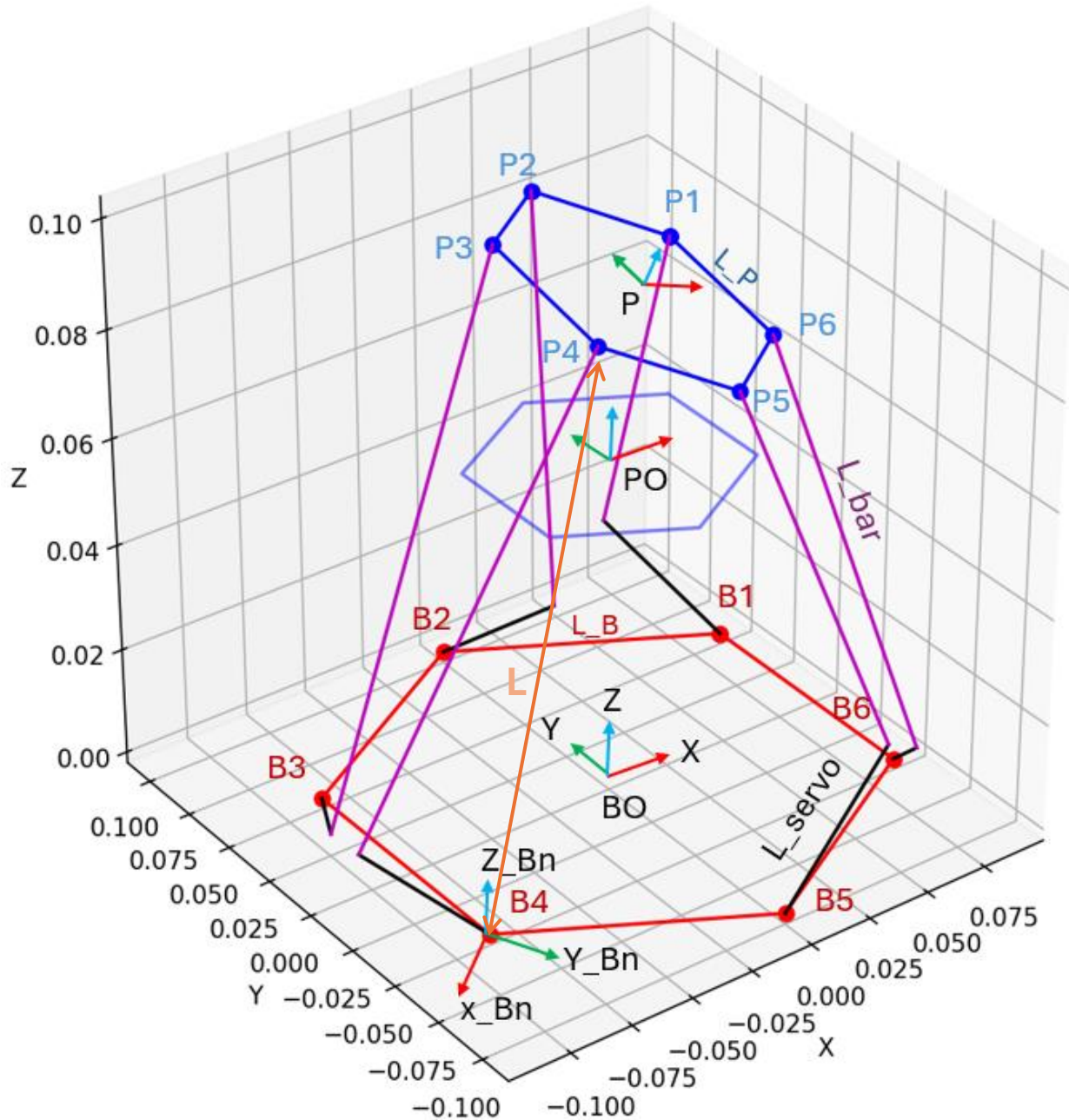
To find the required servo rotations, multiple physical constraints must be satisfied.

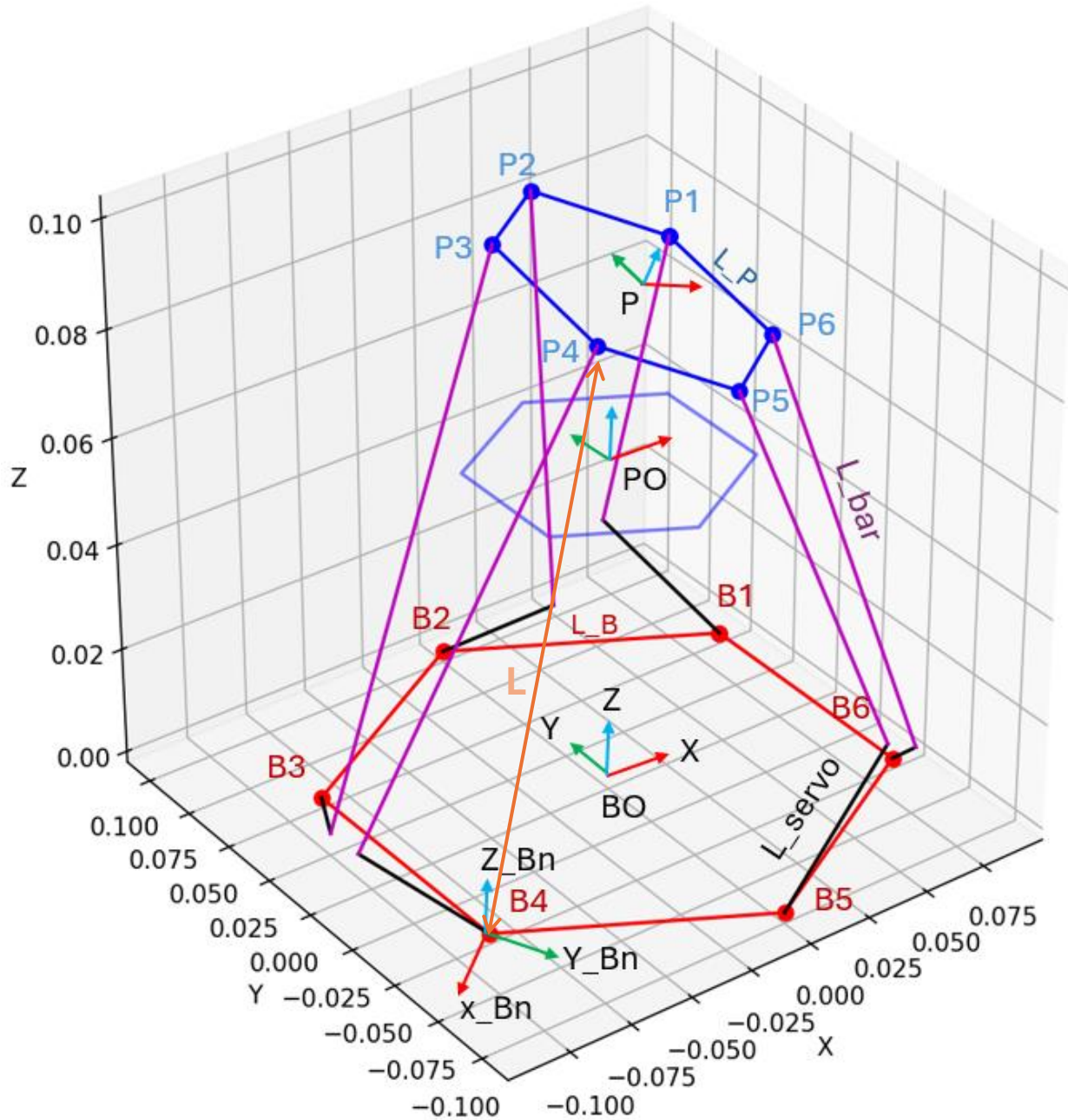
First, the length between the platform joint  $P_n$  and base joints  $B_n$  must satisfy the following as derived earlier.

$$L_n = |{}^{B0}P_{P_n} - {}^{B0}P_{B_n}| = |{}^{Bn}P_{P_n} - {}^{Bn}P_{B_n}|$$

Second, the servo arm can only be on the YZ plane of the base joints' coordinate systems. I.e., the servo rotates around the x-axis of base joint's x-axis.

$$y_{Bn}^2 + z_{Bn}^2 = L_{servo}^2$$





## Calculations

Third, since the length from the end-effector (tip of the servo arm) and the platform joint  $P_n$  is connected by a bar, this length must be constant.

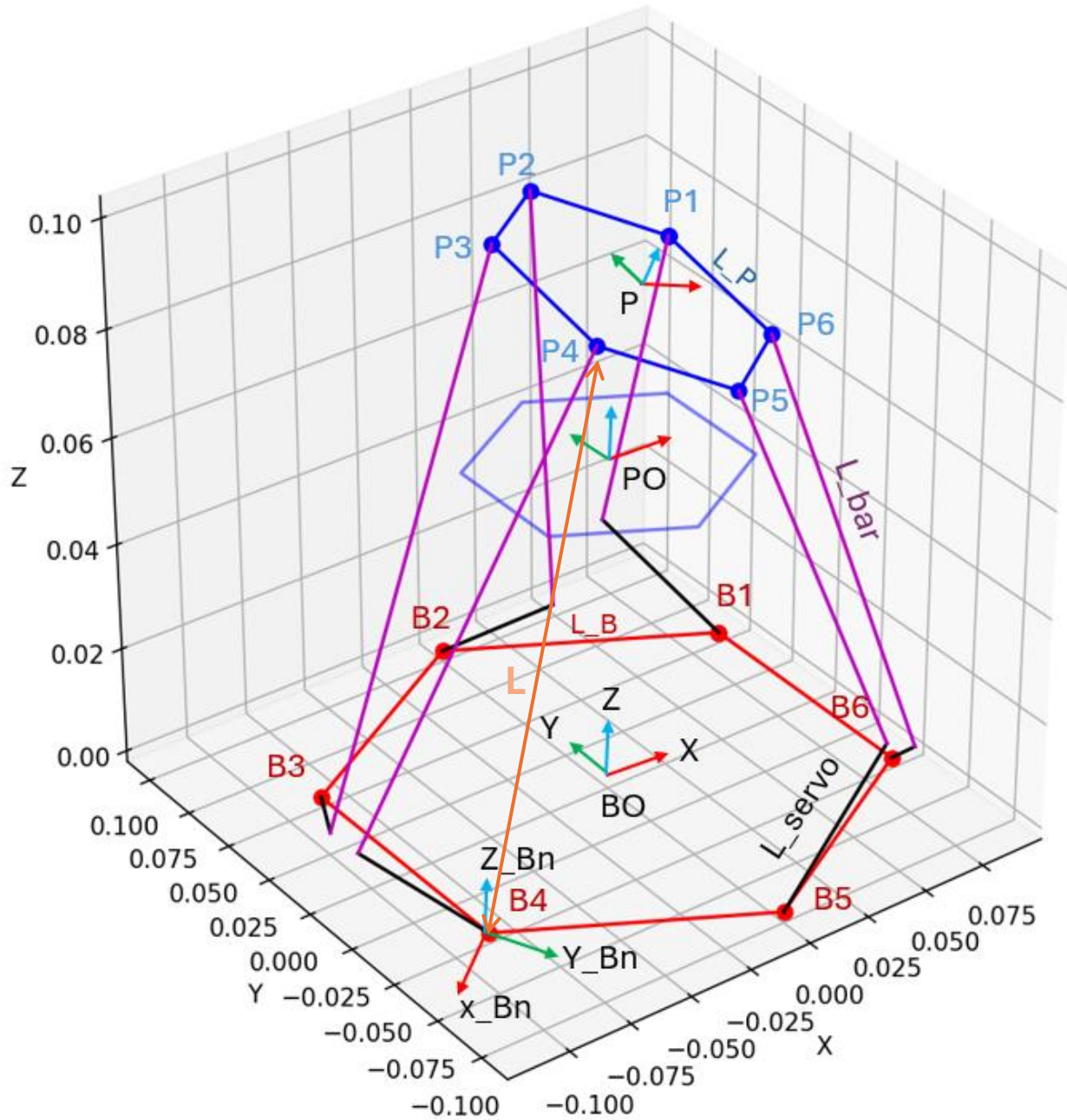
$$(x_{P_n} - x_{B_n})^2 + (y_{P_n} - y_{B_n})^2 + (z_{P_n} - z_{B_n})^2 = L_{\text{bar}}^2$$

Where all coordinates are described relative to base joint  $B_n$ .

Finally, since the joint between the servo arm and bar can only be on the YZ plane of  $B_n$ ,

$$x_{B_n} = 0$$





## Calculations

All constraints:

$$L_n = |{}^{B0}P_{Pn} - {}^{B0}P_{Bn}| = |{}^{Bn}P_{Pn} - {}^{Bn}P_{Bn}|$$

$$y_{Bn}^2 + z_{Bn}^2 = L_{servo}^2$$

$$(x_{Pn} - x_{Bn})^2 + (y_{Pn} - y_{Bn})^2 + (z_{Pn} - z_{Bn})^2 = L_{bar}^2$$

$$x_{Bn} = 0$$

# Calculations

By substitution, following equations can be found.

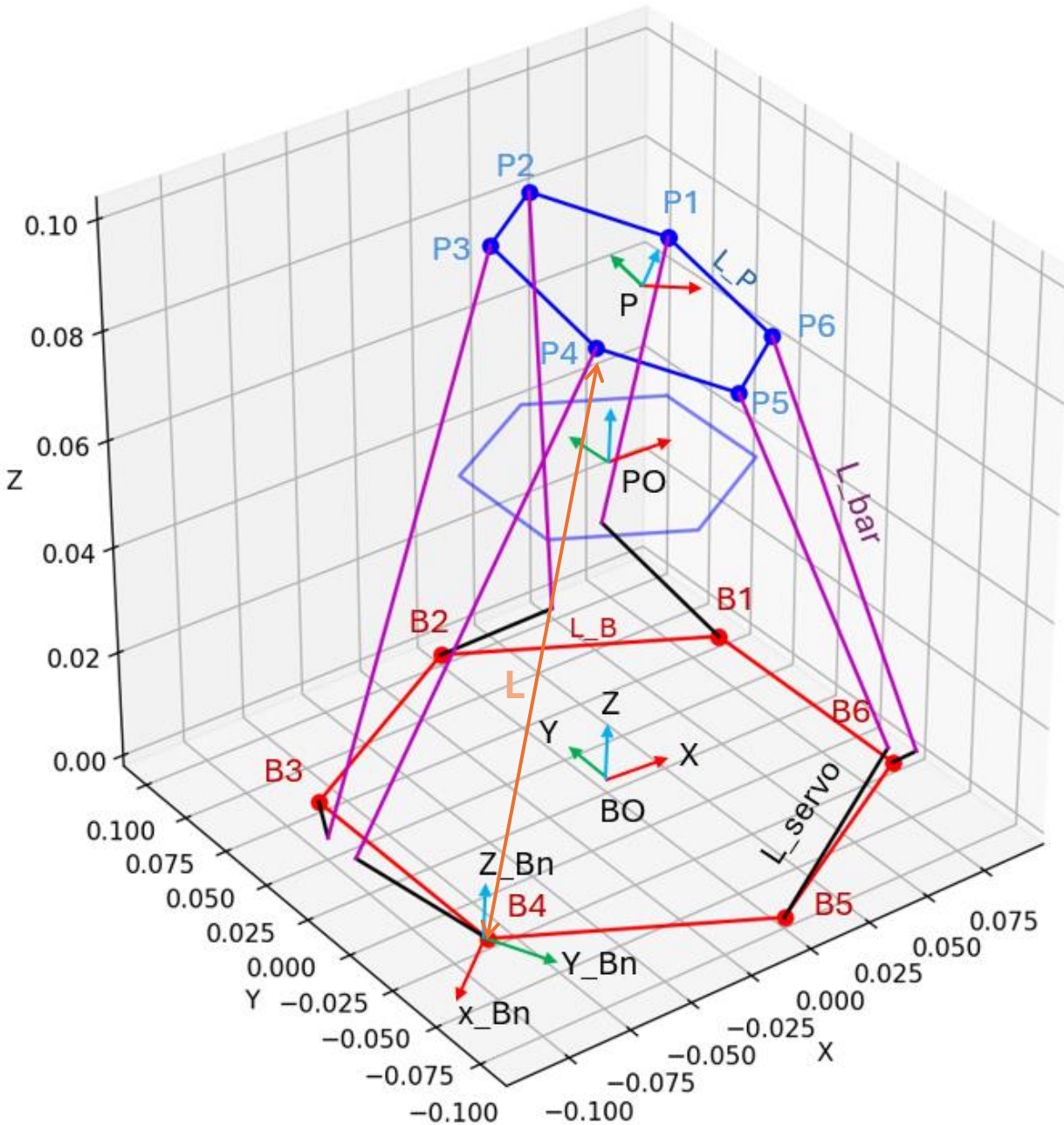
$$(4y_{Pn}^2 + 4z_{Pn}^2) \cdot y_{Bn}^2 + 4y_{Pn}D \cdot y_{Bn} + D^2 - 4z_{Pn}^2L_{servo}^2 = 0$$

$$z_{Bn} = \sqrt{L_{servo}^2 - y_{Bn}^2}$$

Where,

$$D = L_{bar}^2 - L_{servo}^2 - x_{Pn}^2 - y_{Pn}^2 - z_{Pn}^2$$

Solving the quadratic equation, it is possible to find  $y_{Bn}$ , and by substituting,  $z_{Bn}$  can be found.



# Calculations

Once  $y_{Bn}$  and  $z_{Bn}$  are found, check the solution satisfy the final constraint,

$$L_n = |{}^{B0}P_{Pn} - {}^{B0}P_{Bn}| = |{}^{Bn}P_{Pn} - {}^{Bn}P_{Bn}|$$

Where,

$${}^{Bn}P_{Pn} = [x_{Pn}, y_{Pn}, z_{Pn}]^T$$

$${}^{Bn}P_{Bn} = [x_{Bn}, y_{Bn}, z_{Bn}]^T$$

Finally, the servo angles can be found by,

$$\theta = \arctan\left(\frac{z_{Bn}}{y_{Bn}}\right)$$

