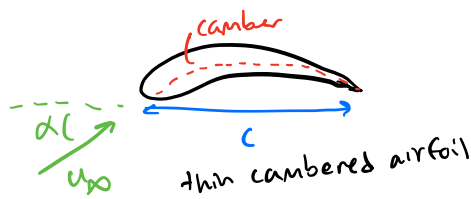
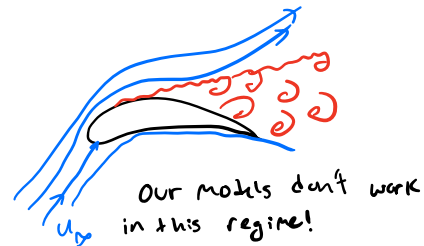
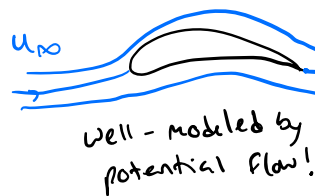
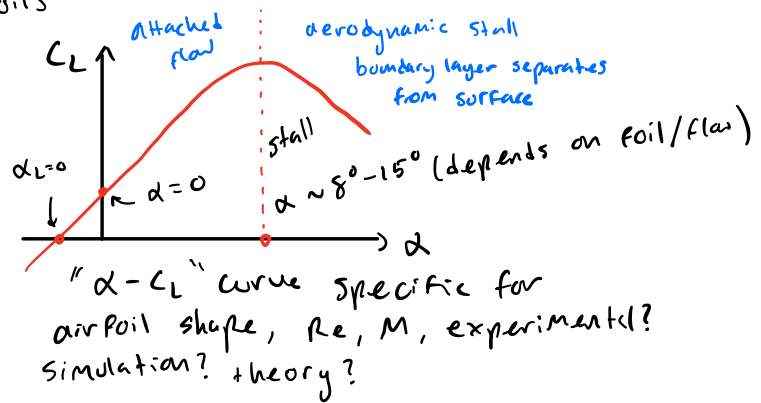


Potential flow over airfoils



As $\alpha \uparrow$, $C_L \uparrow$, until aerodyn. stall



Techniques for flow models:

1. Joukowski Transformation
 - complex analysis



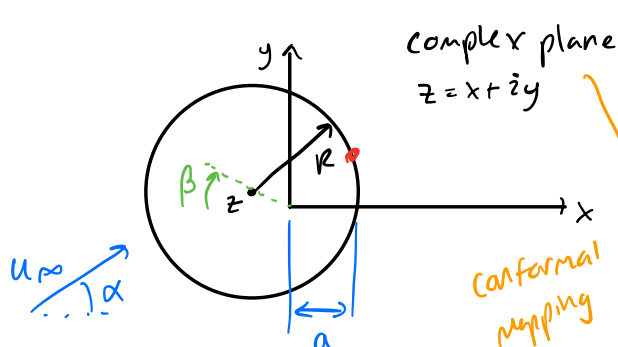
2. Thin airfoil theory
 - use potential flow elements to construct arbitrary airfoil shapes

3. Computational Resources
 - Input any airfoil geometry & compute flow fields & forces

- * 4. Wind tunnel testing

~ next semester

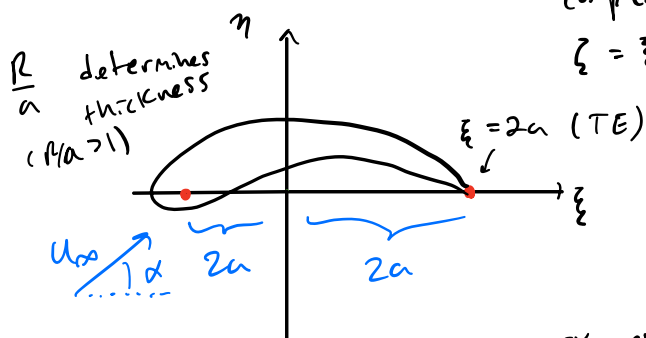
L23: Joukowski Transform



$$F(z) = \phi + i\psi$$

$$F(z) = U_{\infty} e^{-i\alpha} \left\{ (z - z_0) + \frac{R^2 e^{2i\alpha}}{(z - z_0)} \right\} - \frac{i\Gamma}{2\pi} \ln \left\{ \frac{(z - z_0) e^{-i\alpha}}{R} \right\}$$

β determines camber



complex plane
 $\zeta = \xi + i\eta$

$$\frac{\zeta}{a} = \frac{z}{a} + \frac{a}{z}$$

$$\zeta = z + \frac{a^2}{z}$$

surface of airfoil:

$$\frac{\zeta}{a} = 1 + \frac{R}{a} \left\{ e^{i\theta} - e^{i\beta} \right\} + \left[1 + \frac{R}{a} \left\{ e^{i\theta} - e^{i\beta} \right\} \right]^{-1}$$

(z-plane)

Joukowski class of airfoils!

$$\frac{dF}{dz} = u - iv \quad (\text{Cauchy-Riemann eqns})$$

$$\frac{dF}{d\zeta} = u_{\zeta} - i u_{\eta} = \frac{dF}{dz} \cdot \frac{dz}{d\zeta}$$

mapping

cylinder solution

$C_p \rightarrow$ forces!

Lecture 24: Source panel method

Current method: given ψ or $\phi \rightarrow$ determine geometry $\rightarrow \vec{V}, C_p, C_D, C_L$

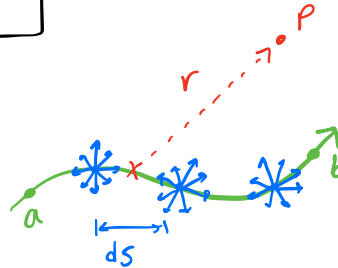
Panel methods: given geometry \rightarrow compute ϕ or ψ

preliminary concept: source sheet

Imagine arbitrary point P ,
distance r from element ds

$$d\phi = \frac{\lambda ds}{2\pi} \ln r$$

contribution of element to
potential function at P



each element ds has strength
equal to λds

source sheet has strength
per unit length $\lambda = \lambda(s)$

$$\phi_P = \int_a^b \frac{\lambda ds}{2\pi} \ln r$$

flow potential at P
(contribution from all elements)

Strategy

- 1) Define geometry (airfoil), divide into N "panels"
- 2) Sum contribution from each panel
- 3) Enforce B.C. : no flow through walls ; $\vec{V}_n = 0$
- 4) Results yield a system of N equations
- 5) Solve

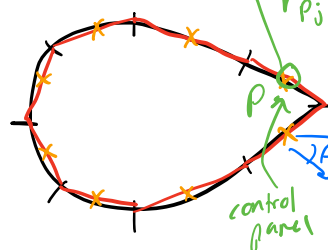
e.g. $N=8$ panels

point P has a potential function
influenced by all 8 panels

enforce $\vec{V}_n = 0$ at control panel

$$v_n = \frac{\partial}{\partial n_i} [\phi(x_i, y_i)]$$

$$v_n + V_\infty \cos \beta_i = 0$$



$$r_{Pj} = \sqrt{(x-x_j)^2 + (y-y_j)^2}$$

distance to P from panel j

$$\Delta \phi_j = \frac{\lambda_j}{2\pi} \int \ln r_{Pj} ds_j$$

$$\phi = \sum_{j=1}^N \Delta \phi_j$$

Next, to apply B.C., we move P to midpoint
of we call this the control panel

I_{ij} is a function of geometry only (not flow)

$$V_n = \frac{\lambda_i}{2} + \sum_{j=1}^N \frac{\lambda_j}{2\pi} \int_j \frac{\partial}{\partial n} (\ln r_{ij}) ds_j$$

contrib. from self contrib. from other panels

$$\boxed{\frac{\lambda_i}{2} + \sum_{j=1}^N \frac{\lambda_j}{2\pi} I_{ij} + V_\infty \cos \beta_i = 0}$$

source panel method ($i \neq j$)

→ Solve for $\lambda_1, \lambda_2, \lambda_3$, etc.

$$V_s = \frac{\partial \Phi}{\partial s} = \sum_{j=1}^N \frac{\lambda_j}{2\pi} \frac{\partial}{\partial s} (\ln r_{ij}) ds_j$$

$V_i = V_s + V_{\infty, s}$ = velocity @ panel surface

$$C_{p, i} = 1 - (V_i/V_\infty)^2$$

Notes

- input any geometry ✓
- non-lifting bodies, drag estimation