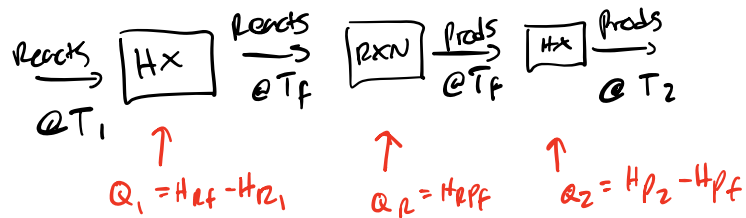


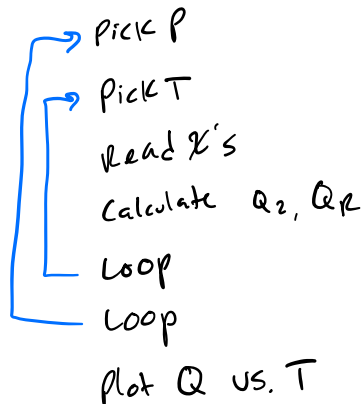
HW12 due Monday 12/16 latest

### Recap



To determine  $T_2$ :

- Assume  $T_1 = T_f$
- Net heat  $Q = Q_R + Q_2$
- Pick chemical model
- Use plots like fig. 2.14 ( $x$ 's vs.  $T$ ;  $P$  as param.)



values of  $T$  where  $Q=0$  called adiabatic flame temp  
(all heat goes into raising  $T$  of products)

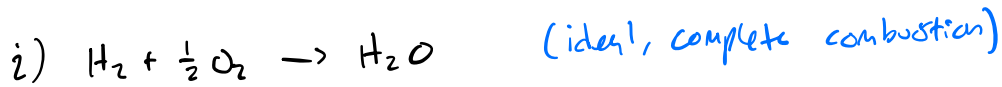
In fig. 2.15, shape/values of curves depend on chemical model.

~~~~~

Revisit  $H_2 - O_2$  rxn to compare complete vs. incomplete comb.

$$Q = Q_2 + Q_P = 0 \quad (\text{adiabatic})$$

$$H_{P_2} - H_{P_f} = -H_{R_{P_f}} \quad (1)$$



$$H_{R_{P_f}} = -241.83 \frac{\text{MJ}}{\text{kmol}} \quad (@T_f = 298\text{K}) \quad \begin{array}{cc} +0 & +0 \\ \uparrow & \uparrow \\ H_2 & O_2 \end{array}$$

$$Q_2 = H_{P_2} - H_{P_f}$$

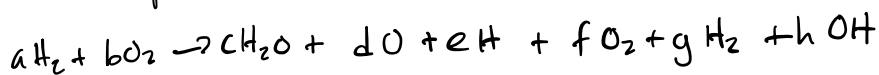
$$H_P(T) = \int_{0K}^T \bar{C}_P(T) dT$$

Plotted in fig. 2.5 (solve for  $H_{P_2}$  & find  $H_{P_2}$  on chart)

enforcement of eq. (1)  $\left\{ \begin{array}{l} \text{enter fig. 2.5 w/ } \bar{h} = 241.8 \text{ MJ/kmol} \\ \text{exit w/ } T = 5000\text{K} \end{array} \right. \quad @ P = 100 \text{ atm}$

Note that @ 5000K  $H_2O$  dissociates a lot!  
 $\rightarrow$  our choice of model not accurate

Instead pick model:



$\rightarrow$  pick  $P, T$ , etc.

Generate fig. 2.15 & find  $T_{\text{adiabatic}}$  on  $Q=0$  line

$$\rightarrow T_{\text{adb}} \approx 3800\text{K}$$

& read corresponding  $x$ 's from fig. 2.14

## Summary

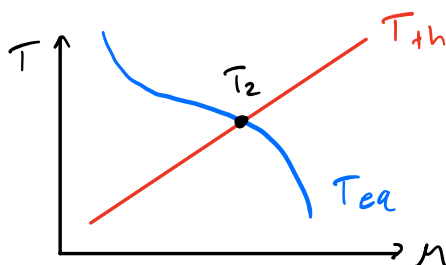
- select chemical model
- combine thermodynamics & chem. EQ.  
into single plot (like fig. 2.15)
- Determine  $T_{adb}$  from  $Q=0$  in fig. 2.15
- Determine composition from 2.14

In HW11 p. 4

$$\text{unknowns} \begin{cases} M \\ v \\ \xi \\ T \end{cases}$$

- pick  $M$
- Determine  $v$  &  $\xi$  from mass balance
  - Determine  $T_{th}$  from thermo (e-bal)
  - "  $T_{eq}$  from chem. EQ via  $K_p$  (analyt. expr. for  $K_p(T)$ )
- loop

plot  $T$  vs.  $M$



Intersection is  $T_2$

→ balancing heats of formation & thermo, i.e. chemistry & thermo

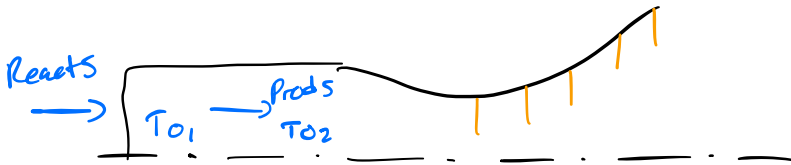
the higher  $M$ , the more complete combustion, thus higher  $T$   
(less waste used to decompose products)

For a well-designed combustion chamber, the time for mixing & the reaction altogether  $\ll$  residence time

→ chem. EQ. is established

usually  $T$  high enough for some dissociation to occur

## § 5 Evaluation of ISP ( $u_e$ )



$$T_{02} = T_{\text{adib}} = T_2 = T_0$$

$\leftarrow$  in 1-D gas dynamics

Previously  
in nozzle:

$r = \text{const}$ ,  $p \downarrow$ ,  $T \downarrow$  → this changes chem EQ!!  
- recombination of products  
-  $\gamma$  changes

could calculate new  $\gamma$  & properties at different segments of nozzle - However gas is moving fast now, so chemical equilibrium doesn't complete

→ Non-equilibrium flow