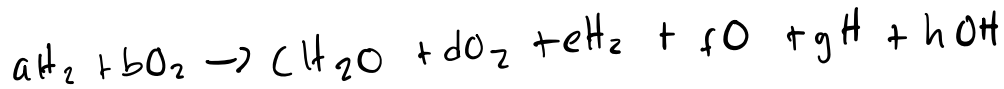


## Recap



$$\text{Mass bal.} \quad \begin{cases} 2a = 2c + 2e + g + h \\ 2b = c + 2d + f + h \end{cases}$$

$$\text{Equil.} \quad \begin{cases} K_p, P_m^{-1} = \frac{c^2 d}{c^2 (c + d + e + f + g + h)} \\ \vdots \end{cases}$$

①

→ Kps in plots

②

③

solve system of nonlinear algebraic eqns ①-⑥

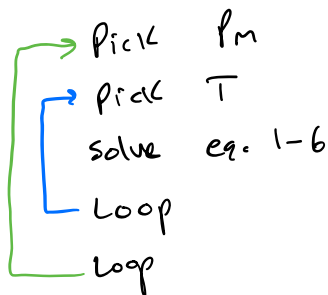
④

⑤

⑥

If  $T, P_m$  known → Find  $c, d, e, \dots$   
= product composition

If  $T, P_m$  unknown,



For  $\text{H}_2\text{O}$ , simplified reactions are in fig. 2.13  
more complex rxn in fig. 2.14

## Remarks

- low temperature  $\rightarrow$  less dissociation (more  $H_2O$ )
- In simplified system (fig. 2.13) high  $P \rightarrow$  less dissociation
- In more complicated sys. (fig. 2.14)

$H_2, O_2, OH$  curves not monotonic

@ Low  $T$  & high  $P \rightarrow$  lower  $H_2, O_2, OH$  concentration

@ High  $T$  & high  $P \rightarrow$  higher  $H_2, O_2, OH$  concentration

## Summary

If composition of products is known find  $T$  from thermo

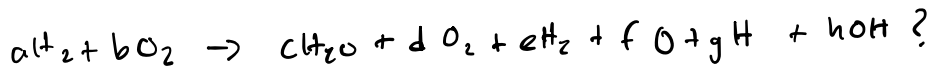
If  $T$  is known, find composition from chem. equil.

What if neither comp. or  $T$  is known?

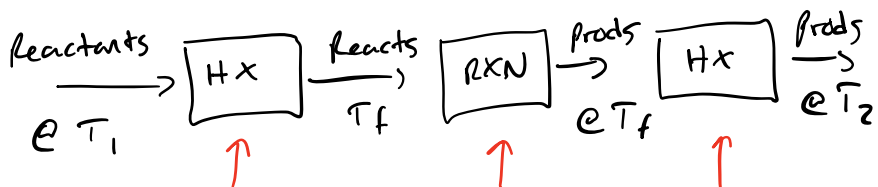
How do we determine both?

## Flame temperature

How much heat is released in



Recall simple model



$$Q_1 = H_{Rf} - H_{Ri} \quad Q_R = H_{Rpf} \quad Q_2 = H_{P_2} - H_{P_1}$$

heat of formation  
from reactants to products  
@  $T_f$

For simplicity, assume  $T_i = T_f \rightarrow Q_1 = 0$

$$H_{RPF} = \sum_j (n_j Q_{fj})_{\text{prods}} - \sum_i (n_i Q_{fi})_{\text{reacts}}$$

$$Q_2 = H_{P_2} - H_{RPF} = \sum_j n_j (\bar{h} - \bar{h}_0)_{\text{prods}}$$

$\bar{h} = \frac{\text{enthalpy}}{\text{mole}}$

enthalpy @  $T_f$

enthalpy @  $T_2 (=T)$

In this class  $\bar{h}(T) = \bar{c}_p T$   
more rigorously,

$$\bar{h}(T) = \int_{0K}^T \bar{c}_p(T) dT$$

Net heat exchanged between sys. & surr

$$Q = \cancel{Q_1}^0 + Q_P + Q_2$$

If  $Q > 0$ , supplied to sys  
 $Q < 0$ , removed from sys.

From fig. 2.14, for each  $T, P$  pair, have all  $x_j$ 's (i.e.  $n_j$ 's)

Can plot  $Q$  vs.  $T$  w/  $P$  as parameter

Results in fig. 2.15

### Remarks

@ Low  $T$ ,  $Q < 0$ : Even after products reach  $T = 3000K$  ( $P = 1 \text{ atm}$ )  
Heat is released to outside

@ High  $T$ ,  $Q > 0$ : Even after combustion, for products to reach  $4000K$   
(at  $P_i = 1 \text{ atm}$ ), must supply heat

- @ Low  $P$ , High dissociation requires more heat to reach a high temperature
- Line through  $Q=0$  intersects the  $Q$ -lines (parameterized by  $P$ ) @ values of  $T$  called "adiabatic flame temperature"
- corresponds to  $T_2$  in schematic provided system is insulated

Revisit example to compare complete vs. incomplete combustion  
w/o dissociation      w/ dissociation

Recall figs 2.13 (simplified) & 2.14 (more complete model)

$$Q = \underbrace{H_{Rf} - H_{Ri}}_{Q_1} + \underbrace{H_{Rpf}}_{Q_R} + \underbrace{(H_{P2} - H_{Pf})}_{Q_2}$$