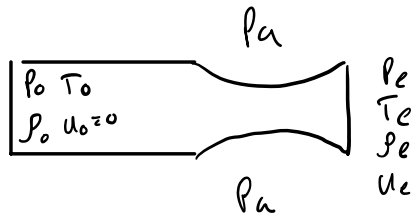


Important



combustion chamber
 \equiv
 stagnation conditions
 \equiv
 Reservoir

stagnation: $u_0 = 0$

In reality, $u_0 \neq 0$ just enough
 for combustion products to enter
 the nozzle

$$\frac{u_0^2}{2} \ll h_0$$

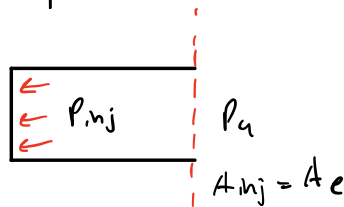
$P_a \equiv$ ambient pressure
 in general:

- i) $P_e \neq P_a$
- ii) $P_a \neq 1 \text{ atm}$

Qualitative physical description

i) No nozzle

→ Thrust due to pressure
 against CC end wall



ii) Purely convergent nozzle

- assume A_e is the same
 as no nozzle.

- area of end wall is larger
 than before

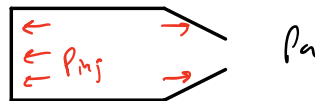
- P_{inj} same as before

→ Pressure against ^{inside} convergent walls acts against thrust

→ Pressure against outside of convergent wall acts with thrust

→ $P_{inj} - P_a$ same as before but A_{inj} larger than before

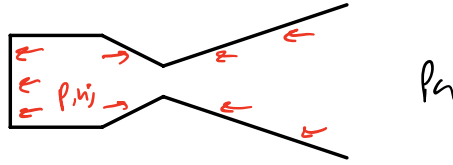
→ Net result: higher thrust than before



iii) Convergent-divergent nozzle

- P inside divergent wall is with thrust

- P outside divergent wall is against thrust



- $P(x)$ inside divergent decreases monotonically

- in "first part" of div: $P(x) > P_a$

- in "second part" of div: $P(x) < P_a$

→ Net effect: higher thrust than i) & ii)

All this is still described by

$$J = \dot{m} u_e + (P_e - P_a) A_e$$

The case $P_e = P_a$ is called "optimum expansion"

Must develop the math to predict

$\left. \begin{matrix} \dot{m} \\ P_e \\ u_e \end{matrix} \right\}$ Based on $\left\{ \begin{matrix} \text{chemical properties} \\ \text{nozzle geometry} \\ \text{stagnation conditions} \end{matrix} \right.$

In general, for assigned chemical species & stag. cond

$\left. \begin{matrix} P = P(x) \\ \rho = \rho(x) \\ T = T(x) \\ u = u(x) \end{matrix} \right\}$ Because $\left\{ \begin{matrix} A = A(x) \\ \text{shock wave} \\ \dot{Q} \neq 0, \text{ heat transfer} \\ \mu \neq 0, \text{ viscous effects} \end{matrix} \right. \}$ ignore

Start w/ $A = A(x)$, NO SHOCKS, $\dot{Q} = \dot{M} = 0$

Strategy:

o) introduce Mach #

i) Develop $p = p(M)$, $\rho = \rho(M)$, $T = T(M)$, $u = u(M)$

ii) Develop $M = M(A(x))$ Relation

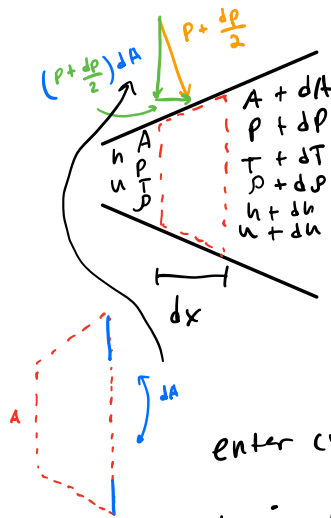
iii) Reassemble

→ 4 unknowns
 ↳ 4 equations

$\left\{ \begin{array}{l} \text{cons. mass} \\ \text{cons. momentum} \\ \text{cons. energy} \\ \text{Eq. of state} \end{array} \right.$	we'll use ideal gas law
	→ can use more complex eq.s

1. Governing equations

Write in form for infinitesimally small volume



Mass

$$\rho u A = \text{const.}$$

$$d(\rho u A) = 0 \quad u A d\rho + \rho A du + \rho u dA = 0$$

$$\div \rho u A :$$

$$\boxed{\frac{d\rho}{\rho} + \frac{du}{u} + \frac{dA}{A} = 0}$$

Momentum

Recall $\frac{d}{dt} \int_{CV} \rho u \, dV + \int_{CS} u \rho \mathbf{u} \cdot d\mathbf{A} = - \int_{CS} p \, d\mathbf{A} + \mathbf{F}_{\text{shear}} \quad \overset{SS}{\text{SS}}$

enter CV: negative

$$- u \dot{m} + (u + du) \dot{m} = pA - (p + dp)(A + dA) + (p + \frac{dp}{2}) dA$$

$$\underset{\substack{\uparrow \\ \rho u A}}{du \dot{m}} = \cancel{pA} - \cancel{pA} - \cancel{p dA} - \cancel{dpA} - \cancel{dp dA} + \cancel{pA} + \frac{dp}{2} dA$$

\downarrow H.O.T.
 \downarrow H.O.T.

→ divide by dx

$$\rho u A \frac{du}{dx} = - A \frac{dp}{dx}$$

→ $\boxed{\rho u \frac{du}{dx} = - \frac{dp}{dx}}$ Euler's Eqn