

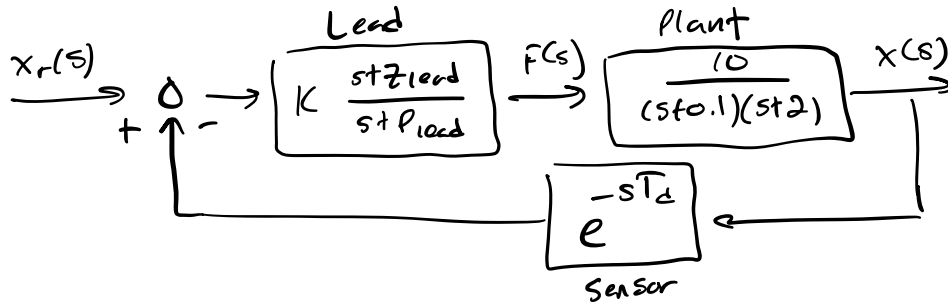
Problem 1

$$G(s) = \frac{x(s)}{F(s)} = \frac{10}{(s+0.1)(s+2)}$$

→ lead compensated feedback, $T_d = 0.015$

$$PM > 60^\circ, GM > 15 \text{ dB}$$

ω_{BW} as high as possible



→ Assume 75° possible from lead

$$\varphi_{des} = -180^\circ + PM = -180^\circ + 60^\circ = -120^\circ$$

$$\varphi_{des} = \angle G(s) + \varphi_{lead} = -120^\circ = \angle G(s) + 75^\circ$$

$$\rightarrow \angle G(s)|_{\omega_{des}} = -195^\circ \rightarrow \text{MATLAB: } \omega_{des} \approx 32 \text{ rad/s}$$

$$\varphi_{lead} \approx 75^\circ: \alpha = \frac{1 - \sin 75^\circ}{1 + \sin 75^\circ} = 0.01733, \frac{1}{\alpha} = 57.7, \text{ high } \omega \text{ OK}$$

$$z = \omega_{max} \sqrt{\alpha} \approx 4.213$$

$$p = \frac{\omega_c}{\sqrt{\alpha}} \approx 243.064$$

$$\rightarrow D_{lead} = K \left(\frac{s + 4.213}{s + 243.064} \right)$$

$$|G(j\omega_c) D(j\omega_c) H(j\omega_c)| = 1 \rightarrow \text{MATLAB} \rightarrow K = 779.33$$

$$\rightarrow D_{lead} = 779.33 \left(\frac{s + 4.213}{s + 243.064} \right)$$

Check in MATLAB:

$$PM = 60.2^\circ \checkmark, GM = 11.7 \text{ dB } \times$$

→ Iterate, lower ω_c until GM met

$$\omega / \omega_c = 22 \text{ rad/s}, PM = 66.8^\circ \checkmark, GM = 15.1 \text{ dB } \checkmark$$

Problem 2

$$\text{EOM: } \begin{cases} I_1 \ddot{\theta}_1 + b_s \dot{\theta}_1 - b_s \dot{\theta}_2 + k_s \theta_1 - k_s \theta_2 = \tau_1 \\ I_2 \ddot{\theta}_2 - b_s \dot{\theta}_1 + b_s \dot{\theta}_2 - k_s \theta_1 + k_s \theta_2 = 0 \end{cases}, \quad G(s) = \frac{\theta_2(s)}{\tau_1(s)}$$

a) $G(s)$

$$I_2 s^2 \theta_2(s) - b_s s \theta_1(s) + b_s s \theta_2(s) - k_s \theta_1(s) + k_s \theta_2(s) = 0$$

$$(I_2 s^2 + b_s s + k_s) \theta_2(s) = (b_s s + k_s) \theta_1(s) \rightarrow \theta_1(s) = \theta_2(s) \frac{I_2 s^2 + b_s s + k_s}{b_s s + k_s} \quad (1)$$

$$I_1 s^2 \theta_1(s) + b_s s \theta_1(s) - b_s s \theta_2(s) + k_s \theta_1(s) - k_s \theta_2(s) = \tau_1(s)$$

$$(I_1 s^2 + b_s s + k_s) \theta_1(s) + (-b_s s - k_s) \theta_2(s) = \tau_1(s) \quad (2)$$

Sub (1) into (2):

$$\frac{(I_1 s^2 + b_s s + k_s)(I_2 s^2 + b_s s + k_s)}{(b_s s + k_s)} \theta_2(s) - (b_s s + k_s) \theta_2(s) = \tau_1(s)$$

$$\rightarrow \frac{\theta_2(s)}{\tau_1(s)} = G(s) = \left[\frac{(I_1 s^2 + b_s s + k_s)(I_2 s^2 + b_s s + k_s)}{(b_s s + k_s)} - (b_s s + k_s) \right]^{-1}$$

$$\rightarrow G(s) = \frac{(b_s s + k_s)}{(I_1 s^2 + b_s s + k_s)(I_2 s^2 + b_s s + k_s) - (b_s s + k_s)^2}$$

$$\rightarrow G(s) = \frac{0.002 s + 36}{s^2 (0.01 s^2 + 0.00202 s + 36.36)}$$

b) Lead compensator, $PM = 60^\circ$, $\omega_c = 3 \text{ rad/s}$, Find G_M

$$\varphi_{des} = -120^\circ$$

$$\angle G(s) |_{\omega=3 \text{ rad/s}} = -180^\circ \rightarrow \varphi_{lead} = 60^\circ$$

$$\rightarrow \alpha = \frac{1 - \sin 60^\circ}{1 + \sin 60^\circ} = 0.0718$$

$$z = \omega_c \sqrt{\alpha} \approx 0.804, \quad p = \frac{\omega_c}{\sqrt{\alpha}} \approx 11.2$$

$$\rightarrow \text{MATLAB: } D_{lead} = 33.85 \frac{(s + 0.804)}{(s + 11.2)}$$

Nyquist / Rlocus: $GM \approx 2.06$

c)

lead & low pass

$$\rightarrow \left(K \frac{s+z_{lead}}{s+p_{lead}} \left(\frac{w_{lp}}{s+w_{lp}} \right) \right) \rightarrow \text{matlab}$$

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% Written by Kyle Adler for ME446

Problem 1

find wdes where angle $G(s) = -195\text{deg}$

```
s = tf('s');
Gsys = 10/( (s+0.1)*(s+2) );
Td = 0.01; % seconds, time delay
H = exp(-s*Td); %time delay function
bode(Gsys*H)
wc = 22; % wdes, initially 32, iterated down to 22 to achieve GM requirement

% find lead gain
K=1; Dlead = K*(s+4.213)/(s+243.064); % lead with K=1 to solve for K
[m,p] = bode(Gsys*H*Dlead,wc)
K = 1/m
Dlead = K*(s+4.213)/(s+243.064);

% evalutate system
margin(Gsys*H*Dlead)
```

$m =$

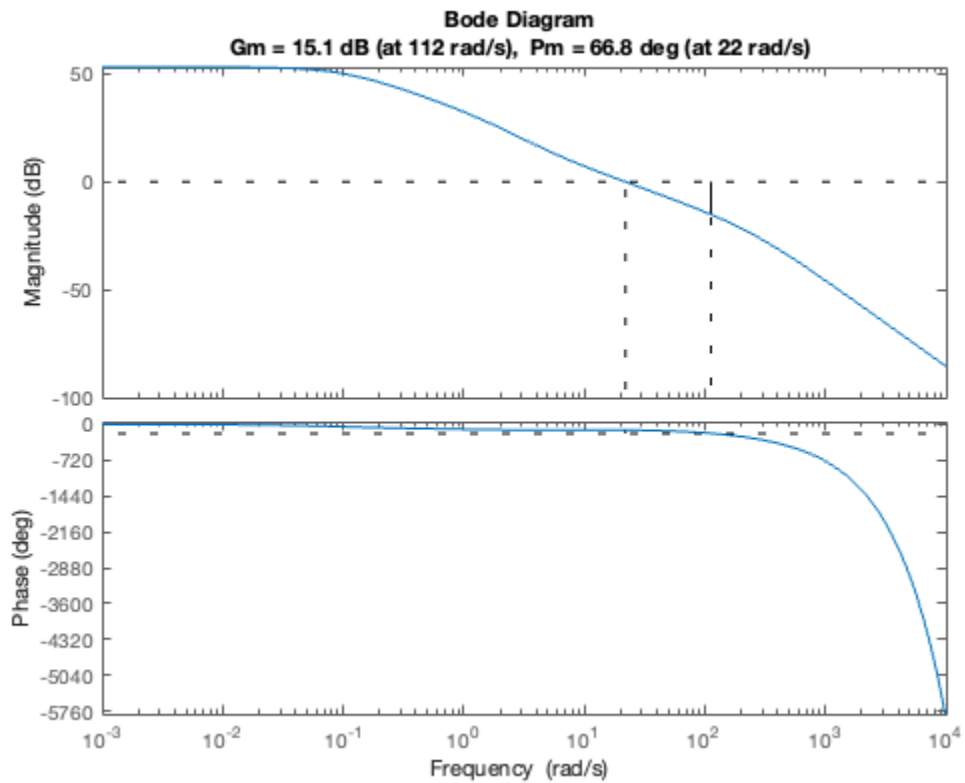
0.0019

$p =$

-113.1629

$K =$

529.5244



Problem 2b

```
bs = 0.002; ks = 36; I1 = 1.0; I2 = 0.01; % constants
Gsys = (bs*s+ks) / ( (I1*s^2+bs*s+ks)*(I2*s^2+bs*s+ks)-(bs*s+ks)^2 );
wc = 3; % given
[m,p] = bode(Gsys,wc)
```

```
% design lead
K=1; Dlead = K*(s+0.804)/(s+11.2);
[m,p] = bode(Gsys*Dlead,wc)
K=1/m
Dlead = K*(s+0.804)/(s+11.2);
sysCL = feedback(Gsys*Dlead,1);
sysOL = Gsys*Dlead
figure; nyquist(sysOL)
figure; rlocus(sysOL)
%step(sysCL)
```

$m =$

0.1103

$p =$

-180.0000

$m =$

0.0295

$p =$

-119.9978

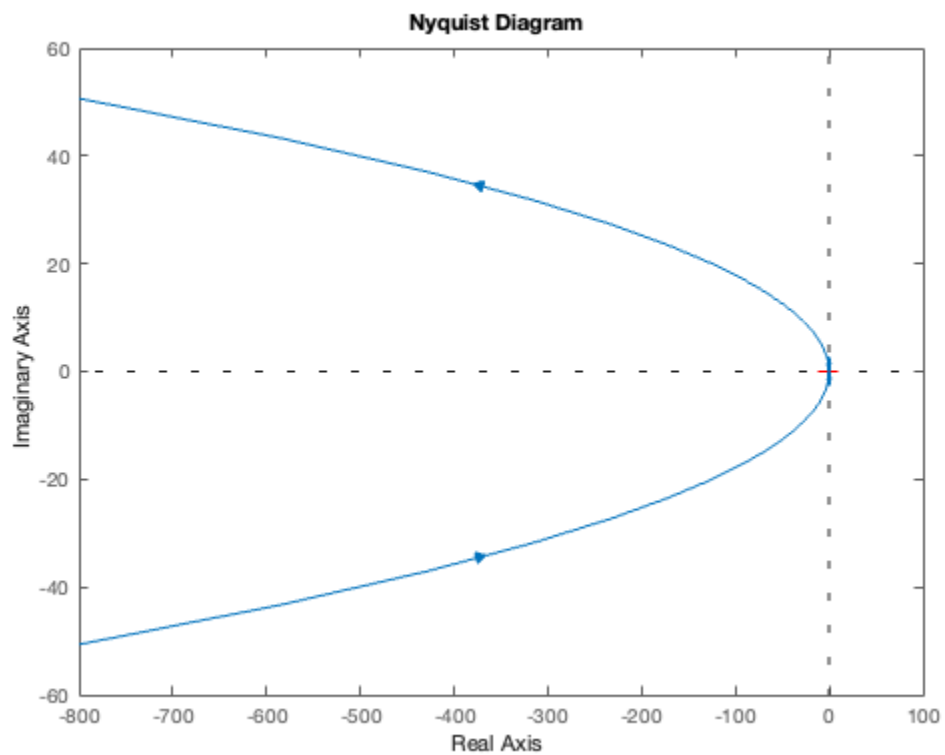
$K =$

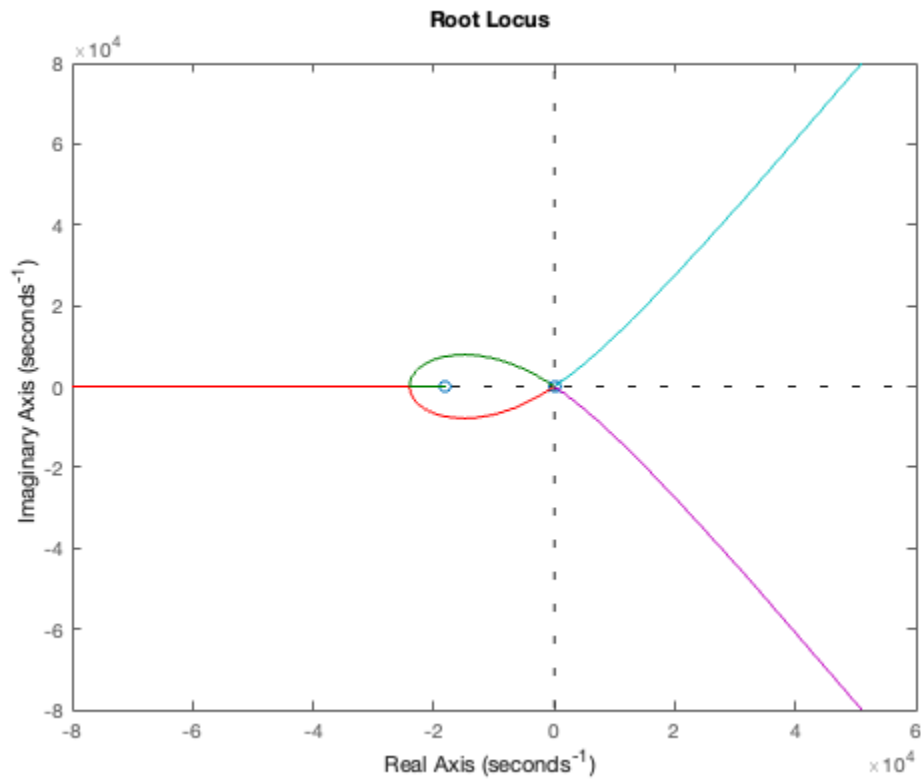
33.8508

$sysOL =$

$$\frac{0.0677 s^2 + 1219 s + 979.8}{0.01 s^5 + 0.114 s^4 + 36.38 s^3 + 407.2 s^2}$$

Continuous-time transfer function.





2c

```
bs = 0.002; ks = 36; I1 = 1.0; I2 = 0.01; % constants
Gsys = (bs*s+ks) / ( (I1*s^2+bs*s+ks)*(I2*s^2+bs*s+ks)-(bs*s+ks)^2 );
wc = 0.5; % given
[m,p] = bode(Gsys,wc)

% design lead
phi = 63
alpha = (1-sind(phi))/(1+sind(phi));
p = wc*sqrt(alpha);
z = wc/sqrt(alpha);
Dlead = (s+p)/(s+z);
[m,p] = bode(Gsys*Dlead,wc)
K=1/m
Dlead = K*Dlead

% low pass
wlp = 10;
lp = wlp/(s+wlp);
sysOL = Gsys*Dlead*lp
margin(sysOL)
```

$m =$

3.9607

$p =$

-180.0000

$\phi =$

63

$m =$

0.9509

$p =$

-117.0000

$K =$

1.0517

$D_{lead} =$

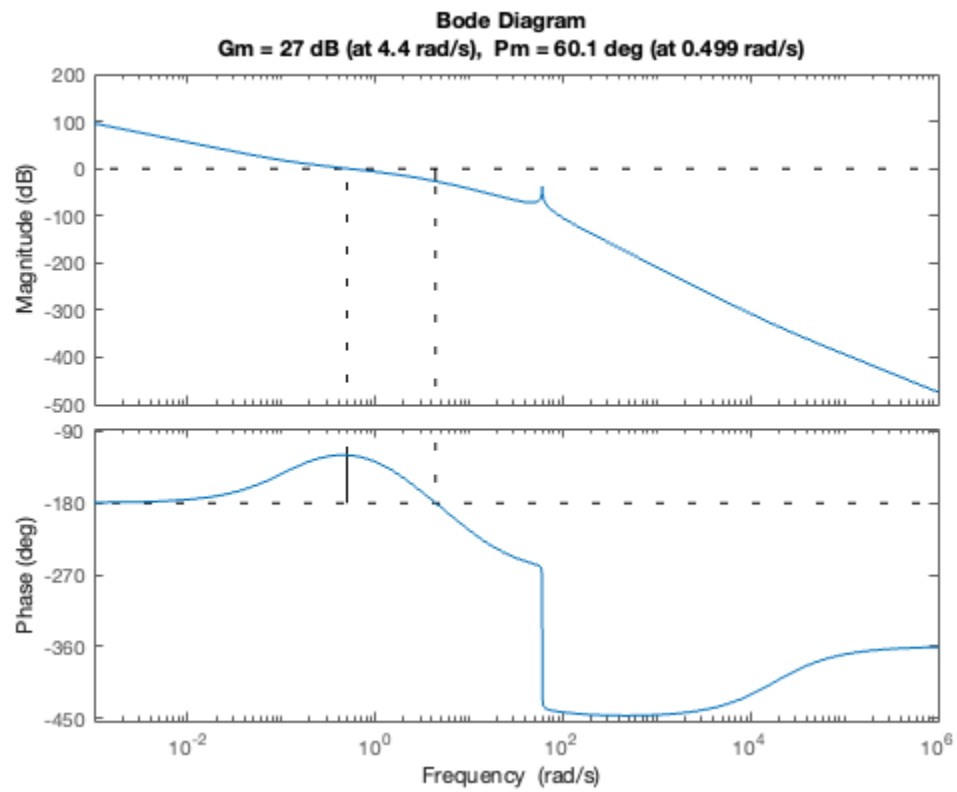
$$\frac{1.052 s + 0.1262}{s + 2.083}$$

Continuous-time transfer function.

$sysOL =$

$$\frac{0.02103 s^2 + 378.6 s + 45.45}{0.01 s^6 + 0.1228 s^5 + 36.59 s^4 + 439.4 s^3 + 757.3 s^2}$$

Continuous-time transfer function.



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