

Recap

$$\left\{ \begin{array}{l} \rho u A = \dot{m} \quad \text{OR} \quad \frac{d\rho}{\rho} + \frac{du}{u} + \frac{dA}{A} = 0 \\ \rho u \frac{du}{dx} = -\frac{dp}{dx} \\ dh + u du = 0 \quad \text{OR} \quad h + \frac{u^2}{2} = h_0 \\ p = \rho R T \end{array} \right.$$

$h_0 \equiv \text{stag. enthalpy}$


$$a = \sqrt{\left(\frac{\partial p}{\partial \rho}\right)_s} = \sqrt{\gamma p / \rho} = \sqrt{\gamma R T}$$


general perfect gas

$$M = \frac{u}{a}$$

$$\frac{dp}{\rho u^2} (1 - M^2) = \frac{dA}{A} \Rightarrow \text{sign of } dp \text{ depends on } \left\{ \begin{array}{l} \text{sign of } dA \\ \text{" " of } (1 - M^2) \end{array} \right.$$

$M < 1$ case





$$dA < 0 \Rightarrow \underbrace{dp < 0}_{\text{"nozzle"}} \Rightarrow du > 0$$


$$dA > 0 \Rightarrow \underbrace{dp > 0}_{\text{"diffuser"}} \Rightarrow du < 0$$

entirely analogous to
incomp. ($\rho = \text{const}$) case
Not quantitatively though
only sign

$M > 1$ case



$$dA < 0 \Rightarrow \underbrace{dp > 0}_{\text{diffuser}} \Rightarrow du < 0$$


$$dA > 0 \Rightarrow \underbrace{dp < 0}_{\text{nozzle}} \Rightarrow du > 0$$

Area-Mach # Relations

Start from Energy:

$$h + \frac{u^2}{2} = h_0 \quad (\text{adiabatic flow})$$

$$h = c_p T \quad (c_p = \text{const}; h(T=0) = 0)$$

Recall $\begin{cases} a^2 = \gamma R T \rightarrow T = \frac{a^2}{\gamma R} \\ c_p = \frac{\gamma}{\gamma-1} R \\ M = \frac{u}{a} \end{cases}$

$$c_p T + \frac{u^2}{2} = c_p T_0 \quad \div \text{ by } c_p T$$

$$\frac{T_0}{T} = 1 + \frac{u^2}{2 \frac{\gamma}{\gamma-1} R \frac{a^2}{\gamma R}} \rightarrow \frac{T_0}{T} = \left(1 + \frac{\gamma-1}{2} M^2 \right) \geq 1 \Rightarrow \boxed{T < T_0}$$

(I) stag. temp is highest

For isentropic (adiabatic + frictionless)

$$\frac{T_1}{T_2} = \left(\frac{P_1}{P_2} \right)^{\frac{\gamma}{\gamma-1}} = \left(\frac{P_1}{P_2} \right)^{\frac{1}{\gamma-1}}$$

then

$$\boxed{\begin{aligned} \frac{P_0}{P} &= \left(1 + \frac{\gamma-1}{2} M^2 \right)^{\frac{\gamma}{\gamma-1}} \quad (\text{II}) \\ \frac{P_0}{P} &= \left(1 + \frac{\gamma-1}{2} M^2 \right)^{\frac{1}{\gamma-1}} \quad (\text{III}) \end{aligned}}$$

Velocity

$$\begin{cases} u = Ma \\ a = \sqrt{\gamma R T} \\ T = T_0 \left(1 + \frac{\gamma-1}{2} M^2 \right)^{-1} \end{cases}$$

$$\Rightarrow u = M \sqrt{\frac{\gamma R T_0}{1 + \frac{\gamma-1}{2} M^2}} \quad (\text{IV})$$

From (III):

$$P = P_0 \left(1 - \frac{\gamma-1}{2} M^2 \right)^{\frac{1}{1-\gamma}} \quad \leftarrow \text{flip sign}$$

and $P_0 = \frac{P_0}{R T_0} \leftarrow \text{Set by inj. pumps}$
 $\quad \quad \quad \leftarrow \text{" " comb. process}$

Mass flux $\equiv \frac{\text{mass flow rate}}{\text{unit Area}}$

$$= \frac{\dot{m}}{A} = \rho u = \underbrace{\frac{p_0}{RT_0} \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{1}{1-\gamma}}}_{\rho} \cdot \underbrace{M \sqrt{\frac{\gamma RT_0}{1 + \frac{\gamma-1}{2} M^2}}}_{u}$$

$$\Rightarrow \frac{p_0 \sqrt{\gamma}}{\sqrt{RT_0}} M \left[\frac{1}{1 + \frac{\gamma-1}{2} M^2} \right]^{\frac{1}{\gamma-1} - \frac{1}{2}} = \frac{\dot{m}}{A}$$

For fixed \dot{m} , look for value of M that maximizes $\frac{\dot{m}}{A}$

$$\rightarrow \text{Set } \frac{\partial \left(\frac{\dot{m}}{A} \right)}{\partial M} = 0$$

\rightarrow It happens at $M=1$

Indicate values of A, T, p, ρ, u attained @ $M=1$ w/ * superscript

$$A(M=1) = A^*, \quad p(M=1) = p^* \text{ etc.}$$

$\Rightarrow \frac{\dot{m}}{A}$ is max @ $M=1$

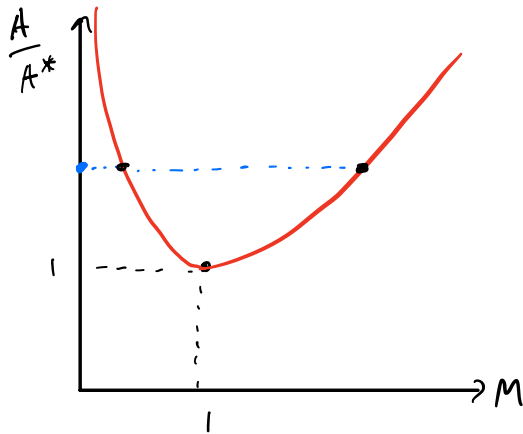
$$\text{there we have } \frac{\dot{m}}{A^*} = \sqrt{\frac{\gamma}{RT_0}} \left(\frac{2}{\gamma+1} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (\text{V})$$

\div max value by generic value of mass flux

$$\frac{\frac{\dot{m}}{A^*}}{\frac{\dot{m}}{A}} = \frac{A}{A^*} = \frac{1}{M} \left[\frac{2}{\gamma-1} \left(1 + \frac{\gamma-1}{2} M^2 \right) \right]^{\frac{\gamma+1}{2(\gamma-1)}}$$

Since $\dot{m} = \text{const.}$, $\frac{\dot{m}}{A}$ maximum where A is minimum

$\rightarrow A^*$ coincides w/ minimum area "throat"



Remarks

i) sonic conditions ($M=1$) can only be reached at a throat (area minimum)

ii) curve "looks" like a nozzle but x-axis is M not x

iii) curve has both subsonic & supersonic branches

→ same value of A/A^* may correspond to $M < 1$ or $M > 1$