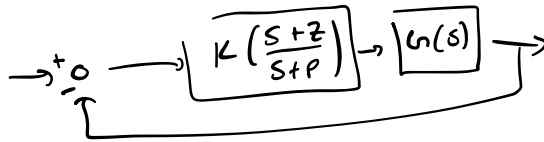


Faster response: $\omega_c \uparrow$
 More damping: $PM \uparrow$

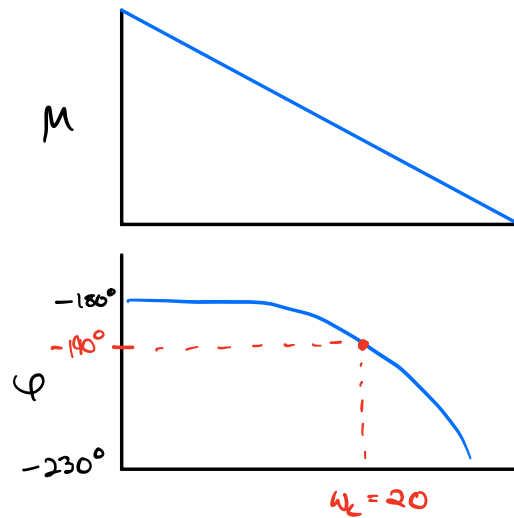
Lead compensation



Design for:

- $PM = 60^\circ$
- CL ω_{bw} as high as possible

$G(s)$ response:



For lead compensator:

- max phase is 90° but has too much high-freq. amplification
- Assume we consist 70° of phase w/o excessive high-freq. amp.

\rightarrow can set ω_c as high as 20 r/s & maintain $PM = 60^\circ$

For 70° from lead @ $\omega_c = 20$ r/s

$$\alpha = \frac{z}{p} \rightarrow \text{lead ratio: } \frac{1}{\alpha} \quad (20-30)$$

$$\alpha = \frac{1 - \sin(\phi_{max})}{1 + \sin(\phi_{max})}, \quad \phi_{max} = 70^\circ$$

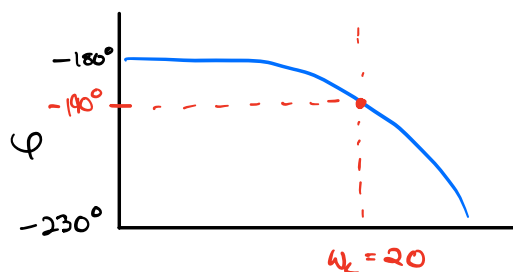
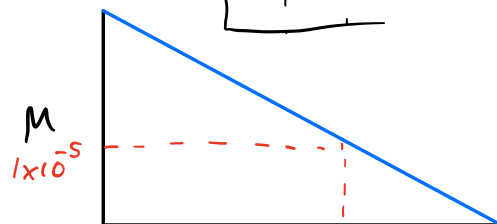
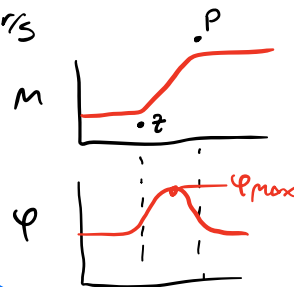
$$\alpha \approx 0.031, \quad LR(\frac{1}{\alpha}) \approx 30$$

$$z = \omega_{max} \sqrt{\alpha} \approx 3.53$$

$$p = \omega_{max} / \sqrt{\alpha} \approx 113.4$$

$$D_{lead}(s) = K \frac{s + 3.53}{s + 113.4}$$

$$|D \cdot G|_{\omega=\omega_c} = 1$$



↓

$$|DC(j\omega_c)G(j\omega_c)|_{\omega_c=20} = \left| K \frac{20j+3.53}{20j+113.4} \right| \cdot \underbrace{|G(20j)|}_{1 \times 10^{-5}}$$

$$\rightarrow | = K \frac{\sqrt{20^2 + 3.53^2}}{\sqrt{20^2 + 113.4^2}} \cdot 1 \times 10^{-5} \rightarrow K \approx 5.67 \times 10^5$$

$$\rightarrow D_{lead}(s) = 5.67 \times 10^5 \frac{s+3.53}{s+113.4}$$

Calculate phase:

$$\angle G(j\omega_c) = -190^\circ$$

$$\angle [D_{lead}(j\omega_c) \cdot G(j\omega_c)] =$$

$$= \angle D + (-190) = \left[\text{atan} \frac{20}{3.53} - \text{atan} \frac{20}{113.4} \right] + (-190^\circ)$$

70° as designed

$$= -120^\circ$$

Steady state errors

$$\omega_c < \omega_{BW} < 2\omega_c$$

$$\omega_c \sim \omega_{BW} \sim \text{speed of response}$$

$$\zeta \approx PM/100$$

We've looked at:

- stability ✓
- speed of response ✓
- damping ratio ✓
- steady state error ?

Integral control