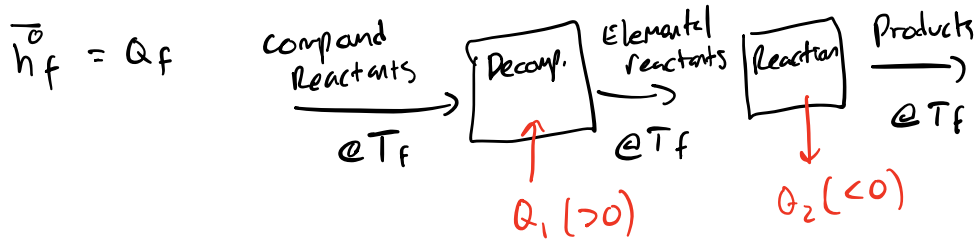


Recap

Heat of formation = Enthalpy of formation = Heat of reaction



$$Q_1 = -\sum_i (n_i Q_{f,i})_{\text{Reactants}} \quad (>0) \text{ supply heat}$$

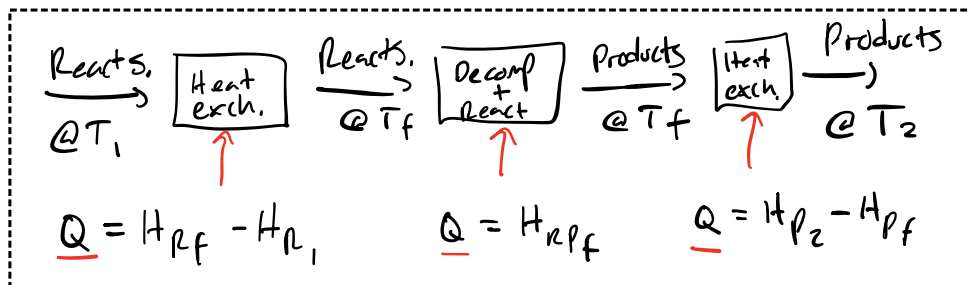
$$Q_2 = \sum_j (n_j Q_{f,j})_{\text{Products}} \quad (<0) \text{ release (take away) heat}$$

i, j indices to count thru all reactants & products

$$Q_1 + Q_2 \equiv H_{RPf}$$

In general, reactants & products do not enter/exit

@ T_f \rightarrow Redraw sketch



\uparrow adiabatic container, $\Rightarrow Q_{\text{Net}} = 0$

$$H_{Rf} - H_{Ri} = \sum_i \left[n_i \bar{c}_{p,i} (T_f - T_i) \right]_{\text{Reactants}}$$

$$H_{Rf} = \sum_j (n_j Q_{f,j})_{\text{products}} - \sum_i (n_i Q_{f,i})_{\text{Reactants}}$$

$$H_{P2} - H_{Pf} = \sum_j \left[n_j \bar{c}_{p,j} (T_2 - T_f) \right]_{\text{products}}$$

$$Q_{\text{net}} = 0$$

$$\begin{aligned} \sum_j \left[n_j \bar{c}_{p,j} (T_2 - T_f) \right]_{\text{products}} &= \sum_i \left[n_i \bar{c}_{p,i} (T_f - T_i) \right]_{\text{Reactants}} \\ &+ \sum_i (n_i Q_{f,i})_{\text{Reactants}} - \sum_j (n_j Q_{f,j})_{\text{products}} \end{aligned}$$

$T_2 \equiv$ adiabatic flame temperature

T_f known
 T_i " (in this class, usually $T_i = T_f$)

$\bar{c}_{p,i,j}$ known, $Q_{f,i,j}$ known, n_i , known

If n_j known (product composition),

can calculate T_2

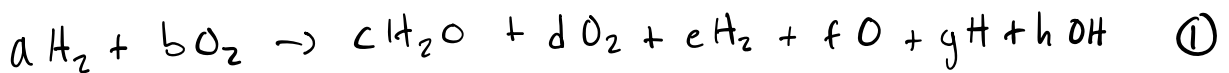
Composition of Products

Problem: compos. of prod. (n_j) depends upon T

$$\uparrow T_2 \quad " \quad " \quad n_j$$

e.g. w/in certain temp. range, water resulting from

$H_2 + \frac{1}{2} O_2$ react. dissociates into various components.



Book uses $A H_2 + B O_2 \rightarrow n_{H_2O} H_2O \dots$

a, b known

c, d, e, f, g, h unknown

to determine \uparrow , need 6 eqs

- start w/ mass balance

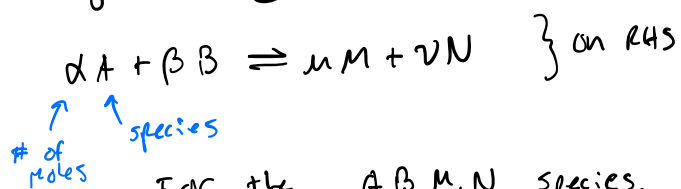
1 eqn for H atoms,

" " " O "

\rightarrow need 4 more - they come from chemical equilibrium

In (1), chem. equil. occurs entirely on RHS

In general, @ equil.



For the A, B, M, N species,

partial pressures are P_A, P_B, P_M, P_N

AND $\frac{P_i}{P_m} = X$ (mole frac)

From chemistry:

$$\frac{P_M^M P_N^v}{P_A^\alpha P_B^\beta} = K_p(T) \quad \text{const. of equilibrium}$$

There is also an equil. const. based on mole fractions themselves

$$K_n(T) \equiv \frac{X_M^M X_N^v}{X_A^\alpha X_B^\beta} = \frac{\left(\frac{P_M}{P_m}\right)^M \left(\frac{P_N}{P_m}\right)^v}{\left(\frac{P_A}{P_m}\right)^\alpha \left(\frac{P_B}{P_m}\right)^\beta} = P_m^{\alpha+\beta-M-v} K_p(T)$$

Typically, $K_p(T)$ $\begin{cases} \text{tabulated} \\ \text{plotted} \\ \text{analytical expr.} \end{cases}$

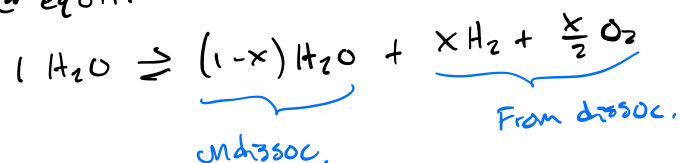
Ex. 1 mol H_2O heated to 3600 K @ 1 atm

A fraction x of that mole dissociates into

H_2 & O_2 K_p available in fig. 2.12

Task: determine x

@ equil.



mole count on RHS:

$(1-x)$ moles undissoc. H_2O

x " H_2

$\frac{x}{2}$ " O_2

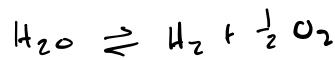
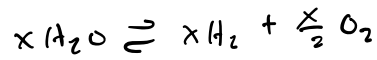
$1 + \frac{x}{2}$

$$x_{H_2O} = \frac{1-x}{1 + \frac{x}{2}}$$

$$x_{H_2} = \frac{x}{1 + \frac{x}{2}}$$

$$x_{O_2} = \frac{x/2}{1 + x/2}$$

Dissol. Equil. is



$$\Rightarrow K_p = \frac{(P_{H_2})^1 (P_{O_2})^{1/2}}{(P_{H_2O})^1}$$

And

$$K_p = \frac{x_{H_2} (x_{O_2})^{1/2}}{x_{H_2O}} = \frac{\left(\frac{x}{1 + \frac{x}{2}}\right) \left(\frac{x/2}{1 + \frac{x}{2}}\right)^{1/2}}{\frac{1-x}{1 + x/2}} = \frac{x^{3/2}}{(1-x)\sqrt{2+x}}$$