

Recall boat

$$u_j = \frac{D}{\rho A} + u_b ; J = D$$

power to keep u_b const.

Propulsion efficiency

$$\eta_p = \frac{\text{what I want}}{\text{what I spend}} = \frac{J \cdot u_b}{\dot{W}_{\text{pump}}} = \frac{\dot{m}(u_j - u_b) u_b}{\frac{1}{2} \dot{m}(u_j^2 - u_b^2)} = \frac{2 u_b}{u_j + u_b}$$

work or power

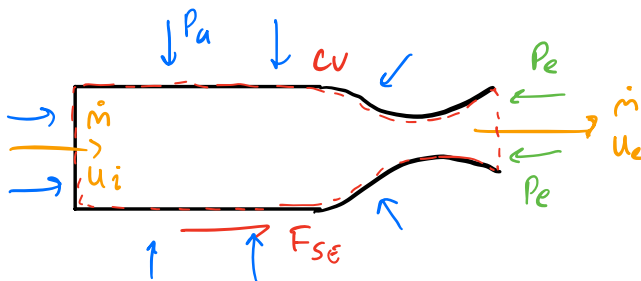
Conflicting needs

For high thrust,
need high u_j
For high η_p
need low u_j

III Rocket performance

cons. momentum for rocket:

$P = P_a$ everywhere outside except exit



In general:

- i) $P_e \neq P_a$
- ii) $P_e \neq 1 \text{ atm}$
- iii) $P_a \neq 1 \text{ atm}$
- iv) $u_i \ll u_e$
- v) Cannot use Bernoulli ($P + \frac{1}{2} \rho u^2 = \text{const}$)
b/c " only valid for $\rho = \text{const}$.

Apply

$$\frac{d}{dt} \int_{CV} \rho \underline{u} dV + \int_{CS} \rho \underline{u} \underline{u} \cdot d\underline{A} = - \int_{CS} P d\underline{A} + \underline{F}_e$$

$$\frac{d}{dt} \int_{CV} \rho \underline{u} dV = 0, \text{ steady state}$$

neglect u_i , P_e, u_e uniform over A_e

$$\int_{CS} \rho \underline{u} \underline{u} \cdot d\underline{A} = u_e \hat{i} (P_e u_e A_e) = \dot{m} u_e \hat{i}$$

$P = P_a = \text{const}$, everywhere on CV except A_e , where $P = P_e$
 $P_e = P_a + P_c - P_a$

$$- \int_{CS} P d\underline{A} = - \int_{CS} P_a d\underline{A} - \int_{A_e} (P_e - P_a) d\underline{A} = (P_a - P_e) A_e \hat{i}$$

Reassemble

$$\dot{m} u_e \hat{i} + (p_e - p_a) A_e \hat{i} = F_{se} \hat{i} \quad \leftarrow \text{stand force balancing thrust}$$

$$\rightarrow T = F_{se} \text{ in magnitude}$$

$$\rightarrow T = \dot{m} u_e + (p_e - p_a) A_e \quad \text{in } -\hat{x} \text{ direction}$$

if engine moves at constant velocity
 \rightarrow velocities relative to CV

$$\text{then: } T = \dot{m} u_{e,xyz} + (p_e - p_a) A_e$$

From now on, remember that u is relative to CV (drop subscript)

We'll have to learn how u_e & p_e relate to:

- nozzle shape
- cc conditions

Rocket parameters

$$T = \dot{m} u_e + (p_e - p_a) A_e$$

$$= \underbrace{\rho_e u_e A_e}_{\dot{m}_e} u_e + (p_e - p_a) A_e \quad \leftarrow \text{prioritize } u_e \text{ over } \rho_e$$

$$= \rho_e A_e u_e^2 + (p_e - p_a) A_e$$

mission req's:

- payload
- altitude
- final velocity

affected by:

{ thrust
" duration
limits imposed on thrust by
gas dynamics & combustion
limits imposed on acceleration
by structural req's
relative magnitude of { m_e
 m_p
 m_s

Useful to define equivalent exhaust velocity

$$u_{eq} \equiv u_c + \left(\frac{p_e - p_a}{\dot{m}} \right) A_e \quad \text{such that} \quad \mathcal{T} = \dot{m} u_{eq}$$

Recall impulse

$$I \equiv \int F dt \quad ; \quad \text{in present case, } F = \mathcal{T}$$

call burn period t_b . Assume $u_{eq} = \text{const}$ w.r.t. time

$$I = \int_0^{t_b} \dot{m} u_{eq} dt = u_{eq} \int_0^{t_b} \dot{m} dt = u_{eq} M_p$$

$$\Rightarrow \frac{I}{M_p} = u_{eq} = \frac{\mathcal{T}}{\dot{m}}$$

Define "specific impulse"

$$I_{sp} \equiv \frac{I}{M_p g_e} = \frac{u_{eq}}{g_e}$$

total change in impulse
per unit weight propellant

$$[I_{sp}] = S$$

I_{sp} is another way to describe
exhaust velocity

no matter where rocket is,

g_e is always accel. of gravity on earth