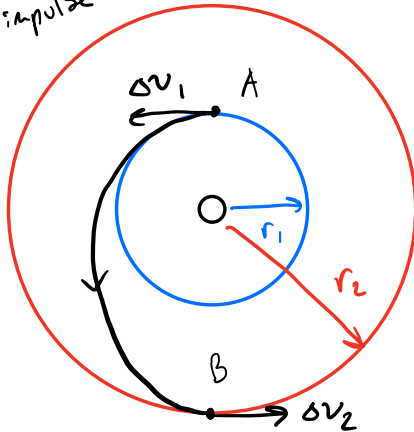


Recap: Hohmann vs. Bi-elliptic

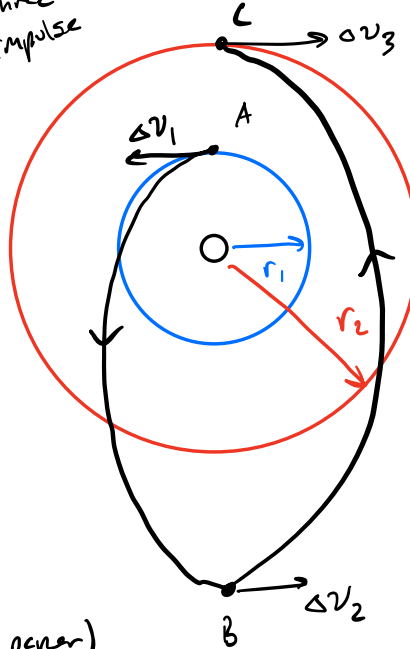
Hohmann

Two impulse



Bi-elliptic

Three impulse



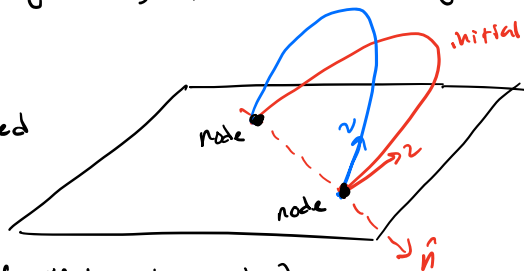
Comparison Summary (grossing paper)

- \forall 2- Δv maneuvers, Hohmann is ^{for all} most optimal (lowest Δv)
- for $r_c/r_A \lesssim 15.58$, Bi-elliptic has lower Δv_{tot} (if $r_B > r_A$)
See slide 18 in L16
- the tradeoff for bielliptic is much higher transfer time

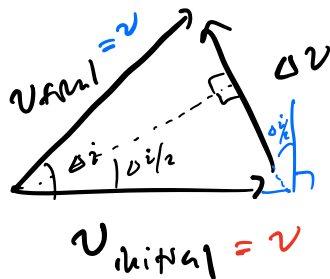
Next: Plane change

"Simple plane change" \rightarrow inclination change, i

- in this case
- no change in speed
 - " " " " γ
(constant e, θ, ω)
 - no change in Ω (must be at a node)



Apply plane change on
line of nodes like axis
of rotation



[Isosceles]

$$\therefore \frac{\Delta v}{2} = v \sin\left(\frac{\Delta i}{2}\right)$$

$$\Delta v = 2v \sin\left(\frac{\Delta i}{2}\right) \quad \text{For a tangential burn } (r=0)$$

Note: thrust applied at $90^\circ + \Delta i/2$ from original dir.

For non-tangential burn ($r \neq 0$) need proj. of v into θ dir.

$$\therefore \Delta v = 2v \sin\left(\frac{\Delta i}{2}\right) \cos \theta \quad \begin{array}{l} \text{simple plane change} \\ \text{for non-tangential} \end{array}$$

Remarks

1) Expensive!

if $\Delta i = 60^\circ$, then $\Delta v = v$! Same as initial v !

2) Need to check both nodes (they are not necessarily at equatorial plane)
(the speeds not necessarily the same)

→ make plane change @ low speed node

3) Suppose $\Delta i = 90^\circ$ large!

$$\Delta v = 2v \sin 45^\circ = 2v \frac{\sqrt{2}}{2} = \sqrt{2} v = v\sqrt{2}$$

Example 1: simple plane change for circular orbit

gives: $v = 5.89 \text{ km/s}$, $e = 0$, $\Delta i = 15^\circ$

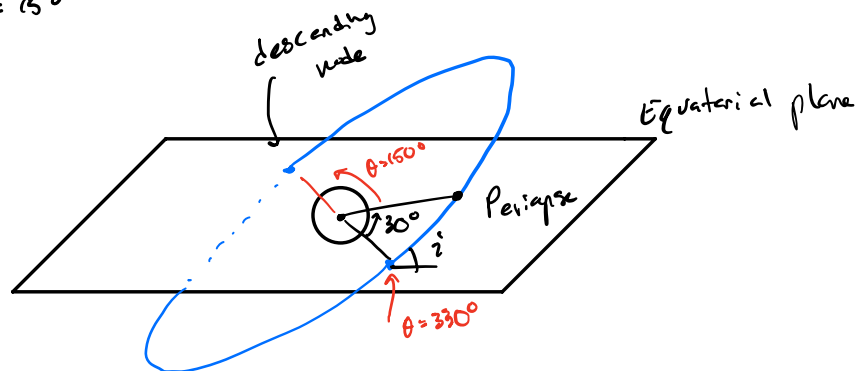
then: $e = 0$, circular $\delta = 0$ everywhere, tangential

$$\therefore \Delta v = 2v \cos \delta \sin \frac{\Delta i}{2} = 2(5.89) \sin(7.5^\circ)$$

$$\Delta v = 1.54 \text{ km/s}$$

Example 2 elliptical orbit

given: $e = 0.3$ $p = 17,858.8 \text{ km}$, $\omega = 30^\circ$, target $\theta = 330^\circ$ (change here)
 $\Delta i = 15^\circ$



Determine Δv :

→ need v → requires r, a , elliptical equations of θ

$$\therefore p = a(1 - e^2) \rightarrow a = \frac{p}{1 - e^2} = \frac{17,858.8 \text{ km}}{1 - 0.3^2} = 19,625 \text{ km}$$

$$\therefore r = \frac{p}{1 + e \cos \theta} = \frac{17,858.8}{1 + 0.3 \cos(330^\circ)} = 14,175.8 \text{ km}$$

around earth:

$$v = \sqrt{\mu \left(\frac{2}{r} - \frac{1}{a} \right)} = 5.99 \text{ km/s} \quad \text{vis uva}$$

$$\gamma = \tan^{-1} \left(\frac{e \sin \theta}{1 + e \cos \theta} \right) = -0.116 \text{ rad} = -6.7^\circ$$

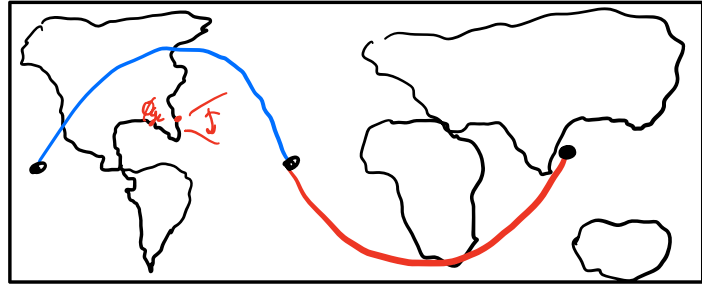
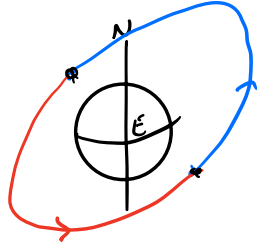
$$\text{Finally: } \Delta v = 2v \sin \left(\frac{\Delta i}{2} \right) \cos(\gamma) = 2(5.99) \sin \left(\frac{15^\circ}{2} \right) \cos(-6.7^\circ) \\ = \boxed{1.55 \text{ km/s}}$$

Note try descending node instead (further from perigee i.e. slower)
 → $\Delta v = 0.412 \text{ km/s}$ (better @ $\theta = 150^\circ$)

Motivation: complication: earth spins

"Ground tracks" → observer's view of orbit path (ECE)

→ track path from node to node



$\Delta N^\circ = \text{angle ground track traverses for one period}$

timing related to Earth spin period

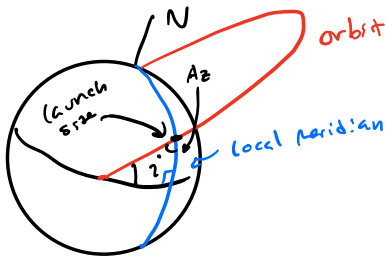
$$T_E = 24 \text{ hours}, \quad \omega_E = \frac{360^\circ}{24 \text{ hr}} = 15^\circ/\text{hr}$$

$$\therefore \text{orbital period } T = \frac{\text{Node disp one orbit}}{\omega_E} = \frac{360^\circ - \Delta N}{15^\circ/\text{hr}}$$

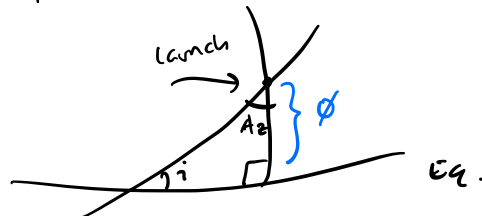
Ground tracks shaped by:

- inclination
- orbital period
- perigee location

Implications \rightarrow launch geometry affects possible inclinations



Spherical triangle:



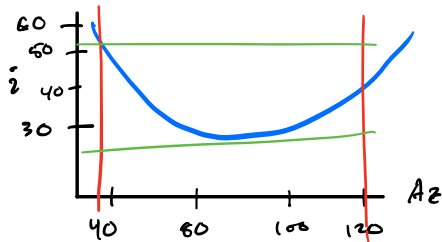
triangle

$$\cos i = -\cos A_z \cos 90^\circ + \sin A_z \sin 90^\circ \cos \phi$$

$\phi = \text{latitude of launch}$

$$\rightarrow \cos i = \sin A_z \cos \phi$$

plot $i = f(A_z)$



Cape Canaveral

$$\phi_{gc} = 28.533^\circ$$

$$A_z = 35^\circ - 120^\circ$$

concerns

- airspace
- failure (debris)

→ can get orbits $i = 30^\circ - 60^\circ$

Remarks

$$-\cos i = \sin A_z \cos \phi_{gc} \rightarrow \sin |A_z| \leq 1 \rightarrow i \geq \phi_{gc}$$

- minimize i by maximizing A_z

$$-\text{to target } i \text{ \& launch location, } A_z = \sin^{-1} \left(\frac{\cos i}{\cos \phi_{gc}} \right)$$

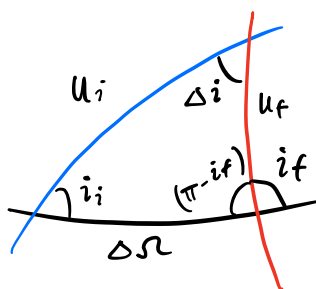
Example 3 in US, want $i = 90^\circ$

$$\text{USAF East } \phi_{gc} = 28.533^\circ$$

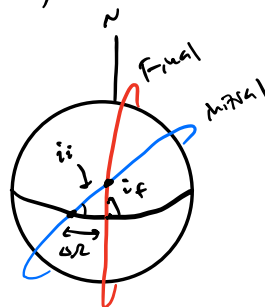
$$\text{USAF West } \phi_{gc} = 34.669^\circ$$

$$A_z = \sin^{-1} \left(\frac{\cos(90^\circ)}{\cos(\phi_{gc})} \right)$$

Example 4 suppose after launch, need plane change
General rotations (change both i & Ω)



$$\text{let } u_i = \omega + \theta$$



Set up & Solve