Making Flips with Quadrotors in Constrained Environments

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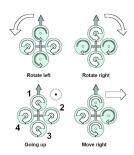


- Introduction
- System Modeling
- 3 Control of Quadrotors
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(a) DJI Phantom quadcopter (UAV) [9].



(b) Quadrotor Concept. Width of the arrows is proportional to the angular speed of the propellers [1].

Figure: Commercial quadrtotor platform (left) and quadrotor concept (right).

Properties of the quadrotor:

- Under-actuated system.
- · Controls all DOFs.

Remark

Rotational and translational dynamics are coupled.

Goal of the master thesis:

- Study of multi-flip maneuvers.
- Use different control methods.
- Performing the maneuvers in a constrained environment.



(a) Quadrotor performing a triple flip.[6]



(b) Quadrotor going though a loop [2].

Figure: Representation of the issues to be tackled in this master thesis.

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Principal **forces** and **torques** are generated by the propellers' rotations.

- Forces Decomposed into 2 parts:
 - · Weight.
 - · Resulting lift.

$$\overrightarrow{F_{\xi}} = \overrightarrow{P} + \sum \overrightarrow{f_i} \tag{1}$$

which results in [4]:

$$\overrightarrow{F}_{\xi} = \begin{bmatrix} 0 \\ 0 \\ -mg \end{bmatrix} + b \begin{bmatrix} 0 \\ 0 \\ \omega_1^2 + \omega_2^2 + \omega_3^2 + \omega_4^2 \end{bmatrix}$$
 (2)

• Torques - 2 parts:

- Relation between the velocities of the rotors.
- Gyroscopic effects due to the change of orientation direction of the rotors.

$$\tau = \tau_{\mathsf{a}} + \tau_{\mathsf{G}} \tag{3}$$

which results in [4]:

$$\tau = \begin{bmatrix} \tau_1 \\ \tau_2 \\ \tau_3 \end{bmatrix} = \tau_a + \tau_G = \begin{bmatrix} I(f_4 - f_2) - qJ_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\ I(f_3 - f_1) + pJ_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\ d(\omega_1^2 - \omega_2^2 + \omega_3^2 - \omega_4^2) \end{bmatrix}$$
(4)

Motors are controlled with torques and thrust using 4 control inputs.

$$u_1=u$$
 (thrust) $u_2= au_\phi$ $u_3= au_ heta$ $u_4= au_\psi$

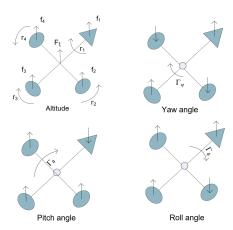


Figure: Quadrotor model with motor torques and Euler angles [4].

- Rigid structure.
- Symmetric structure.
- CoG and origin of body-fixed frame coincide.
- Propellers are rigid.
- Thrust and drag are proportional to the square of the velocity of the propeller.

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- Computed using Euler-Lagrange or Newton-Euler formalism.
- Decomposed to 2 different parts [4]
 - Translational model:

$$\begin{cases}
m\ddot{x} = (\sin\psi\sin\phi + \cos\psi\sin\theta\cos\phi)u \\
m\ddot{y} = (-\sin\phi\cos\psi + \sin\psi\sin\theta\cos\phi)u \\
m\ddot{z} = \cos\theta\cos\phi u - mg
\end{cases}$$
(5)

$$\begin{cases} \dot{p} = qr \frac{(l_{yy} - l_{zz})}{l_{zz}} + \frac{1}{l_{zz}} (f_4 - f_2) - \frac{1}{l_{zz}} q J_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\ \dot{q} = pr \frac{(l_{zz} - l_{zz})}{l_{yy}} + \frac{1}{l_{yy}} (f_3 - f_1) + \frac{1}{l_{yy}} p J_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\ \dot{r} = pq \frac{(l_{zz} - l_{yy})}{l_{zz}} + \frac{1}{l_{zz}} d(\omega_1^2 - \omega_2^2 + \omega_2^2 - \omega_1^2) \end{cases}$$
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For small pitch and roll angles of order 2, a simplified dynamic model is obtained:

• Translational model:

$$\begin{cases}
m\ddot{x} = (\phi \sin \psi + \theta \cos \psi)u \\
m\ddot{y} = (-\phi \cos \psi + \theta \sin \psi)u \\
m\ddot{z} = u - mg
\end{cases} (7)$$

$$\begin{cases}
\ddot{\phi} = \dot{\theta}\dot{\psi}\frac{(l_{yy} - l_{zz})}{l_{xx}} + \frac{l}{l_{xx}}(f_4 - f_2) - \frac{1}{l_{xx}}\dot{\theta}J_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\
\ddot{\theta} = \dot{\psi}\dot{\phi}\frac{(l_{zz} - l_{xx})}{l_{yy}} + \frac{l}{l_{yy}}(f_3 - f_1) + \frac{1}{l_{yy}}\dot{\phi}J_r(\omega_1 - \omega_2 + \omega_3 - \omega_4) \\
\ddot{\psi} = \dot{\theta}\dot{\phi}\frac{(l_{xx} - l_{yy})}{l_{zz}} + \frac{1}{l_{zz}}d(\omega_1^2 - \omega_2^2 + \omega_3^2 - \omega_4^2)
\end{cases}$$
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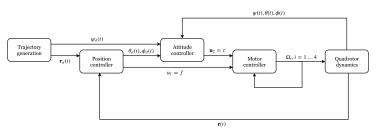


Figure: General control architecture for the position and attitude of a quadrotor [3].

- Position controller: drives translational dynamics errors to 0.
- Attitude controller: drives rotational dynamics errors to 0.
- Motor controller: receives the control intputs $\boldsymbol{u} = \begin{bmatrix} f & \tau \end{bmatrix}^T$ and maps them to Ω_i^* for each rotor.

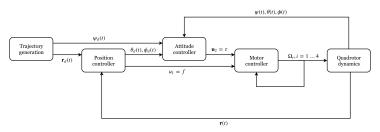


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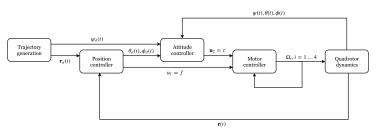


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What is MPC?

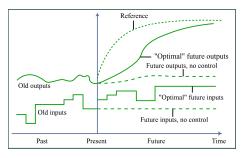


Figure: Basic idea of MPC [5].

- It is a feedback control algorithm.
- It uses a model to precit future outputs.
- It Solves an online optimization problem to select the optimal control

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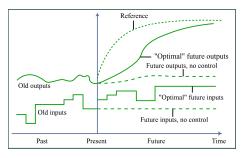


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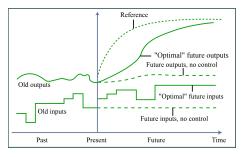


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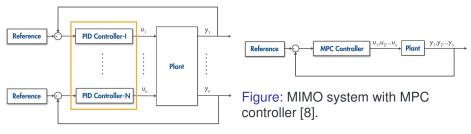


Figure: MIMO system with PIDs [8].

- Can control MIMO systems.
- Explicitly accounts for constraints.
- Can handle nonlinear and time-varying plant dynamics.

Remark

MPC requires a **powerful**, **fast** processor with a **large** memory.

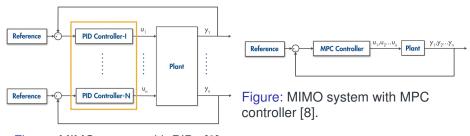


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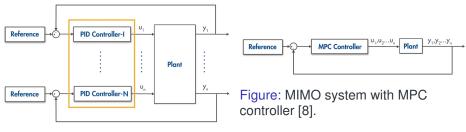


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- Weights

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- The computational complexity of the MPC algorithm.

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MPC Design parameters:

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Choosing proper values for these parameters is important as they affect:

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- · Linear time-invariant MPC.
- Adaptive MPC.
- Gain-Scheduled MPC.
- Nonlinear MPC.

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In Adaptive MPC:

- A linear model is computed on the fly as the operating conditions change.
- At each time step, the internal plant model used by the MPC is updated with this linear model.

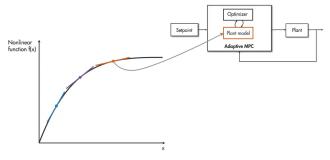


Figure: Example of Adaptive MPC [7].

Remark

The structure of the optimization problem remains the same across different operating points.

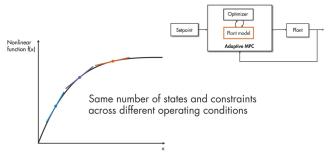


Figure: Example of Adaptive MPC [7].

In Gain-Scheduled MPC:

- Linearization is done offline at the operating points of interest.
- A linear MPC controller is then designed for each operating point.

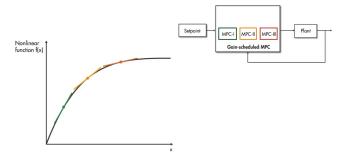


Figure: Example of Gain-Scheduled MPC [7].

Remark

Each controller is **independent** from the other.

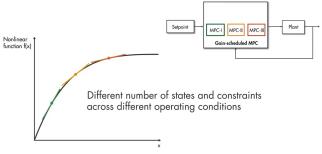


Figure: Example of Gain-Scheduled MPC [7].

For Nonlinear MPC, useful if:

- System is non-linearizable.
- Existence of nonlinear constraints.
- Existence of nonlinear cost function.

Nonlinear MPC

Most powerful methods: uses the most accurate representation of the plant ⇒ More accurate predictions.

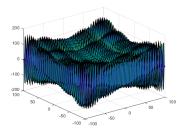


Figure: Example of a non-convex optimization problem.

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