

Friction Drag
(flow over a flat plate parallel to the flow)

Laminar Boundary Layer:

$$C_D = \frac{1.328}{\sqrt{\text{Re}_L}}$$

Turbulent Boundary Layer:

$$C_D = \frac{0.074}{\text{Re}_L^{1/5}} \quad 5 \cdot 10^5 < \text{Re}_L < 10^7 \quad \text{or} \quad C_D = \frac{0.455}{(\log(\text{Re}_L))^{2.58}} \quad \text{Re}_L < 10^9$$

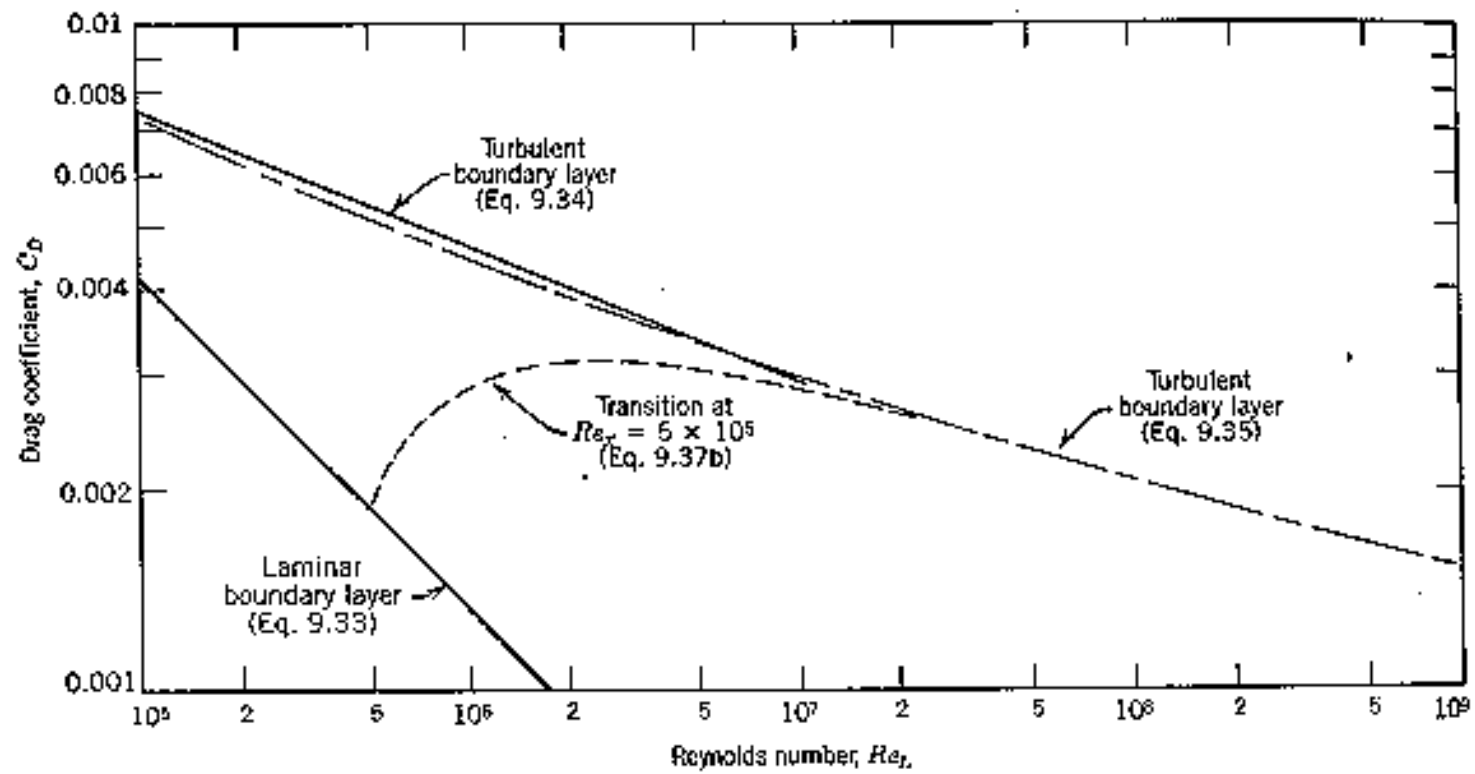
Laminar + Transition+Turbulent Boundary Layer:

$$C_D = \frac{0.074}{\text{Re}_L^{1/5}} - \frac{1740}{\text{Re}_L} \quad 5 \cdot 10^5 < \text{Re}_L < 10^7$$

or

$$C_D = \frac{0.455}{(\log(\text{Re}_L))^{2.58}} - \frac{1610}{\text{Re}_L} \quad 5 \cdot 10^5 < \text{Re}_L < 10^9$$

Drag Coefficient for Smooth Flat Plate Parallel to the Flow



Flow Over Flat Plate Normal to the Flow

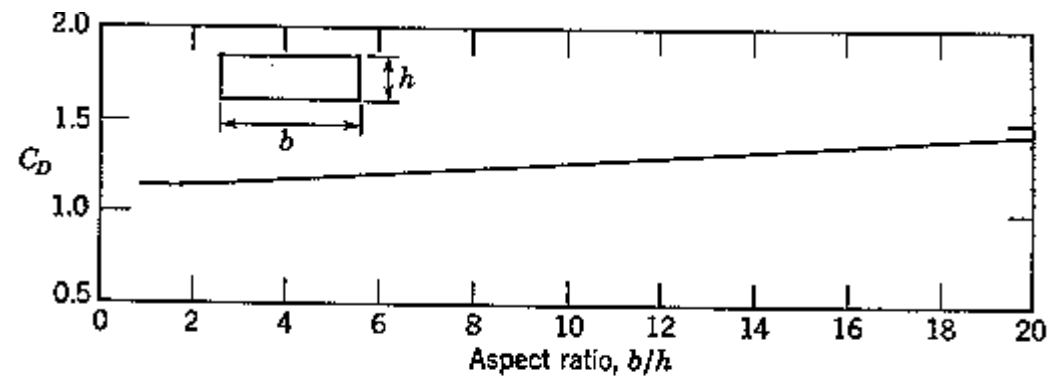
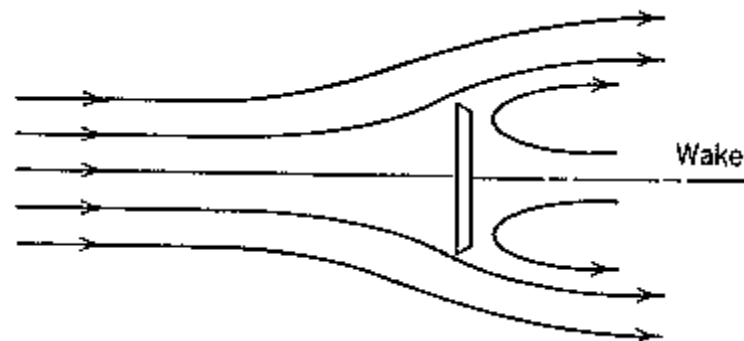
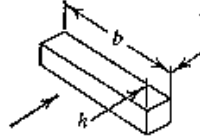
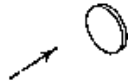



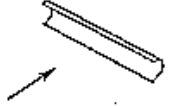



Fig. 9.10 Variation of drag coefficient with aspect ratio for a flat plate of finite width normal to the flow with $Re_h > 1000$ [14].

Drag Coefficients for Selected Objects

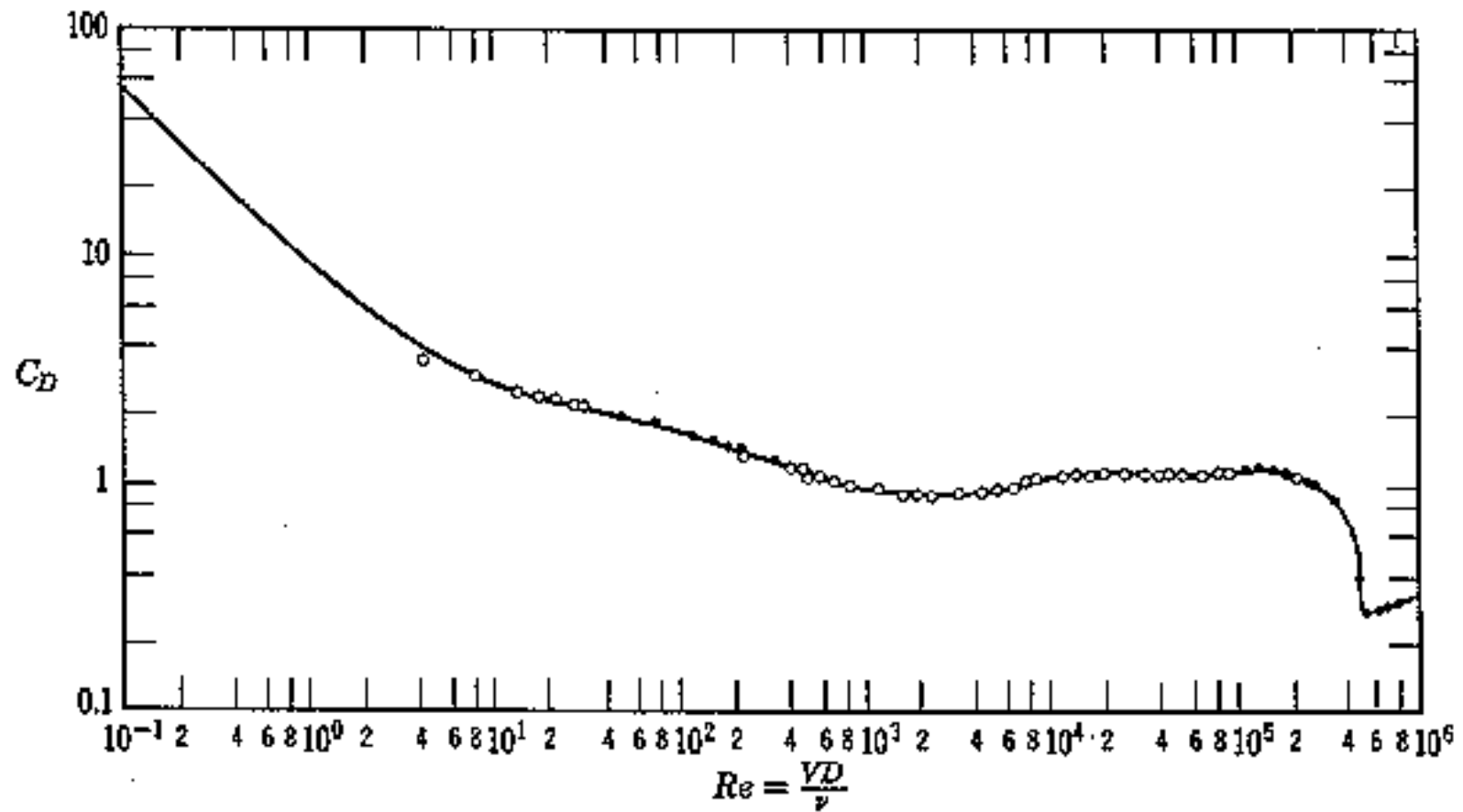
Table 9.3 Drag Coefficient Data for Selected Objects ($Re \geq 10^3$)^a

Object	Diagram	$C_D(Re \geq 10^3)$	
Square cylinder		$b/h = \infty$	2.05
		$b/h = 1$	1.05
Disk			1.17
Ring			1.20 ^b
Hemisphere (open end facing flow)			1.42
Hemisphere (open end facing downstream)			0.38
C-section (open side facing flow)			2.30
C-section (open side facing downstream)			1.20,

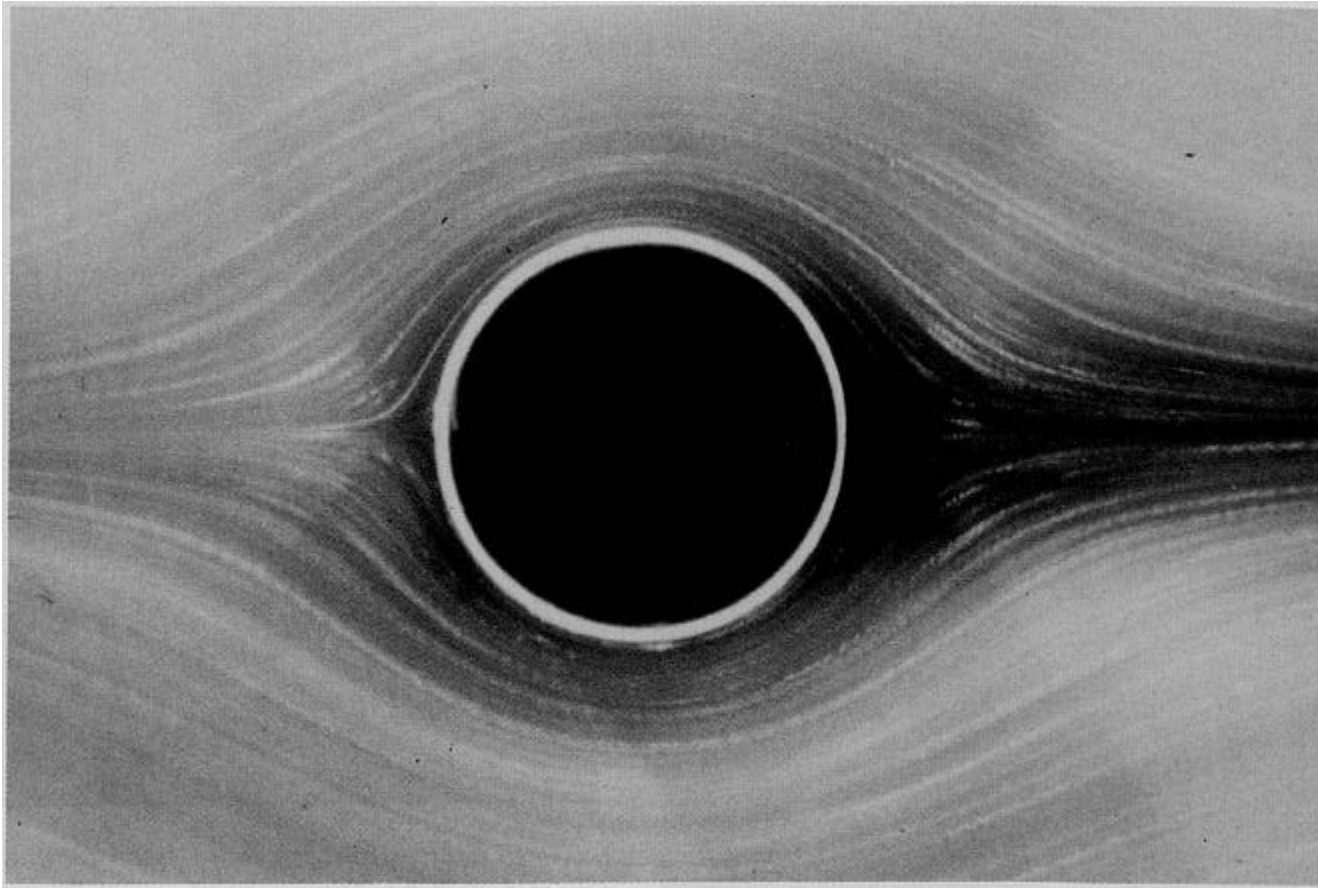
^a Data from [14].

^b Based on ring area.

Pressure Distribution Around Smooth Circular Cylinder

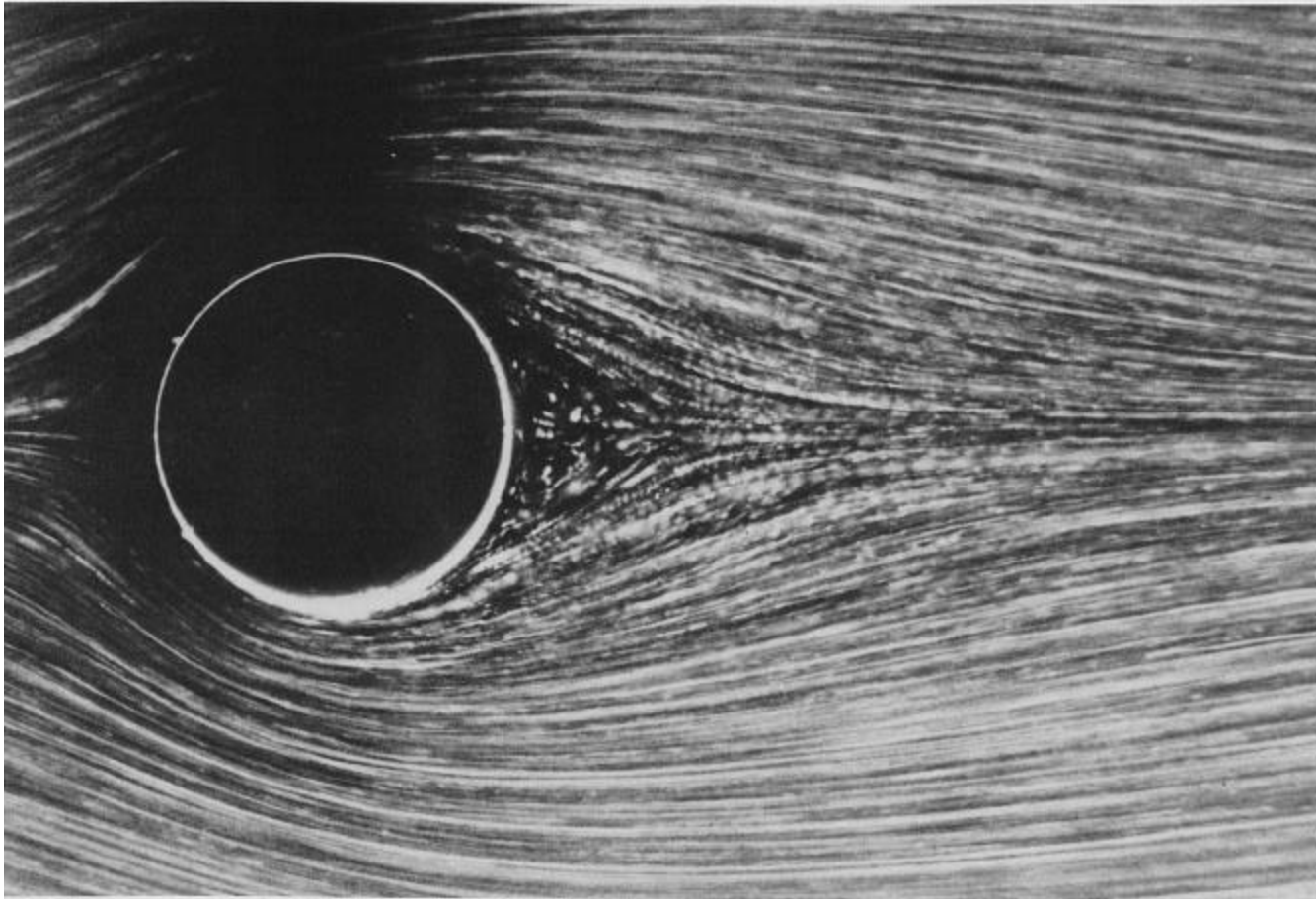


Visualization of Flow Around Smooth Circular Cylinder
 $Re=0.16$



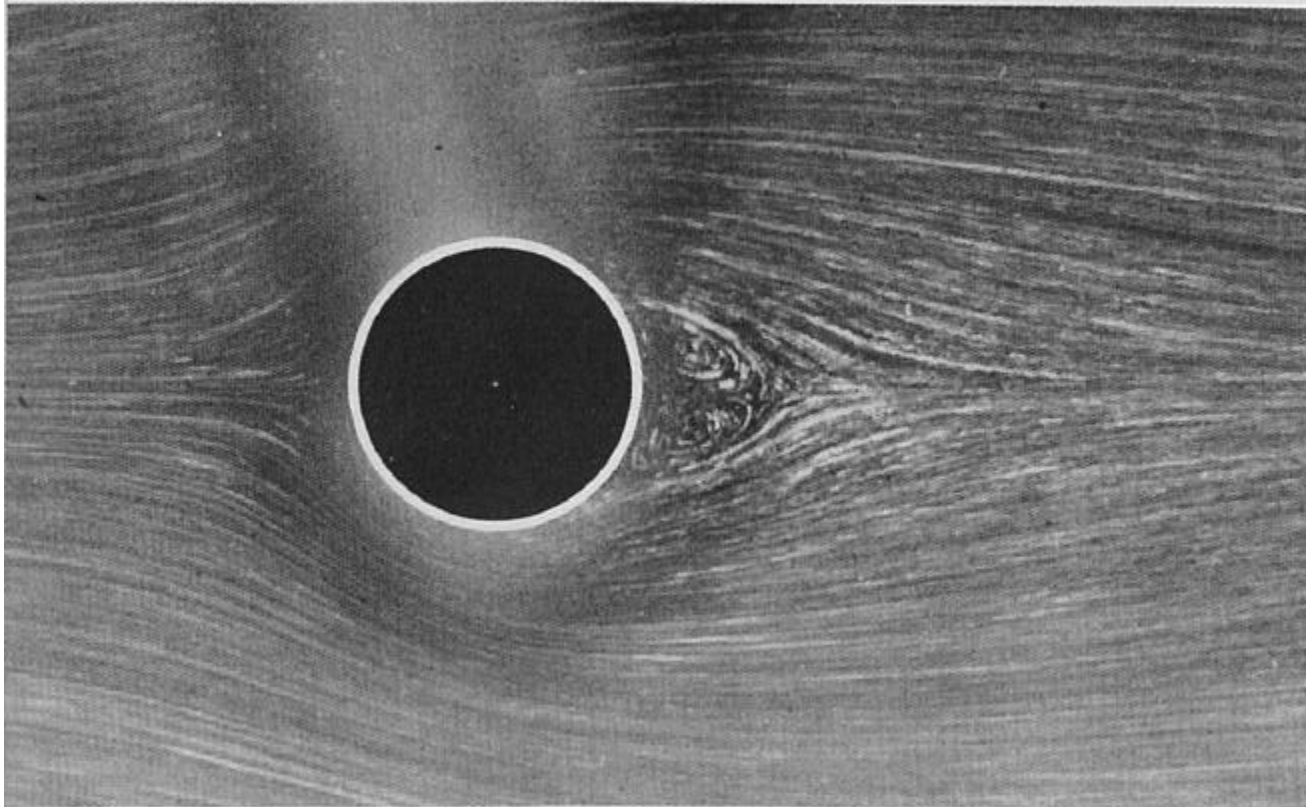
From Van Dyke (1982)

Visualization of Flow Around Smooth Circular Cylinder
 $Re=9.6$



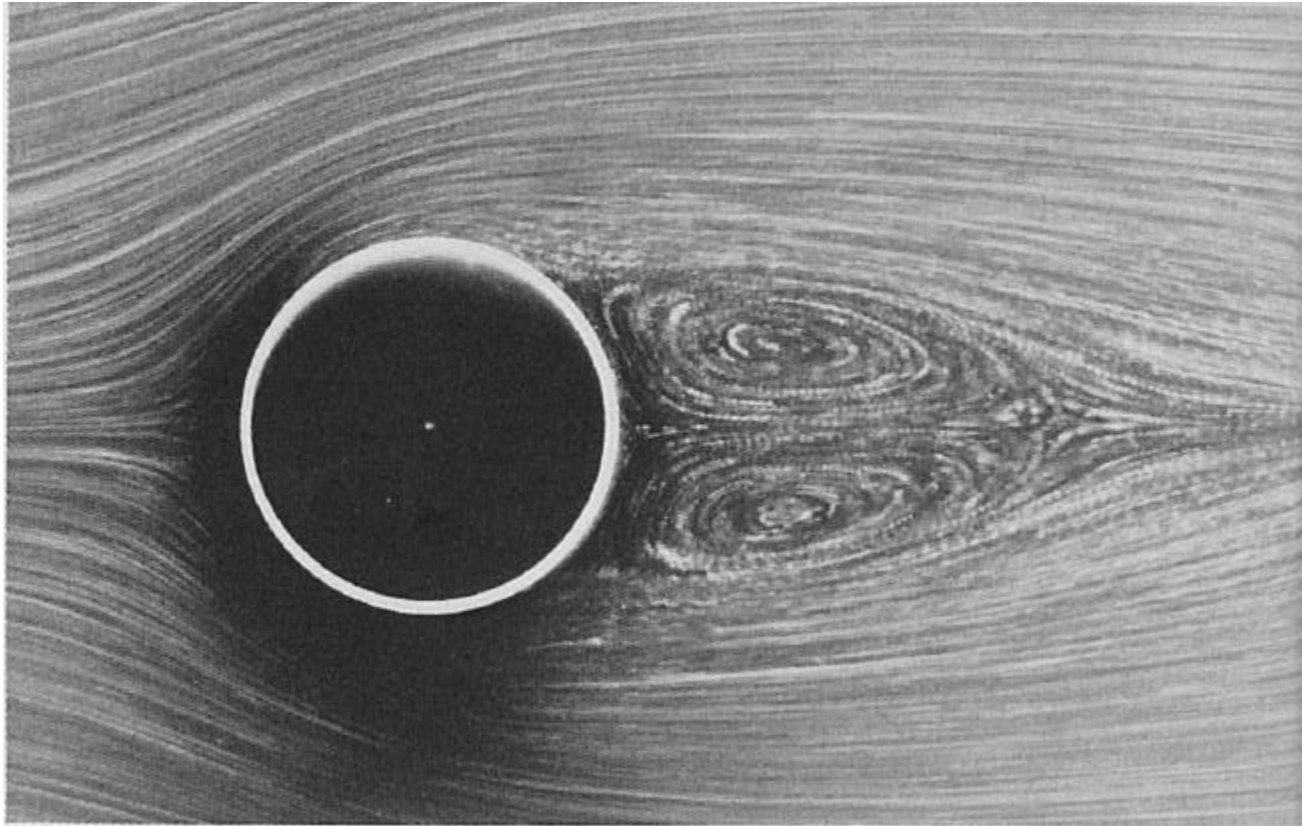
From Van Dyke (1982)

Visualization of Flow Around Smooth Circular Cylinder
 $Re=13.1$



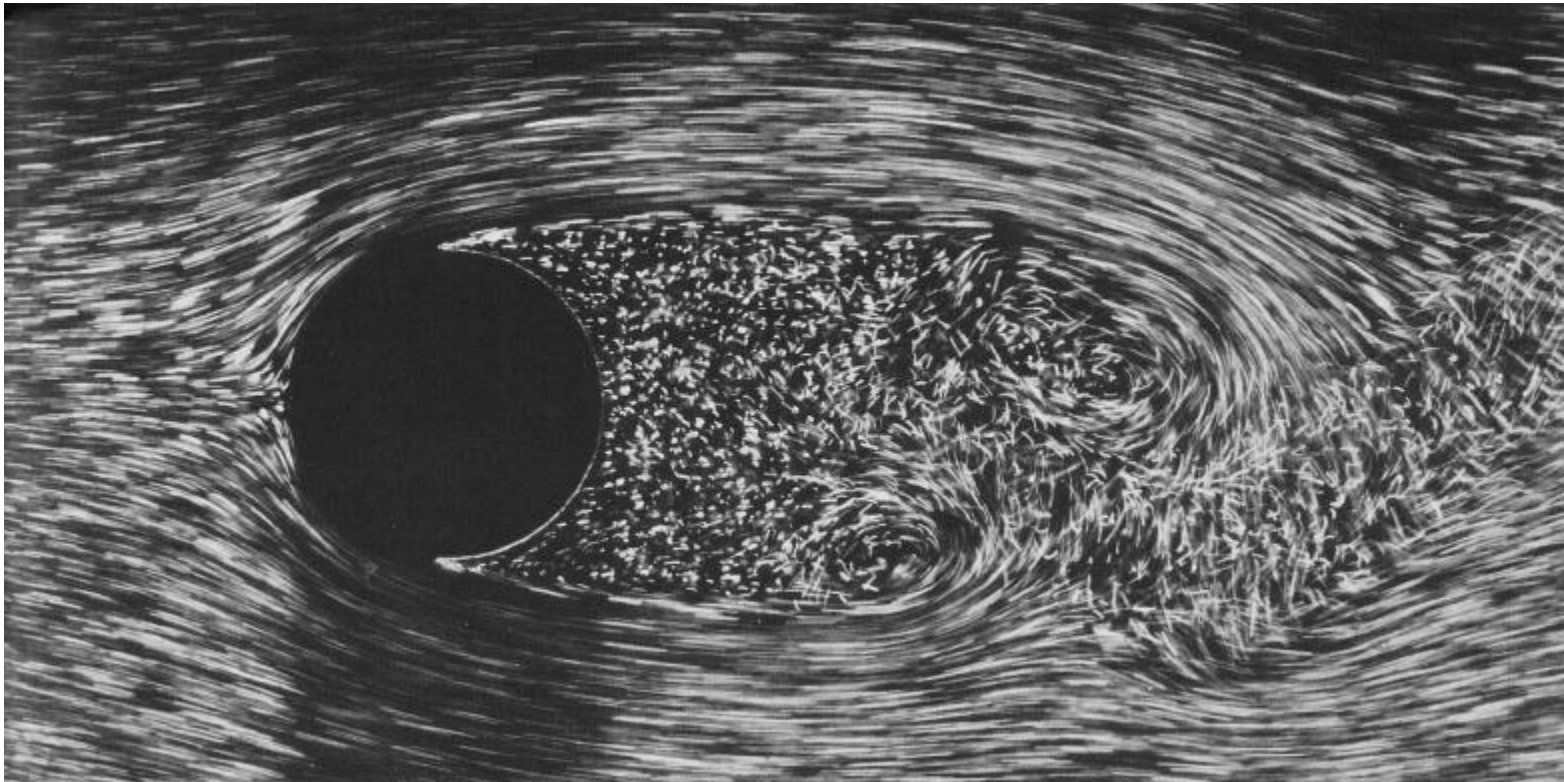
From Van Dyke (1982)

Visualization of Flow Around Smooth Circular Cylinder
 $Re=26$



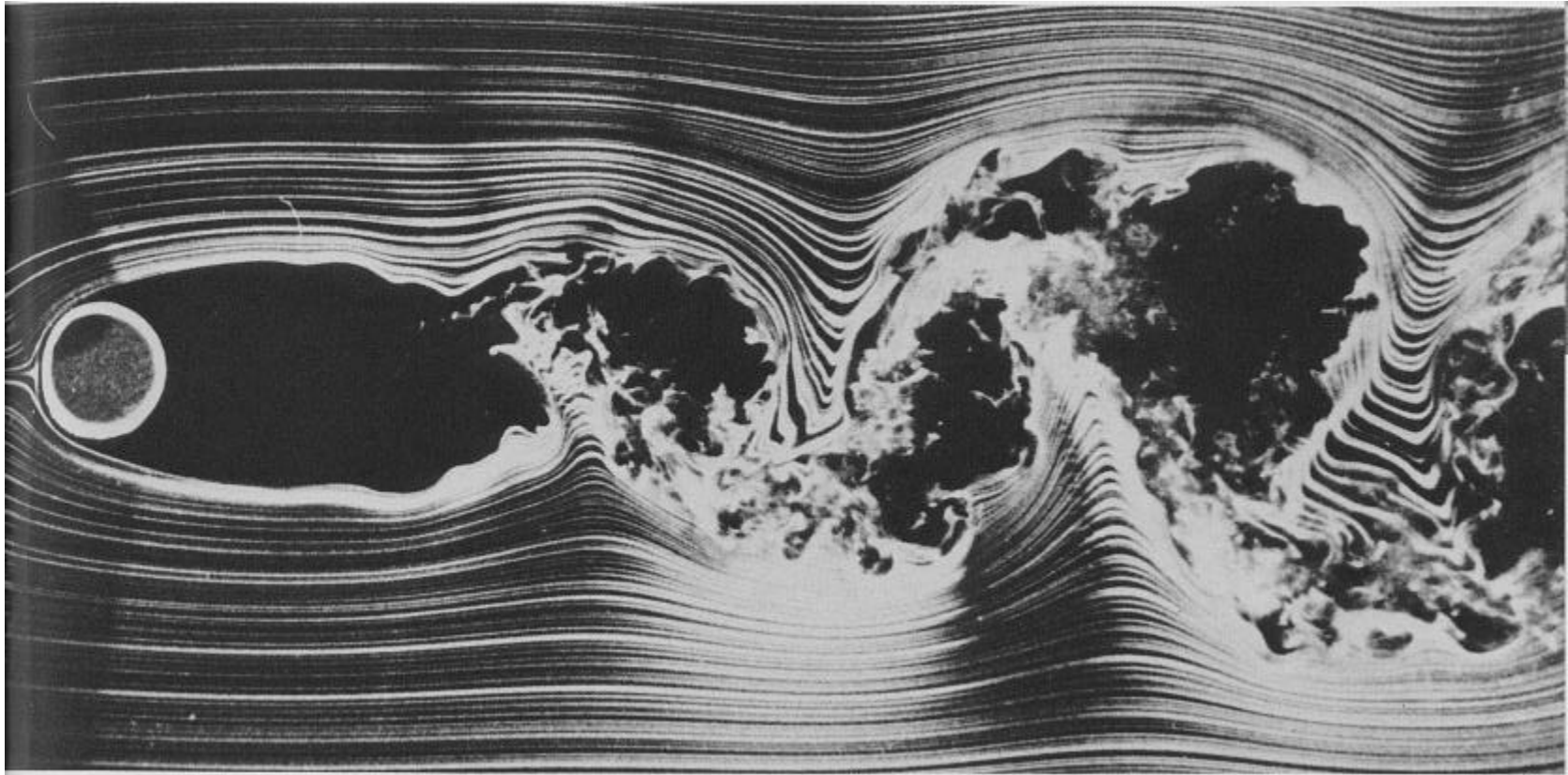
From Van Dyke (1982)

Visualization of Flow Around Smooth Circular Cylinder
 $Re=2,000$



From Van Dyke (1982)

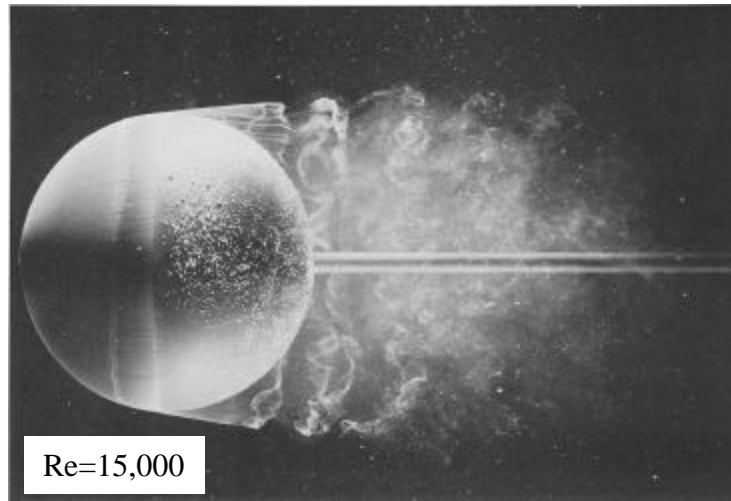
Visualization of Flow Around Smooth Circular Cylinder
 $Re=10,000$



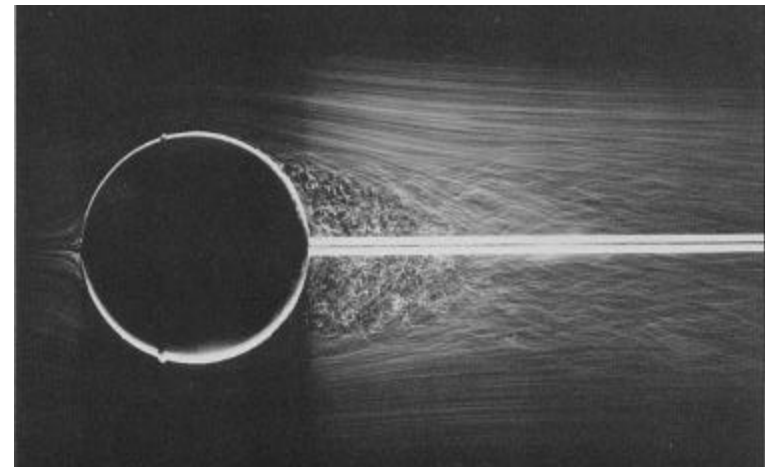
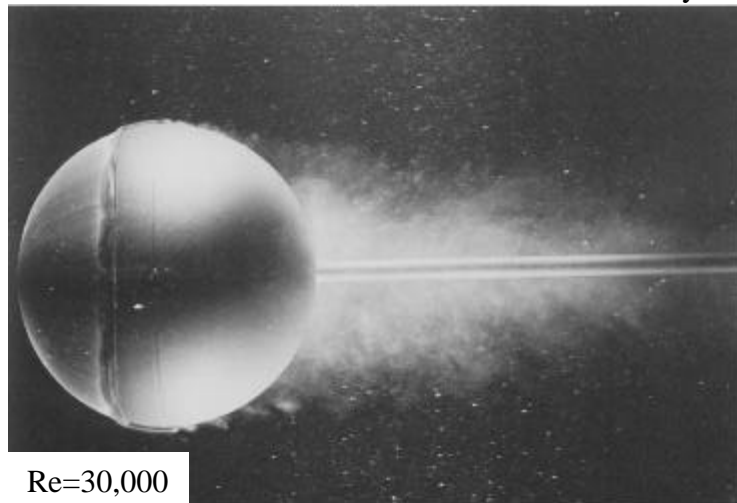
From Van Dyke (1982)

Visualization of Flow Around Smooth Circular Cylinder $Re=10,000$

Boundary Layer is Laminar

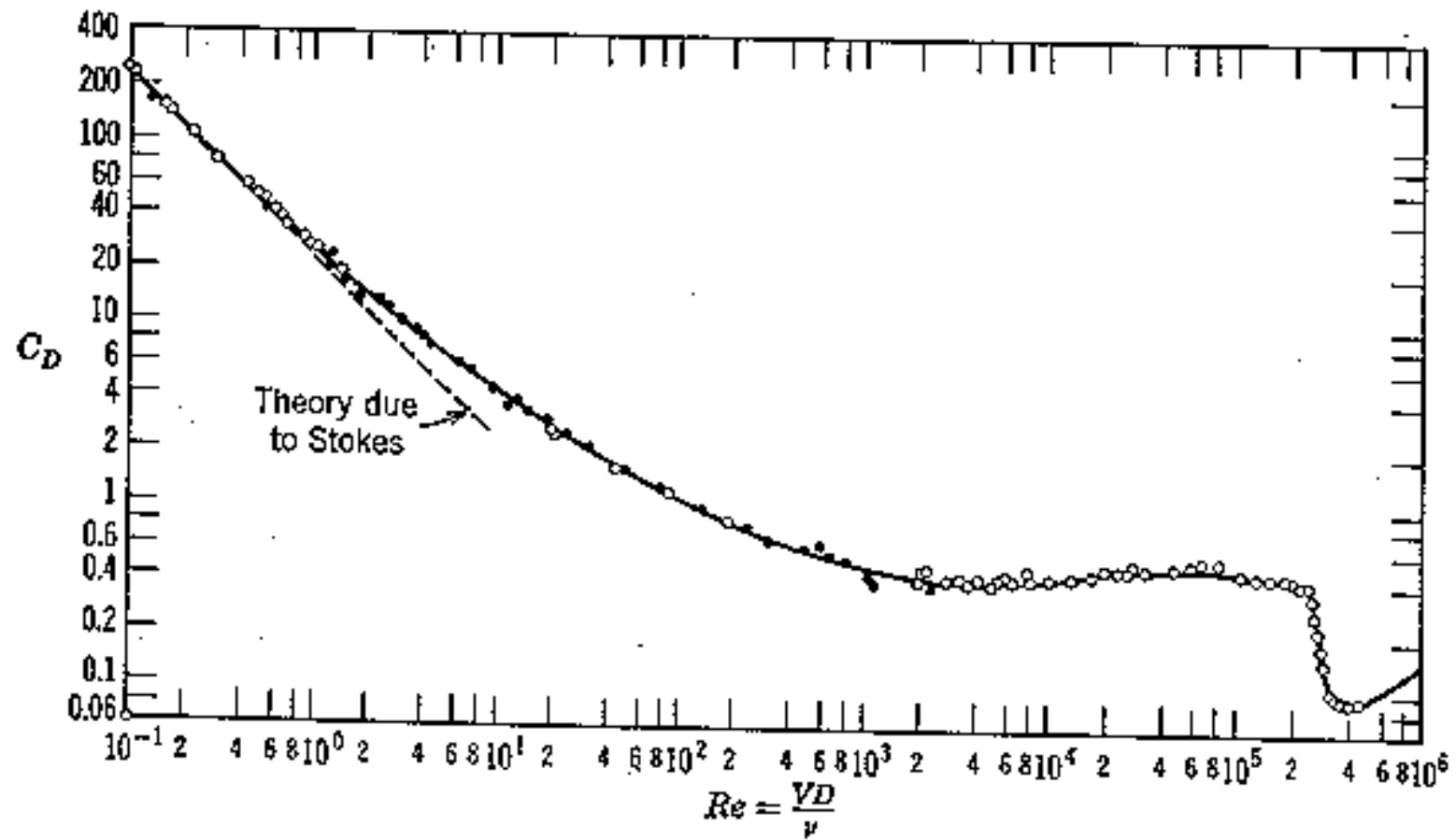


Boundary Layer is made Turbulent through tripping

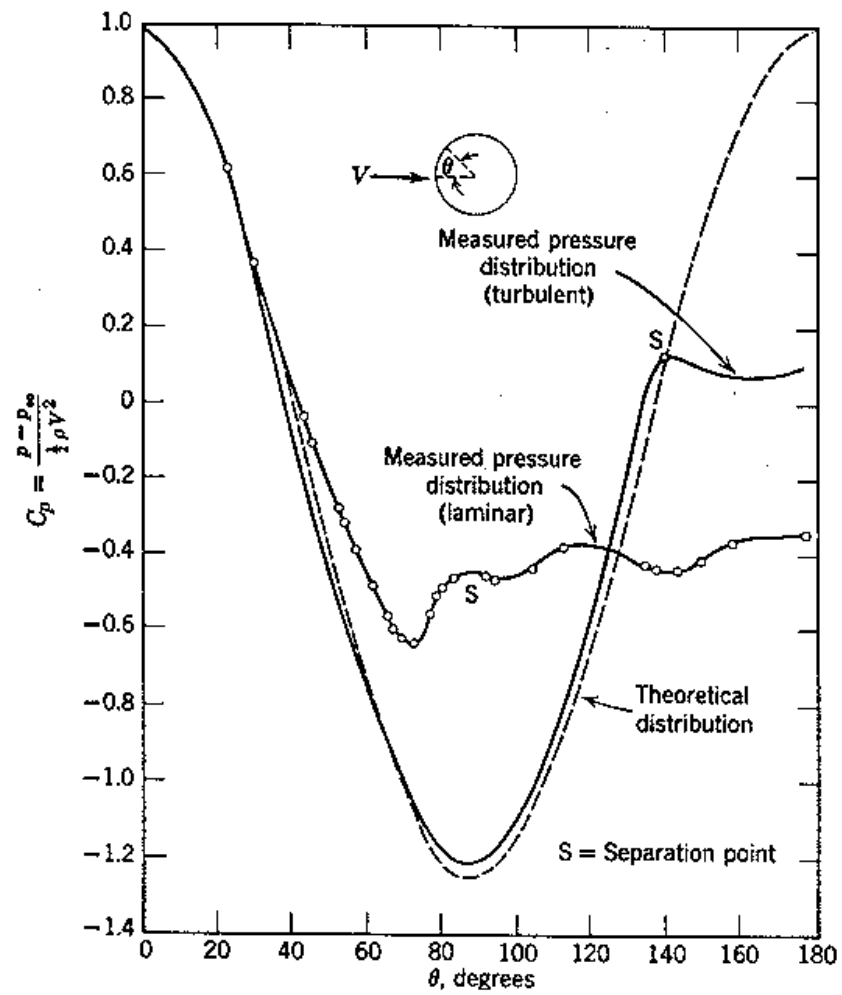


From Van Dyke (1982)

Drag Coefficients for a Smooth Sphere

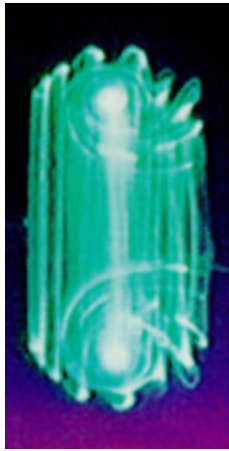


Pressure Distribution Around Smooth Sphere

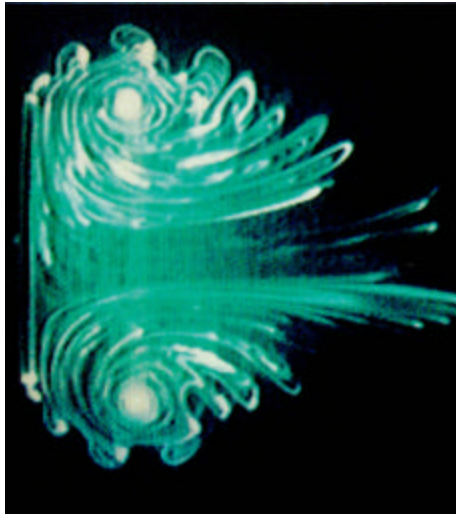


Visualization of Flow Structure Behind a Moving Disk

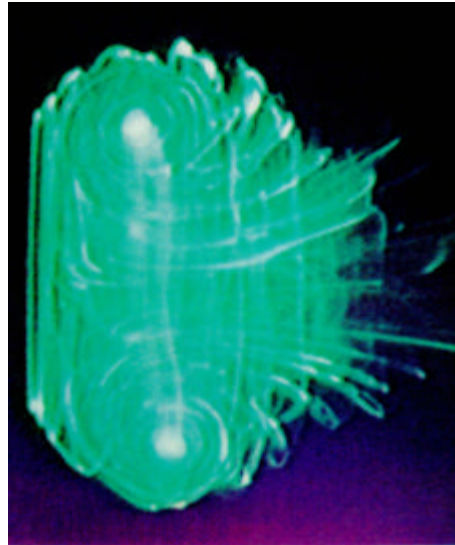
$Re=6,200-4,200$



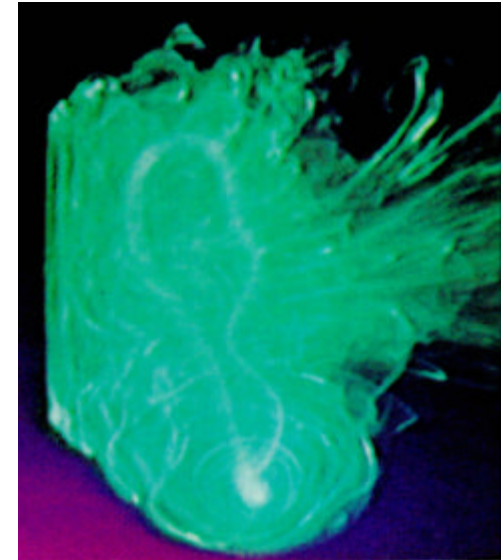
t_1



t_2



t_3



t_4

Disk motion is from right to left

From Higuchi and Belligand (Physics of Fluids, 1992)

Effect of Streamlining on Drag Coefficient

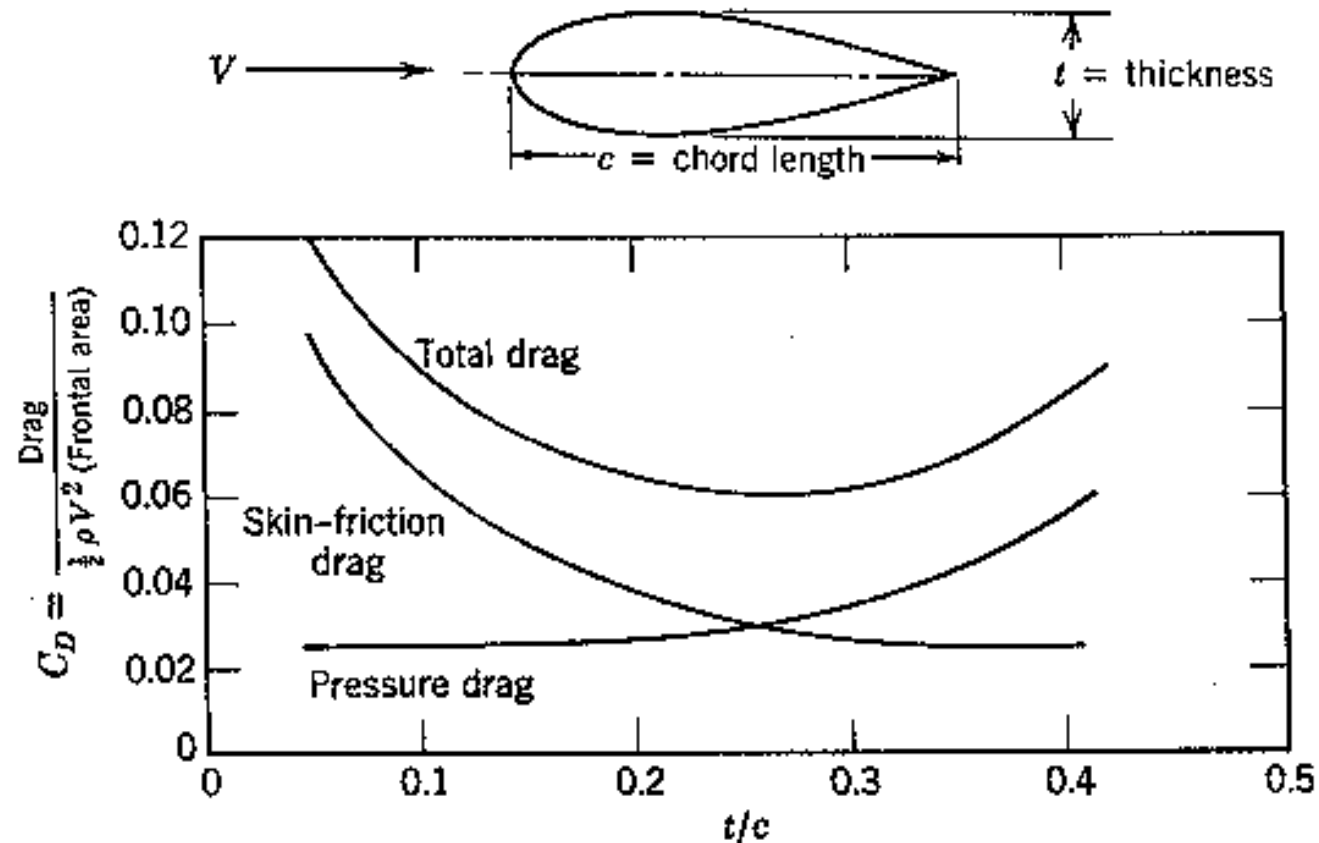
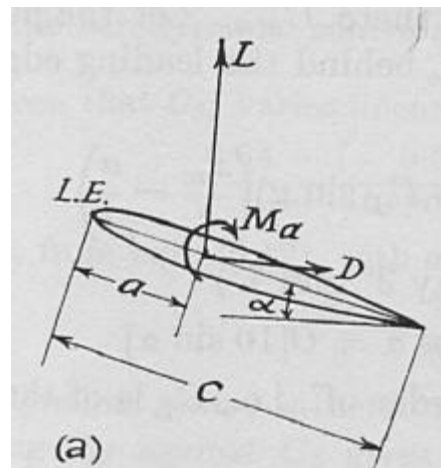
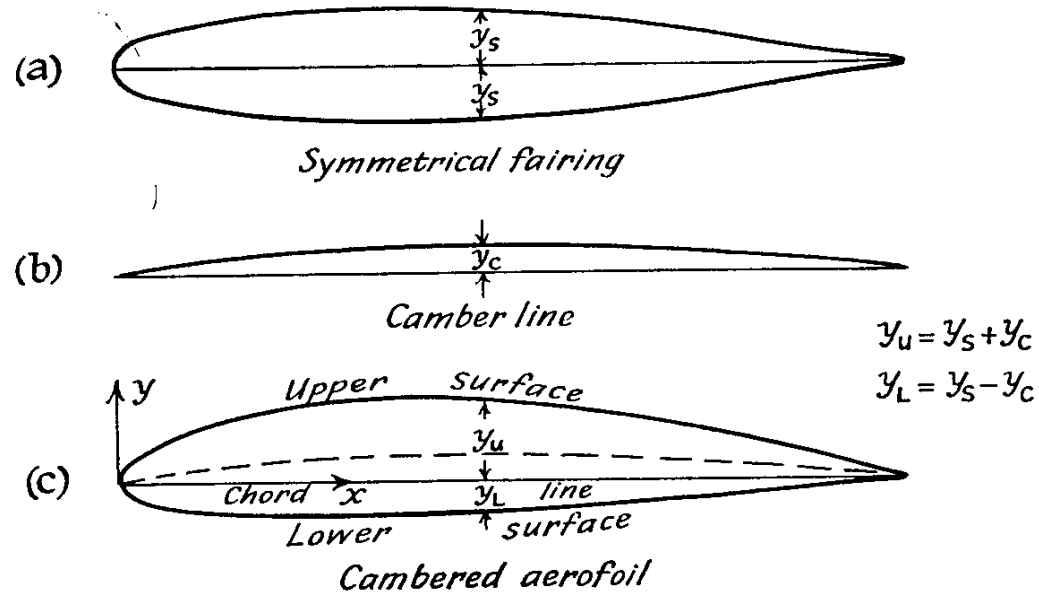


Fig. 9.14 Drag coefficient on a streamlined strut as a function of thickness ratio, showing contributions of skin friction and pressure to total drag [18].

Airfoils: Geometrical Aspects



α : Angle of Attack

Airfoils: Terminology

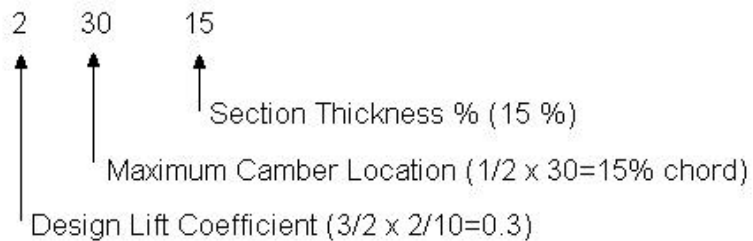
Lift Coefficient:

$$C_L = \frac{|\vec{L}|}{\frac{1}{2} \rho U^2 A_p}$$

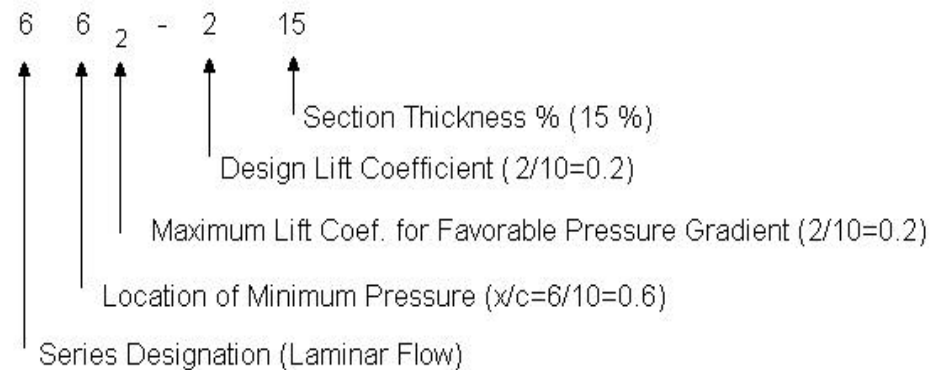
A_p = planform area of the wing (maximum projected area)

Example of Airfoil Section Shape Designations

Conventional: 23015



Laminar Flow: 66₂-215



Pressure Distribution Around Airfoils

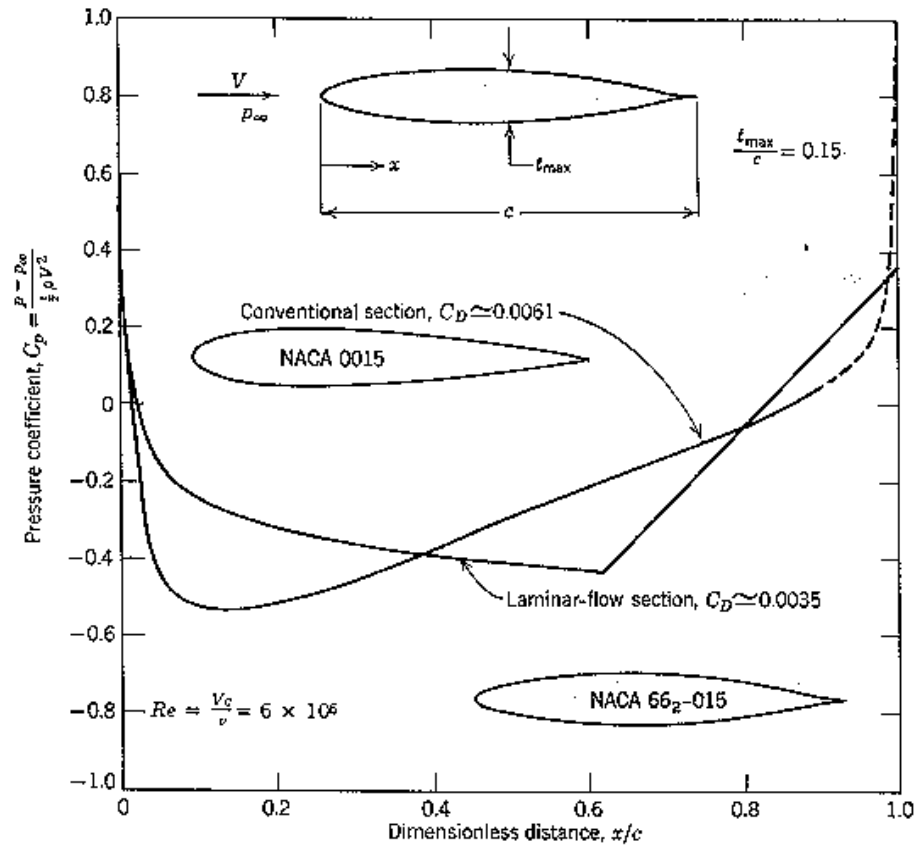
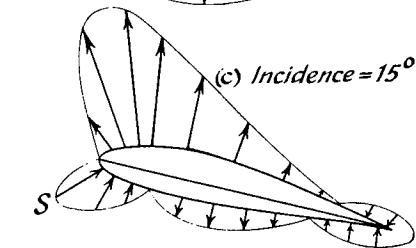
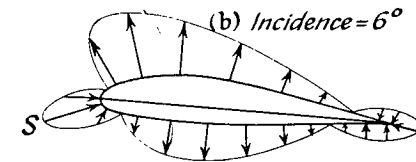
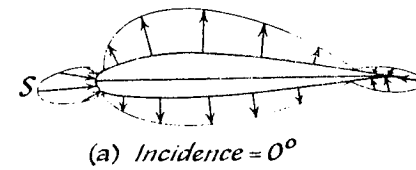


Fig. 9.15 Theoretical pressure distributions at zero angle of attack for two symmetric airfoil sections of 15 percent thickness ratio. (Data from [19].)



Length of arrows $\propto C_p$
 S denotes C_p at stagnation where $C_{ps} = \text{unity}$
 Direction of arrows indicates +ve or -ve C_p

Airfoil Lift and Drag Coefficients

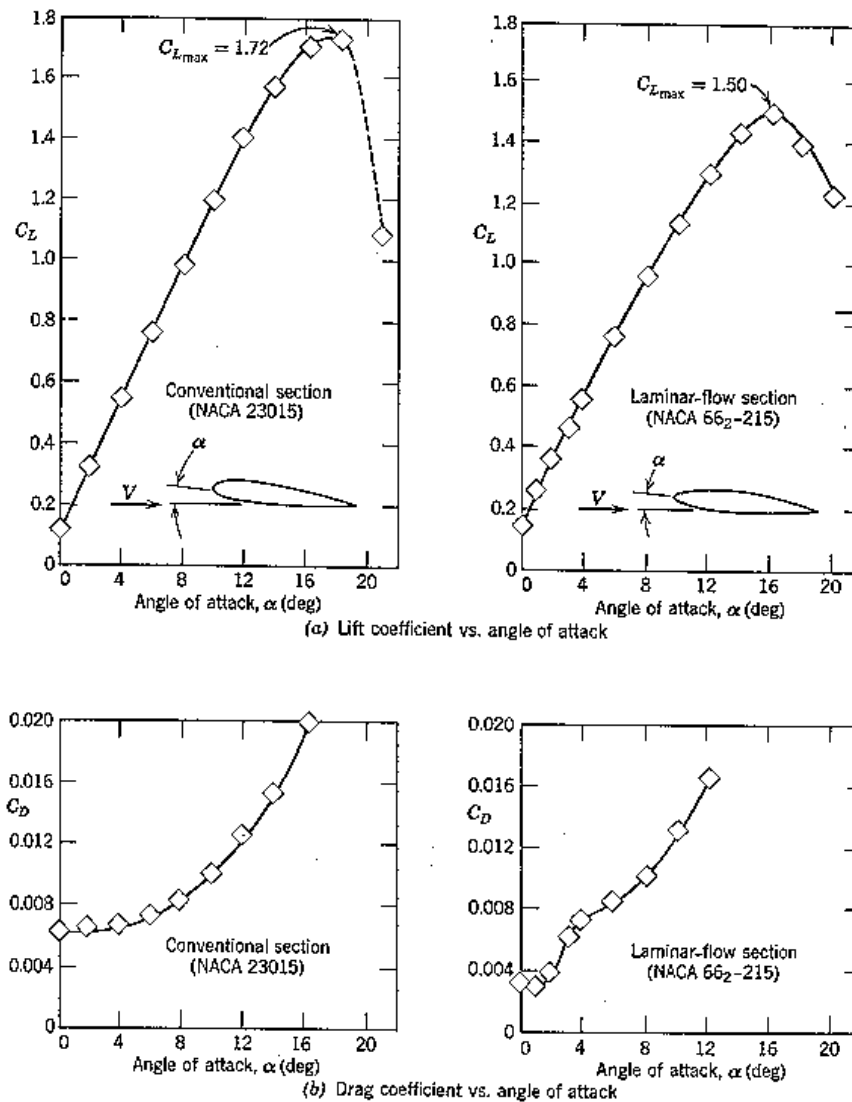
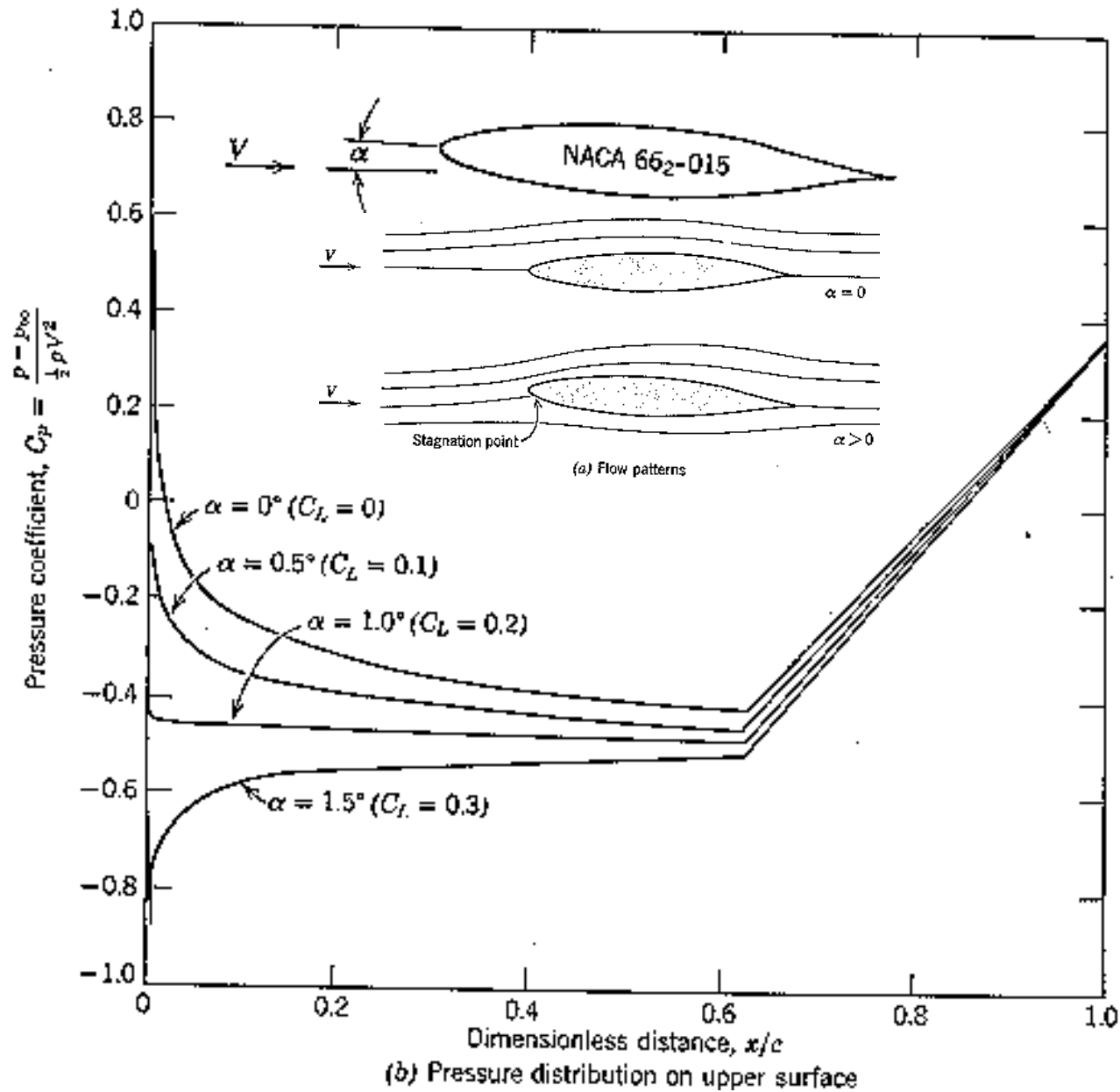
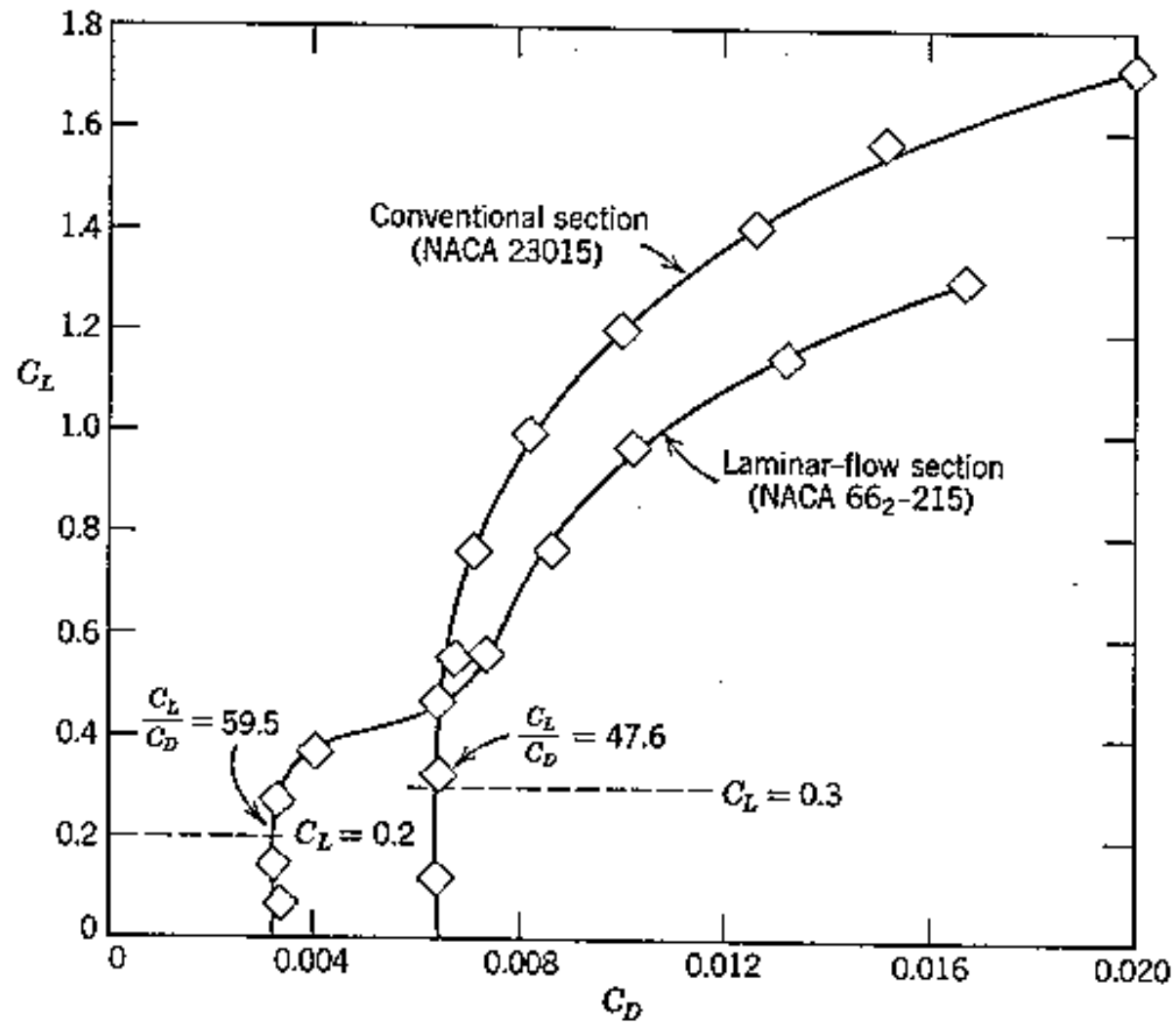


Fig. 9.17 Lift and drag coefficients versus angle of attack for two airfoil sections of 15 percent thickness ratio. (Data from [19].)

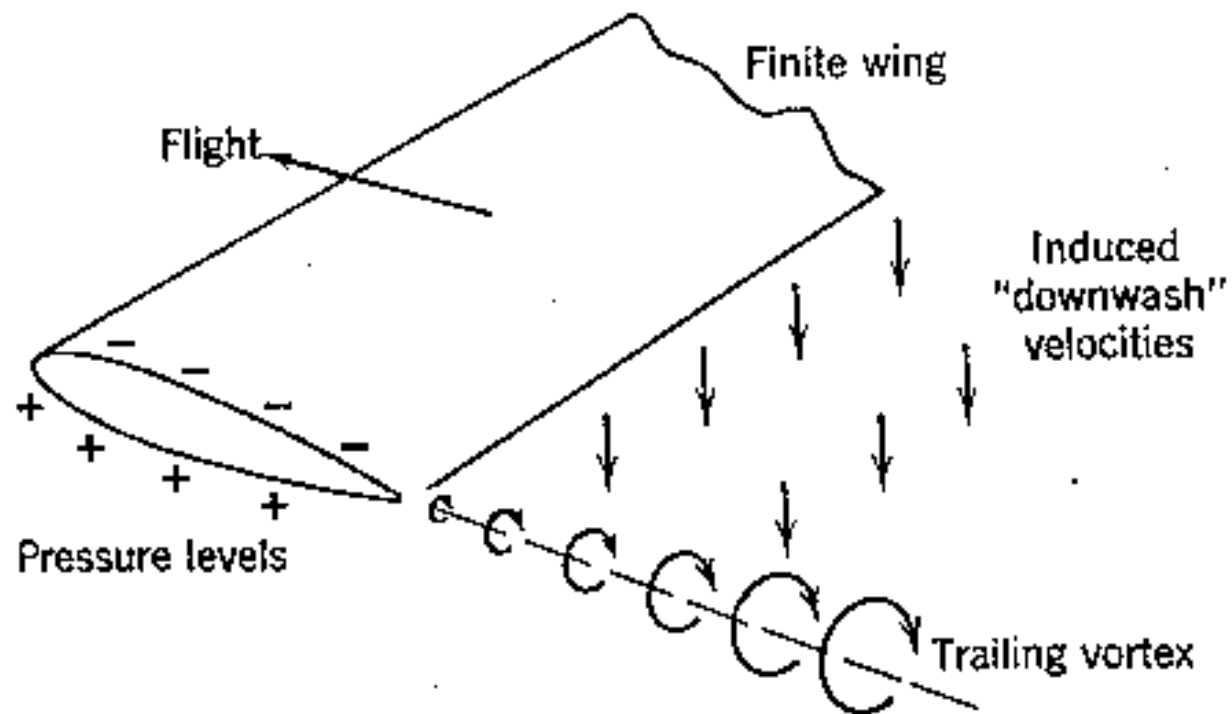
Effect of Angle of Attack on Flow Pattern and Theoretical Pressure Distribution for an Airfoil



Airfoil-Lift and Drag Polars



Trailing Vortices of a Finite Wing



Trailing Vortices in the Wake of an Aircraft



Cessna Citation VI
Wing Span 16.3 m
Wing Area 29m²
V=170 knots (313 km/hr)
Re=1.1x10⁷ based on mean
aerodynamic chord of 2.1 m)

From Higuchi (Physics of Fluids, 1993)
Photograph by P. Bowen of Cessna Aircraft Co.

Finite Wingspan Effects

Aspect Ratio:
$$ar = \frac{b^2}{A} = \frac{(\text{wingspan})^2}{\text{Planform Area}}$$

Approximate Lift Coefficient Dependence on Angle of Attack: $C_L \approx \text{Const} \cdot \alpha$

Effective Increase of Angle of Attack Due to Finite Wingspan:
$$\Delta\alpha \approx \frac{C_L}{\pi \cdot ar}$$

Induced Drag Due to Finite Wingspan: $C_{D,i} = \Delta C_D \approx C_L \cdot \Delta\alpha$

$$C_D \approx C_{D,\infty} + C_{D,i} = C_{D,\infty} + \frac{C_L^2}{\pi \cdot ar}$$

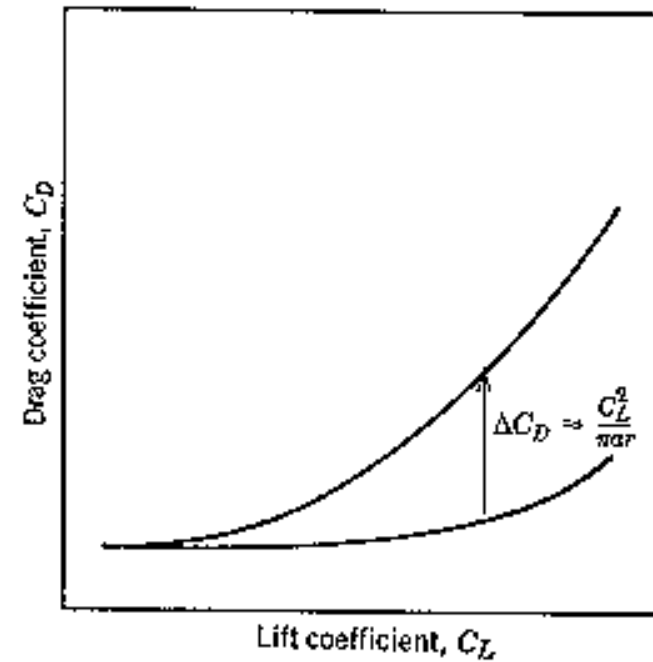
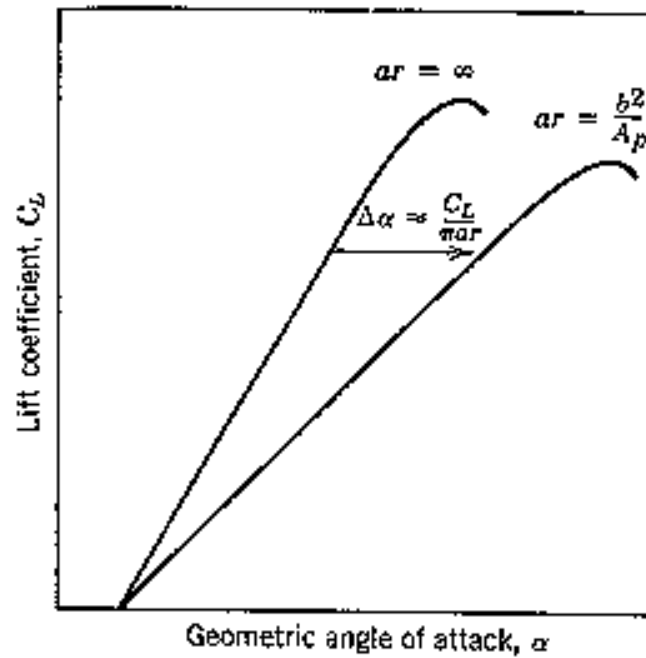
is the Total Drag for Finite Wingspan

Drag Polar Approximation for Complete Aircraft:

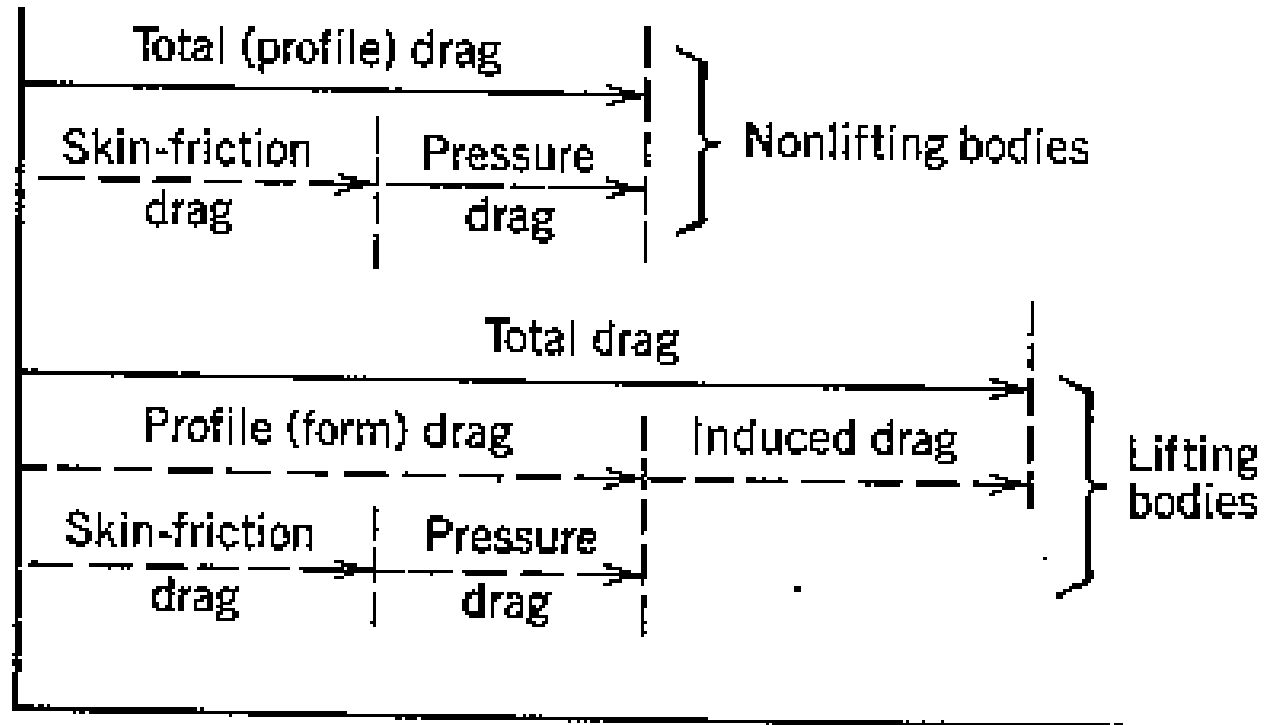
$$C_D \approx C_{D,0} + C_{D,i} = C_{D,0} + \frac{C_L^2}{\pi \cdot ar}$$

$C_{D,0}$ is the drag coefficient at Zero Lift

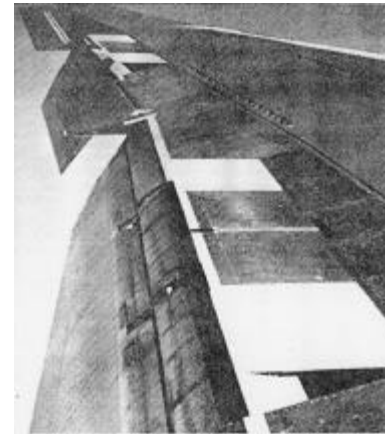
Lift and Drag Coefficients for a Finite-Aspect-Ratio Wing



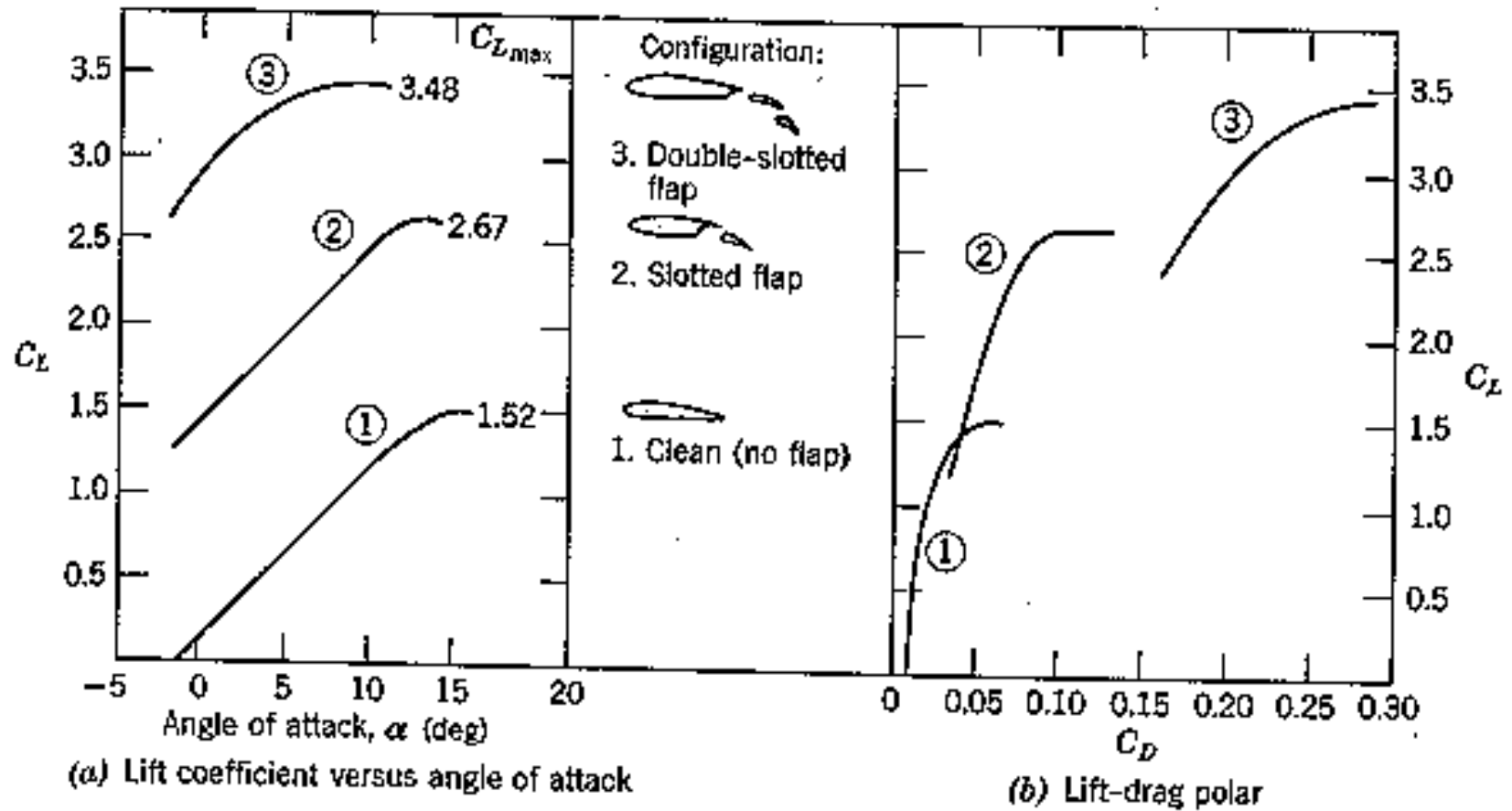
Drag Breakdown on Non-Lifting and Lifting Bodies



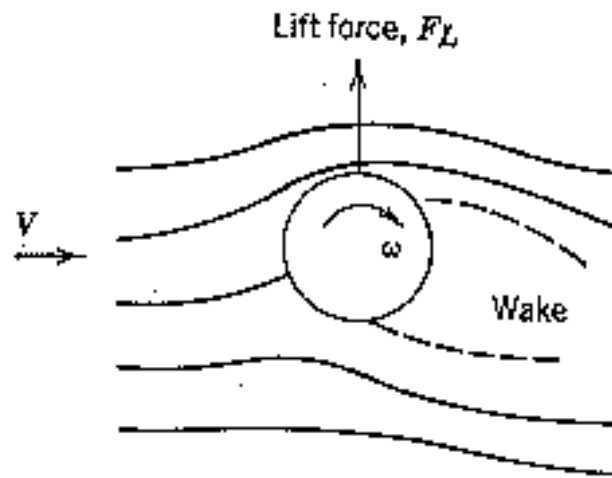
Use of Flaps for Landing Speed Reduction
Use of Spoilers as Lift Destroyers



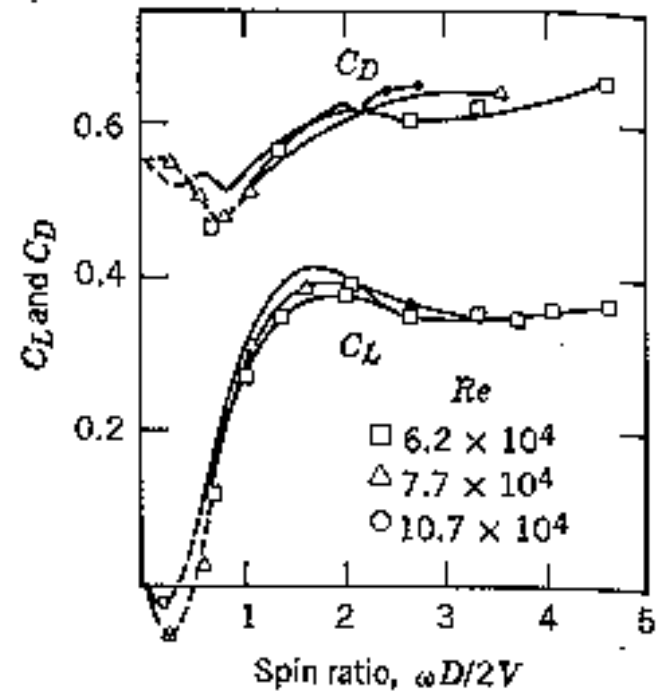
Effects of Flaps



Drag and Lift on Smooth Spinning Sphere



(a) Flow pattern



(b) Lift coefficient

Sailing With a Rotating Cylinder Sail

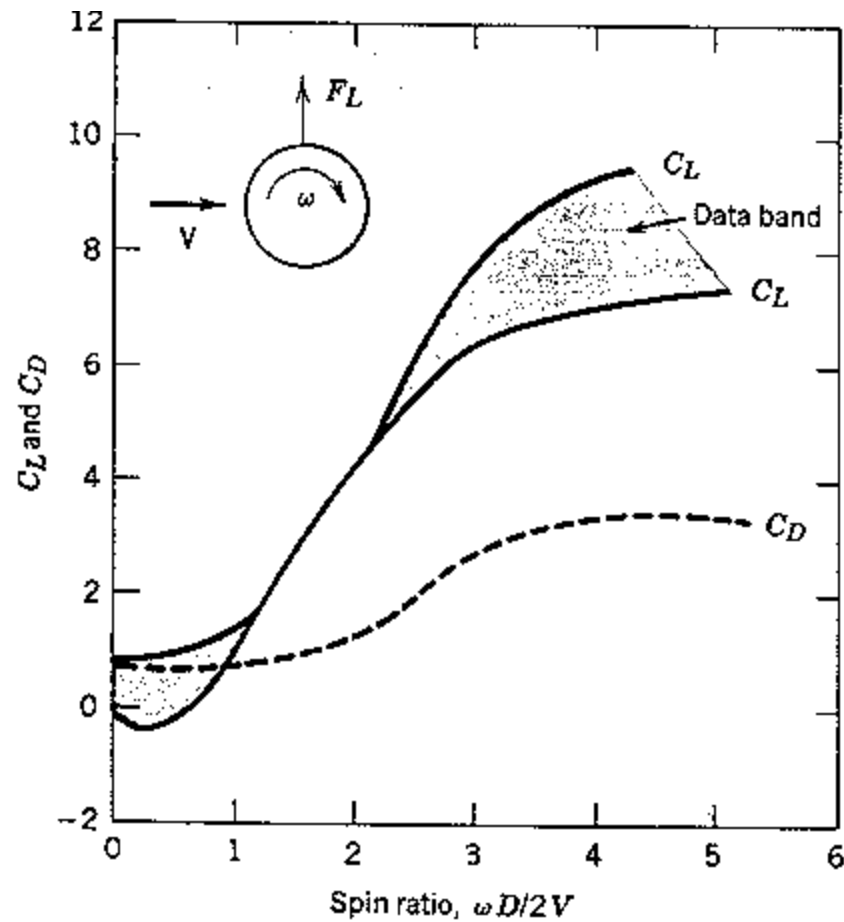
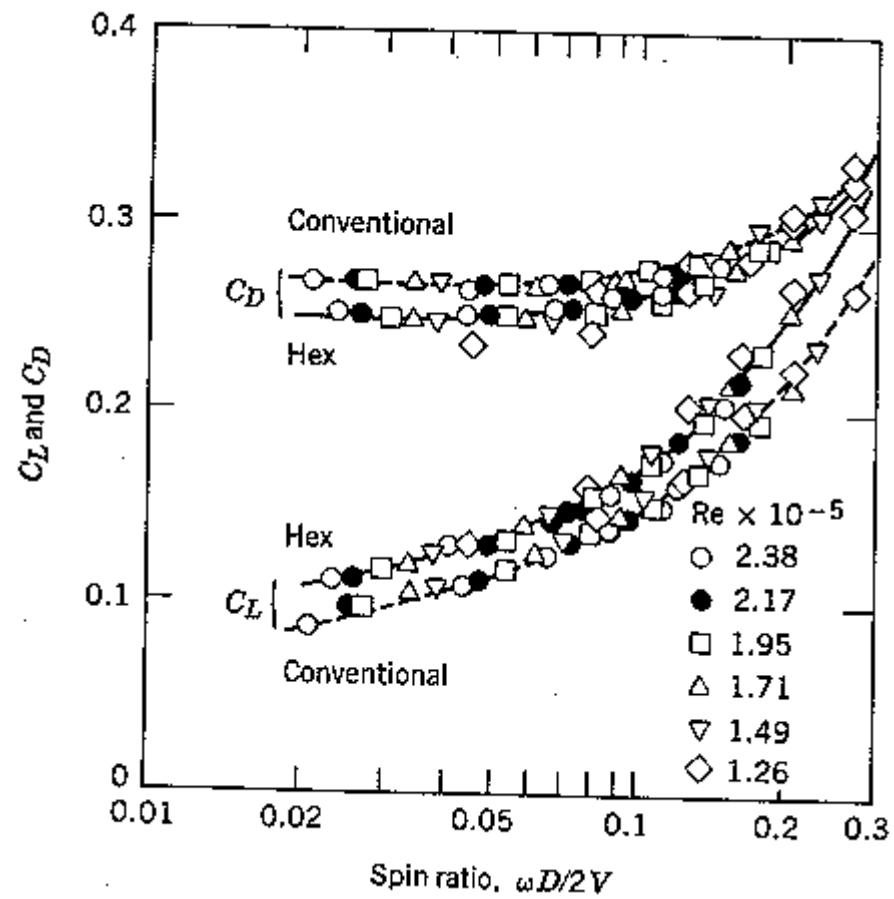


Fig. 9.29 Lift and drag of a rotating cylinder as a function of relative rotational speed: Magnus force. (Data from [32].)

Lift and Drag Coefficients of Golf Balls



Pressure Distribution on an Automobile

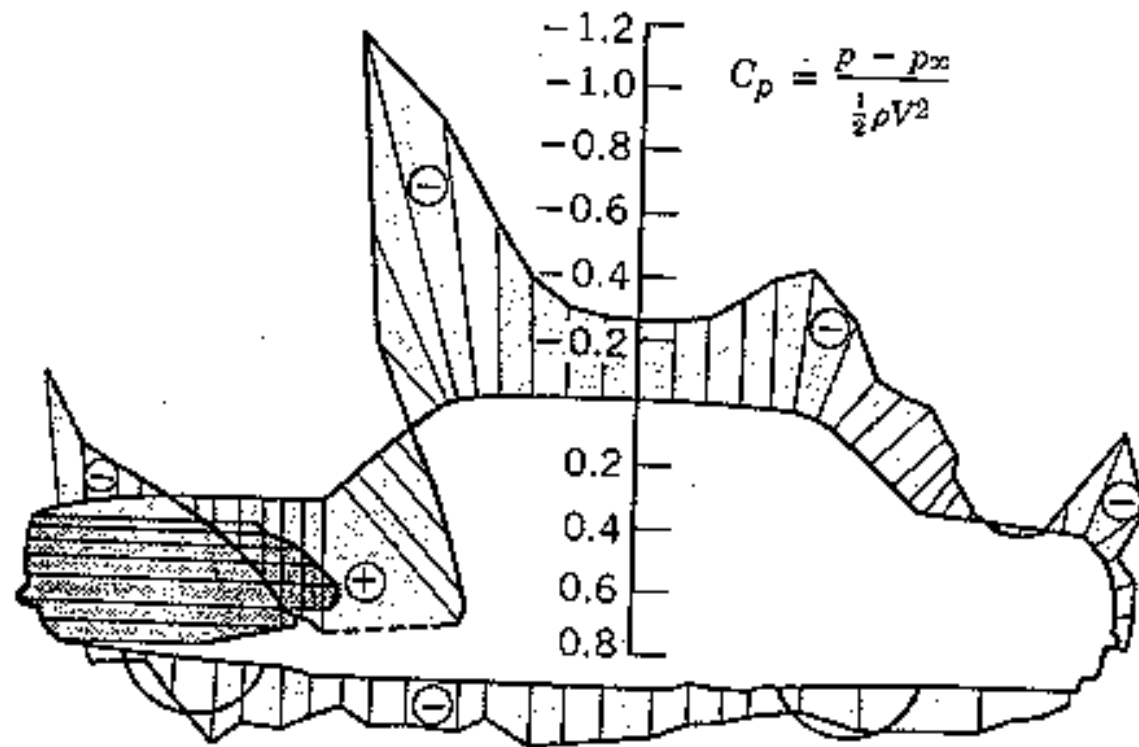


Fig. 9.25 Pressure distribution along the centerline of an automobile [28].