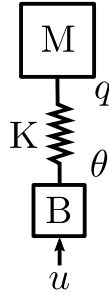


Should we really use \bar{q} ?

1 Spring-mass

1.1 The system



Dynamics equation:

$$u - K(\theta - q) = B\ddot{\theta} \quad (1)$$

$$K(\theta - q) = M\ddot{q} + g(q) \quad (2)$$

Defining desired motor side position according to link side position:

$$K(\theta_d - q_d) = M\ddot{q}_d \quad (3)$$

Control input:

$$u = -K_q\tilde{q} - D_q\dot{\tilde{q}} + M\ddot{q}_d + B\ddot{\theta}_d + \hat{g}(q) \quad (4)$$

$$\tilde{q} = q - q_d$$

1.2 Problem formulation

Closed loop dynamics:

$$M\ddot{q}_d + B\ddot{\theta}_d - B\ddot{\theta} - K_q\tilde{q} - D_q\dot{\tilde{q}} + \hat{g}(q) = M\ddot{q} + g(q) \quad (5)$$

Power balance equation with flow $\dot{\theta}$:

$$\underbrace{\dot{\theta} \underbrace{M\ddot{q}_d}_{K(\theta_d - q_d)}}_{\dot{q} \underbrace{K(\theta_d - q_d)}_{M\ddot{q}_d} + (\dot{\theta} - \dot{q})K(\theta_d - q_d)} + \dot{\theta} B\ddot{\theta}_d - \dot{\theta} B\ddot{\theta} - \dot{\theta}(K_q \tilde{q} + D_q \dot{\tilde{q}}) + \dot{\theta} \hat{g}(q) = \underbrace{\dot{\theta} \underbrace{(M\ddot{q} + g(q))}_{K(\theta - q)}}_{\dot{q} \underbrace{K(\theta - q)}_{M\ddot{q} + g(q)} + (\dot{\theta} - \dot{q})K(\theta - q)} \quad (6)$$

Power balance equation with flow $\dot{\theta}_d$:

$$\underbrace{\dot{\theta}_d \underbrace{M\ddot{q}_d}_{K(\theta_d - q_d)}}_{\dot{q}_d \underbrace{K(\theta_d - q_d)}_{M\ddot{q}_d} + (\dot{\theta}_d - \dot{q}_d)K(\theta_d - q_d)} + \dot{\theta}_d B\ddot{\theta}_d - \dot{\theta}_d B\ddot{\theta} - \dot{\theta}_d(K_q \tilde{q} + D_q \dot{\tilde{q}}) + \dot{\theta}_d \hat{g}(q) = \underbrace{\dot{\theta}_d \underbrace{(M\ddot{q} + g(q))}_{K(\theta - q)}}_{\dot{q}_d \underbrace{K(\theta - q)}_{M\ddot{q} + g(q)} + (\dot{\theta}_d - \dot{q}_d)K(\theta - q)} \quad (7)$$

Subtracting (6) from (7):

$$\dot{q} M\ddot{\tilde{q}} + \underbrace{\dot{\theta} B\ddot{\tilde{\theta}}}_{\stackrel{?}{=} \dot{S}} + \underbrace{\dot{\theta} K_q \tilde{q} - \dot{\theta} \hat{g}(q) + \dot{q} g(q)}_{\stackrel{?}{=} \dot{S}/0} = - \underbrace{\dot{\theta} D_q \dot{\tilde{q}}}_{\stackrel{?}{=} P_D} \quad (8)$$

1.3 Only regulation and Albu-schaeffer idea

Closed loop dynamics (8) will boil down to:

$$\dot{q} M\ddot{\tilde{q}} + \dot{\theta} B\ddot{\tilde{\theta}} + \dot{\theta} K_q \tilde{q} - \dot{\theta} \hat{g}(q) + \dot{q} g(q) = -\dot{\theta} D_q \dot{\tilde{q}} \quad (9)$$

According to [1] the storage function for the closed loop system is:

$$S_{tot} = \underbrace{\frac{1}{2} \dot{\theta} B \dot{\tilde{\theta}} + \frac{1}{2} (\theta - q) K (\theta - q) + \underbrace{\frac{1}{2} \tilde{q} K_q \tilde{q} - V_g(\bar{q})}_{-V_l} - \underbrace{\frac{1}{2} l(\bar{q}(\theta)) K^{-1} l(\bar{q}(\theta))}_{S_l}}_{-V_{\tilde{l}}} + \frac{1}{2} \dot{q} M \dot{\tilde{q}} + V_g(q) \quad (10)$$

where:

$$l(\bar{q}(\theta)) = -K_q \tilde{q}(\theta) + g(\bar{q}(\theta)) \quad (11)$$

$$\tilde{q}(\theta) = \bar{q}(\theta) - q_d \quad (12)$$

$$\bar{q}(\theta) = h^{-1}(\theta) \quad (13)$$

and $h^{-1}(\theta)$ is corresponding q to this θ in static case. Thus, for this static q we have:

$$l(\bar{q}(\theta)) = K(\theta - \bar{q}(\theta)) \quad (14)$$

and as a result S_l in equation (10) will be:

$$S_l = -\frac{1}{2}(\theta - \bar{q}(\theta))K(\theta - \bar{q}(\theta)) \quad (15)$$

why should we have this storage function in S_{tot} ? Before proceeding, we have:

$$\frac{\partial V_l}{\partial \bar{q}} = -K_q \tilde{\bar{q}} + g(\bar{q}) = l(\bar{q}) \quad (16)$$

which makes sense because $\dot{q}l(q)$ is the power going out of controller, and thus for the overall storage function the notion of $-V_l$ is used. Now, we also have:

$$\begin{aligned} \frac{\partial V_l}{\partial \theta} &= -\frac{\partial \bar{q}}{\partial \theta} K_q \tilde{\bar{q}} + \frac{\partial \bar{q}}{\partial \theta} g(\bar{q}) + (1 - \frac{\partial \bar{q}}{\partial \theta}) \underbrace{K(\theta - \bar{q}(\theta))}_{l(\bar{q})} \\ &= \frac{\partial \bar{q}}{\partial \theta} \underbrace{(-K_q \tilde{\bar{q}} + g(\bar{q}))}_{l(\bar{q})} + l(\bar{q}) - \frac{\partial \bar{q}}{\partial \theta} l(\bar{q}) \\ &= l(\bar{q}) \end{aligned} \quad (17)$$

References

- [1] A. Albu-Schäffer, C. Ott, and G. Hirzinger. Passivity based cartesian impedance control for flexible joint manipulators. *IFAC Proceedings Volumes*, 37(13):901–906, 2004.