

# Final Quiz - Comprehensive Worked Examples

This document contains detailed worked examples covering all major problem types that may appear on the quiz, based on homework assignments, class slides, and typical exam problems.

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## SECTION 1: TRANSFER FUNCTIONS & CIRCUIT ANALYSIS

### EXAMPLE 1.1: Finding H(s) from Op-Amp Circuit (HW07-P1)

**Problem:** For the inverting op-amp circuit with  $R_1 = 1 \text{ kohm}$ ,  $R_f = 2 \text{ kohm}$ ,  $C = 0.5 \text{ microF}$  in feedback, find  $H(s) = V_2(s)/V_1(s)$ .

**Solution:**

**Step 1:** Identify impedances - Input impedance:  $Z_{in} = R_1 = 1000 \text{ ohm}$  - Feedback impedance (parallel RC):

$$Z_f = R_f \parallel \frac{1}{sC} = \frac{R_f \cdot \frac{1}{sC}}{R_f + \frac{1}{sC}} = \frac{R_f}{1 + sR_fC}$$

**Step 2:** Apply inverting amplifier formula

$$H(s) = -\frac{Z_f}{Z_{in}} = -\frac{R_f/(1 + sR_fC)}{R_1}$$

**Step 3:** Substitute values

$$H(s) = -\frac{2000}{1000(1 + s \cdot 2000 \cdot 0.5 \times 10^{-6})}$$

$$H(s) = -\frac{2}{1 + 0.001s} = -\frac{2000}{s + 1000}$$

**Answer:**  $H(s) = -\frac{2000}{s+1000}$  (first-order low-pass with gain 2 and cutoff at 1000 rad/s)

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### EXAMPLE 1.2: Lead Network Analysis (HW08-P1)

**Problem:** For the RC network with two series RC branches in voltage divider configuration, find: (a) Input impedance  $Z(s) = V_1(s)/I_1(s)$  (b) Transfer function  $H(s) = V_2(s)/V_1(s)$  in form  $H(s) = K \frac{s+\beta}{s+\alpha}$  (c) Design for  $H(s)$  with  $\beta = 1000$ ,  $\alpha = 100$

**Solution:**

**Part (a):** Input impedance (series combination)

$$Z(s) = R_1 + \frac{1}{sC_1} + R_2 \parallel \frac{1}{sC_2}$$

For parallel branch:

$$R_2 \parallel \frac{1}{sC_2} = \frac{R_2}{1 + sR_2C_2}$$

**Part (b):** Voltage divider for  $H(s)$

$$H(s) = \frac{Z_{output}}{Z_{total}} = \frac{R_2/(1 + sR_2C_2)}{R_1 + 1/(sC_1) + R_2/(1 + sR_2C_2)}$$

After algebraic manipulation:

$$H(s) = K \frac{s + 1/(R_2C_2)}{s + 1/(R_{eq}C_{eq})}$$

where K depends on component values.

**Part (c):** Design with  $C_1 = C_2 = C$

Given:  $\beta = 1000$ ,  $\alpha = 100$

$$\text{From zero: } \beta = \frac{1}{R_2C} = 1000 \Rightarrow R_2 = \frac{1}{1000C}$$

$$\text{From pole: } \alpha = \frac{1}{R_{eq}C} = 100 \Rightarrow R_{eq} = \frac{1}{100C}$$

Choose  $C = 1 \text{ microF}$ : -  $R_2 = 1 \text{ kohm}$  - Need to solve for  $R_1$  based on pole constraint

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### EXAMPLE 1.3: Series RLC Bandpass (HW07-P3)

**Problem:** Given  $R = 20 \text{ ohm}$ ,  $L = 1 \text{ H}$ ,  $C = 1 \text{ microF}$ , find  $H(s) = V_2(s)/V_1(s)$  where  $V_2$  is across  $R$ .

**Solution:**

**Step 1:** Total impedance

$$Z_{total} = R + sL + \frac{1}{sC}$$

**Step 2:** Voltage divider (output across  $R$ )

$$H(s) = \frac{R}{R + sL + \frac{1}{sC}} = \frac{R \cdot sC}{sRLC + s^2LC + 1}$$

**Step 3:** Substitute values

$$H(s) = \frac{20s \cdot 10^{-6}}{s \cdot 20 \cdot 1 \cdot 10^{-6} + s^2 \cdot 1 \cdot 10^{-6} + 1}$$

Multiply numerator and denominator by  $10^6$ :

$$H(s) = \frac{20s}{s^2 + 20s + 10^6}$$

**Step 4:** Find resonant frequency

$$\omega_0 = \sqrt{\frac{1}{LC}} = \sqrt{\frac{1}{1 \times 10^{-6}}} = 1000 \text{ rad/s}$$

**Step 5:** At resonance ( $\omega = 1000 \text{ rad/s}$ )

$$H(j1000) = \frac{20 \cdot j1000}{(j1000)^2 + 20(j1000) + 10^6} = \frac{j20000}{j20000} = 1$$

**Maximum output at resonance!**

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## SECTION 2: PARTIAL FRACTION EXPANSION

### EXAMPLE 2.1: Basic PFE with Two Real Poles

**Problem:** Find inverse Laplace transform of  $F(s) = \frac{100000}{(s+100)(s+1000)}$

**Solution:**

**Step 1:** Setup PFE

$$F(s) = \frac{k_1}{s + 100} + \frac{k_2}{s + 1000}$$

**Step 2:** Cover-up method for  $k_1$  (pole at  $s = -100$ )

$$k_1 = \left[ (s + 100) \cdot \frac{100000}{(s + 100)(s + 1000)} \right]_{s=-100}$$

$$k_1 = \frac{100000}{-100 + 1000} = \frac{100000}{900} = 111.11$$

**Step 3:** Cover-up method for  $k_2$  (pole at  $s = -1000$ )

$$k_2 = \left[ (s + 1000) \cdot \frac{100000}{(s + 100)(s + 1000)} \right]_{s=-1000}$$

$$k_2 = \frac{100000}{-1000 + 100} = \frac{100000}{-900} = -111.11$$

**Step 4:** Inverse Laplace transform

$$f(t) = 111.11e^{-100t} - 111.11e^{-1000t} \text{ for } t \geq 0$$

**Answer:**  $f(t) = 111.11(e^{-100t} - e^{-1000t})u(t)$

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**EXAMPLE 2.2: PFE with s Term in Numerator (HW08-P3b)**

**Problem:** Find partial fraction expansion of  $H(s) = \frac{10^4 s}{(s+10)(s+1000)}$  in form  $K \left( \frac{\alpha}{s+\alpha} - \frac{\beta}{s+\beta} \right)$

**Solution:**

**Step 1:** Factor out constant K

$$H(s) = 10^4 \cdot \frac{s}{(s+10)(s+1000)}$$

**Step 2:** Standard PFE

$$\frac{s}{(s+10)(s+1000)} = \frac{k_1}{s+10} + \frac{k_2}{s+1000}$$

**Step 3:** Cover-up for k1

$$k_1 = \left[ \frac{s}{s+1000} \right]_{s=-10} = \frac{-10}{-10+1000} = \frac{-10}{990} = -0.0101$$

**Step 4:** Cover-up for k2

$$k_2 = \left[ \frac{s}{s+10} \right]_{s=-1000} = \frac{-1000}{-1000+10} = \frac{-1000}{-990} = 1.0101$$

**Step 5:** Rewrite in requested form

$$H(s) = 10^4 (1.0101 \cdot \frac{1}{s+1000} - 0.0101 \cdot \frac{1}{s+10})$$

$$H(s) = 10101 \left( \frac{1000}{s+1000} - \frac{10}{s+10} \right)$$

$$H(s) = 10.1 \left( \frac{1000}{s+1000} - \frac{10}{s+10} \right)$$

**This shows:** K = 10.1, alpha = 1000, beta = 10

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**EXAMPLE 2.3: Repeated Poles (HW06-P4a)**

**Problem:** Given step response  $v_2(t) = 24(1 - e^{-50t} - 50te^{-50t})u(t)$ , find H(s).

**Solution:**

**Step 1:** Take Laplace transform

$$V_2(s) = 24 \left[ \frac{1}{s} - \frac{1}{s+50} - \frac{50}{(s+50)^2} \right]$$

**Step 2:** Common denominator

$$\begin{aligned} V_2(s) &= 24 \cdot \frac{(s+50)^2 - s(s+50) - 50s}{s(s+50)^2} \\ &= 24 \cdot \frac{s^2 + 100s + 2500 - s^2 - 50s - 50s}{s(s+50)^2} \\ &= 24 \cdot \frac{2500}{s(s+50)^2} = \frac{60000}{s(s+50)^2} \end{aligned}$$

**Step 3:** Find H(s) (input is step, so  $V_1(s) = 1/s$ )

$$H(s) = \frac{V_2(s)}{V_1(s)} = V_2(s) \cdot s = \frac{60000}{(s+50)^2}$$

**This has a repeated pole at s = -50**

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## SECTION 3: SINUSOIDAL STEADY-STATE & FREQUENCY RESPONSE

### EXAMPLE 3.1: Finding Output for Sinusoidal Input (HW07-P1)

**Problem:** Given  $H(s) = -\frac{2000}{s+1000}$ , find  $v_2(t)$  for various inputs.

**General Method:** 1. Substitute  $s = j\omega$  2. Find  $|H(j\omega)|$  and  $\angle H(j\omega)$  3. Output:  $v_2(t) = A|H(j\omega)| \cos(\omega t + \theta + \angle H(j\omega))$

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**Case (a):  $v_1(t) = 5\cos(10t)$  V ( $\omega = 10$  rad/s, much less than cutoff)**

$$H(j10) = -\frac{2000}{j10 + 1000} = -\frac{2000}{1000 + j10}$$

Magnitude:

$$|H(j10)| = \frac{2000}{\sqrt{1000^2 + 10^2}} = \frac{2000}{\sqrt{1000100}} \approx 2.0$$

Phase (negative sign contributes 180 degrees):

$$\angle H(j10) = 180^\circ - \arctan(10/1000) = 180^\circ - 0.57^\circ = 179.4^\circ$$

**Answer:**  $v_2(t) = 10 \cos(10t + 179.4^\circ)$  V

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**Case (b):  $v_1(t) = 5\cos(1000t)$  V ( $\omega =$  cutoff frequency)**

$$H(j1000) = -\frac{2000}{j1000 + 1000} = -\frac{2000}{1000(1 + j)}$$

Magnitude:

$$|H(j1000)| = \frac{2000}{1000\sqrt{2}} = \frac{2}{\sqrt{2}} = \sqrt{2} \approx 1.414$$

Phase:

$$\angle H(j1000) = 180^\circ - 45^\circ = 135^\circ$$

**Answer:**  $v_2(t) = 7.07 \cos(1000t + 135^\circ)$  V (This is -3 dB point!)

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**Case (c):  $v_1(t) = 5\cos(100000t)$  V ( $\omega$  much greater than cutoff)**

$$H(j10^5) = -\frac{2000}{j10^5 + 1000} \approx -\frac{2000}{j10^5}$$

Magnitude:

$$|H(j10^5)| = \frac{2000}{10^5} = 0.02$$

Phase:

$$\angle H(j10^5) = 180^\circ - 90^\circ = 90^\circ$$

**Answer:**  $v_2(t) = 0.1 \cos(10^5 t + 90^\circ)$  V

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### EXAMPLE 3.2: Extracting H(s) from Bode Plot (HW07-P4 & P5)

**Problem Type 1:** Low-pass  $H(s) = K \frac{\alpha}{s+\alpha}$

**Given from Bode plot:** - DC gain = 6 dB - Phase = -45 degrees at  $\omega = 1000$  rad/s

**Solution:**

Phase is -45 degrees at corner frequency, so: **alpha = 1000 rad/s**

DC gain:  $20 \log_{10} K = 6$  dB

$$K = 10^{6/20} = 10^{0.3} = 2$$

**Answer:**  $H(s) = \frac{2 \cdot 1000}{s+1000} = \frac{2000}{s+1000}$

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**Problem Type 2:** High-pass  $H(s) = K \frac{s}{s+\alpha}$

**Given from Bode plot:** - Phase = 45 degrees at  $\omega = 100$  rad/s - High-frequency gain = 0 dB

**Solution:**

For high-pass, phase = 45 degrees at corner, so: **alpha = 100 rad/s**

High-frequency gain (as  $\omega$  approaches infinity):

$$\lim_{\omega \rightarrow \infty} |H(j\omega)| = K$$

From plot: 0 dB means  $K = 1$

**Answer:**  $H(s) = \frac{s}{s+100}$

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## SECTION 4: CIRCUIT DESIGN FROM H(s)

### EXAMPLE 4.1: First-Order Circuit Design (HW06-P1a)

**Problem:** Design circuit for  $H(s) = \frac{200000}{s+100000}$

**Solution:**

**Step 1:** Identify characteristics - First-order low-pass - DC gain  $K = 2$  - Cutoff  $\omega_c = 100000$  rad/s = 100 krad/s

**Step 2:** Choose topology - Non-inverting with RC low-pass

Basic form:  $H(s) = \mu \cdot \frac{1/RC}{s+1/RC}$

**Step 3:** Design RC section for cutoff Choose  $C = 0.1$  microF:

$$\omega_c = \frac{1}{RC} = 100000 \implies R = \frac{1}{100000 \times 0.1 \times 10^{-6}} = 100 \text{ ohm}$$

**Step 4:** Design op-amp gain Need  $\mu = 2$ :

$$\mu = 1 + \frac{R_f}{R_g} = 2 \implies R_f = R_g$$

Choose  $R_g = 10$  kohm, then  $R_f = 10$  kohm

**Final Design:** - Input RC low-pass:  $R = 100$  ohm,  $C = 0.1$  microF - Non-inverting op-amp:  $R_f = R_g = 10$  kohm

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### EXAMPLE 4.2: Parallel Summing Design (HW08-P3c)

**Problem:** Implement  $H(s) = 10.1 \left( \frac{1000}{s+1000} - \frac{10}{s+10} \right)$  using parallel summing.

**Solution:**

**Step 1:** Recognize as difference of two first-order sections

$$H(s) = K_1 \cdot \frac{\alpha_1}{s + \alpha_1} - K_2 \cdot \frac{\alpha_2}{s + \alpha_2}$$

where  $K_1 = 10100$ ,  $\alpha_1 = 1000$ ,  $K_2 = 101$ ,  $\alpha_2 = 10$

**Step 2:** Design first branch ( $\alpha_1 = 1000$ )

RC section: Choose  $C_{11} = 0.1 \text{ microF}$

$$R_{11} = \frac{1}{1000 \times 0.1 \times 10^{-6}} = 10 \text{ kohm}$$

Gain: Need 10100 Use inverting:  $\frac{R_f}{R_{in}} = 10100$  (impractical - use cascade instead)

**Step 3:** Design second branch ( $\alpha_2 = 10$ )

RC section: Choose  $C_{21} = 1 \text{ microF}$

$$R_{21} = \frac{1}{10 \times 1 \times 10^{-6}} = 100 \text{ kohm}$$

**Step 4:** Use summing amplifier to combine with subtraction

The summing stage inverts, so design first stages as inverting to get correct signs.

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### EXAMPLE 4.3: Integrator and Differentiator (HW08-P4)

**Problem:** Find  $H(s)$  for op-amp integrator and explain name.

**Solution:**

**Circuit:** Inverting op-amp with R in input, C in feedback

$$H(s) = -\frac{Z_f}{Z_{in}} = -\frac{1/(sC)}{R} = -\frac{1}{sRC}$$

**Time domain relationship:**

$$V_{out}(s) = -\frac{1}{sRC} V_{in}(s)$$

$$sV_{out}(s) = -\frac{1}{RC} V_{in}(s)$$

$$\frac{dv_{out}}{dt} = -\frac{1}{RC} v_{in}(t)$$

$$v_{out}(t) = -\frac{1}{RC} \int v_{in}(t) dt$$

**This is an integrator!**

**Differentiator:** Swap R and C

$$H(s) = -\frac{R}{1/(sC)} = -sRC$$

This gives:  $v_{out}(t) = -RC \frac{dv_{in}}{dt}$

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## SECTION 5: BUTTERWORTH FILTER DESIGN

### EXAMPLE 5.1: Complete 4th-Order Low-Pass (Class 27)

**Problem:** Design Butterworth low-pass filter: -  $H_{max} = 0 \text{ dB}$  (gain = 1.0) -  $H_{min} = -40 \text{ dB}$  (gain = 0.01)  
-  $f_c = 2 \text{ kHz}$  -  $f_{min} = 8 \text{ kHz}$

**Solution:**

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## PHASE 1: Calculate Required Order

**Step 1:** Convert to linear and rad/s - Hmax = 1.0 (already linear) - Hmin = 0.01 (already linear) -  $\omega_C = 2\pi \times 2000 = 12566$  rad/s -  $\omega_{MIN} = 2\pi \times 8000 = 50265$  rad/s

**Step 2:** Apply Butterworth order formula (low-pass)

$$n \geq \frac{\ln[(H_{max}/H_{min})^2 - 1]}{2 \ln(\omega_{min}/\omega_C)}$$

$$n \geq \frac{\ln[(1/0.01)^2 - 1]}{2 \ln(50265/12566)} = \frac{\ln(10000 - 1)}{2 \ln(4)}$$

$$n \geq \frac{\ln(9999)}{2 \ln(4)} = \frac{9.210}{2.773} = 3.32$$

**Round UP: n = 4**

**Step 3:** Section breakdown n = 4 (even) → 2 second-order sections, 0 first-order sections

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## PHASE 2: Calculate Butterworth Poles

**Step 4:** Pole angles for n = 4

$$\theta_k = \frac{\pi}{2} + \frac{(2k-1)\pi}{2n} = \frac{\pi}{2} + \frac{(2k-1)\pi}{8}$$

For k = 1, 2, 3, 4: -  $\theta_1 = \pi/2 + \pi/8 = 5\pi/8 = 112.5$  degrees -  $\theta_2 = \pi/2 + 3\pi/8 = 7\pi/8 = 157.5$  degrees -  $\theta_3 = \pi/2 + 5\pi/8 = 9\pi/8 = 202.5$  degrees -  $\theta_4 = \pi/2 + 7\pi/8 = 11\pi/8 = 247.5$  degrees

**Step 5:** Pole locations (normalized, |p| = 1) -  $p_1 = \cos(112.5^\circ) + j \sin(112.5^\circ) = -0.383 + j0.924$  -  $p_2 = \cos(157.5^\circ) + j \sin(157.5^\circ) = -0.924 + j0.383$  -  $p_3 = \cos(202.5^\circ) + j \sin(202.5^\circ) = -0.924 - j0.383$  -  $p_4 = \cos(247.5^\circ) + j \sin(247.5^\circ) = -0.383 - j0.924$

**Use only left-half-plane poles (all have negative real parts)**

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## PHASE 3: Extract Section Parameters

**Section 1:** Pair  $p_1$  and  $p_4$  (conjugates)

$$(s - p_1)(s - p_4^*) = s^2 - (p_1 + p_4)s + p_1 \cdot p_4$$

$$= s^2 - 2(-0.383)s + (0.383^2 + 0.924^2)$$

$$= s^2 + 0.765s + 1$$

Extract parameters: - Coefficient a = 0.765 - Damping ratio:  $\zeta_1 = a/2 = 0.383$  - Quality factor:  $Q_1 = 1/(2 \times 0.383) = 1.307$

**Section 2:** Pair  $p_2$  and  $p_3$  (conjugates)

$$s^2 + 1.848s + 1$$

- Coefficient a = 1.848
  - Damping ratio:  $\zeta_2 = 0.924$
  - Quality factor:  $Q_2 = 0.541$
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## PHASE 4: Design Using Unity Gain Method

**Section 1:**  $\zeta = 0.383$ ,  $\omega_0 = 12566$  rad/s

Choose  $C_1 = 0.1$  microF:

$$C_2 = 4\zeta^2 C_1 = 4(0.383)^2(0.1 \text{ microF}) = 0.0586 \text{ microF}$$

Use standard value: **C2 = 0.056 microF** or **0.068 microF**

$$R_1 = R_2 = \frac{1}{\zeta \omega_0 C_1} = \frac{1}{0.383 \times 12566 \times 0.1 \times 10^{-6}}$$

$$= 2078 \text{ ohm} \approx 2.2 \text{ kohm}$$

**Section 2:**  $\zeta = 0.924$ ,  $\omega_0 = 12566 \text{ rad/s}$

Choose  $C_1 = 0.1 \text{ microF}$ :

$$C_2 = 4(0.924)^2(0.1) = 0.341 \text{ microF}$$

Use standard value: **C2 = 0.33 microF**

$$R_1 = R_2 = \frac{1}{0.924 \times 12566 \times 0.1 \times 10^{-6}} = 861 \text{ ohm}$$

Use standard value: **R1 = R2 = 820 ohm**

## PHASE 5: Cascade Assembly

**Order by Q (LOW to HIGH):**

1. **First stage:** Section 2 ( $Q = 0.541$ , lower)
  - $R_1 = R_2 = 820 \text{ ohm}$
  - $C_1 = 0.1 \text{ microF}$ ,  $C_2 = 0.33 \text{ microF}$
  - Op-amp as buffer ( $\mu = 1$ )
2. **Second stage:** Section 1 ( $Q = 1.307$ , higher)
  - $R_1 = R_2 = 2.2 \text{ kohm}$
  - $C_1 = 0.1 \text{ microF}$ ,  $C_2 = 0.056 \text{ microF}$
  - Op-amp as buffer ( $\mu = 1$ )

**Total H(s):**

$$H_{total}(s) = H_1(s) \times H_2(s)$$

## EXAMPLE 5.2: 3rd-Order Butterworth (Odd Order)

**Problem:** Design 3rd-order Butterworth low-pass with  $f_c = 1 \text{ kHz}$ .

**Solution:**

**Step 1:** Section count  $n = 3$  (odd)  $\rightarrow$  1 first-order + 1 second-order section

**Step 2:** Pole angles

$$\theta_k = \frac{\pi}{2} + \frac{(2k-1)\pi}{6}$$

For  $k = 1, 2, 3$ : -  $\theta_1 = \pi/2 + \pi/6 = 2\pi/3 = 120^\circ \rightarrow p_1 = -0.5 + j0.866$  -  $\theta_2 = \pi/2 + 3\pi/6 = \pi = 180^\circ \rightarrow p_2 = -1$  (REAL pole) -  $\theta_3 = \pi/2 + 5\pi/6 = 4\pi/3 = 240^\circ \rightarrow p_3 = -0.5 - j0.866$

**Step 3:** Second-order section ( $p_1, p_3$ )

$$s^2 + s + 1$$

- $\zeta = 0.5$
- $\omega_0 = 2\pi \times 1000 = 6283 \text{ rad/s}$

**Unity Gain Design:**

Choose  $C_1 = 0.1 \text{ microF}$ :

$$C_2 = 4(0.5)^2(0.1) = 0.1 \text{ microF}$$

$$R_1 = R_2 = \frac{1}{0.5 \times 6283 \times 0.1 \times 10^{-6}} = 3183 \text{ ohm}$$

Use: **R1 = R2 = 3.3 kohm**



**Step 4:** First-order section (p2 at s = -omega\_c)

$$H_{1st}(s) = \frac{1}{1 + s/\omega_c}$$

Passive RC: Choose C = 0.1 microF:

$$R = \frac{1}{6283 \times 0.1 \times 10^{-6}} = 1592 \text{ ohm}$$

Use: **R = 1.6 kohm**

**Step 5:** Cascade order **First-order first, then second-order** (buffer between stages)

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### EXAMPLE 5.3: High-Pass 2nd-Order Butterworth (Class 28)

**Problem:** Design 2nd-order high-pass: - fc = 20 kHz - High-frequency gain = 0 dB - Corner gain = -3 dB (Butterworth characteristic)

**Solution:**

**Step 1:** Recognize standard 2nd-order Butterworth - n = 2 → zeta = 0.707 - omega\_0 = 2pi × 20000 = 125664 rad/s

**Step 2:** Unity Gain Method for HIGH-PASS

**Key difference:** Swap R and C positions from low-pass

Choose R2 = 10 kohm:

$$R_1 = 4\zeta^2 R_2 = 4(0.707)^2(10 \text{ kohm}) = 20 \text{ kohm}$$

$$C_1 = C_2 = C = \frac{1}{\zeta\omega_0 R_2}$$

$$= \frac{1}{0.707 \times 125664 \times 10000} = 1.13 \times 10^{-9} \text{ F}$$

Use: **C1 = C2 = 1.2 nF or 1.0 nF**

**Step 3:** Circuit topology Sallen-Key high-pass: - Capacitors in series with input path - Resistors to ground - Op-amp as buffer

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### EXAMPLE 5.4: High-Pass Order Calculation (Class 28 Example)

**Problem:** Design high-pass Butterworth: - Hmax = 20 dB (gain = 10) - Hmin = -40 dB (gain = 0.01) - fc = 10 kHz - fmin = 1 kHz (note: fmin < fc for high-pass!)

**Solution:**

**Step 1:** Apply HIGH-PASS order formula (note reversed frequencies!)

$$n \geq \frac{\ln[(H_{max}/H_{min})^2 - 1]}{2 \ln(\omega_C/\omega_{min})}$$

Notice: omega\_C in numerator for high-pass (opposite of low-pass)

$$\begin{aligned} n &\geq \frac{\ln[(10/0.01)^2 - 1]}{2 \ln(62832/6283)} = \frac{\ln(999999)}{2 \ln(10)} \\ &= \frac{13.816}{4.605} = 3.0 \end{aligned}$$

**Exactly n = 3** (no need to round up)

**Step 2:** Section breakdown n = 3 → 1 first-order + 1 second-order

**Then proceed with pole calculations and design as before...**

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## SECTION 6: EQUAL ELEMENTS METHOD

### EXAMPLE 6.1: When to Use Equal Elements vs Unity Gain

**Problem:** Design 2nd-order section with: -  $\omega_0 = 1000 \text{ rad/s}$  -  $\zeta = 0.5$

Can we use equal elements method?

**Solution:**

**Equal Elements Constraint:** For equal elements method ( $R_1 = R_2 = R$ ,  $C_1 = C_2 = C$ ):

$$\mu = 3 - 2\zeta$$

For  $\zeta = 0.5$ :

$$\mu = 3 - 2(0.5) = 2$$

**This is valid!** ( $\mu \geq 1$  and  $\zeta < 1$ )

**Equal Elements Design:**

Choose  $C = 0.1 \text{ microF}$ :

$$R = \frac{1}{\zeta\omega_0 C} = \frac{1}{0.5 \times 1000 \times 0.1 \times 10^{-6}} = 20 \text{ kohm}$$

Gain stage: Need  $\mu = 2$

$$\mu = 1 + \frac{R_f}{R_g} = 2 \implies R_f = R_g$$

Choose  $R_g = 10 \text{ kohm}$ , then  $R_f = 10 \text{ kohm}$

**Unity Gain Alternative:**

Choose  $C_1 = 0.1 \text{ microF}$ :

$$C_2 = 4\zeta^2 C_1 = 4(0.5)^2(0.1) = 0.1 \text{ microF}$$

$$R_1 = R_2 = \frac{1}{\zeta\omega_0 C_1} = 20 \text{ kohm}$$

**Both methods work! Equal elements is simpler here.**

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### EXAMPLE 6.2: When Unity Gain is Required

**Problem:** Design 2nd-order section with: -  $\omega_0 = 1000 \text{ rad/s}$  -  $\zeta = 1.5$  (overdamped)

**Solution:**

**Check Equal Elements:**

$$\mu = 3 - 2(1.5) = 0$$

**This fails!** ( $\mu$  must be  $\geq 1$ )

**Must use Unity Gain Method:**

Choose  $C_1 = 0.1 \text{ microF}$ :

$$C_2 = 4\zeta^2 C_1 = 4(1.5)^2(0.1) = 0.9 \text{ microF}$$

$$R_1 = R_2 = \frac{1}{\zeta\omega_0 C_1} = \frac{1}{1.5 \times 1000 \times 0.1 \times 10^{-6}}$$

$$= 6667 \text{ ohm} \approx 6.8 \text{ kohm}$$

**Key Rule:** - Equal elements: ONLY for  $0 < \zeta < 1$  (underdamped) - Unity gain: Works for ALL  $\zeta$  values (including overdamped)

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## SECTION 7: STATE-VARIABLE FILTER (HW08-P5)

### EXAMPLE 7.1: Understanding State-Variable Filter

**Problem:** For the state-variable filter in HW08-P5, derive  $H(s) = V_2(s)/V_1(s)$ .

**Solution:**

**Step 1:** Recognize cascaded integrators

The two right-side op-amps are integrators:

$$V_4(s) = -\frac{1}{sRC}V_2(s)$$

$$V_3(s) = -\frac{1}{sRC}V_4(s) = \frac{1}{(sRC)^2}V_2(s) = s^2(RC)^2V_2(s)$$

**Step 2:** Analyze leftmost op-amp

Non-inverting input (V+): Voltage divider from V1 and V2 feedback

$$V_+(s) = \frac{-sRCR_1V_2(s) + R_2V_1(s)}{R_1 + R_2}$$

Inverting input (V-): Voltage divider from V3 and ground

$$V_-(s) = \frac{s^2(RC)^2R_4V_2(s)}{R_3 + R_4}$$

**Step 3:** Apply ideal op-amp property ( $V_+ = V_-$ )

$$\frac{-sRCR_1V_2(s) + R_2V_1(s)}{R_1 + R_2} = \frac{s^2(RC)^2R_4V_2(s)}{R_3 + R_4}$$

**Step 4:** With  $R_4 = R_3$ , solve for  $H(s)$

After algebraic manipulation:

$$H(s) = \frac{V_2(s)}{V_1(s)} = \frac{\frac{R_2(R_3+R_4)}{(R_1+R_2)R_3}}{s^2(RC)^2\frac{R_4}{R_3} + sRC\frac{R_1(R_3+R_4)}{(R_1+R_2)R_3} + 1}$$

With  $R_4 = R_3$ :

$$H(s) = \frac{K}{\left(\frac{s}{\omega_0}\right)^2 + 2\zeta\left(\frac{s}{\omega_0}\right) + 1}$$

where:  $\omega_0 = \frac{1}{RC}$  -  $2\zeta = 2\frac{R_1}{R_1+R_2}$  -  $K = \frac{R_2(2R_3)}{(R_1+R_2)R_3} = \frac{2R_2}{R_1+R_2}$

**Key Advantage:** Can tune  $\omega_0$  and  $\zeta$  independently!

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## SECTION 8: COMMON MISTAKES TO AVOID

### MISTAKE 1: Wrong Butterworth Order Formula

**WRONG (Low-Pass):**

$$n \geq \frac{\ln[(H_{max}/H_{min})^2 - 1]}{2\ln(\omega_{min}/\omega_C)}$$

with  $\omega_{min} < \omega_C$  (INCORRECT!)

**CORRECT (Low-Pass):**

$$n \geq \frac{\ln[(H_{max}/H_{min})^2 - 1]}{2\ln(\omega_{min}/\omega_C)}$$

with  $\omega_{min} > \omega_C$  (frequency beyond passband)

**CORRECT (High-Pass):**

$$n \geq \frac{\ln[(H_{max}/H_{min})^2 - 1]}{2 \ln(\omega_C/\omega_{min})}$$

with  $\omega_{MIN} < \omega_C$  (frequency below passband)

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### **MISTAKE 2: Forgetting to Scale Poles**

**Problem:** 4th-order Butterworth with  $f_c = 2$  kHz

**WRONG:** Use normalized poles directly in  $H(s)$

**CORRECT:** Scale ALL poles by  $\omega_c$  - Normalized:  $p1 = -0.383 + j0.924$  - Scaled:  $p1 = \omega_c(-0.383 + j0.924) = 12566(-0.383 + j0.924)$

---

### **MISTAKE 3: Wrong Cascade Order**

**WRONG:** Place high-Q section first

**CORRECT:** Always cascade LOW Q to HIGH Q - Prevents overload of high-Q section - Better overall performance

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### **MISTAKE 4: Confusing zeta and Q**

**Relationship:**

$$Q = \frac{1}{2\zeta}$$

**Example:** - If  $\zeta = 0.5$ , then  $Q = 1.0$  (NOT 0.5!) - If  $Q = 1.307$ , then  $\zeta = 0.383$  (NOT 1.307!)

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### **MISTAKE 5: Using Equal Elements When $\zeta \geq 1$**

**Example:**  $\zeta = 1.2$  (overdamped)

**WRONG:** Try equal elements method

$$\mu = 3 - 2(1.2) = 0.6$$

(less than 1, INVALID!)

**CORRECT:** Must use unity gain method

**Rule:** Equal elements ONLY for  $0 < \zeta < 1$

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## **SECTION 9: QUICK FORMULAS REFERENCE**

### **First-Order Sections**

**Low-Pass:**

$$H(s) = K \frac{\alpha}{s + \alpha}$$

- DC gain: K - Cutoff:  $\alpha$  rad/s - Slope: -20 dB/decade

**High-Pass:**

$$H(s) = K \frac{s}{s + \alpha}$$

- High-frequency gain: K - Cutoff:  $\alpha$  rad/s - Slope: +20 dB/decade

### **Second-Order Sections**

**Standard Form:**

$$H(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$

**Key Parameters:** - Resonant frequency:  $\omega_0$  rad/s - Damping ratio:  $\zeta$  - Quality factor:  $Q = 1/(2\zeta)$  - *Bandwidth (low-pass):*  $B = 2\zeta\omega_0$  - *Peak gain (underdamped):*  $K/(2\zeta)$  at  $\omega_0$

## Butterworth Pole Angles

**Formula:**

$$\theta_k = \frac{\pi}{2} + \frac{(2k-1)\pi}{2n}$$

for  $k = 1, 2, \dots, n$

**Common Values:** -  $n=2$ :  $135^\circ, 225^\circ \rightarrow$  conjugate pair -  $n=3$ :  $120^\circ, 180^\circ, 240^\circ \rightarrow$  one real, one conjugate pair -  $n=4$ :  $112.5^\circ, 157.5^\circ, 202.5^\circ, 247.5^\circ \rightarrow$  two conjugate pairs

## Sallen-Key Design Formulas

**Equal Elements ( $R_1=R_2=R$ ,  $C_1=C_2=C$ ):** - Constraint:  $\mu = 3 - 2\zeta$  (*only valid for  $0 < \zeta < 1$* ) -  $R = 1/(\zeta \omega_0 * C)$

**Unity Gain ( $\mu=1$ ,  $R_1=R_2$ ):** -  $C_2 = 4\zeta^2 C_1$  -  $R_1 = R_2 = 1/(\zeta * \omega_0 * C_1)$  - Works for ALL  $\zeta$  values

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## SECTION 10: FINAL CHECKLIST

### Before Submitting Your Answer:

**Transfer Functions:** - ☐ Correct form (low-pass vs high-pass)? - ☐ Units correct (rad/s)? - ☐ Gain at appropriate frequency correct? - ☐ Poles in left-half plane?

**Butterworth Design:** - ☐ Used correct order formula (low-pass vs high-pass)? - ☐ Rounded order UP to integer? - ☐ Calculated poles at correct angles? - ☐ Scaled poles by  $\omega_c$ ? - ☐ Paired conjugate poles correctly? - ☐ Cascaded sections in correct order (low Q to high Q)?

**Circuit Design:** - ☐ Component values realistic (10 ohm to 1 Mohm, 1 pF to 1000 microF)? - ☐ Used standard values when required? - ☐ Correct op-amp configuration (inverting/non-inverting)? - ☐ All grounds and connections shown? - ☐ Gain stages correct?

**Frequency Response:** - ☐ Magnitude units (linear or dB)? - ☐ Phase units (degrees or radians)? - ☐ Correct asymptotic behavior ( $\omega \rightarrow 0$  and  $\omega \rightarrow \infty$ )? - ☐ Corner frequencies correct?

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## APPENDIX: STANDARD COMPONENT VALUES

### Standard Resistor Values (E12 series):

10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 (and multiples)

### Standard Capacitor Values:

**pF range:** 10, 22, 47, 100, 220, 470 **nF range:** 1.0, 2.2, 4.7, 10, 22, 47, 100, 220, 470 **microF range:** 0.1, 0.22, 0.47, 1.0, 2.2, 4.7, 10, 22, 47, 100

### Typical Choices for Design:

- **R:** 1k, 2.2k, 4.7k, 10k, 22k, 47k, 100k
  - **C:** 0.01 microF, 0.1 microF, 1.0 microF, 10 microF
- 

## END OF WORKED EXAMPLES

*Good luck on your quiz! Remember to: 1. Read problems carefully 2. Show your work 3. Check units 4. Verify reasonableness of answers*