

Time and frequency characterization of signals and systems (ch.6)

- ❑ The magnitude-phase representation of Fourier Transform
- ❑ The magnitude-phase representation of the frequency response of LTI systems
- ❑ Time-domain properties of ideal frequency-selective filters
- ❑ Time-domain and frequency-domain aspects of non-ideal filters
- ❑ First- and second-order system

The magnitude-phase representation of FT



Magnitude and phase spectrum

- ❑ Continuous FT $x(t) \xleftrightarrow{\mathcal{F}} X(j\omega) \quad X(j\omega) = |X(j\omega)|e^{j\angle X(j\omega)}$
- ❑ Discrete FT $x[n] \longleftrightarrow X(e^{j\omega}) \quad X(e^{j\omega}) = |X(e^{j\omega})|e^{j\angle X(e^{j\omega})}$
- ❑ Amplitude spectrum: $|X(j\omega)|$ and $|X(e^{j\omega})|$
- ❑ Phase spectrum (angle): $\angle X(j\omega)$ and $\angle X(e^{j\omega})$

The magnitude-phase representation of FT

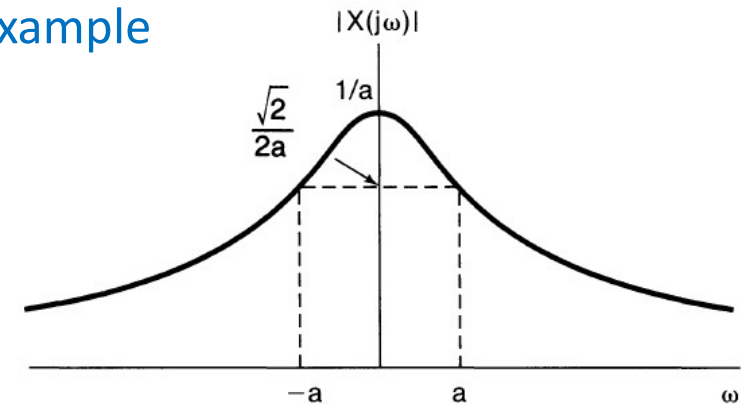


Magnitude spectrum

Continuous time as an example

$$\text{IFT: } x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(j\omega) e^{j\omega t} d\omega$$

- ❑ IFT: decomposition of the signal $x(t)$ into a "sum" of complex exponentials at different frequencies
- ❑ $|X(e^{j\omega})|$: describes the basic frequency content of a signal, and the relative magnitude of the each frequency (complex exponential)
- ❑ $|X(j\omega)|^2$: energy-density spectrum of $x(t)$
- ❑ $|X(j\omega)|^2 d\omega / 2\pi$: energy in the signal between ω and $\omega + d\omega$



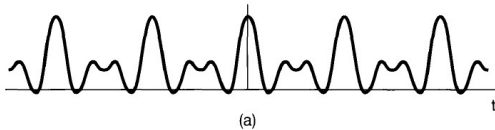
The magnitude-phase representation of FT



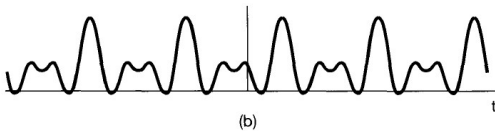
Phase spectrum

- $\angle X(j\omega)$
 - relative phase of the each complex exponential
 - significant effect on the nature of the signal
 - changes in $\angle X(j\omega)$ lead to phase distortion

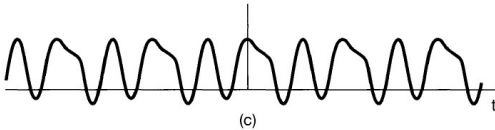
□ **Example 1:** $x(t) = 1 + \frac{1}{2}\cos(2\pi t + \varphi_1) + \frac{1}{2}\cos(4\pi t + \varphi_2) + \frac{1}{2}\cos(6\pi t + \varphi_3)$



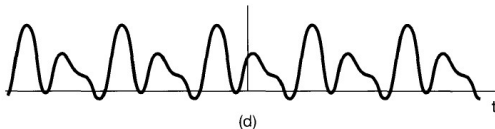
$$\varphi_1 = \varphi_2 = \varphi_3 = 0$$



$$\varphi_1 = 4\text{rad}, \varphi_2 = 8\text{rad}, \varphi_3 = 12\text{rad}$$



$$\varphi_1 = 6\text{rad}, \varphi_2 = -2.7\text{rad}, \varphi_3 = 0.93\text{rad}$$



$$\varphi_1 = 1.2\text{rad}, \varphi_2 = 4.1\text{rad}, \varphi_3 = -7.02\text{rad}$$

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The magnitude-phase representation of LTI



Gain and phase shift

□ For LTI system $x(t) \longrightarrow \boxed{h(t)} \longrightarrow y(t) = x(t) * h(t)$

$$X(j\omega) \longrightarrow \boxed{H(j\omega)} \longrightarrow Y(j\omega) = H(j\omega)X(j\omega)$$

□ The frequency response $H(j\omega) = |H(j\omega)|e^{j\angle H(j\omega)}$

□ $|H(j\omega)|$: Gain of the LTI system; $\angle H(j\omega)$: phase shift of the LTI system

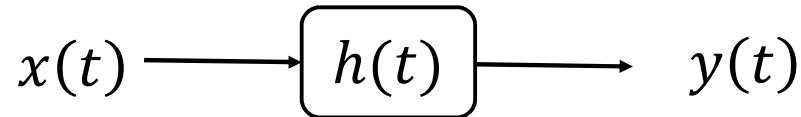
$$Y(j\omega) = H(j\omega)X(j\omega) = |H(j\omega)||X(j\omega)|e^{j(\angle H(j\omega) + \angle X(j\omega))}$$

$$|Y(j\omega)| = |H(j\omega)||X(j\omega)| \quad \angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

The magnitude-phase representation of LTI



Linear phase system



For $H(j\omega) = e^{-j\omega t_0}$

$$|H(j\omega)| = 1 \quad \angle H(j\omega) = -\omega t_0$$

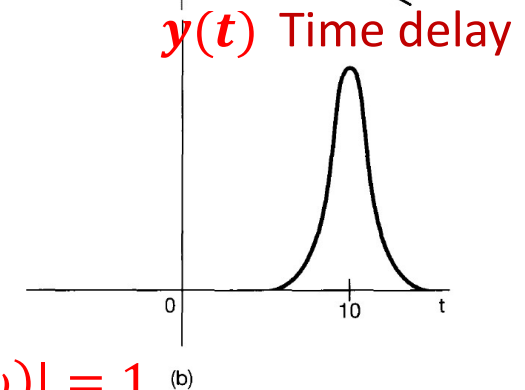
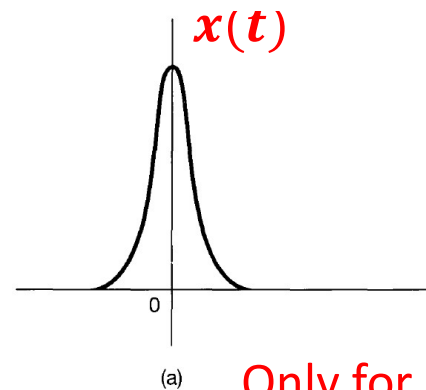
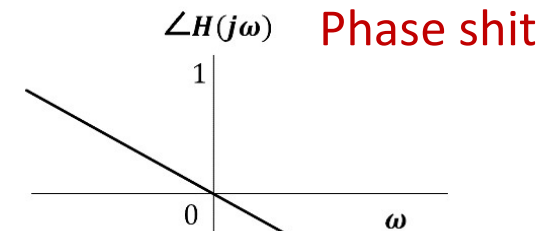
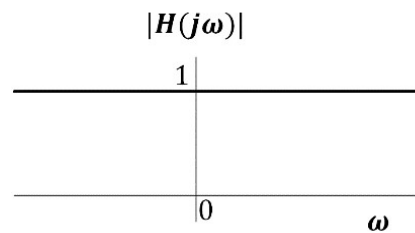
$\angle H(j\omega)$ is a linear function of ω

Output of system:

$$\begin{aligned} Y(j\omega) &= H(j\omega)X(j\omega) \\ &= X(j\omega)e^{-j\omega t_0} \end{aligned}$$

$$y(t) = x(t - t_0)$$

All-pass system



Only for $|H(j\omega)| = 1$

The magnitude-phase representation of LTI



Non-linear phase system

For $H(j\omega) = H_1(j\omega)H_2(j\omega)$

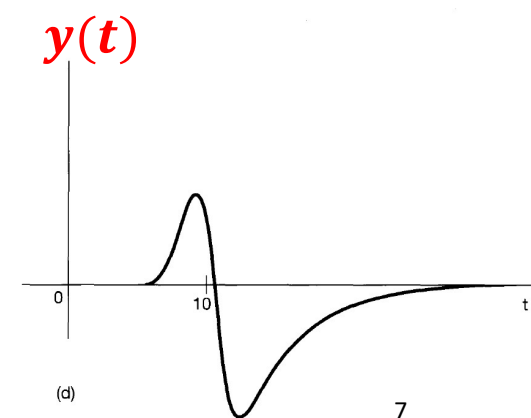
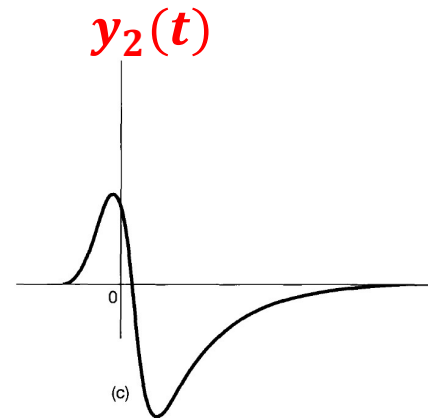
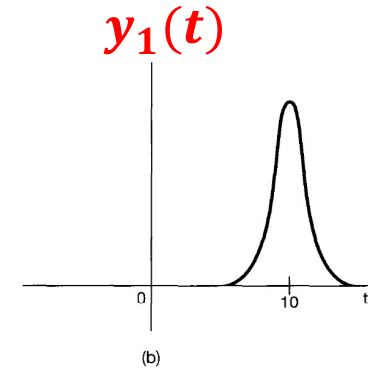
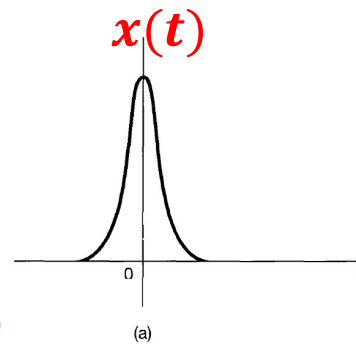
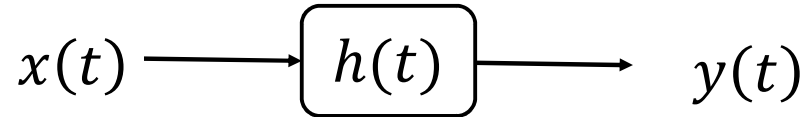
$$H_1(j\omega) = e^{-j\omega t_0}$$

$$H_2(j\omega) = e^{\angle H_2(j\omega)}$$

$\angle H_2(j\omega)$ is a nonlinear function of ω

$$|H(j\omega)| = 1$$

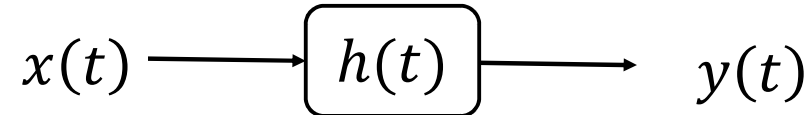
$$\angle H(j\omega) = -\omega t_0 + \angle H_2(j\omega)$$



The magnitude-phase representation of LTI



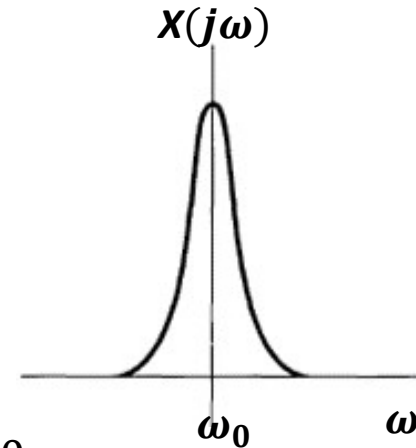
Group delay



- ❑ Consider a system with $\angle H(j\omega)$ a nonlinear function of ω
- ❑ For a narrow band input $x(t)$, $\angle H(j\omega) \simeq -\phi - \alpha\omega$

$$Y(j\omega) \simeq X(j\omega)|H(j\omega)|e^{-j\phi}e^{-j\alpha\omega}$$

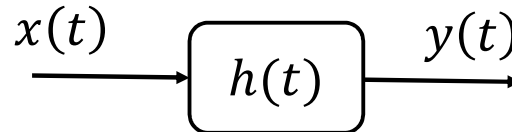
- ❑ The time delay α is referred to as the group delay at $\omega = \omega_0$



$$\tau(\omega) = -\frac{d}{d\omega}\{\angle H(j\omega)\}$$

The magnitude-phase representation of LTI

Group delay: example



□ Consider

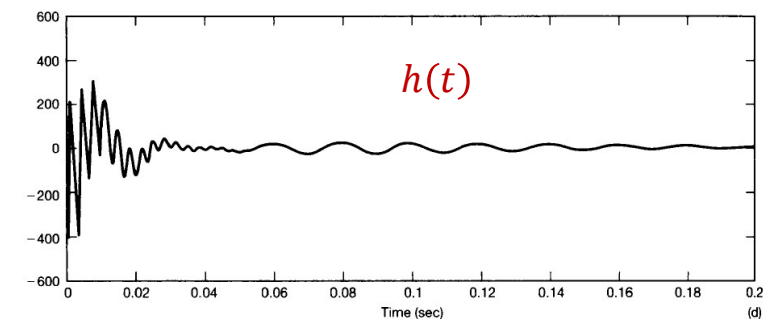
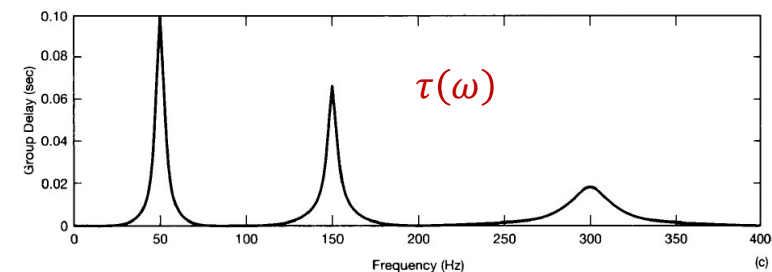
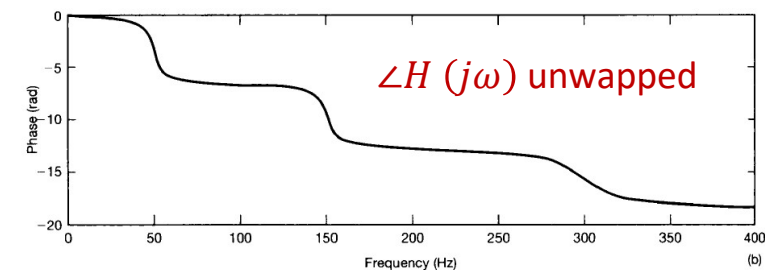
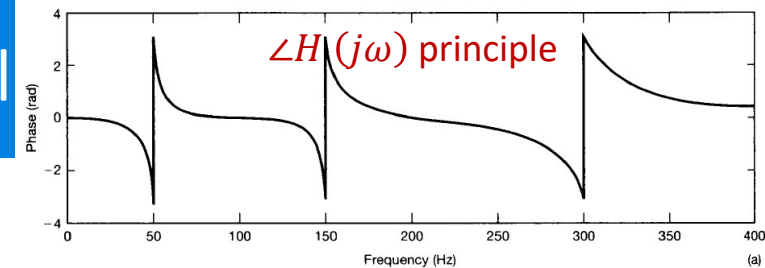
$$H(j\omega) = \prod_{i=1}^3 H_i(j\omega) \quad H_i(j\omega) = \frac{1 + (j\omega/\omega_i)^2 - 2j\zeta_i(\omega/\omega_i)}{1 + (j\omega/\omega_i)^2 + 2j\zeta_i(\omega/\omega_i)}$$

$$\begin{cases} \omega_1 = 315 \text{ rad/sec and } \zeta_1 = 0.066, \\ \omega_2 = 943 \text{ rad/sec and } \zeta_2 = 0.033, \\ \omega_3 = 1888 \text{ rad/sec and } \zeta_3 = 0.058. \end{cases}$$

$$|H_i(j\omega)| = 1 \Rightarrow |H(j\omega)| = 1$$

$$\angle H_i(j\omega) = -2\arctan \left[\frac{2\zeta_i(\omega/\omega_i)}{1 - (\omega/\omega_i)^2} \right]$$

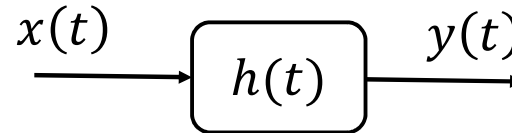
$$\angle H(j\omega) = \sum_{i=1}^3 \angle H_i(j\omega) \quad \tau(\omega) = -\frac{d}{d\omega} \{ \angle H(j\omega) \}$$





The magnitude-phase representation of LTI

Log-Magnitude and Bode Plots



Time domain:

$$y(t) = x(t) * h(t)$$

Convolution

Frequency domain:

$$Y(j\omega) = H(j\omega)X(j\omega)$$

Multiplication

$$|Y(j\omega)| = |H(j\omega)||X(j\omega)|$$

$$\angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

Logarithmic amplitude: $\log|Y(j\omega)| = \log|H(j\omega)| + \log|X(j\omega)|$

Summation

Logarithmic amplitude scale: $20 \log_{10}$, referred to as *decibels* (dB).

Bode plots: Plots of $20\log_{10}|H(j\omega)|$ and $\angle H(j\omega)$ versus $\log_{10}(\omega)$



The magnitude-phase representation of LTI

Log-Magnitude and Bode Plots

Magnitude: Plot of $20\log_{10}|H(j\omega)|$ vs. $\log_{10}(\omega)$

Phase: Plot of $\angle H(j\omega)$ vs. $\log_{10}(\omega)$

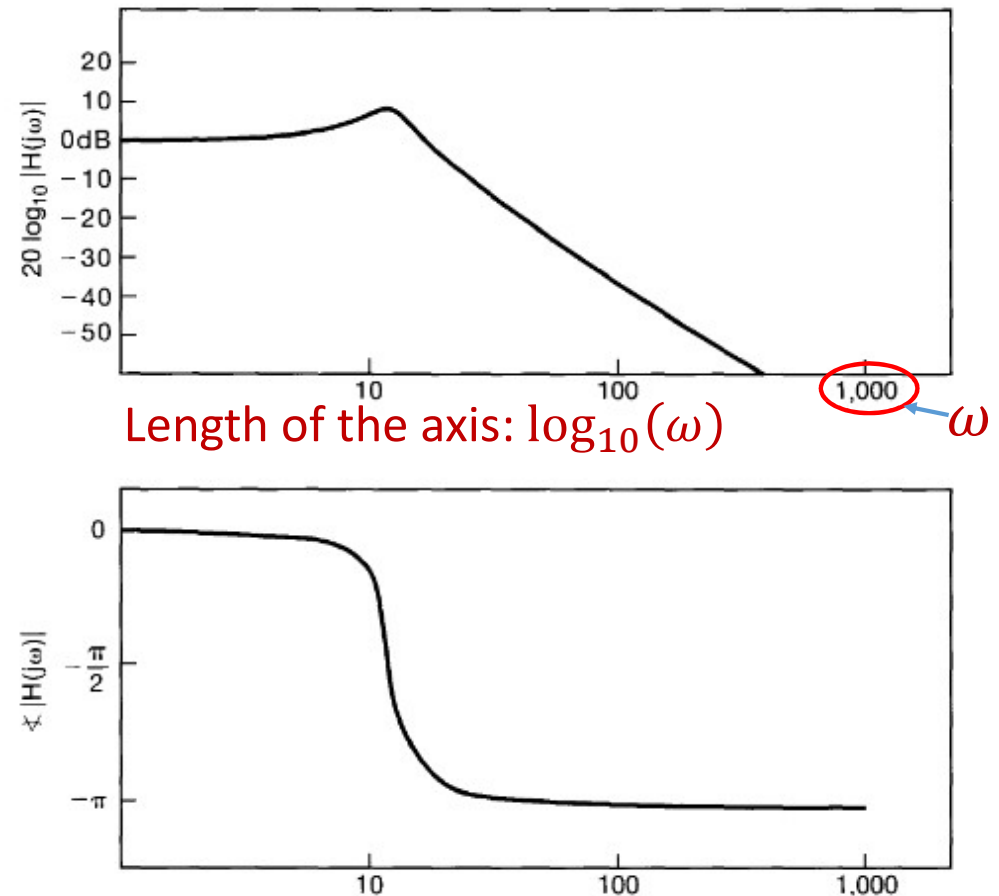


Figure 6.8 A typical Bode plot. (Note that ω is plotted using a logarithmic scale.)

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Time-domain properties of ideal frequency-selective filters



Frequency-selective filters

Low-pass filter

High-pass filter

Band-pass filter

We focus on low-pass filter, similar concepts and results for high-pass and band-pass filters.

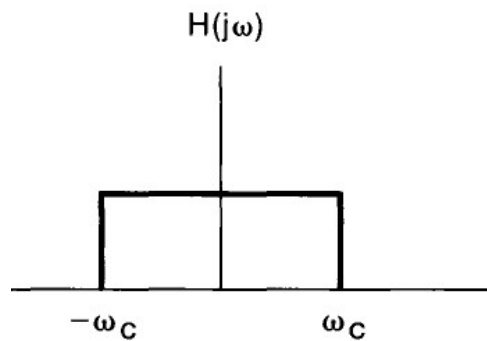
Time-domain properties of ideal frequency-selective filters



Ideal low-pass filters: zero phase

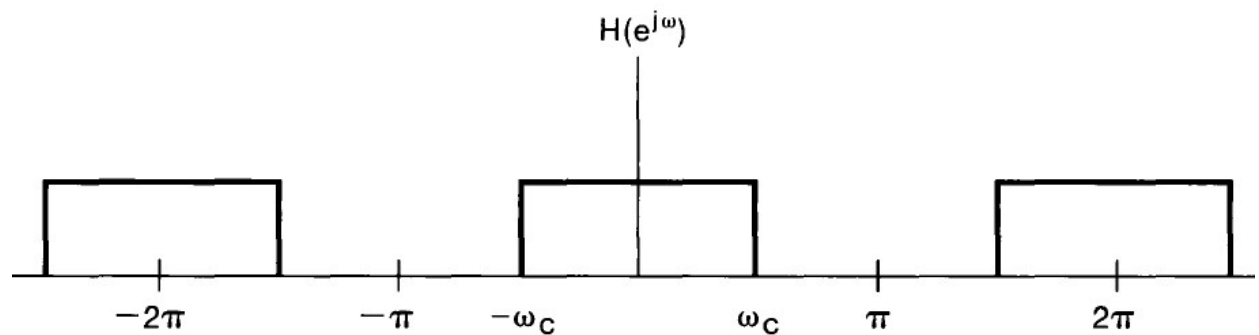
CT

$$H(j\omega) = \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & |\omega| > \omega_c \end{cases}$$



DT

$$H(e^{j\omega}) = \begin{cases} 1, & |\omega| \leq \omega_c \\ 0, & \omega_c < |\omega| < \pi \end{cases}$$



Time-domain properties of ideal frequency-selective filters



Ideal low-pass filters: zero phase

□ Impulse response:

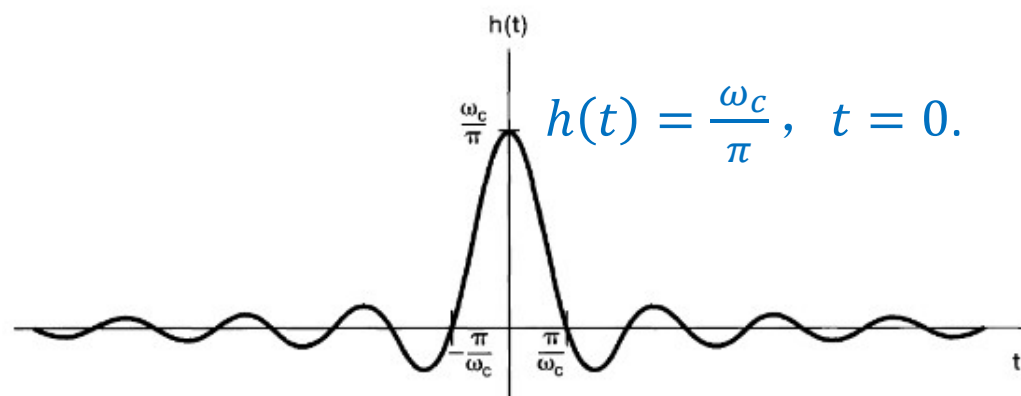
$$h(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(j\omega) e^{j\omega t} d\omega$$

$$= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} 1 \cdot e^{j\omega t} d\omega$$

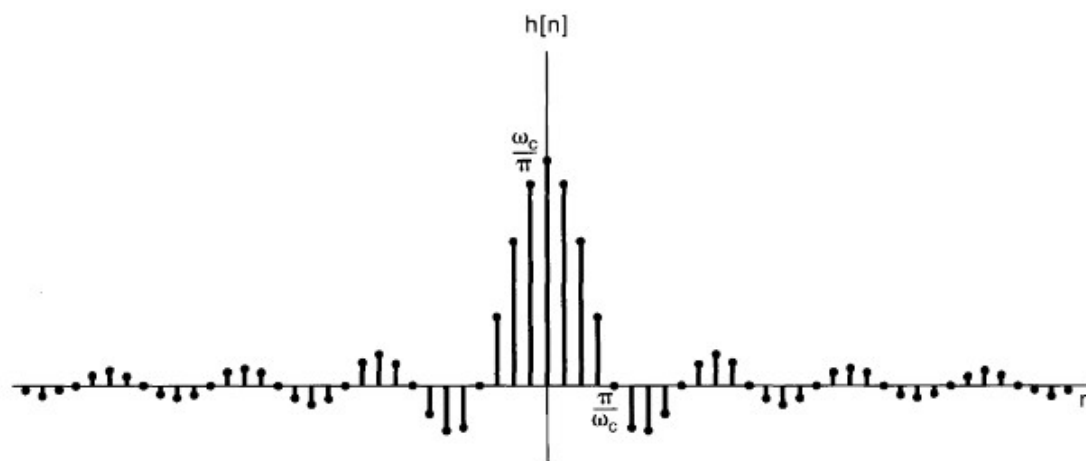
$$= \frac{1}{2\pi} \cdot \frac{1}{jt} e^{j\omega t} \Big|_{-\omega_c}^{\omega_c}$$

$$= \frac{1}{2\pi} \cdot \frac{1}{jt} \cdot 2j \sin(\omega_c t) = \frac{\sin \omega_c t}{\pi t}$$

$$h(n) = \frac{\sin \omega_c n}{\pi n}$$



$h(t) = 0, \omega_c t = k\pi, k \neq 0. \omega_c \uparrow, \text{width of } h(t) \downarrow$



Time-domain properties of ideal frequency-selective filters

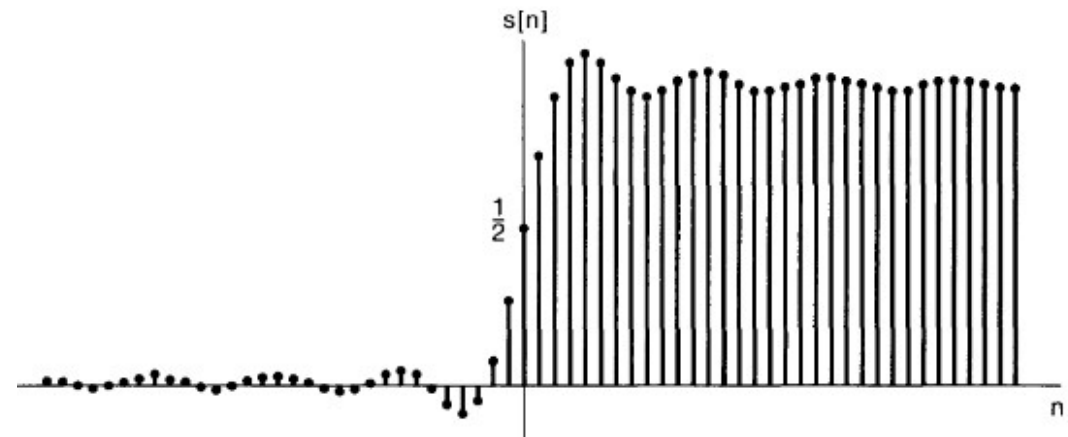
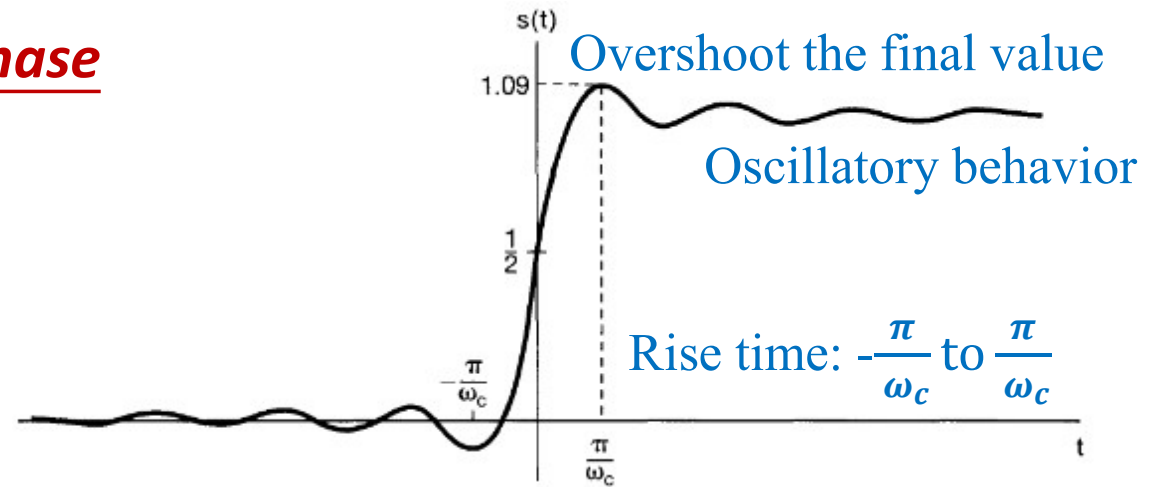


Ideal low-pass filters: zero phase

□ Step response:

$$s(t) = \int_{-\infty}^t h(\tau) d\tau$$

$$s(n) = \sum_{m=-\infty}^n h(m)$$

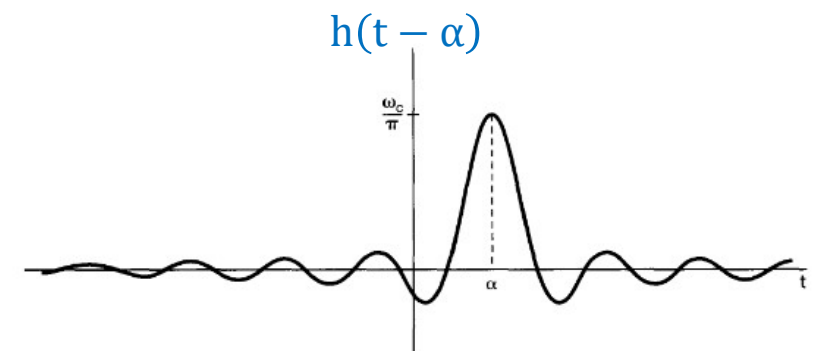
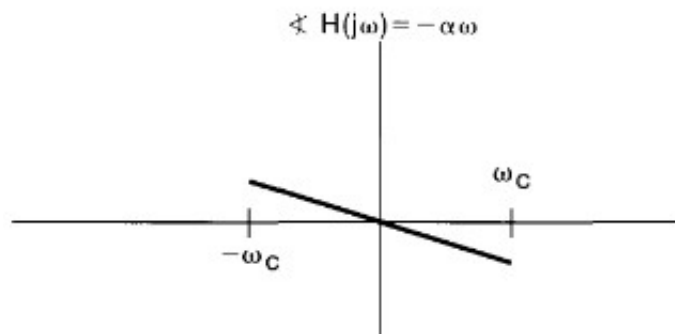
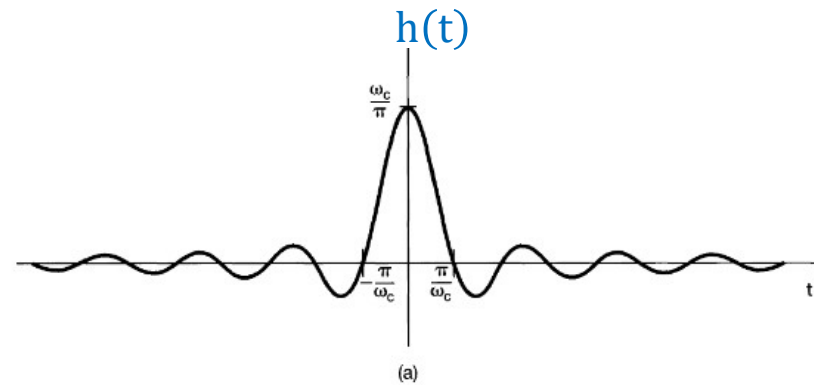
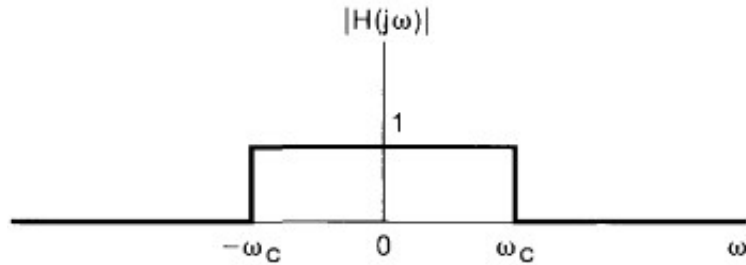


Time-domain properties of ideal frequency-selective filters



Ideal low-pass filters: linear phase

□ Impulse response:



Time and frequency characterization of signals and systems (ch.6)

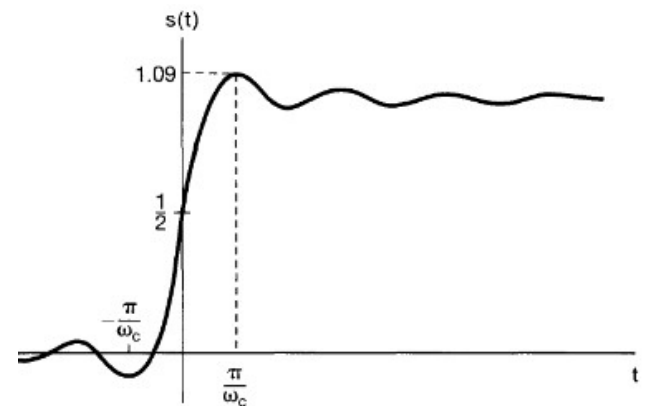
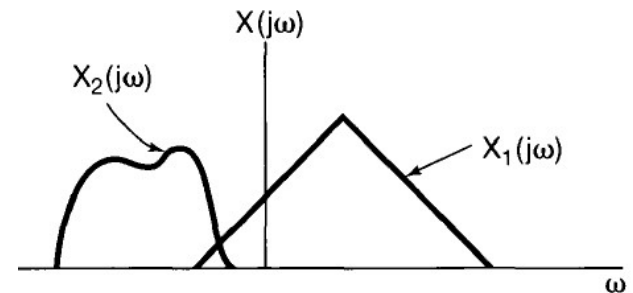
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Non-ideal filters



Why non-ideal filters

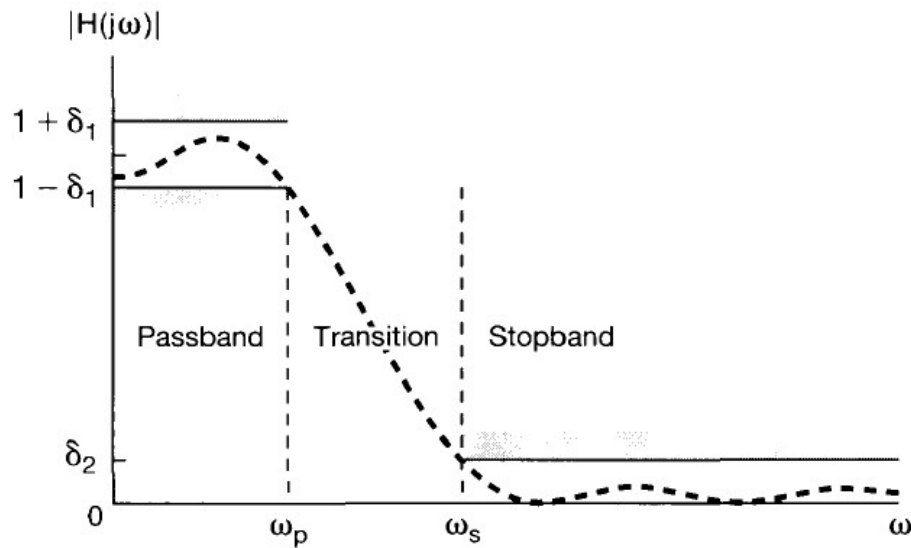
- Gradual transition band is sometimes preferable
- Ideal Low-pass filter is not attainable (not causal)
- The more precisely frequency characteristics, the more complicated or costly the implementation
 - resistors, capacitors, and operational amplifiers in continuous time
 - memory registers, multipliers, and adders in discrete time



Non-ideal filters

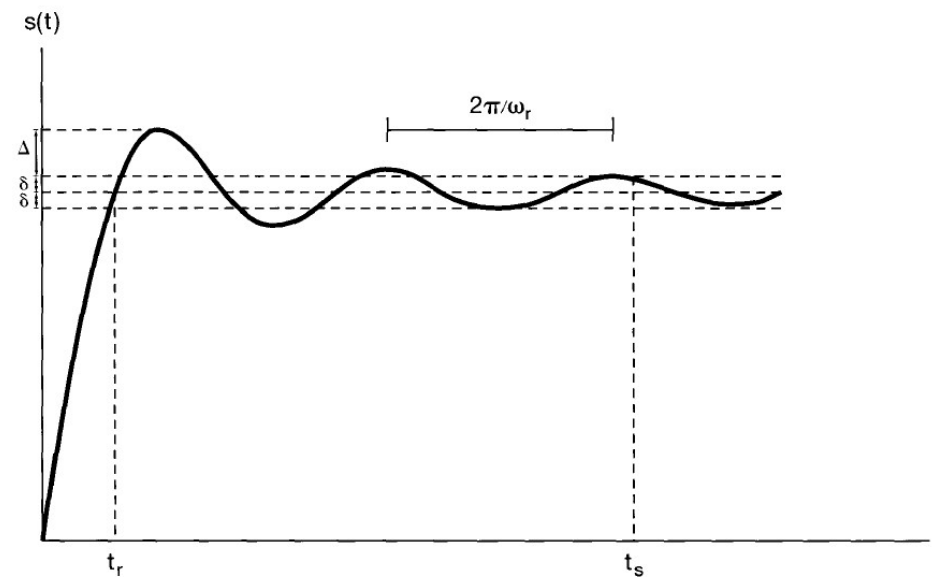


Time and frequency domain



- Pass band $0 - \omega_p$, stop band $\omega > \omega_s$, transition $\omega_s - \omega_p$
- Pass-band ripple δ_1 , stop-band ripple δ_2
- Linear (nearly) linear phase.

Step response of a CT low-pass filter

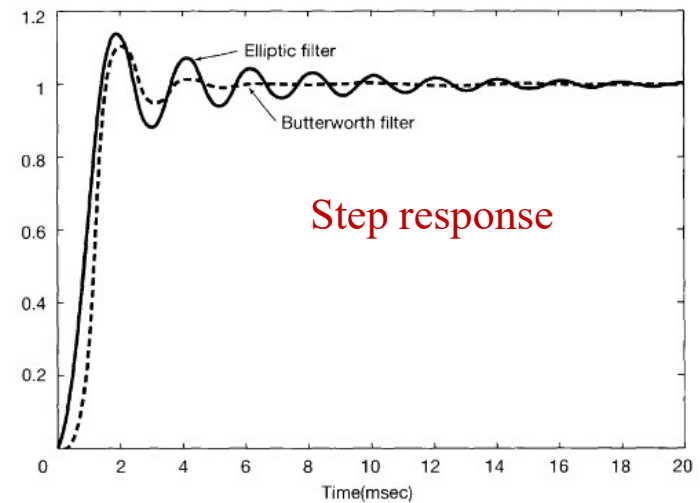
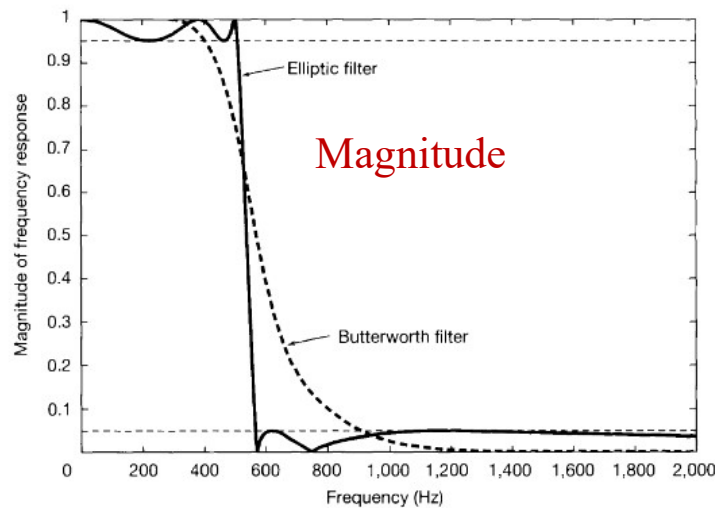


- Rise time: t_r
- Overshoot: Δ
- Ringing frequency: ω_r
- Settling time: t_s

Non-ideal filters



An example



- Fifth-order **Butterworth** filter and a fifth-order **elliptic** filter
- Same cutoff frequency
- Same passband and stopband ripple

Trade-off between time-domain (t_s) and frequency-domain ($\omega_s - \omega_p$).

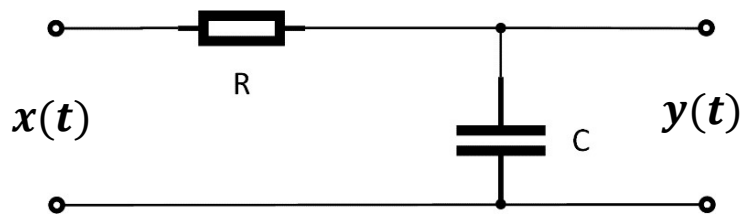
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First-order systems



First-order system (Continuous time)



□ Differential equation:

$$C \frac{dy(t)}{dt} = \frac{x(t) - y(t)}{R}$$
$$\tau \frac{dy(t)}{dt} + y(t) = x(t), \tau = RC$$

□ Frequency response:

$$\tau j\omega Y(j\omega) + Y(j\omega) = X(j\omega)$$

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{1}{j\omega\tau + 1}$$

First-order systems



First-order system (Continuous time)

□ Impulse response $H(j\omega) = \frac{1}{j\omega\tau + 1} = \frac{1/\tau}{j\omega + 1/\tau}$

$$e^{-at}u(t), a > 0 \xleftrightarrow{\mathcal{F}} \frac{1}{j\omega + a}$$

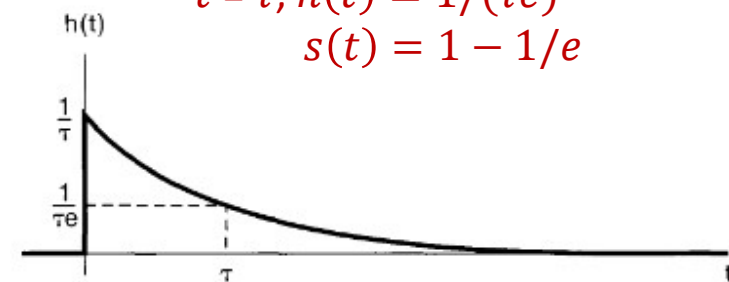
$$h(t) = \frac{1}{\tau} e^{-t/\tau} u(t)$$

□ Step response

$$s(t) = \int_{-\infty}^t h(t') dt' = \frac{1}{\tau} \int_0^t e^{-t'/\tau} dt' = \begin{cases} 0, & t < 0 \\ 1 - e^{-t/\tau}, & t \geq 0 \end{cases}$$

$$s(t) = (1 - e^{-t/\tau}) u(t)$$

- τ : time constant
- $t = \tau, h(t) = 1/(\tau e)$
 $s(t) = 1 - 1/e$



(a)

- $\tau \downarrow, h(t)$ decays more sharply
 $s(t)$ rises more sharply



(b)



First-order systems

Bold Plots (Continuous time)

$$H(j\omega) = \frac{1}{j\omega\tau + 1}$$

$$\square 20\log_{10}|H(j\omega)| = -10\log_{10}[(\omega\tau)^2 + 1]$$

$$\simeq \begin{cases} 0, & \omega \ll 1/\tau \\ -20\log_{10}(\omega) - 20\log_{10}(\tau), & \omega \gg 1/\tau \end{cases}$$

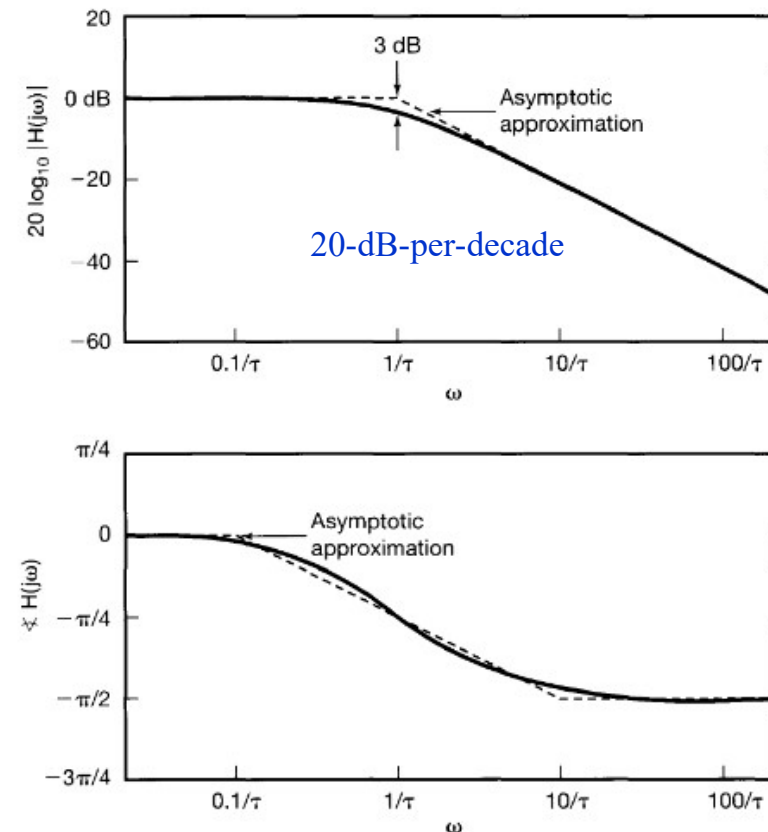
$$\omega = 1/\tau, 20\log_{10}|H(j\omega)| = -10\log_{10}(2) \simeq -3dB$$

$\omega = 1/\tau$: break frequency

$$\square \angle H(j\omega) = -\tan^{-1}(\omega\tau)$$

$$\simeq \begin{cases} 0, & \omega \leq 0.1/\tau \\ -\frac{\pi}{4} [\log_{10}(\omega\tau) + 1], & 0.1/\tau \leq \omega \leq 10/\tau \\ -\pi/2, & \omega \geq 10/\tau \end{cases}$$

$$\omega = 1/\tau, \angle H(j\omega) = -\pi/4$$



$\tau \downarrow$, $h(t)$ and $s(t)$ more sharply, break frequency \uparrow .

Second-order systems



Differential equation

$$m \frac{d^2 y(t)}{dt} = x(t) - ky(t) - b \frac{dy(t)}{dt}$$



$$\frac{d^2 y(t)}{dt} + \left(\frac{b}{m}\right) \frac{dy(t)}{dt} + \left(\frac{k}{m}\right) y(t) = \frac{1}{m} x(t)$$



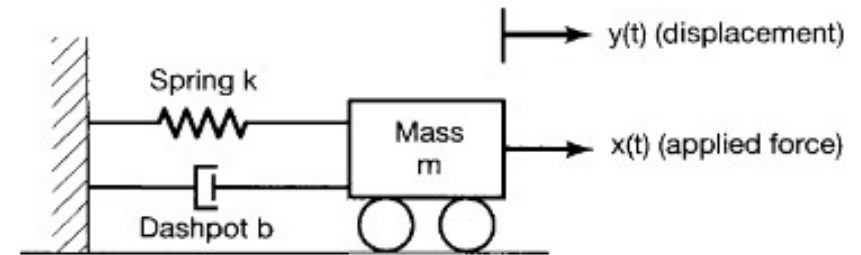
$$\omega_n^2 = \frac{k}{m}$$

$$\omega_n = \sqrt{\frac{k}{m}}$$

$$\zeta = \frac{b}{2\sqrt{km}}$$

$$2\zeta\omega_n = \frac{b}{m}$$

$$\frac{d^2 y(t)}{dt} + 2\zeta\omega_n \frac{dy(t)}{dt} + \omega_n^2 y(t) = \omega_n^2 x(t)$$





Second-order systems

□ Frequency response: $\frac{d^2 y(t)}{dt^2} + 2\zeta\omega_n \frac{dy(t)}{dt} + \omega_n^2 y(t) = \omega_n^2 x(t)$

$$(j\omega)^2 Y(j\omega) + 2\zeta\omega_n (j\omega) Y(j\omega) + \omega_n^2 Y(j\omega) = \omega_n^2 X(j\omega)$$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n (j\omega) + \omega_n^2}$$

□ Impulse response: $H(j\omega) = \frac{\omega_n^2}{(j\omega - c_1)(j\omega - c_2)} = \frac{M_1}{(j\omega - c_1)} - \frac{M_2}{(j\omega - c_2)}$

$$\zeta \neq 1$$

$$c_1, c_2: \text{roots of } (j\omega)^2 + 2\zeta\omega_n (j\omega) + \omega_n^2 = 0$$

$$c_1 = -\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}, \quad c_2 = -\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}$$

$$M_1 = M_2 = M = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \longrightarrow h(t) = M[e^{c_1 t} - e^{c_2 t}]u(t)$$



Second-order systems

□ Impulse response:

$$\zeta = 1 \quad c_1 = c_2 = -\omega_n \quad H(j\omega) = \frac{\omega_n^2}{(j\omega + \omega_n)^2}$$

Critically damped

$$te^{-at}u(t) \xrightarrow{\mathcal{F}} H(j\omega) = \frac{1}{(j\omega + a)^2} \quad \therefore h(t) = \omega_n^2 te^{-\omega_n t} u(t)$$

□ Recall $\zeta \neq 1$ $h(t) = M[e^{c_1 t} - e^{c_2 t}]u(t)$

$$0 < \zeta < 1 \quad h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} [e^{(-\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1})t} - e^{(-\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1})t}] u(t)$$

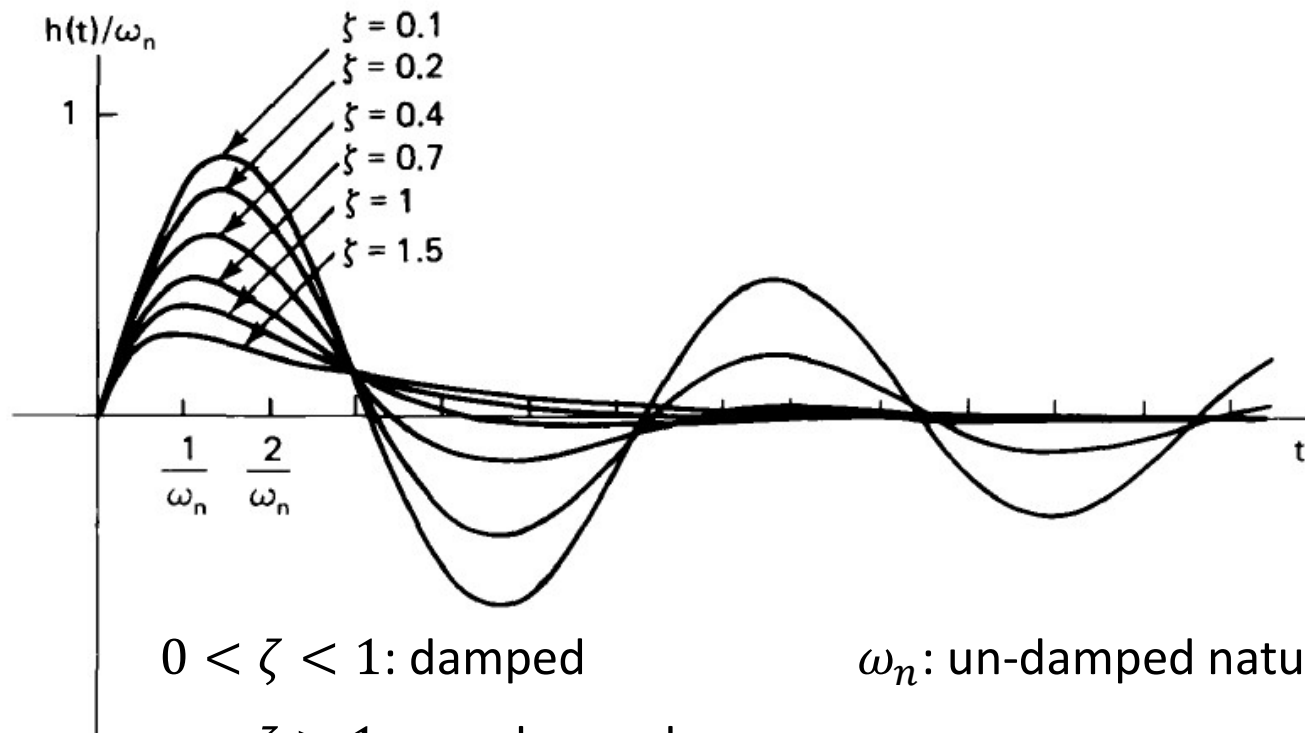
$\zeta > 1$: over damped

$$\begin{aligned} &= \frac{\omega_n e^{-\zeta\omega_n t}}{2\sqrt{\zeta^2 - 1}} [e^{j\omega_n\sqrt{1-\zeta^2}t} - e^{-j\omega_n\sqrt{1-\zeta^2}t}] u(t) \\ &= \frac{\omega_n e^{-\zeta\omega_n t}}{2\sqrt{\zeta^2 - 1}} [2j \sin(\omega_n\sqrt{1-\zeta^2}t)] u(t) = \frac{\omega_n e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} [\sin(\omega_n\sqrt{1-\zeta^2}t)] u(t) \end{aligned}$$

Second-order systems



□ Impulse response:



$0 < \zeta < 1$: damped

ω_n : un-damped natural frequency

$\zeta > 1$: overdamped

$\zeta = 1$: critically damped

ζ : damping ratio

Second-order systems



□ Step response

$\zeta \neq 1$

$$s(t) = \int_{-\infty}^t h(t') dt' = M \int_0^t e^{c_1 t'} - e^{c_2 t'} dt'$$
$$h(t) = M[e^{c_1 t} - e^{c_2 t}]u(t)$$
$$= \begin{cases} 0, t < 0 \\ M\left(\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2}\right)\Big|_0^t = 1 + M\left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2}\right], t \geq 0 \end{cases} = \left\{1 + M\left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2}\right]\right\}u(t)$$

$\zeta = 1$

$$h(t) = \omega_n^2 t e^{-\omega_n t} u(t)$$

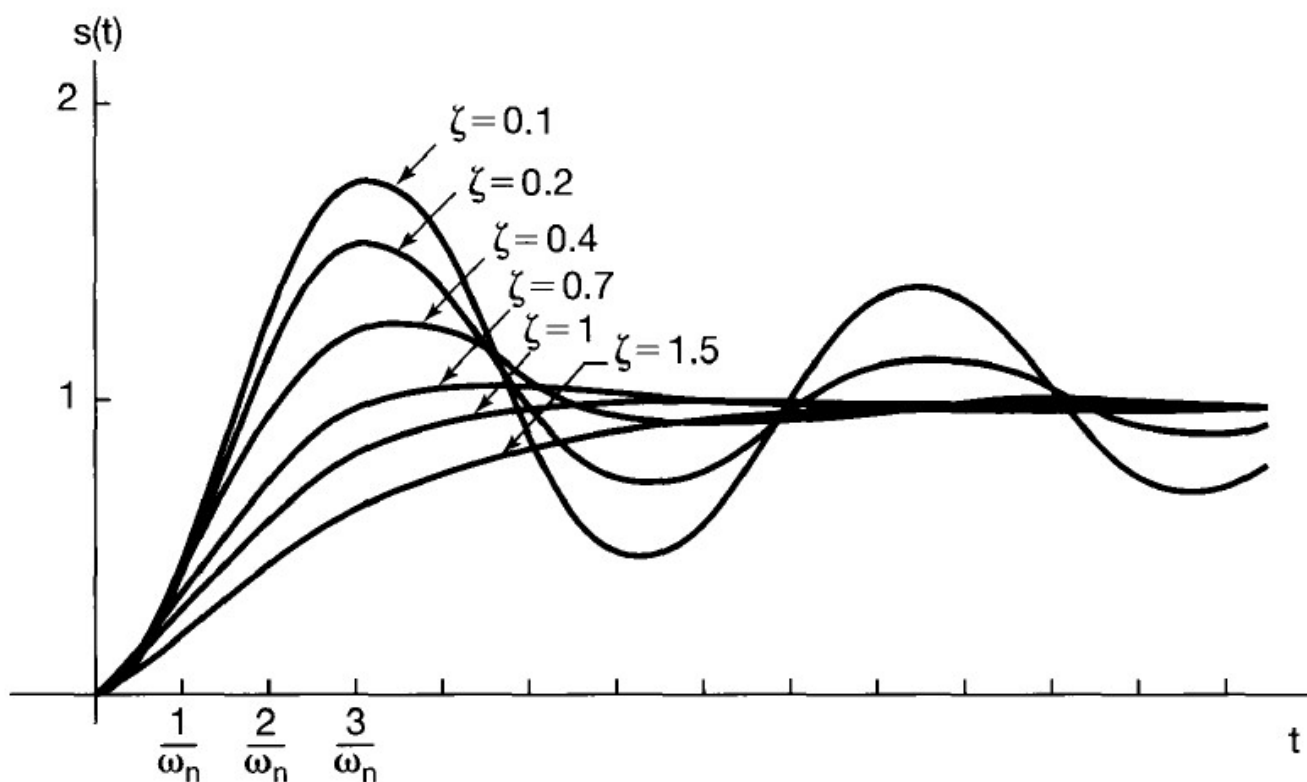
$$s(t) = \int_0^t \omega_n^2 t' e^{-\omega_n t'} dt' = -\omega_n \int_0^t t' d e^{-\omega_n t'}$$
$$= \begin{cases} 0, t < 0 \\ -\omega_n t' e^{-\omega_n t'} \Big|_0^t - \int_0^t e^{-\omega_n t'} d(-\omega_n t') = 1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t}, t \geq 0 \end{cases}$$

$$s(t) = [1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t}]u(t)$$

Second-order systems



□ Step response





Second-order systems

□ Bold plots

$$H(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} = \frac{1}{(j\omega/\omega_n)^2 + 2\zeta(j\omega/\omega_n) + 1}$$

$$20\log_{10}|H(j\omega)| = -20\log_{10}|(j\omega/\omega_n)^2 + 2\zeta(j\omega/\omega_n) + 1|$$

$$= -10\log_{10} \left\{ \left[1 - \left(\frac{\omega}{\omega_n} \right)^2 \right]^2 + 4\zeta^2 \left(\frac{\omega}{\omega_n} \right)^2 \right\}$$

$$\simeq \begin{cases} 0, & \omega \ll \omega_n \\ -40\log_{10}\omega + 40\log_{10}\omega_n, & \omega \gg \omega_n \end{cases}$$

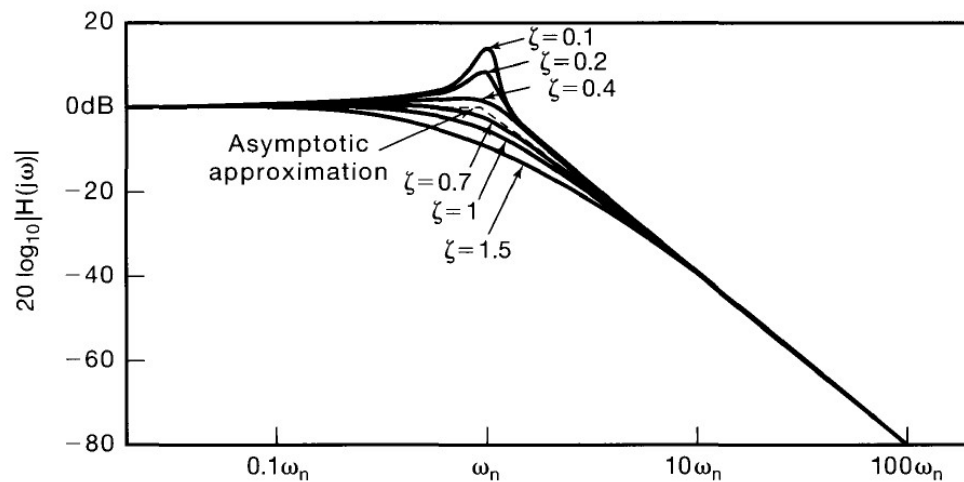
$$\angle H(j\omega) = -\tan^{-1} \left[\frac{2\zeta(\omega/\omega_n)}{1 - (\omega/\omega_n)^2} \right] \simeq \begin{cases} 0, & \omega \leq 0.1\omega_n \\ -\frac{\pi}{2} \left[\log_{10} \left(\frac{\omega}{\omega_n} \right) + 1 \right], & 0.1\omega_n \leq \omega \leq 10\omega_n \\ -\pi, & \omega \geq 10\omega_n \end{cases}$$

Second-order systems



□ Bold plots

$$20\log_{10}|H(j\omega)|$$



$$\angle H(j\omega)$$

