

# **Chapter IV**

## **Forward Kinematics**

**Dr. Song LIU**

**Director of AMNR Lab**

**[liusong@shanghaitech.edu.cn](mailto:liusong@shanghaitech.edu.cn)**

# Robot Forward Kinematics

- Content
  - Link Transformation Matrix
  - Robot Kinematics
  - Forward Kinematics for Spherical Coordinates Articulated Robot
  - Forward Kinematics for Cylindrical Coordinates Articulated Robot
  - Forward Kinematics for Cartesian Coordinates Articulated Robot
  - Kinematics based Mobile Robot Localization (Dead Reckoning)

# Link Transformation Matrix



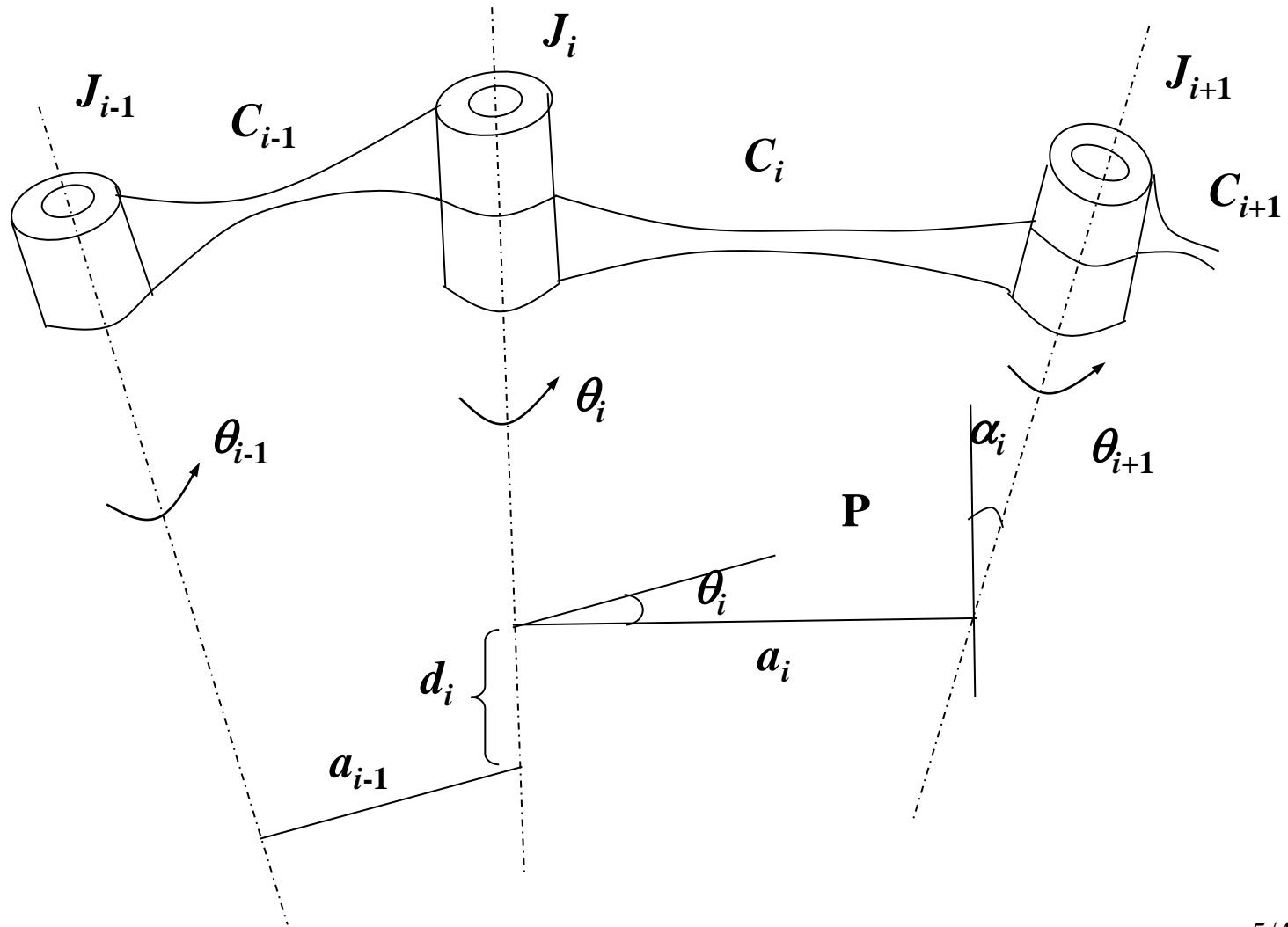
- **Some Concepts :**

- **Joint and Link :** Industrial robots typically consists of several joints and links (which is usually called manipulator). The **joints** are connections between links that permit relative motion between them; while the **links** are rigid bodies that give structure to the robot.
- Joints composed of multiple DOFs can be modelled as the superposition of several joints with single DOF and separate link with zero link length.
- A joint with single DOF can be translational joint or rotatory joint.

# Link Transformation Matrix

- **Axis of Movement:** the axis of movement for joint  $i$  is noted as  $J_i$ . A rotatory joint rotates about  $J_i$ , while a translational joint translates along  $J_i$ .
- **Parameters of Links: (Defined with respect to  $J_i$ )**
  - ✓ **Length  $a_i$ :** the length of the common perpendicular segment of  $J_i$  and  $J_{i+1}$ .
  - ✓ **Link Twist  $\alpha_i$ :** for  $J_i$  and  $J_{i+1}$ ,  $J_i$  and the common perpendicular line determines a plane P. Twist angle is defined as the angle between  $J_{i+1}$  and P.
  - ✓ **Link offset  $d_i$ :** Apart from the first and the last link, for link  $C_i$ , we can find the common perpendiculars of  $J_{i-1}$  and  $J_i$ ,  $J_i$  and  $J_{i+1}$ , noted as  $a_{i-1}$  and  $a_i$ . The distance between  $a_{i-1}$  and  $a_i$  is defined as link offset. ( $J_i$  is perpendicular to  $a_{i-1}$  and  $a_i$ )
  - ✓ **Joint Angle  $\theta_i$ :** the angle between the projections of  $a_{i-1}$  and  $a_i$  on the surface perpendicular to  $J_i$ .
- ❖  $(a_i, \alpha_i, d_i, \theta_i)$  is defined as Denavit-Hartenberg (D-H) parameters.

# Link Transformation Matrix



Question: Which parameters are constant and which parameters are changeable?

# Link Transformation Matrix

## 1.1 Coordinates establishment case I: Origin $O_i$ is located on $J_{i+1}$

➤ **Link Coordinates:** for adjacent links  $C_i$  and  $C_{i+1}$ , we consider  $J_{i-1}$ ,  $J_i$  and  $J_{i+1}$

✓ For middle link  $C_i$ , the coordinates is established as follows:

❑ **Origin  $O_i$ :** the intersection point of  $a_i$  and  $J_{i+1}$

❑  **$Z_i$ -axis:** along  $J_{i+1}$ , also denoted as  ${}^i e_z$

❑  **$X_i$ -axis:** along  $a_i$ , starting from  $O_i$ , also denoted as  ${}^i e_x$

❑  **$Y_i$ -axis:** determined by right-hand rule from  $X_i$  and  $Z_i$  axis, also denoted as  ${}^i e_y$

✓ For first link  $C_1$ , the coordinates is established as follows:

❑ **Origin  $O_1$ :** located on the origin of base coordinates

❑  **$Z_1$ -axis:** along  $J_1$

❑  **$X_1$ -axis:** Arbitrarily determined

❑  **$Y_1$ -axis:** determined by right-hand rule from  $X_1$  and  $Z_1$  axis

✓ For last link  $C_n$ , the coordinates is established as follows (the last link is typically the end-effector):

❑ **Origin  $O_n$ :** located in the geometrical center of end-effector

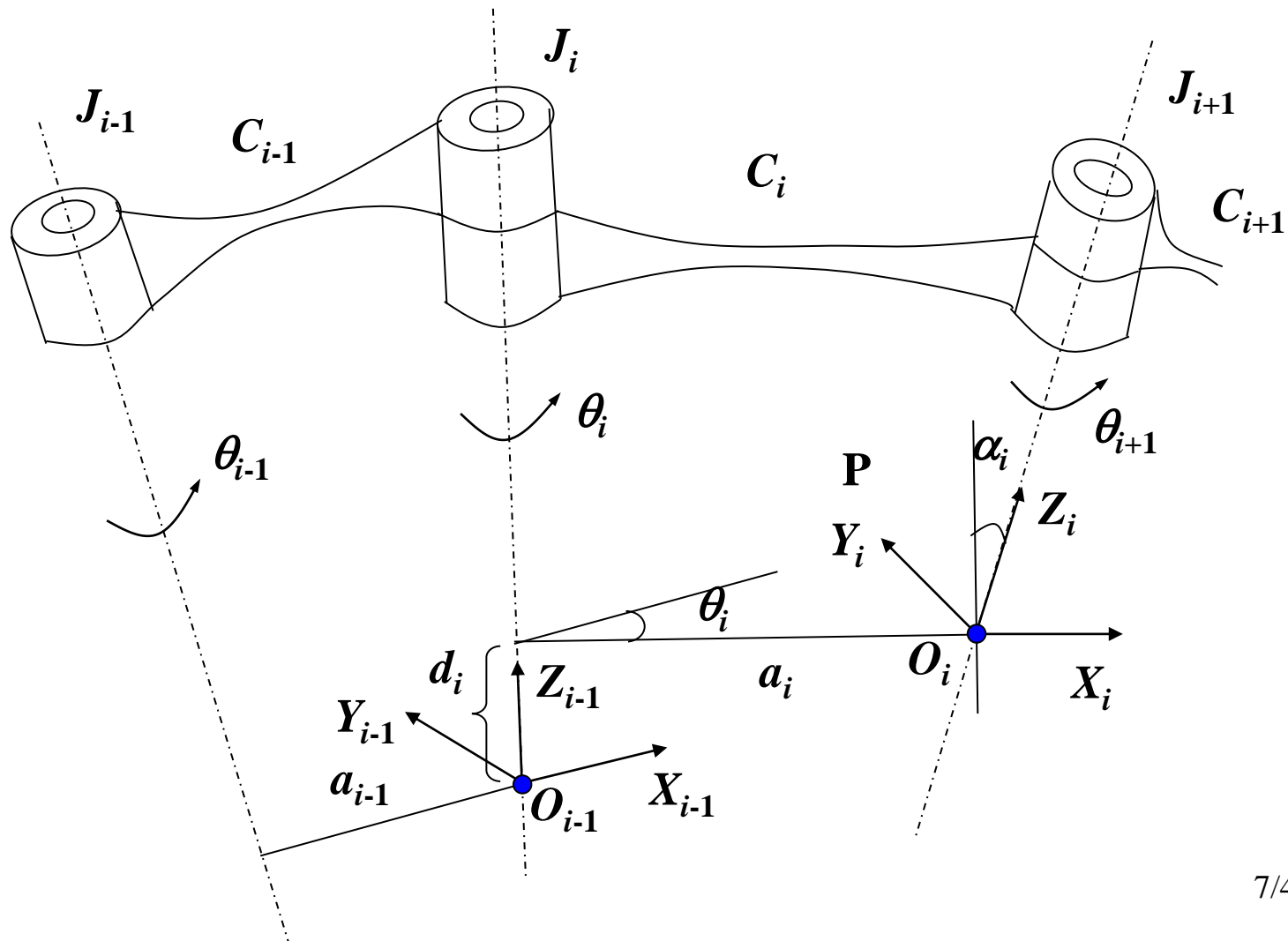
❑  **$Z_n$ -axis:** along the direction from end-effector towards object

❑  **$X_n$ -axis:** along the direction from one-finger to another finger

❑  **$Y_n$ -axis:** determined by right-hand rule from  $X_n$  and  $Z_n$  axis

# Link Transformation Matrix

## 1.1 Coordinates establishment case I: Origin $O_i$ is located on $J_{i+1}$



# Link Transformation Matrix

## 1.1 Coordinates establishment case I: Origin $O_i$ is located on $J_{i+1}$

- **Link Transformation Matrix:** coordinates of  $C_{i-1}$  is transformed to coordinates of  $C_i$  by twice rotation and twice translation.
  - ✓ **First:** rotate about  $Z_{i-1}$ -axis by  $\theta_i$  to align  $X_{i-1}$ -axis to  $X_i$ -axis
  - ✓ **Then:** translate along  $Z_{i-1}$ -axis by  $d_i$  to align  $O_{i-1}$  to the intersection point of  $J_i$  and  $a_i$
  - ✓ **Thereafter:** translate along **the new**  $X_{i-1}$ -axis (now the  $X_i$ -axis) by  $a_i$  to align  $O_{i-1}$  towards  $O_i$
  - ✓ **Finally:** rotate about  $X_i$ -axis by  $\alpha_i$  to align  $Z_{i-1}$ -axis to  $Z_i$ -axis

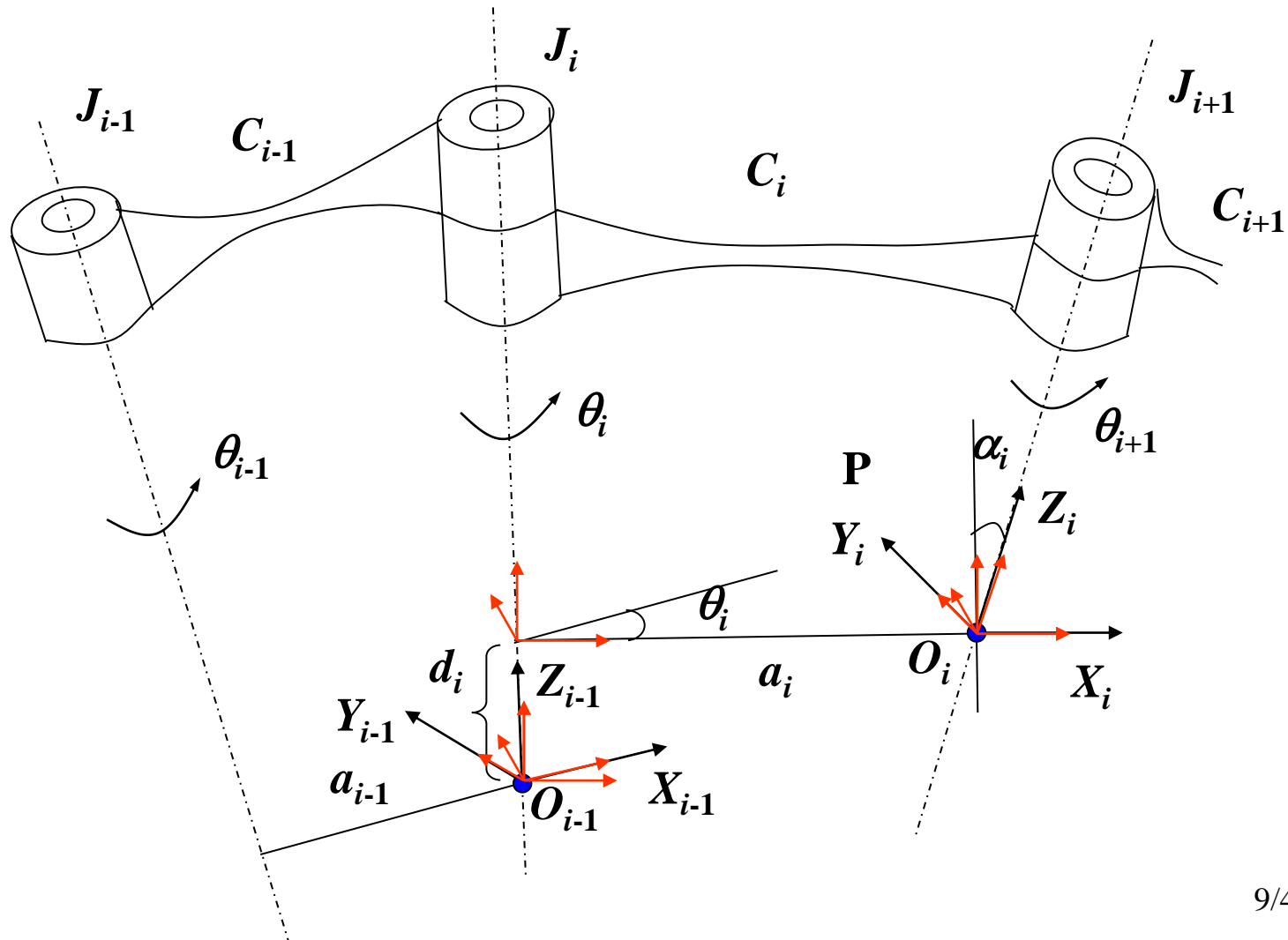
Now, coordinates  $O_{i-1}X_{i-1}Y_{i-1}Z_{i-1}$  and coordinates  $O_iX_iY_iZ_i$  completely overlaps each other. The above mentioned procedure transforming coordinates of  $C_{i-1}$  to coordinates of  $C_i$  can be mathematically described by four times homogeneous transformations.



# Link Transformation Matrix

## 1.1 Coordinates establishment case I: Origin $O_i$ is located on $J_{i+1}$

Graphical Depiction of the Link Coordinates Transformation Process



# Link Transformation Matrix

## 1.1 Coordinates establishment case I: Origin $O_i$ is located on $J_{i+1}$

- Link Transformation Matrix (D-H Matrix):

$$T_i = \text{Rot}(z, \theta_i) \text{Trans}(0, 0, d_i) \text{Trans}(a_i, 0, 0) \text{Rot}(x, \alpha_i)$$

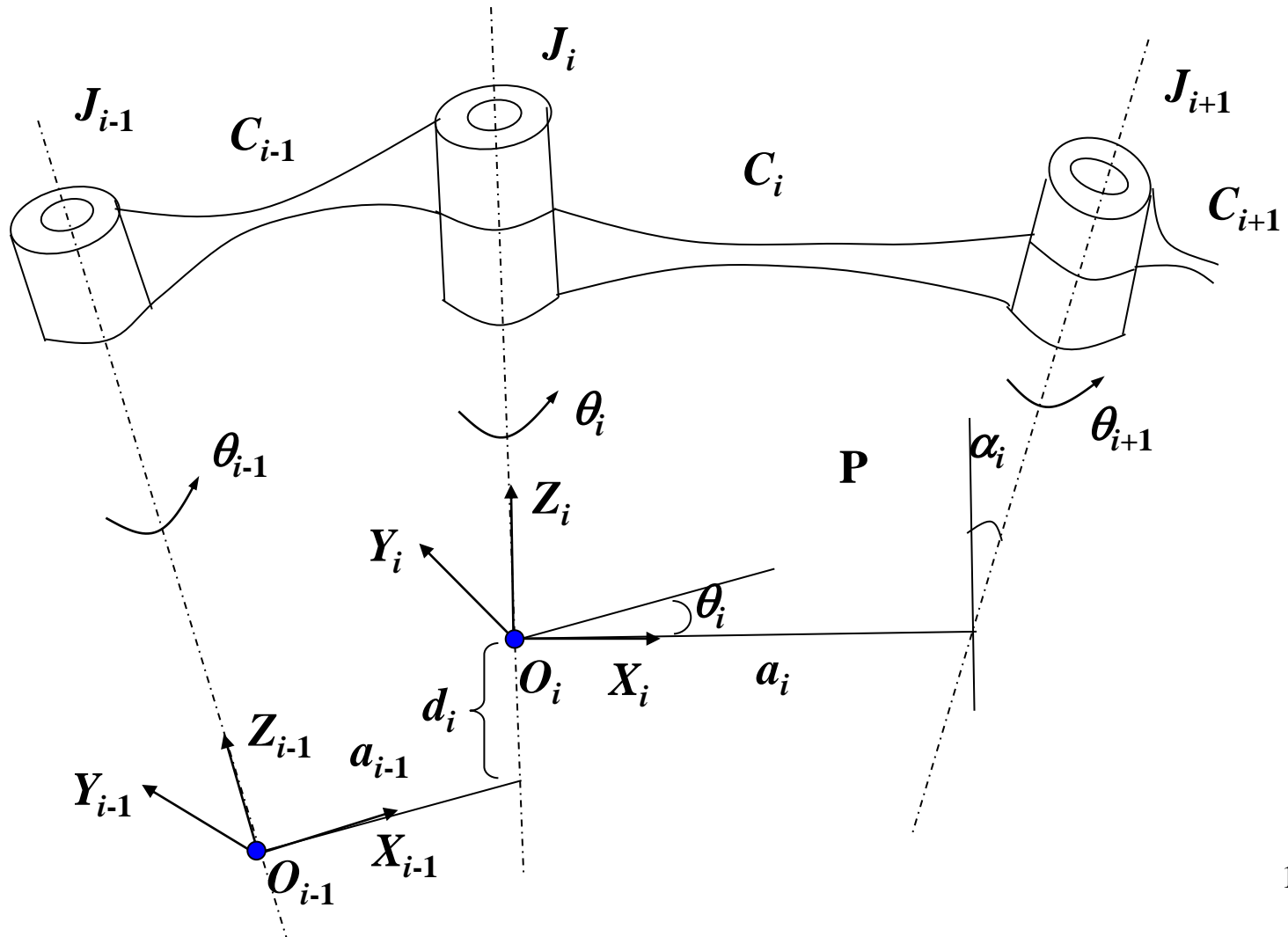
$$= \begin{bmatrix} \cos \theta_i & -\sin \theta_i & 0 & 0 \\ \sin \theta_i & \cos \theta_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \alpha_i & -\sin \alpha_i & 0 \\ 0 & \sin \alpha_i & \cos \alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cos \alpha_i & \sin \theta_i \sin \alpha_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cos \alpha_i & -\cos \theta_i \sin \alpha_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

The Link Transformation Matrix  $T_i$  of link  $C_i$  fully depends on the D-H parameters of  $C_i$ , which actually describes how end-effector is affected by the link  $C_i$ .

# Link Transformation Matrix

## 1.2 Coordinates establishment case II: Origin $O_i$ is located on $J_i$



# Link Transformation Matrix

## 1.2 Coordinates establishment case II: Origin $O_i$ is located on $J_i$

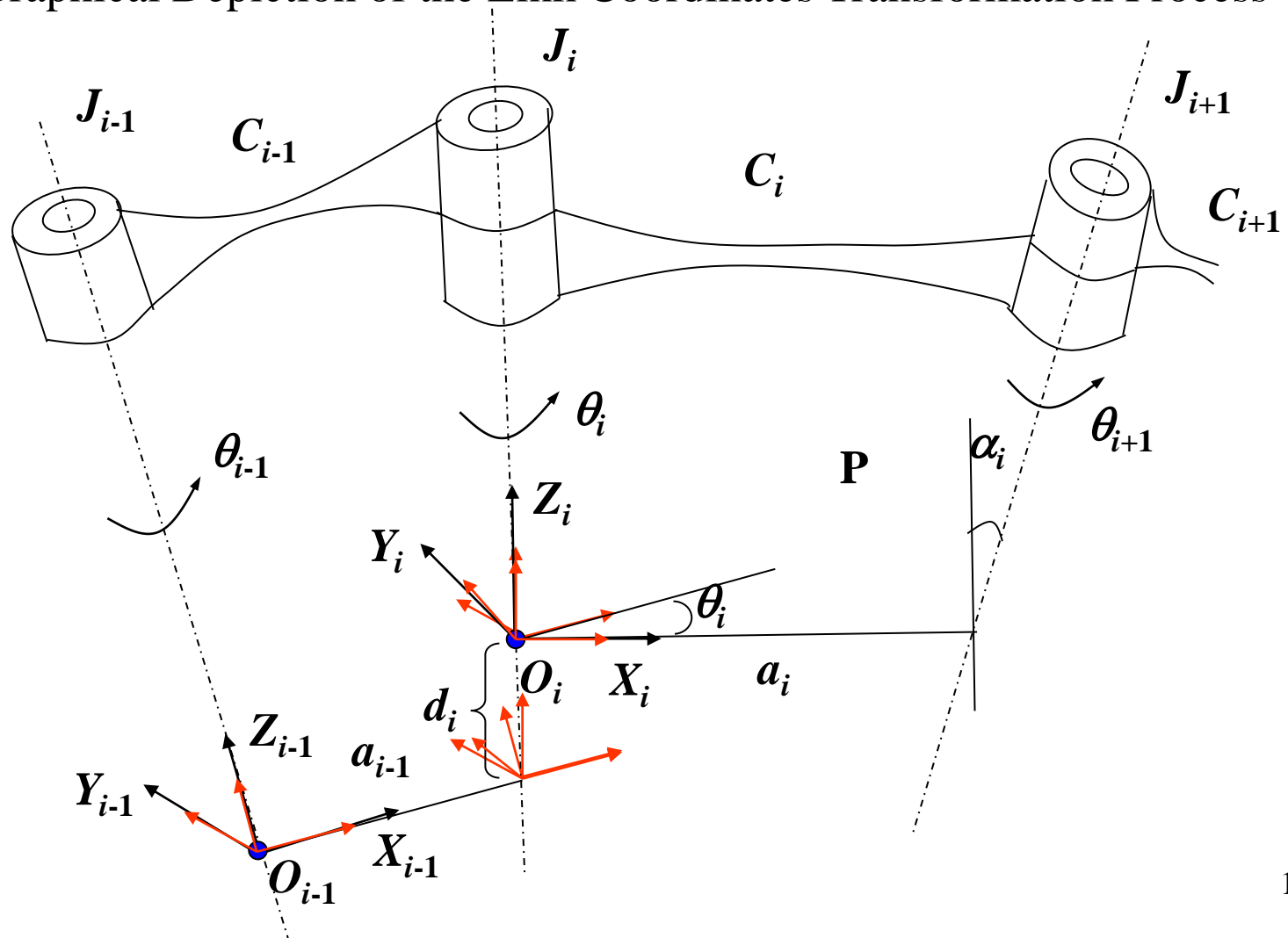
- **Link Transformation Matrix:** coordinate of  $C_{i-1}$  is transformed to coordinates of  $C_i$  by twice rotation and twice translation.
  - ✓ **First:** translate along  $X_{i-1}$ -axis by  $a_{i-1}$  to align  $O_{i-1}$  towards the intersection point of  $J_{i-1}$  and  $a_i$
  - ✓ **Then:** rotate about  $X_i$ -axis by  $\alpha_{i-1}$  to align  $Z_{i-1}$ -axis to  $Z_i$ -axis
  - ✓ **Thereafter:** translate along  $Z_i$ -axis by  $d_i$  to align the **new**  $O_{i-1}$  to  $O_i$
  - ✓ **Finally:** rotate about  $Z_i$ -axis by  $\theta_i$  to align the **new**  $X_{i-1}$ -axis to  $X_i$ -axis

Now, coordinates  $O_{i-1}X_{i-1}Y_{i-1}Z_{i-1}$  and coordinates  $O_iX_iY_iZ_i$  completely overlaps each other. The above mentioned procedure transforming coordinates of  $C_{i-1}$  to coordinates of  $C_i$  can be mathematically described by four times homogeneous transformations.

# Link Transformation Matrix

## 1.2 Coordinates establishment case II: Origin $O_i$ is located on $J_i$

Graphical Depiction of the Link Coordinates Transformation Process



# Link Transformation Matrix

## 1.2 Coordinates establishment case II: Origin $O_i$ is located on $J_i$

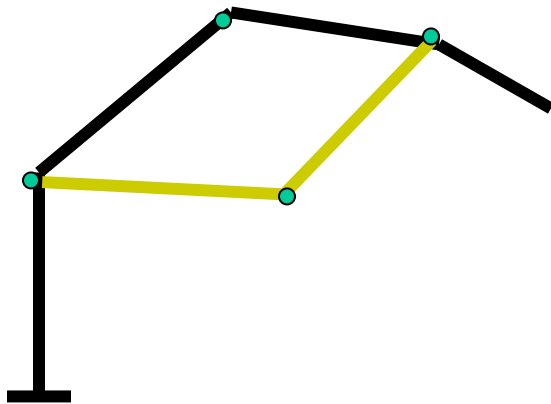
### D-H Matrix:

$$\begin{aligned}
 T_i &= \text{Trans}(a_{i-1}, 0, 0) \text{Rot}(x, \alpha_{i-1}) \text{Trans}(0, 0, d_i) \text{Rot}(z, \theta_i) \\
 &= \begin{bmatrix} 1 & 0 & 0 & a_{i-1} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \alpha_{i-1} & -\sin \alpha_{i-1} & 0 \\ 0 & \sin \alpha_{i-1} & \cos \alpha_{i-1} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta_i & -\sin \theta_i & 0 & 0 \\ \sin \theta_i & \cos \theta_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
 &= \begin{bmatrix} \cos \theta_i & -\sin \theta_i & 0 & a_{i-1} \\ \sin \theta_i \cos \alpha_{i-1} & \cos \theta_i \cos \alpha_{i-1} & -\sin \alpha_{i-1} & -d_i \sin \alpha_{i-1} \\ \sin \theta_i \sin \alpha_{i-1} & \cos \theta_i \sin \alpha_{i-1} & \cos \alpha_{i-1} & d_i \cos \alpha_{i-1} \\ 0 & 0 & 0 & 1 \end{bmatrix}
 \end{aligned}$$

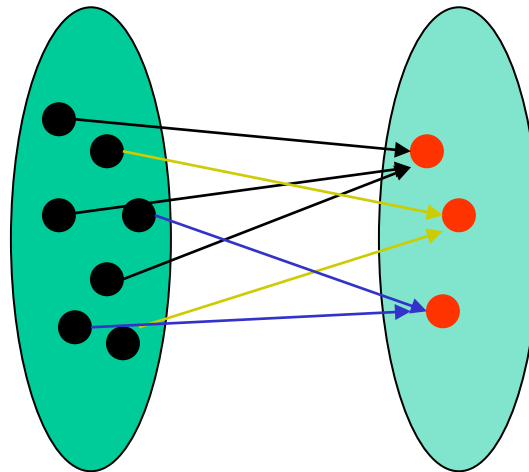
In this circumstance, the Link Transformation Matrix  $T_i$  of link  $C_i$  depends on the D-H parameters of both  $C_{i-1}$  and  $C_i$ ,

# Robot Forward Kinematics

- **Joint Space:** for a industrial robot with  $n$  DOFs, the position and orientation of all links can be described by a group of joint variables ( $d_i$  or  $\theta_i$ ), which are called joint vector or joint coordinates. The space represented by the joint vector is called the joint space.
- **Forward Kinematics:** Joint Space  $\rightarrow$  End Cartesian Space, one-to-one mapping
- **Inverse Kinematics:** End Cartesian Space  $\rightarrow$  Joint Space, one-to-many mapping



Different joint vectors may yield the same end coordinate.



The mapping relationship between joint space to end coordinates

# Robot Forward Kinematics

➤ **Forward Kinematics :** For an industrial robot having  $n$  DOFs, the D-H matrices of each link are  $T_1, T_2, \dots, T_n$ , then the pose of the robot end (a robot end is typically mounted with an end-effector) is:

$$T = T_1 T_2 T_3 \dots T_n$$

Though we have the two approaches to establish link coordinates and get different D-H matrices, we will always get the same robot end pose if the base coordinates are the same.

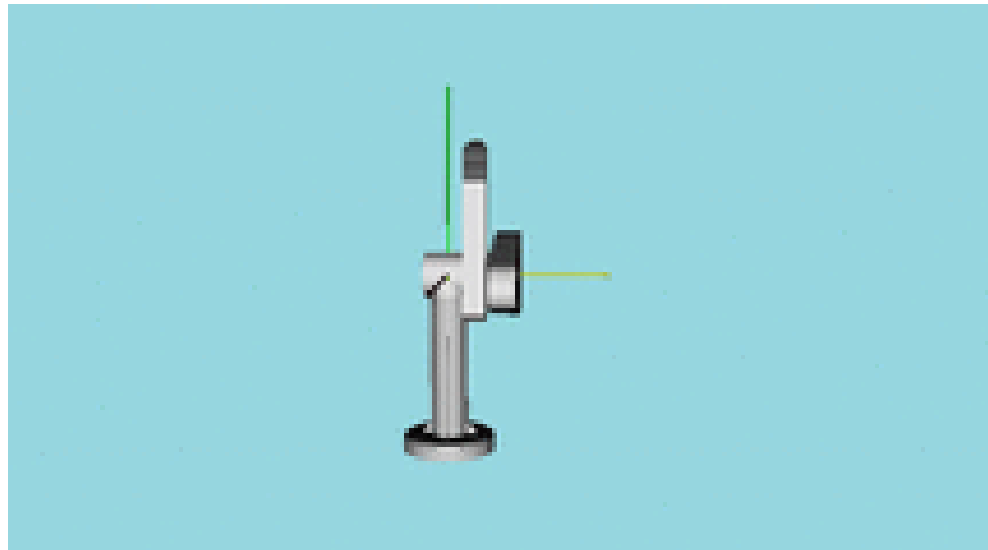
The pose of robot end with respect to  $C_{i-1}$  is :

$${}^{i-1}T_n = T_i T_{i+1} \dots T_n$$



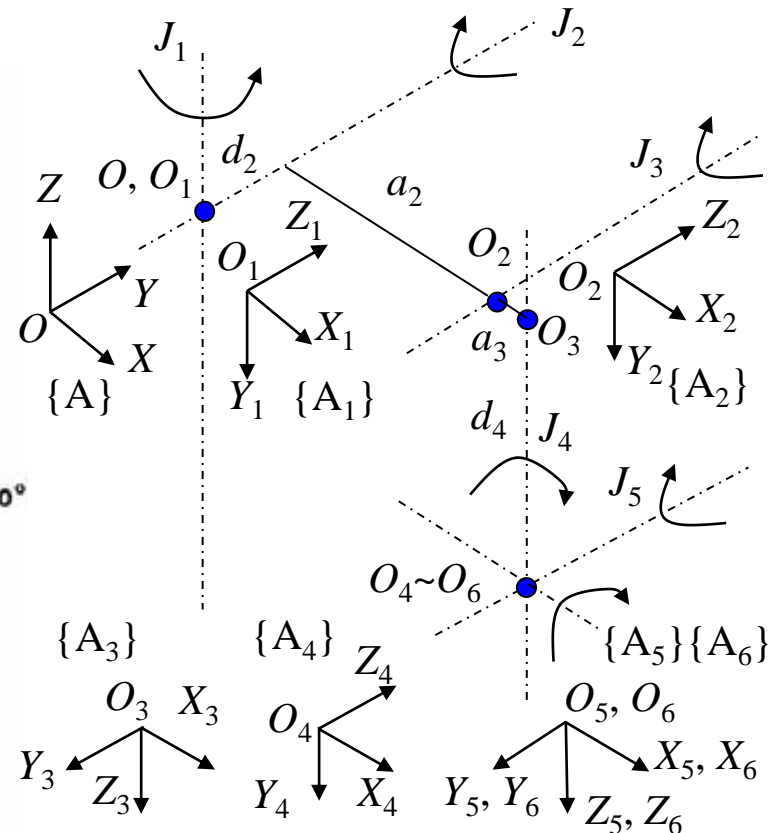
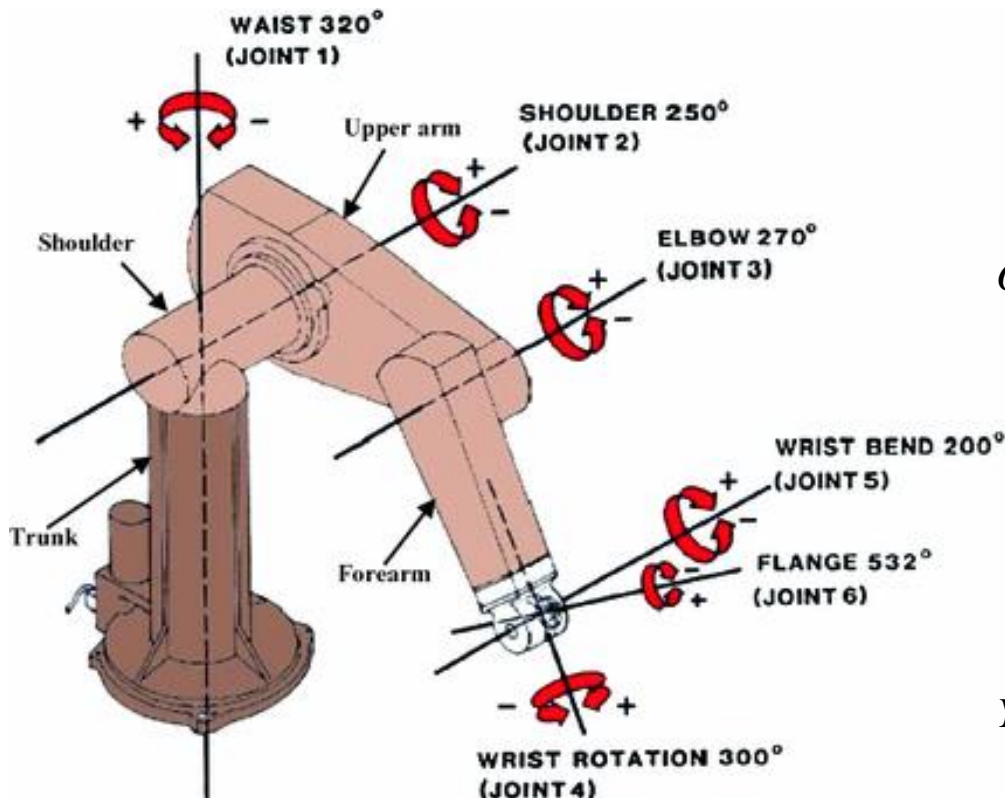
# Regarding PUMA560 Robot

The PUMA 560 (Programmable Universal Machine for Assembly) is the industrial robot arm developed by Victor Scheinman at pioneering robot company Unimation and released in 1978. It is perhaps one of the best known robots ever manufactured and was subject of the researches both in the academic institutions and industry.



# 3 Forward Kinematics for Spherical Coordinates Articulated Robot

## 3.1 PUMA560



Unimation PUMA560 Coordinates Establishment

Note no end-effector is attached to robot end;  $O$  overlaps  $O_1$

## 3.1 Forward Kinematics for Spherical Coordinates Articulated Robot

- D-H Parameters :

Link	$\theta_i$	$\alpha_i$	$a_i$	$d_i$
1	$\theta_1$	$-90^\circ$	0	0
2	$\theta_2$	$0^\circ$	$a_2$	$d_2$
3	$\theta_3$	$-90^\circ$	$a_3$	0
4	$\theta_4$	$90^\circ$	0	$d_4$
5	$\theta_5$	$-90^\circ$	0	0
6	$\theta_6$	$0^\circ$	0	0

# 3.1 Forward Kinematics for Spherical Coordinates Articulated Robot

## • D-H Matrix :

$$T_i = \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cos \alpha_i & \sin \theta_i \sin \alpha_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cos \alpha_i & -\cos \theta_i \sin \alpha_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_1 = \begin{bmatrix} \cos \theta_1 & 0 & -\sin \theta_1 & 0 \\ \sin \theta_1 & 0 & \cos \theta_1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2 = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & a_2 \cos \theta_2 \\ \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ 0 & 0 & 1 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_3 = \begin{bmatrix} \cos \theta_3 & 0 & -\sin \theta_3 & a_3 \cos \theta_3 \\ \sin \theta_3 & 0 & \cos \theta_3 & a_3 \sin \theta_3 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_4 = \begin{bmatrix} \cos \theta_4 & 0 & \sin \theta_4 & 0 \\ \sin \theta_4 & 0 & -\cos \theta_4 & 0 \\ 0 & 1 & 0 & d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

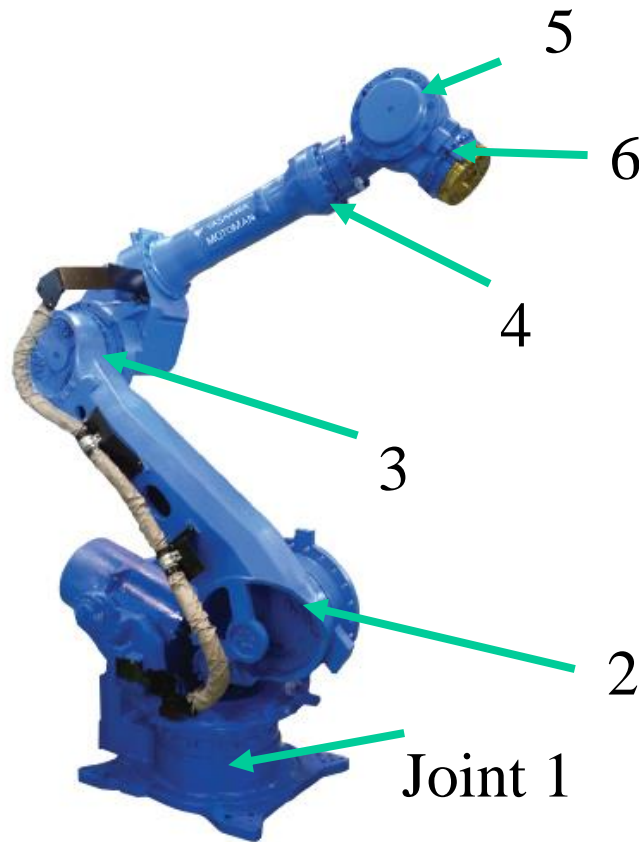
$$T_5 = \begin{bmatrix} \cos \theta_5 & 0 & -\sin \theta_5 & 0 \\ \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_6 = \begin{bmatrix} \cos \theta_6 & -\sin \theta_6 & 0 & 0 \\ \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Robot End Pose/Position:  $T = T_1 T_2 T_3 T_4 T_5 T_6$

## 3.2 Forward Kinematics for Yaskawa K10

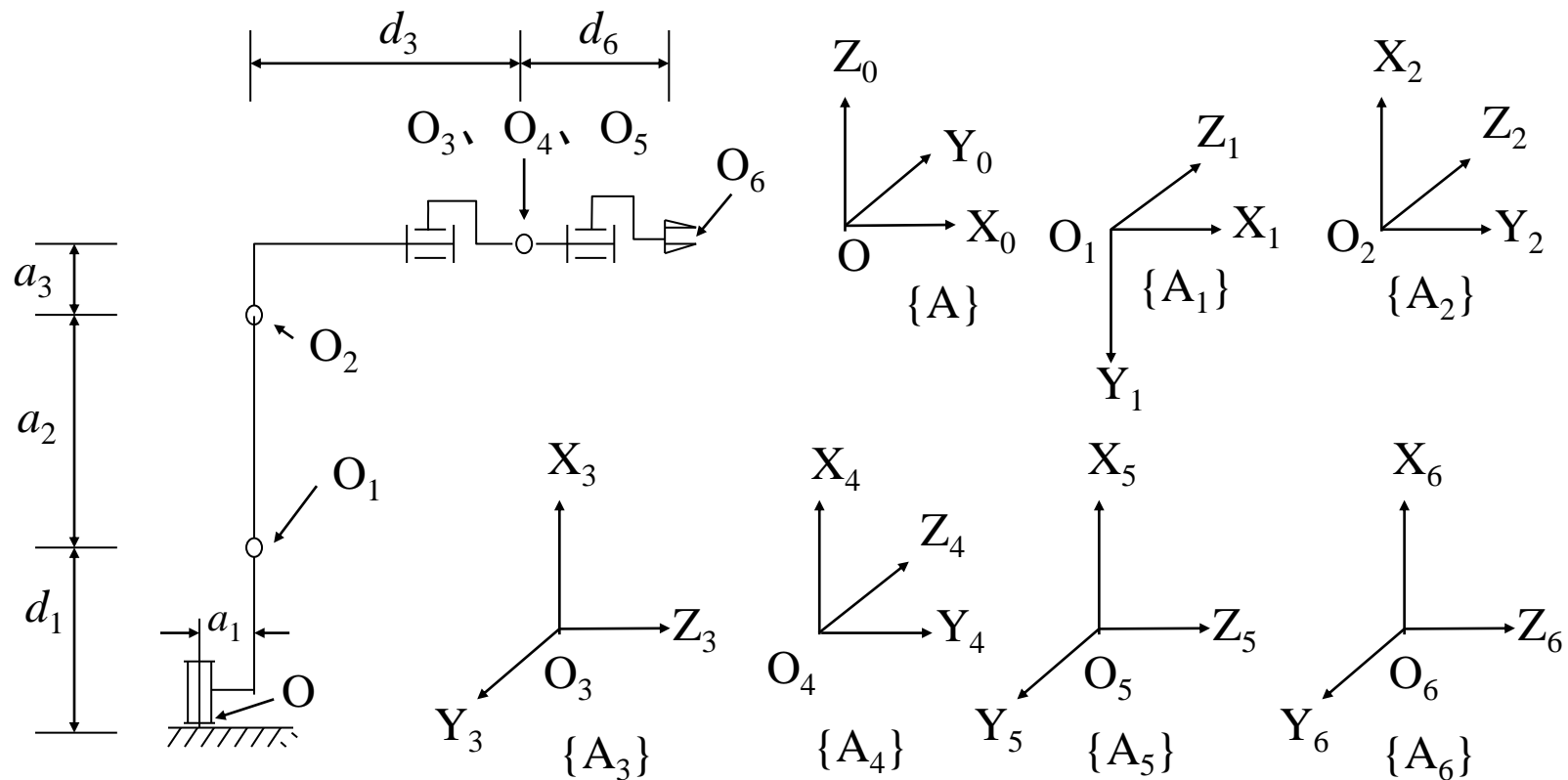
- Joint Configuration of Yaskawa K10



Yaskawa K10 in industry

## 3.2 Forward Kinematics for Yaskawa K10

- Coordinates Establishment



Note an end-effector is attached to robot end;  $O$  does not overlap  $O_1$

## 3.2 Forward Kinematics for Yaskawa K10

- D-H Matrix

$$T_1 = \text{Rot}(Z, \theta_1) \text{Trans}(a_1, 0, d_1) \text{Rot}(X, -90^\circ)$$

$$= \begin{bmatrix} \cos \theta_1 & 0 & -\sin \theta_1 & a_1 \cos \theta_1 \\ \sin \theta_1 & 0 & \cos \theta_1 & a_1 \sin \theta_1 \\ 0 & -1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2 = \text{Rot}(Z_1, -90^\circ + \theta_2) \text{Trans}(a_2, 0, 0)$$

$$= \begin{bmatrix} \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ -\cos \theta_2 & \sin \theta_2 & 0 & -a_2 \cos \theta_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_3 = \text{Rot}(Z_2, \theta_3) \text{Trans}(a_3, 0, 0) \text{Rot}(X_2, -90^\circ) \text{Trans}(0, 0, d_3)$$

$$= \begin{bmatrix} \cos \theta_3 & 0 & -\sin \theta_3 & a_3 \cos \theta_3 - d_3 \sin \theta_3 \\ \sin \theta_3 & 0 & \cos \theta_3 & a_3 \sin \theta_3 + d_3 \cos \theta_3 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_4 = \text{Rot}(Z_3, \theta_4) \text{Rot}(X_3, 90^\circ)$$

$$= \begin{bmatrix} \cos \theta_4 & 0 & \sin \theta_4 & 0 \\ \sin \theta_4 & 0 & -\cos \theta_4 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_5 = \text{Rot}(Z_4, \theta_5) \text{Rot}(X_4, -90^\circ)$$

$$= \begin{bmatrix} \cos \theta_5 & 0 & -\sin \theta_5 & 0 \\ \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_6 = \text{Rot}(Z_5, \theta_6) \text{Trans}(0, 0, d_6)$$

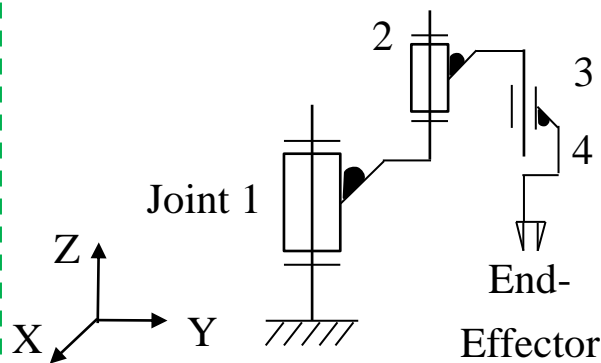
$$= \begin{bmatrix} \cos \theta_6 & -\sin \theta_6 & 0 & 0 \\ \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Robot End Pose/Position:

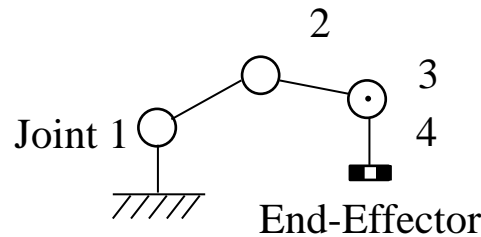
$$T = T_1 T_2 T_3 T_4 T_5 T_6$$

# SCARA is an acronym for **S**elective **C**ompliance **A**rticulated **R**obot **A**rm

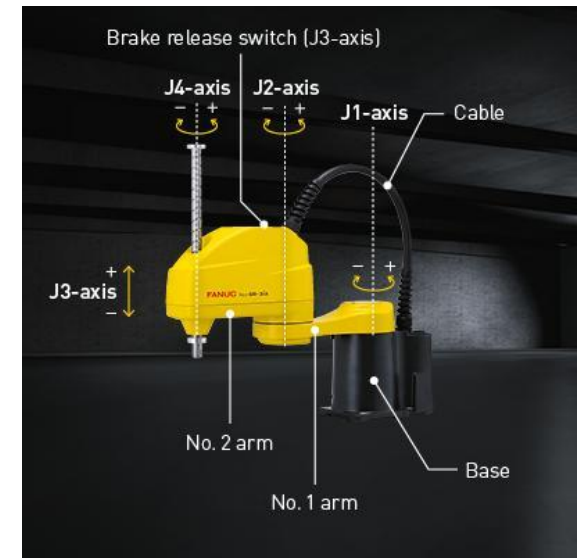
## Cylindrical Coordinates Robot



Side View



Top View

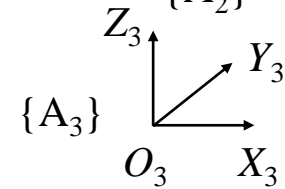
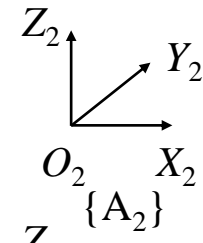
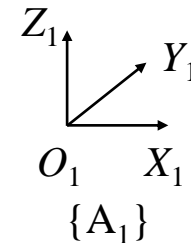
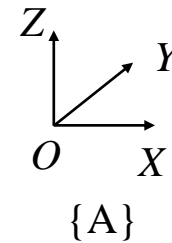
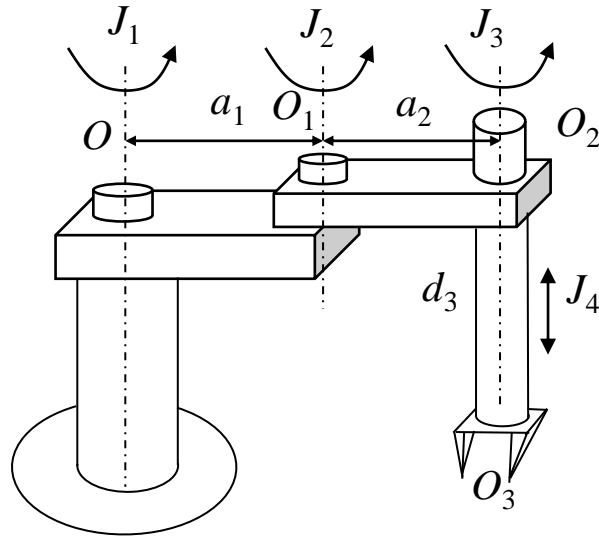


(1) All four joint axes are parallel; (2) Joint 1-3 can be viewed to be in the same surface; (3) End-effector's orientation and position is weakly correlated; Joint 4 determines the position along **Z**; Joint 3 Determines the orientation; Joint 1 and 2 determines the end-effectors position in **X-Y** plane.



# 4 Forward Kinematics for Cylindrical Coordinates Articulated Robot

## SCARA Cylindrical Coordinates Robot



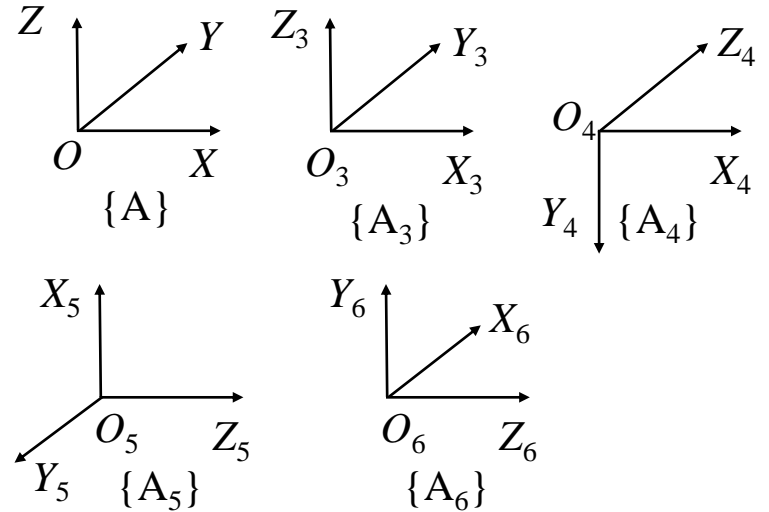
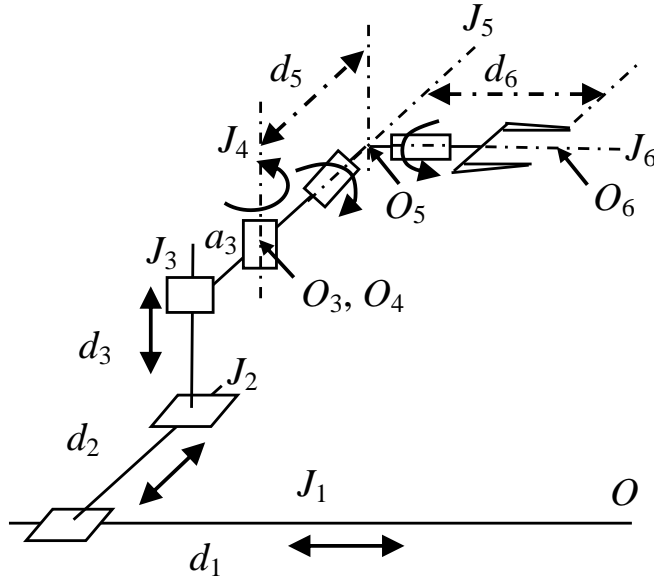
$$T_1 = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 & a_1 \cos \theta_1 \\ \sin \theta_1 & \cos \theta_1 & 0 & a_1 \sin \theta_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2 = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & a_2 \cos \theta_2 \\ \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_3 = \begin{bmatrix} \cos \theta_3 & -\sin \theta_3 & 0 & 0 \\ \sin \theta_3 & \cos \theta_3 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T = T_1 T_2 T_3 = \begin{bmatrix} \cos(\theta_1 + \theta_2 + \theta_3) & -\sin(\theta_1 + \theta_2 + \theta_3) & 0 & a_1 \cos \theta_1 + a_2 \cos(\theta_1 + \theta_2) \\ \sin(\theta_1 + \theta_2 + \theta_3) & \cos(\theta_1 + \theta_2 + \theta_3) & 0 & a_1 \sin \theta_1 + a_2 \sin(\theta_1 + \theta_2) \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# 5 Forward Kinematics for Cartesian Coordinates Articulated Robots



$$T_3 = \begin{bmatrix} 1 & 0 & 0 & d_1 \\ 0 & 1 & 0 & d_2 + a_3 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad T_4 = \text{Rot}(Z_3, \theta_4) \text{Rot}(X_3, -90^\circ) \quad T_5 = \text{Rot}(Z_4, -90^\circ + \theta_5) \text{Trans}(0, 0, d_5) \text{Rot}(X_4, -90^\circ)$$

$$= \begin{bmatrix} \cos \theta_4 & 0 & -\sin \theta_4 & 0 \\ \sin \theta_4 & 0 & \cos \theta_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad = \begin{bmatrix} \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ -\cos \theta_5 & 0 & \sin \theta_5 & 0 \\ 0 & -1 & 0 & d_5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_6 = \text{Rot}(Z_5, -90^\circ + \theta_6) \text{Trans}(0, 0, d_6)$$

$$= \begin{bmatrix} \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ -\cos \theta_6 & \sin \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# 5 Forward Kinematics for Cartesian Coordinates Articulated Robots

$$T = T_3 T_4 T_5 T_6$$

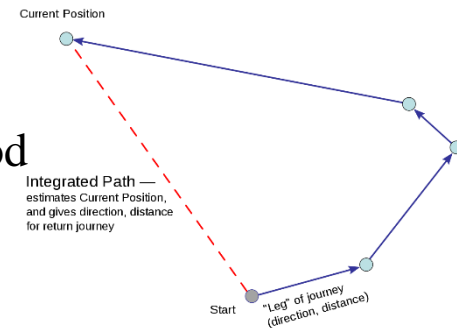
$$= \begin{bmatrix} 1 & 0 & 0 & d_1 \\ 0 & 1 & 0 & d_2+a_3 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta_4 & 0 & -\sin \theta_4 & 0 \\ \sin \theta_4 & 0 & \cos \theta_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ -\cos \theta_5 & 0 & \sin \theta_5 & 0 \\ 0 & -1 & 0 & d_5 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ -\cos \theta_6 & \sin \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_4 \sin \theta_5 & \sin \theta_4 & \cos \theta_4 \cos \theta_5 & d_1 - d_5 \sin \theta_4 \\ \sin \theta_4 \sin \theta_5 & -\cos \theta_4 & \sin \theta_4 \cos \theta_5 & d_2+a_3 + d_5 \cos \theta_4 \\ \cos \theta_5 & 0 & -\sin \theta_5 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ -\cos \theta_6 & \sin \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_4 \sin \theta_5 \sin \theta_6 - \sin \theta_4 \cos \theta_6 & \cos \theta_4 \sin \theta_5 \cos \theta_6 + \sin \theta_4 \sin \theta_6 & \cos \theta_4 \cos \theta_5 & d_1 - d_5 \sin \theta_4 + d_6 \cos \theta_4 \cos \theta_5 \\ \sin \theta_4 \sin \theta_5 \sin \theta_6 + \cos \theta_4 \cos \theta_6 & \sin \theta_4 \sin \theta_5 \cos \theta_6 - \cos \theta_4 \sin \theta_6 & \sin \theta_4 \cos \theta_5 & d_2+a_3 + d_5 \cos \theta_4 + d_6 \sin \theta_4 \cos \theta_5 \\ \cos \theta_5 \sin \theta_6 & \cos \theta_5 \cos \theta_6 & -\sin \theta_5 & d_3 - d_6 \sin \theta_5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# 6 Kinematics based Localization for Mobile Robots

- For mobile robot, localization is fundamental for navigation.
- Two categories of mobile robot localization method:
  - ✓ Absolute method: GPS, Landmark method, Triangulation Method
  - ✓ Relative methods: Dead Reckoning
- Dead reckoning, a.k.a. pass integration, is the process of calculating current position of some moving object by using a previously determined position, and then incorporating estimations of speed, heading direction, and course over elapsed time.
- Characteristics:
  - ✓ Dead reckoning is a kinematics based mobile robot localization method.
  - ✓ Dead reckoning suffers from accumulated errors.
  - ✓ Dead reckoning is suitable short term localization, like indoor localization.
  - ✓ Dead reckoning is widely applied, like in **inertial navigation** system, to provide very accurate directional information.



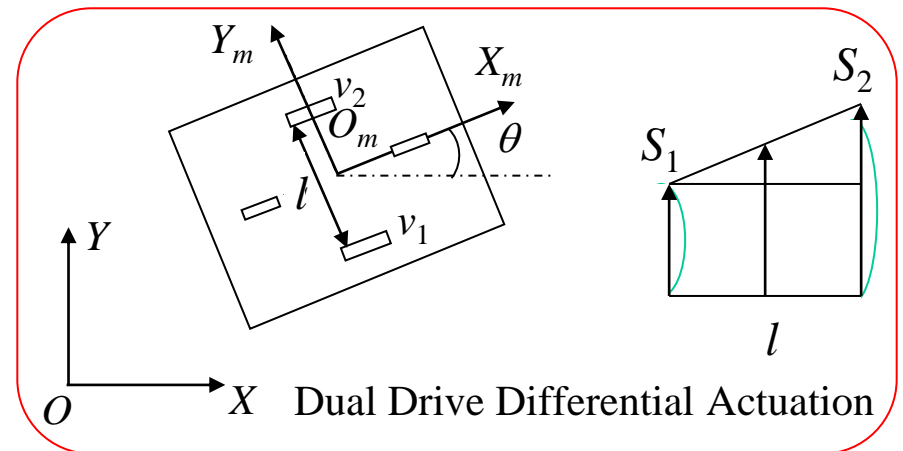
# 6 Kinematics based Localization for Mobile Robots

- Kinematics of a mobile robot is to **determine the pose**, including position and orientation of a mobile robot, along moving, which inherently localize a mobile robot.
- Kinematics of mobile robot is defined with respect to **Velocity** (vs. kinematics is defined with respect to joint space for articulated robot).
- Dead Reckoning Approach:

$$\left\{ \begin{array}{l} \dot{x} = \frac{v_1 + v_2}{2} \cos \theta \\ \dot{y} = \frac{v_1 + v_2}{2} \sin \theta \\ \dot{\theta} = \frac{v_1 - v_2}{L} \end{array} \right. \quad \left\{ \begin{array}{l} S = \frac{S_1 + S_2}{2} \\ \tan \theta = \frac{S_2 - S_1}{l} \end{array} \right.$$

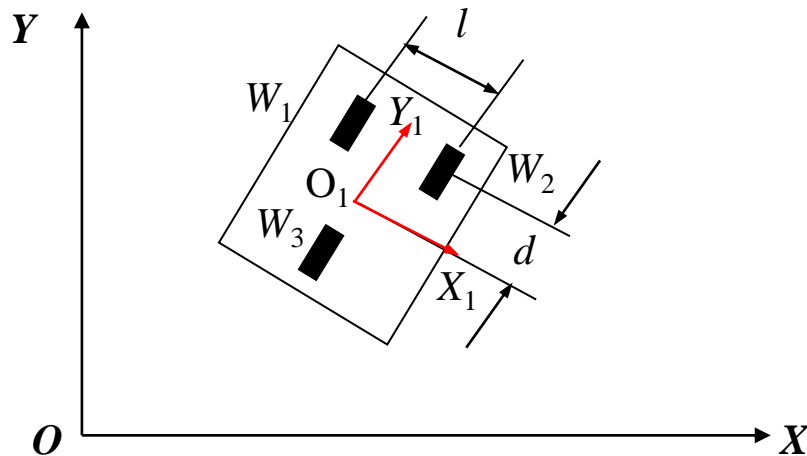
Representation 1

Representation 2



# 6 Kinematics based Localization for Mobile Robots

## Dead Reckoning represented by Coordinate Transformation



$$T_1 = \begin{bmatrix} m_x & n_x & p_x \\ m_y & n_y & p_y \\ 0 & 0 & 1 \end{bmatrix}$$

Initial Pose and Parameter Definition

# 6 Kinematics based Localization for Mobile Robots

## Dead Reckoning represented by Coordinate Transformation

- Linear Motion

- ✓ The robot cannot move along  $X_1$ -axis.
- ✓ We are talking about differential motion.

$$T_{1M} = T_1 \text{Trans}(0, \Delta S)$$

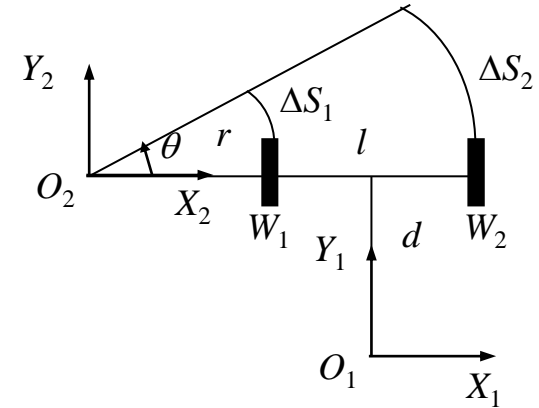
$$= \begin{bmatrix} m_x & n_x & p_x \\ m_y & n_y & p_y \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & \Delta S \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} m_x & n_x & p_x + \Delta S n_x \\ m_y & n_y & p_y + \Delta S n_y \\ 0 & 0 & 1 \end{bmatrix}$$

# 6 Kinematics based Localization for Mobile Robots

## Dead Reckoning represented by Coordinate Transformation

- Circular Motion case 1

$$\text{sig}\Delta S_1 = \text{sig}\Delta S_2 \quad |\Delta S_2| > |\Delta S_1|$$



Rotatory Center  $O_2$  locates on the left side of  $W_1$

$$T_{1M} = T_2 \text{ Trans}(r + l / 2, -d)$$

$$= T_1 \text{ Trans}(-r - l / 2, d) \text{ Rot}(\theta) \text{ Trans}(r + l / 2, -d)$$

$$= \begin{bmatrix} m_x & n_x & p_x \\ m_y & n_y & p_y \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & -r - l / 2 \\ 0 & 1 & d \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & r + l / 2 \\ 0 & 1 & -d \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} m_x \cos \theta + n_x \sin \theta & -m_x \sin \theta + n_x \cos \theta & (m_x \cos \theta + n_x \sin \theta - m_x)(r + l / 2) + (m_x \sin \theta - n_x \cos \theta + n_x)d + p_x \\ m_y \cos \theta + n_y \sin \theta & -m_y \sin \theta + n_y \cos \theta & (m_y \cos \theta + n_y \sin \theta - m_y)(r + l / 2) + (m_y \sin \theta - n_y \cos \theta + n_y)d + p_y \\ 0 & 0 & 1 \end{bmatrix}$$

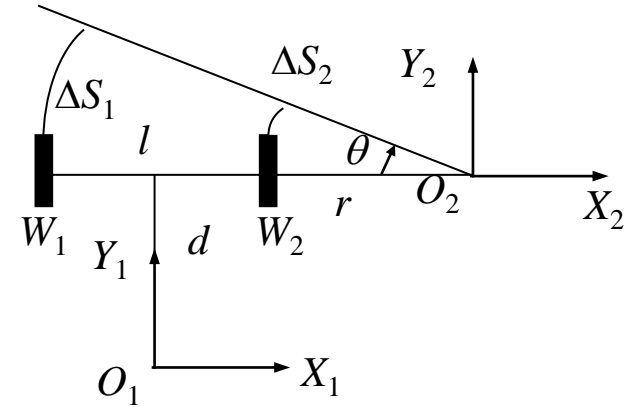


# 6 Kinematics based Localization for Mobile Robots

## Dead Reckoning represented by Coordinate Transformation

- Circular Motion case 2

$$\text{sig}\Delta S_1 = \text{sig}\Delta S_2 \quad |\Delta S_2| < |\Delta S_1|$$



Rotatory center  $O_2$  locates on right side of  $W_2$

$$T_{1M} = T_2 \text{ Trans}(-r-l/2, -d)$$

$$= T_1 \text{ Trans}(r+l/2, d) \text{ Rot}(\theta) \text{ Trans}(-r-l/2, -d)$$

$$= \begin{bmatrix} m_x & n_x & p_x \\ m_y & n_y & p_y \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & r+l/2 \\ 0 & 1 & d \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & -r-l/2 \\ 0 & 1 & -d \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} m_x \cos \theta + n_x \sin \theta & -m_x \sin \theta + n_x \cos \theta & (m_x \cos \theta + n_x \sin \theta - m_x)(-r-l/2) + (m_x \sin \theta - n_x \cos \theta + n_x)d + p_x \\ m_y \cos \theta + n_y \sin \theta & -m_y \sin \theta + n_y \cos \theta & (m_y \cos \theta + n_y \sin \theta - m_y)(-r-l/2) + (m_y \sin \theta - n_y \cos \theta + n_y)d + p_y \\ 0 & 0 & 1 \end{bmatrix}$$

# 6 Kinematics based Localization for Mobile Robots

## Dead Reckoning represented by Coordinate Transformation

- Circular Motion case 3

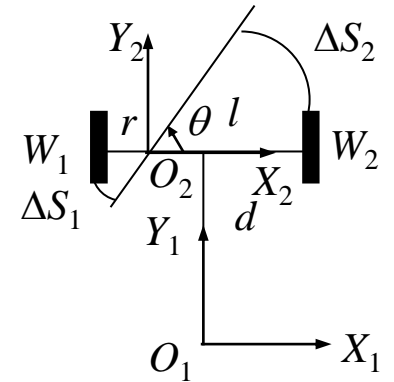
$$\text{sig}\Delta S_1 = -\text{sig}\Delta S_2$$

$$T_{1M} = T_2 \text{ Trans}(-r + l/2, -d)$$

$$= T_1 \text{ Trans}(r - l/2, d) \text{ Rot}(\theta) \text{ Trans}(-r + l/2, -d)$$

$$= \begin{bmatrix} m_x & n_x & p_x \\ m_y & n_y & p_y \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & r - l/2 \\ 0 & 1 & d \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & -r + l/2 \\ 0 & 1 & -d \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} m_x \cos \theta + n_x \sin \theta & -m_x \sin \theta + n_x \cos \theta & (m_x \cos \theta + n_x \sin \theta - m_x)(-r + l/2) + (m_x \sin \theta - n_x \cos \theta + n_x)d + p_x \\ m_y \cos \theta + n_y \sin \theta & -m_y \sin \theta + n_y \cos \theta & (m_y \cos \theta + n_y \sin \theta - m_y)(-r + l/2) + (m_y \sin \theta - n_y \cos \theta + n_y)d + p_y \\ 0 & 0 & 1 \end{bmatrix}$$



Rotatory center  $O_2$  locates  
between  $W_1$  and  $W_2$

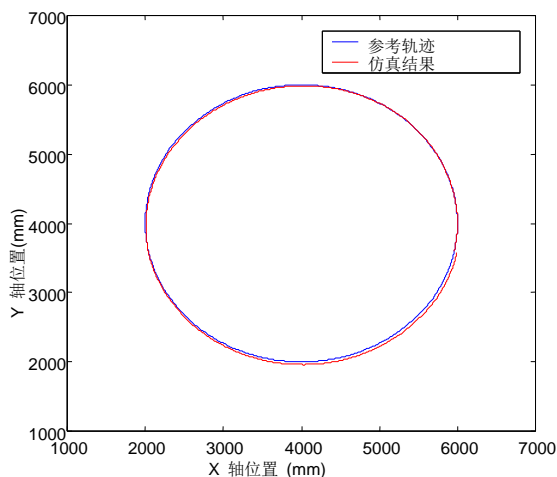
# Appendix

## An Improved Dead Reckoning Method for Mobile Robot with Redundant Odometry Information

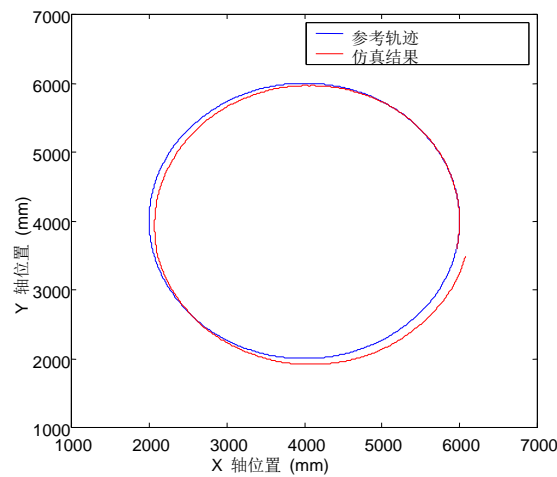
- De Xu, Min Tan, Gang Chen
- Institute of Automation, Chinese Academy of Sciences, Beijing, 100190, P.R.C.
- By visiting the following URL through campus wifi  
<https://ieeexplore.ieee.org/stamp/stamp.jsp?tp=&arnumber=1238497>

# Appendix-Simulation Results

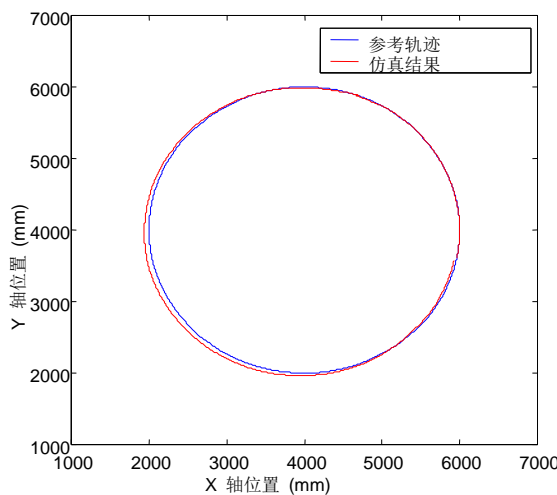
Triple wheel mobile robot parameters :  $l=600\text{mm}$ ,  $d=400\text{mm}$ ,  $h=800\text{mm}$ .  
Circular movement radius: 2000mm. Noise are added in simulation.



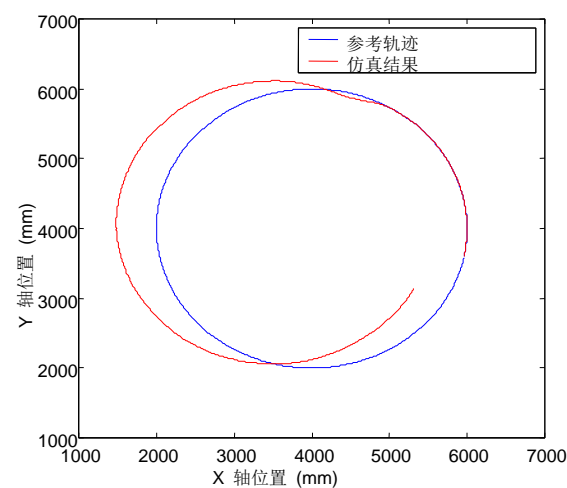
(a) 利用 W1-W3 数据获得的实验结果



(b) 只利用 W1 和 W2 信息的仿真结果



(c) W1 遇到凸起时利用 W1-W3 数据的仿真结果



(d) W1 遇到凸起时利用 W1 和 W2 数据的仿真结果

*THANK YOU*

