

Multi-Mode Electric Propulsion Thermal Analysis

Emilio R. Gordon*

University of Illinois at Urbana-Champaign, Urbana, IL 61801

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I. Introduction

This document serves as a summary for the Spring 2018 semester work accomplished by the Multi-Mode Micro-Propulsion (MMMP) undergraduate thermal research team. Multi-mode micro-propulsion is a potential game-changing technology enabling rapidly composable small satellites with unprecedented mission flexibility. Previous research has proven the conceptual understandings and technical capabilities for a single thruster emitter. Current research is focused on creating an array of emitters with this paper focusing on the thermal properties that will allow this to happen.

II. Thermal Modeling Setup

The goal of the thermal modeling was to create a low fidelity analytical model of the heat transfer in a relevant multi-channel array thruster, and explore the effects of manifold surface area and thermal resistance on the equilibrium temperature of the manifold. It is desirable to keep the manifold cool ($< \sim 100^{\circ}\text{C}$) to prevent propellant decomposition, while the micro-channel array is hot ($\sim 150 - 400^{\circ}\text{C}$) for propellant ignition and sustained combustion. The model presented in the paper explores how the manifold parameters will affect its equilibrium temperature.

The thermal model presented in Figure 1 consist of two stacked blocks, the array and the manifold. For the simple analysis used in Section III and Section IV, the array is kept at a fixed temperature. Heat is transferred from the array block via conduction to the manifold, for now, ignoring the radiative heat transfer between the two. Finally, heat is lost from the manifold via radiation to space. No other heat addition or loss sources are considered.

*Undergraduate Research Assistant, Aerospace Engineering, 104 S.Wright Street, Student Member AIAA

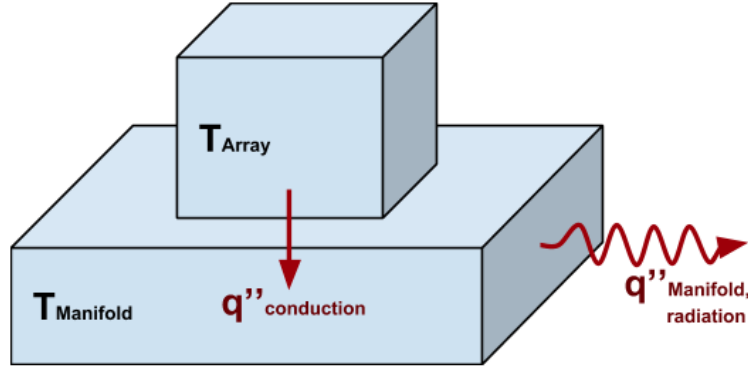


Fig. 1 Model for simple heat transfer between the array, manifold and the space environment.

The objective of the analysis as mentioned is to study the effects of manifold surface area and thermal resistance on the equilibrium temperature of the manifold. To satisfy this, data was collected for a range of manifold geometries and thermal contact conductivities as listed in Figure 2.

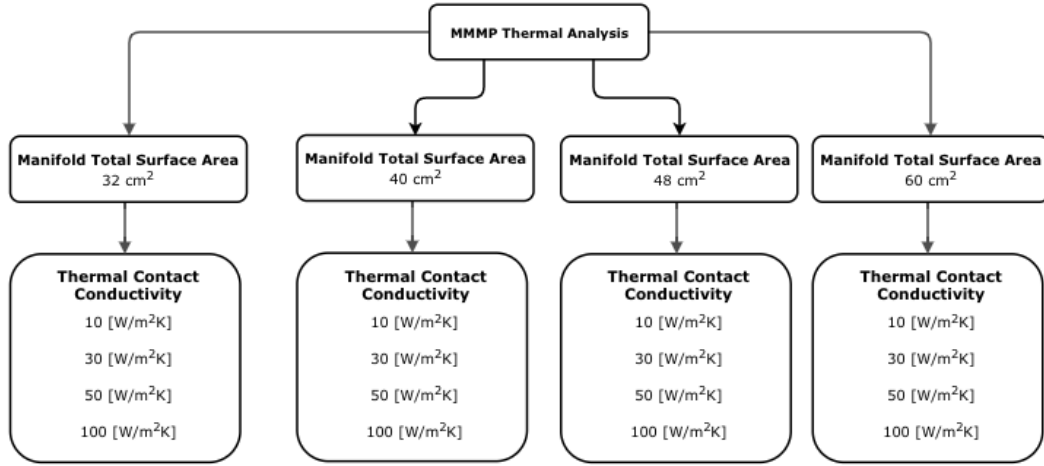


Fig. 2 Design Points for Thermal Analysis

III. Steady State Analytical Model

From the model, it is a safe assumption that the conduction between the array and the manifold is governed by the thermal resistance on the contact surface, expressed in Equation 1. Note that Equation 1, is a function of the thermal contact resistance but, as mentioned in Section II, the varied parameter is the thermal contact conductivity. This was done to allow for a smoother transition between the analytical model and simulation. Recall however that resistivity is simply the inverse of conductivity, $R = \frac{1}{K}$. In addition, the radiation loss from the manifold is governed by the

Stefan-Boltzmann law for perfect black body representation shown in Equation 2. The resulting heat balance is given by Equation 3.

$$q_{\text{conduction}} = \frac{1}{R} (T_{\text{array}} - T_{\text{manifold}}) \quad (1)$$

$$q_{\text{radiation}} = \sigma \varepsilon A_{sm} T_{\text{manifold}}^4 \quad (2)$$

$$q''_{\text{conduction}} A_{\text{contact}} = q_{\text{radiation}} \quad (3)$$

The manifold temperature, T_{Manifold} is easily solved for from the heat balance equation, Equation 3 and is a function of the manifold emissivity, ε , surface area, A_{sm} , contact area between the Array and Manifold, (A_{contact}), thermal resistance between manifold and array block, R , the array temperature, T_{array} and the Stefan-Boltzmann constant, σ .

$$\frac{\sigma \varepsilon A_{\text{manifold}}}{A_{\text{contact}}} T_{\text{manifold}}^4 + T_{\text{manifold}} = T_{\text{array}} \quad (4)$$

For simplicity, the analytical model will assume a manifold temperature and calculate the corresponding array temperature using Equation 4. The analytical model was performed in Excel* using the values shown below.

- Emissivity:

An emissivity of $\varepsilon = 0.36$ was used, typical for stainless steel.

- Contact Area:

The contact area was calculated along the base of a 6cm square array. Considering the array rest on the manifold atop a 5-mm wide wedge on two of the four sides, the contact area is fixed at $A_{\text{contact}} = 0.006 [m^2] = 600 [mm^2]$.

The entire array base is not in contact with the manifold because of the hollow dead propellant space within the manifold.

- Exposed Manifold Surface Area:

The manifold is fully exposed along five of its six sides. The face in contact with the array loses $0.012 [m^2] = 12000 [mm^2]$. This is the case for all the manifolds being tested. As a result, when computing the radiation output of the manifold, the surface area utilized is simply the area lost by the array subtracted from the total baseline manifold surface area (Ignoring the area caused by the dead space).

- Manifold Temperature:

Manifold Temperatures were computed along a range from -200C to 200C. Note that these values are converted into Kelvin for the computation of T_{array} and then converted back into Celsius.

These values remained constant while analytical models tested the geometries and contact conductivities as listed above in Section II.

*Analytical Model Location: UofIBox < Multimode R&D Team < Thermal Team Workspace < Data < Thermal Analysis.xlsx

Results indicate that a smaller thermal contact conductivity (larger thermal contact resistance) between the array and the manifold enables the manifold to stay cooler. Within the surface areas investigated, the results suggest that with low thermal conductivities, the manifold can be maintained at or below 100C for array temperatures as high as 650C

IV. Steady State Simulation

A. Simulation Set Up

- 1. Geometry*
- 2. Mesh*
- 3. Contacts, Boundary Conditions and Parameters*
- 4. Solution Parameters*
- 5. Design Points*

B. Results

V. Procedure for Paper Submission

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Table 1 Transitions selected for thermometry

Line	Transition		J''	Frequency, cm^{-1}	FJ , cm^{-1}	$G\nu$, cm^{-1}
	ν''					
a	0	P ₁₂	2.5	44069.416	73.58	948.66
b	1	R ₂	2.5	42229.348	73.41	2824.76
c	2	R ₂₁	805	40562.179	71.37	4672.68
d	0	R ₂	23.5	42516.527	1045.85	948.76

Line drawings must be clear and sharp. Make sure that all lines and graph points are dark and distinct and that

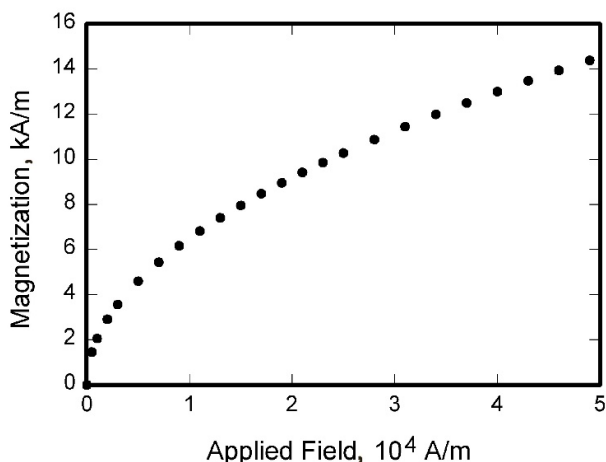


Fig. 3 Magnetization as a function of applied fields.

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command environment.

A sample equation is included here, formatted using the preceding instructions:

$$\int_0^{r_2} F(r, \varphi) dr d\varphi = [\sigma r_2 / (2\mu_0)] \int_0^\infty \exp(-\lambda |z_j - z_i|) \lambda^{-1} J_1(\lambda r_2) J_0(\lambda r_i) \lambda d\lambda \quad (5)$$

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A parenthetical statement at the end of a sentence is punctuated outside of the closing parenthesis (like this). (A parenthetical sentence is punctuated within parenthesis.) Use American, not English, spellings (e.g., “color,” not “colour”). The serial comma is preferred: “A, B, and C” instead of “A, B and C.”

Be aware of the different meanings of the homophones “affect” (usually a verb) and “effect” (usually a noun), “complement” and “compliment,” “discreet” and “discrete,” “principal” (e.g., “principal investigator”) and “principle” (e.g., “principle of measurement”). Do not confuse “imply” and “infer.”

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Appendix

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