## AEE 500

# Peridynamic Modelling of Materials and Fracture

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### 1 Introduction

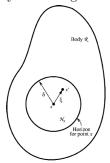
Peridynamics is a non-local continuum theory where discontinuities within a continua are handled with integral equtions. The integration consists of a domain of influence which is typically a spherical domain with a radius,  $\delta$ , where the quantity of interest is integrated (averaged) over the neighborhood of the location of interest. Considering balance of linear momentum in both local and non-local formulations, following relations show differentiation-to-integration change in both theories;

$$\rho \dot{\mathbf{v}} = \frac{\partial \sigma}{\partial x} + \rho \mathbf{b} \tag{1}$$

$$\rho \dot{\mathbf{v}} = \int_{H_x} \mathbf{f} \, dV + \mathbf{b} \tag{2}$$

(1) is known as the Cauchy's first law of motion where  $\sigma(\mathbf{x},t)$  is the Cauchy stress tensor whereas (2) is the Peridynamic equation of motion where  $\mathbf{f}$  if the Peridynamic force density vector,  $\rho$  is the mass density and  $\mathbf{b}$  is the body force density. The integration domain is set by a parameter  $\delta$  which defines a domain of influence or neighborhood at a point  $\mathbf{x}$ .

Figure 1: Peridynamic neighborhood in a body



The integration over the domain of influence is usually used in proofs or derivations whereas when a body is discritized into points, summation over a neighborhood is preferred;

$$\rho_k \dot{\mathbf{v}}_k = \sum_{j=1}^{N_k} \mathbf{f}(x_k, x_j, ..., t) V_j + \mathbf{b}_k$$
(3)

In the following chapters, construction of peridynamic force vector and vector states, constitutive models and solution techniques are discussed.

#### 2 Vector States

**Preliminary Identities:** Vector states or *Peridynamic States* are mappings from pairs of points to some quantities. [Silling and Lehoucq(2010)] A peridynamic state  $A\langle \bullet \rangle$  is a function over a vector. Depending on return value it maybe scalar state, vector state or double state which returns second - order tensors.

Some of the identities of states are given below;

$$Identitiy State : \underline{X}\langle \vec{\xi} \rangle = \vec{\xi}$$
 (4)

$$Null State : \underline{0}\langle \vec{\xi} \rangle = \vec{0} \tag{5}$$

$$Dot \, Product : \underline{A} \bullet \underline{B} = \int_{H} \underline{A} \langle \vec{\xi} \rangle \cdot \underline{B} \langle \vec{\xi} \rangle \, dV_{\xi} \tag{6}$$

$$Norm: \|\underline{A}\| = \sqrt{\underline{A} \bullet \underline{A}} \tag{7}$$

Fretchet Derivative of Functions of States: Define a potential function,  $\psi(\bullet)$ , which is a function of a scalar state, its *Fretchet derivative*,  $\nabla \psi$ , is defined such that;

$$\psi(\underline{A} + \underline{a}) = \psi(\underline{A}) + \nabla \psi(\underline{A}) \cdot \underline{a} + o(\|\underline{a}\|) \tag{8}$$

#### 3 Constitutive Models

**Deformation State:** Constitutive model in peridynamics provides the internal force vector state as a function of deformation vector state. Deformation state,  $\underline{Y}[\vec{x}, t]$ , maps the relative distances (bonds) in reference configurations to deformed images such that;

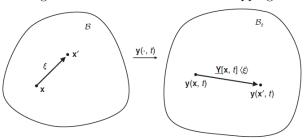
$$\underline{Y}[\vec{x}, t] \langle \vec{\xi} \rangle = \vec{y}(\vec{x}', t) - y(\vec{x}, t) \tag{9}$$

The vectors that denote the relative positions or bond vectors in reference and deformed configurations are denoted as ;

$$\vec{\xi} = \vec{x'} - \vec{x} \tag{10}$$

$$\vec{\eta} = \vec{y'} - \vec{y} \tag{11}$$

Figure 2: Deformation state as a mapping



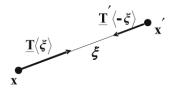
**Force State:** Internal forces within the continuum are defined by the counteracting force vectors in ordinary state based theory. Force vector state, then, is a mapping over the bond vector  $\vec{\xi}$  such that;

$$\vec{t}(\vec{x}, \vec{x}', t) = \underline{T}[\vec{x}, t] \langle \vec{\xi} \rangle \tag{12}$$

Force state is called ordinary if following holds,

$$\underline{T} = \hat{\underline{T}} = t\underline{M} \tag{13}$$

Figure 3: Ordinary state based force vectors



Ordinary state based

$$\underline{M} = \frac{\underline{Y}}{|\underline{Y}|} \tag{14}$$

If the material is elastic, free energy density only depends on  $\underline{Y}$  such that,

$$\hat{\underline{T}} = \nabla \hat{W} \tag{15}$$

where  $\nabla \hat{W}$  is the Fretchet derivative of free energy density.

In ordinary state based peridynamics, peridynamic equation of motion 2 takes the form of;

$$\rho \dot{\mathbf{v}} = \int_{V} (\mathbf{t} - \mathbf{t'}) \, dV + \rho \mathbf{b} \tag{16}$$

where,

$$\vec{t}(\vec{x}, \vec{x}', t) = \underline{T}\langle \vec{\xi} \rangle = \underline{T}\langle \vec{x'} - \vec{x} \rangle \tag{17}$$

$$\vec{t'}(\vec{x}, \vec{x'}, t) = T\langle \vec{\xi'} \rangle = T\langle \vec{x} - \vec{x'} \rangle \tag{18}$$

**Linear Elastic Solids:** Suppose the free energy density of a material is given as,

$$W(\theta, \underline{e}^d) = \frac{\kappa \theta^2}{2} + \frac{\alpha}{2} (\underline{\omega} \underline{e}^d) \cdot \underline{e}^d$$
 (19)

where  $\kappa$  is the bulk modulus,  $\theta$  is the volumetric strain (dilatation),  $\alpha$  is the shear modulus,  $\underline{\omega}$  is the influence scalar state,  $\underline{e}^d$  is the distortional (deviatoric) part of the extension scalar state such that;

$$\underline{x} = |\underline{X}| \tag{20}$$

$$\underline{e} = |\underline{Y}| - \underline{x} \tag{21}$$

$$\theta = 3 \frac{(\omega x) \cdot \underline{e}}{(\omega x) \cdot \underline{x}} \tag{22}$$

$$\underline{e}^d = \underline{e} - \frac{\theta \underline{x}}{3} \tag{23}$$

These relations results in force vector state as

$$t\vec{M} = \left(\frac{3}{m}\kappa\theta\underline{\omega}|\vec{\xi}| + \frac{15\mu}{m}\underline{\omega}\underline{e}^d\right)\frac{\vec{\eta} + \vec{\xi}}{|\vec{\eta} + \vec{\xi}|}$$
(24)

As oppose to these relations, [Madenci and Oterkus(2013)] made use of different formulations based on similar decompositions over ordinary state based peridynamics theory. According to [Madenci and Oterkus(2013)], strain energy density and dilatation of a material is given as;

$$W_{(k)} = a\theta_{(k)}^2 + \sum_{j=1}^{N} b\omega_{(k)(j)}((|\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}| - |\vec{\xi}_{(k)(j)}|)V_{(j)}$$
 (25)

$$\theta_{(k)} = d \sum_{j=1}^{N} \frac{|\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}|}{|\vec{\xi}_{(k)(j)}|} \frac{\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}}{|\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}|} \cdot \vec{\xi}_{(k)(j)} V_{(j)}$$
(26)

where the subscript k denotes the hosting material point of a neighborhood in a body and subscript j denotes the  $j^{th}$  neighbor of material point  $x_{(k)}$ . Note that the integrations over the domain are transformed into summations.

This volumetric and distorsional decomposition of the strain energy density is reflected over the force vectors such that,

$$t_{(k)(j)} = \frac{1}{2} A \frac{\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}}{|\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}|}$$
(27)

$$t_{(j)(k)} = -\frac{1}{2}B\frac{\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}}{|\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}|}$$
(28)

$$A = 4\omega_{(k)(j)} \left( d \frac{\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}}{|\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}|} \cdot \frac{\vec{\xi}_{(k)(j)}}{|\vec{\xi}_{(k)(j)}|} a\theta_{(k)} + b \left( |\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}| - |\vec{\xi}_{(k)(j)}| \right) \right)$$
(29)

$$B = 4\omega_{(j)(k)} \left( d \frac{\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}}{|\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}|} \cdot \frac{\vec{\xi}_{(j)(k)}}{|\vec{\xi}_{(j)(k)}|} a\theta_{(j)} + b \left( |\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}| - |\vec{\xi}_{(j)(k)}| \right) \right)$$

$$(30)$$

where, a,d and b are called peridynamic parameters which are yet to be determined based on material properties. For an isotropic material model in three dimensions, these parameters are resolved into;

$$a = \frac{1}{2}(\kappa - \frac{5\mu}{3})\tag{31}$$

$$b = \frac{15\mu}{2\pi\delta^5} \tag{32}$$

$$d = \frac{9}{4\pi\delta^4} \tag{33}$$

The influence scalar state  $\omega_{(k)(j)}$  is also given as;

$$\omega_{(k)(j)} = \frac{\delta}{|\xi_{(k)(j)}|} \tag{34}$$

**Damage Models:** [Silling and Askari(2005)] shows that a critical threshold value for a bond can be determined such that if it stretches beyond that it maybe eliminated. The relation to Grifith's fracture theory as follows for bond based models,

$$s_c = \sqrt{\frac{5G_0}{9\kappa\delta}} \tag{35}$$

where,  $G_0$  is the Critical Energy Release Rate. [Madenci and Oterkus(2013)] also utilizes a similar threshold value deriving for ordinary state based models,

$$s_c = \begin{cases} \sqrt{\frac{G_c}{(3\mu + (\frac{3}{4}^4)(\kappa - \frac{5\mu}{3}))\delta}} & , 3 - D\\ \sqrt{\frac{G_c}{(\frac{6}{\pi}\mu + \frac{16}{9\pi^2}(\kappa - 2\mu))\delta}} & , 2 - D \end{cases}$$

When the critical stretch value is reached, the bond must be eliminated. So, a step function  $\mu(s_{(k)(j)}, t)$  is embedded in 26,29 and 30 such that;

$$\theta_{(k)} = d \sum_{j=1}^{N} \mu_{(k)(j)} \frac{|\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}|}{|\vec{\xi}_{(k)(j)}|} \frac{\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}}{|\vec{\xi}_{(k)(j)} + \vec{\eta}_{(k)(j)}|} \cdot \vec{\xi}_{(k)(j)} V_{(j)}$$

$$A = 4\omega_{(k)(j)} \left( \left( d \frac{\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}}{|\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}|} \cdot \frac{\vec{\xi}_{(k)(j)}}{|\vec{\xi}_{(k)(j)}|} a\theta_{(k)} + b\mu_{(k)(j)} \left( |\vec{\eta}_{(k)(j)} + \vec{\xi}_{(k)(j)}| - |\vec{\xi}_{(k)(j)}| \right) \right)$$

$$(37)$$

$$B = 4\omega_{(j)(k)} \left( d \frac{\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}}{|\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}|} \cdot \frac{\vec{\xi}_{(j)(k)}}{|\vec{\xi}_{(j)(k)}|} a\theta_{(j)} + b\mu_{(k)(j)} \left( |\vec{\eta}_{(j)(k)} + \vec{\xi}_{(j)(k)}| - |\vec{\xi}_{(j)(k)}| \right) \right)$$

$$(38)$$

As the damage progresses in a body, a local damage index notation maybe used to quantify the progression of a crack at a material point  $x_{(k)}$  such that;

$$\varphi(\vec{x_{(k)}}, t) = 1 - \frac{\int_{H} \mu(\vec{\xi}, t) dV}{\int_{H} dV} = 1 - \frac{\sum_{j=1}^{N_{(k)}} \mu_{(k)(j)} dV_{(j)}}{\sum_{j=1}^{N_{(k)}} dV_{(j)}}$$
(39)

**Time Integration:** As suggested in [Littlewood(2015)] explicit time integration with central difference scheme maybe utilized for a transient analysis with peridynamic formulations.

Scheme requires a midstep,  $t^{n+\frac{1}{2}}$ , update on the velocity and displacement of each point. Following to this update, internal forces are computed utilizing the peridynamic constitutive model and resulting acceleration of each point is calculated. Second velocity update is then done using updated velocity and accelerations.

Algorithm is as follows;

- 1. Initalize:  $n = 0, t = 0, \vec{u} = \vec{0}, \vec{a} = \vec{0}$ . Set initial conditions,
- 2. Set:  $\Delta t$ ,
- 3. Calculate:  $t^{n+1} = t^n + \Delta t$ ,  $t^{n+\frac{1}{2}} = \frac{1}{2}(t^n + t^{n+1})$ ,
- 4. Update:  $\vec{v}^{n+\frac{1}{2}} = \vec{v}^n + (t^{n+\frac{1}{2}} t^n)\vec{a}^n$ ,
- 5. Update:  $\vec{u}^{n+1} = \vec{u}^n + \vec{v}^{n+\frac{1}{2}} \Delta t$ ,
- 6. Calculate:  $\vec{f}_{int}^{n+1} = \sum_{j=1}^{N} \left( \vec{t}(\vec{\xi}, \vec{\eta}^{n+1}) \vec{t}'(\vec{\xi}, \vec{\eta}^{n+1}) \right) V_j$ ,
- 7. Calculate:  $\vec{f}^{n+1} = \vec{f}_{int}^{n+1} + \vec{f}_{ext}^{n+1}, \vec{a}^{n+1} = \mathbf{M}^{-1} \vec{f}^{n+1},$
- 8. Update:  $\vec{v}^{n+1} = \vec{v}^{n+\frac{1}{2}} + (t^{n+1} t^{n+\frac{1}{2}})\vec{a}^{n+1}$ ,
- 9. Go to 3.

Since explicit time integration methods are conditionally stable, a stable time step must be set. [Silling and Askari(2005)] showed that such a time step maybe calculated with;

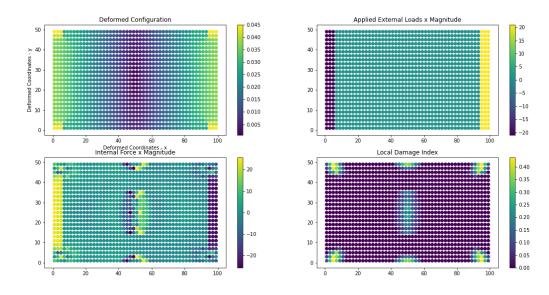
$$\Delta t = \min \sqrt{\frac{2\rho}{\sum_{j=1} C_{ij}^{eff} V_j}} \tag{40}$$

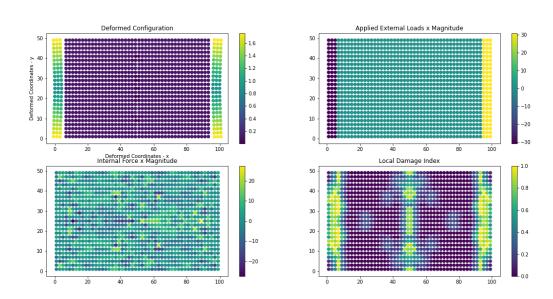
$$C_{ij}^{eff} = \frac{1}{|\vec{\xi}|} \frac{18\kappa}{\pi \delta^4} \tag{41}$$

where an effective modulus  $C_{ij}$  is used as suggested.  $\Delta t$  for all material points are calculated and the minimum is selected as the stable step.

# 4 Example

**Uniaxially Loaded Plate:** As an example case, a plate example is shown below.





#### References

- [Silling and Lehoucq(2010)] S. Silling and R. Lehoucq, "Peridynamic theory of solid mechanics," in Advances in Applied Mechanics, ser. Advances in Applied Mechanics, H. Aref and E. van der Giessen, Eds. Elsevier, 2010, vol. 44, pp. 73–168. [Online]. Available: https://www.sciencedirect.com/science/article/pii/S0065215610440028
- [Madenci and Oterkus(2013)] E. Madenci and E. Oterkus, *Peridynamic Theory and Its Applications*, 06 2013.
- [Silling and Askari(2005)] S. Silling and E. Askari, "A meshfree method based on the peridynamic model of solid mechanics," *Computers & Structures*, vol. 83, no. 17, pp. 1526–1535, 2005, advances in Meshfree Methods. [Online]. Available: https://www.sciencedirect.com/science/article/pii/S0045794905000805
- [Littlewood(2015)] D. J. Littlewood, "Roadmap for peridynamic software implementation," 10 2015. [Online]. Available: https://www.osti.gov/biblio/1226115

#### 5 Code:

```
class Body:
        config1=[
             'Deformation',
             'Velocity',
             'Acceleration',
             'InternalForce',
6
             'ExternalForce'
7
8
        def __init__(self,ConstitutiveModel,ReferenceCoordinates,Volumes,de_
9
10
             self.delta=delta
11
             {\tt self.ReferenceCoordinates=ReferenceCoordinates}
12
            self.Volumes = Volumes
             \verb|self.ConstitutiveModel=ConstitutiveModel|\\
             [self.__setattr__(name,

    zeros(shape=self.ReferenceCoordinates.shape))
                 for name in self.config1
16
17
             self.MaterialPointSetup()
18
             self.MassMatrix = eye(N=len(self.ReferenceCoordinates)) *
19
             \rightarrow self.Volumes * self.ConstitutiveModel.Rho#kg
             self.InverseMassMatrix = inv(self.MassMatrix)
21
        def MaterialPointSetup(self):
22
             self.MaterialPointList = [
23
                 MaterialPointInABody(label, self)
24
                 for label in range(len(self.ReferenceCoordinates))
25
26
27
    class MaterialPoint:
28
        def __init__(self,ReferenceCoordinates):
29
30
             self.ReferenceCoordinates = ReferenceCoordinates
31
    class MaterialPointInABody:
33
        def __init__(self,label,Body):
34
            self.Body = Body
35
            self.label = label
36
            self.ReferenceCoordinates =
37

→ self.Body.ReferenceCoordinates[self.label]

            self.volume = self.Body.Volumes[self.label]
38
            self.GetNeighbors()
39
             self.BondDamageScalars =
40
             \  \, \hookrightarrow \  \, ones ( shape={\tt self.NeighborList.shape,dtype=bool} )
41
42
        def ReferenceRelativePositionVectors(self):
43
             return self.Body.ReferenceCoordinates[self.NeighborList]-self.R
44
             \hookrightarrow eferenceCoordinates
        def DeformedRelativePositionVectors(self):
45
```

```
return self.ReferenceRelativePositionVectors() +

    self.Body.Deformation[self.NeighborList]-self.Deformation()

        def StretchScalars(self):
47
            stretchs=( norm ( self.DeformedRelativePositionVectors(),
            \rightarrow axis=1) - norm(self.ReferenceRelativePositionVectors(),ax
              is=1))/norm(self.ReferenceRelativePositionVectors(),axis=1)
            self.BondDamageScalars = self.BondDamageScalars*
49
            stretchs = stretchs * (self.BondDamageScalars).astype(int)
            return stretchs
        def LambdaScalars(self):
            return (self.ReferenceRelativePositionVectors() *
                self.DeformedRelativePositionVectors()).sum(axis=1) /
                norm(self.ReferenceRelativePositionVectors(),axis=1) /
                norm(self.DeformedRelativePositionVectors(),axis=1)
        def DilatationScalar(self):
54
            return self.Body.ConstitutiveModel.d * self.Body.delta *

→ self.Body.Volumes[self.NeighborList].flatten()).sum()
        def StrainEnergyDensityScalar(self):
            return self.Body.ConstitutiveModel.a *

    self.DilatationScalar()**2 + self.Body.ConstitutiveModel.b

            \rightarrow * (self.Body.delta/norm(self.ReferenceRelativePositionVecto
            \rightarrow rs().axis=1) *
            \hookrightarrow (norm(self.DeformedRelativePositionVectors(),axis=1)-norm(s
            \rightarrow elf.ReferenceRelativePositionVectors(),axis=1))**2*self.Bod

    y.Volumes[self.NeighborList]).sum()

        def DeformedRelativeDeformationDirectionVectors(self):
58
            return self.DeformedRelativePositionVectors()/norm(self.Deforme
            \rightarrow dRelativePositionVectors(),axis=1).reshape((self.DeformedRe
            → lativePositionVectors().shape[0],1))
        def InternalForceScalars(self):
60
            return ( 2 * self.Body.ConstitutiveModel.a *
61

→ self.Body.ConstitutiveModel.d * self.Body.delta *

    self.LambdaScalars() * self.DilatationScalar() /
            → norm(self.ReferenceRelativePositionVectors(),axis=1) + 2 *
               self.Body.ConstitutiveModel.b * self.Body.delta *

    self.StretchScalars())

62
        def InternalForceVectorsHost(self):
            return (self.DeformedRelativeDeformationDirectionVectors() *
            \rightarrow self.InternalForceScalars().reshape((self.InternalForceScal \mid
               ars().shape[0],1)) *
               self.Body.Volumes[self.NeighborList].reshape((self.Body.Vol

    umes[self.NeighborList].shape[0],1)).sum(axis=0)

        def InternalForceVectorsNeighbors(self):
64
            return self.DeformedRelativeDeformationDirectionVectors() *
            \rightarrow self.InternalForceScalars().reshape((self.InternalForceScal
            \rightarrow ars().shape[0],1)) *

→ self.volume

        def UpdateInternalForceVectors(self):
            self.Body.InternalForce[self.label,:] +=

→ self.InternalForceVectorsHost()
            self.Body.InternalForce[self.NeighborList,:] -=

    self.InternalForceVectorsNeighbors()
```

```
69
        def GetNeighbors(self):
70
            self.NeighborList = where(
71
                 (norm(self.ReferenceCoordinates-self.Body.ReferenceCoordina_
72

    tes,axis=1)<=self.Body.delta)
</pre>
                 \rightarrow *(norm(self.ReferenceCoordinates-self.Body.ReferenceCoo_|

    rdinates,axis=1)!=0.)

                )[0]
73
74
        def Deformation(self):
75
            return self.Body.Deformation[self.label]
76
        def LocalDamageIndex(self):
77
            return 1 - (self.Body.Volumes[self.NeighborList].flatten()*self |
78
                .BondDamageScalars.astype(int)).sum() /
             class IsotropicMaterial3D:
79
        def __init__(self,Kappa,Mu,Rho,delta):
80
            self.Kappa = Kappa
81
            self.Mu = Mu
            self.Rho = Rho
            self.a = 1 / 2 * ( Kappa - 5 * Mu / 3)
            self.b = 15 * Mu / 2 / pi / delta**5
85
            self.d = 9 / 4 / pi / delta**4
86
87
    class IsotropicMaterialPlaneStress:
88
        def __init__(self,Kappa,Mu,Rho,delta,thickness,Gc):
89
            self.Kappa = Kappa
90
            self.Mu = Mu
91
            self.Rho = Rho
            self.a = 1 / 2 * (Kappa-2*Mu)
            self.b = 6 * Mu / pi / thickness / delta**4
            self.d = 2 / pi/ thickness / delta**3
            self.delta = delta
96
            self.Gc = Gc
97
            self.sc = self.critical_stretch()
98
        def critical_stretch(self):
99
            return (self.Gc / (6 / pi * self.Mu + 16 / 9 / pi**2 *
100
             101
102
    class ExplicitIntegrator:
        def __init__(self,Body,max_steps=10000):
            self.Body=Body
            self.Time = 0.0
105
            self.step=0
106
            self.max_steps=max_steps
107
            self.SetDeltaTime()
108
        def SetDeltaTime(self):
109
            CTS=1.
110
            for MP in self.Body.MaterialPointList:
111
112
                CpEffs = 18 * self.Body.ConstitutiveModel.Kappa /

→ norm(MP.ReferenceRelativePositionVectors(),axis=1) / pi

                 \rightarrow / self.Body.delta**4
                CTSi = (2*self.Body.ConstitutiveModel.Rho / (CpEffs*self.Bo |
113
                 \rightarrow dy.Volumes[MP.NeighborList]).sum()/1000)**0.5
```

```
if CTSi<CTS:
114
                      CTS=CTSi
115
             self.DeltaTime = CTS*0.7
116
117
         def integrate(self):
118
             Time1Step = self.Time+self.DeltaTime
119
             TimeHalfStep = 0.5*(Time1Step+self.Time)
120
             VelocityHalfStep = self.Body.Velocity +
121

→ self.Body.Acceleration*(TimeHalfStep - self.Time)

             self.Body.Deformation += VelocityHalfStep * self.DeltaTime
122
             self.Body.InternalForce[:,:]=0.
123
             [MP.UpdateInternalForceVectors() for MP in
124
                 \verb|self.Body.MaterialPointList||\\
             self.Body.Acceleration =
125
                 matmul(self.Body.InverseMassMatrix,(self.Body.InternalForce
                 +self.Body.ExternalForce)*self.Body.Volumes)
             self.Body.Velocity = VelocityHalfStep +
126
              \hookrightarrow (Time1Step-TimeHalfStep)*self.Body.Acceleration
             self.Time+=self.DeltaTime
             self.step+=1
     def main func():
130
         Kappa = 140 * 10**9 #Pascal = N/m2
131
         Kappa = Kappa *(1/1000)**2#N/mm2
132
         Mu = 80 * 10**9 #Pascal = N/m2
133
         Mu = Mu *(1/1000)**2#N/mm2
134
         Rho = 8050 \# kg/m3
135
         Rho=Rho*(1/1000)**3#kg/mm3
136
         nu = (1-Mu/Kappa)/(1+Mu/Kappa)
137
         E = Kappa * 2 * (1-nu)
         KIc = 12 \#MPa*m = N/mm2 * m**1/2
139
         GIc = KIc**2*1000/E # N/mm
140
         I = 100.
141
         W=L/2.
142
         t = 3.
143
         dx = 0.5*4
144
         delta = dx*3.1
145
         metal = IsotropicMaterialPlaneStress(Kappa,Mu,Rho,delta,t,GIc)
146
147
         Plate=array([[x,y] for x in arange(dx/2,L+dx/2,dx) for y in
          \rightarrow arange(dx/2,W+dx/2,dx)])
         Volumes = array([[L*W*t/len(Plate)] for i in range(len(Plate))])
         example=Body(metal, Plate, Volumes,delta)
150
         Left_Application = where((Plate[:,0]>=L-3*dx))[0]
         Right_Application = where((Plate[:,0]<=3*dx))[0]</pre>
151
         Total_Applied_Force = 1*W*t
152
         example.ExternalForce[Left_Application,0] =
153
         → Total_Applied_Force/(len(Left_Application))
         example.ExternalForce[Right_Application,0] =
154
         → -Total_Applied_Force/(len(Right_Application))
155
         integrator = ExplicitIntegrator(example)
         return example, integrator, Left_Application, Right_Application, Total_ |
         \hookrightarrow Applied_Force
     if __name__=='__main__':
157
```

```
158
         example,integrator,Left_Application,Right_Application,Total_Applied

    _Force=main_func()

         from matplotlib import pyplot as plt
159
         import pickle
160
         while integrator.step<1500:
161
             integrator.integrate()
162
             if not integrator.step%250:
163
                 print(integrator.step)
164
                  fig,ax = plt.subplots(2,2)
                  fig.set_size_inches(18,9)
                  ax1 = ax[0][0]
                  ax1.set_autoscale_on(False)
168
                  ax1.set_xlim(-5,105)
169
                  ax1.set_ylim(-2.5,52.5)
170
                  im1=ax1.scatter(example.ReferenceCoordinates[:,0] + example_
171
                      .Deformation[:,0],example.ReferenceCoordinates[:,1] +
                      example.Deformation[:,1],c=norm(example.Deformation,axi
                     s=1))
                  fig.colorbar(im1,ax=ax1)
172
                  ax1.set_title('Deformed Configuration')
                  ax1.set_xlabel('Deformed Coordinates - x')
                  ax1.set_ylabel('Deformed Coordinates - y')
175
                  ax2=ax[0][1]
176
                  ax2.set_xlim(-5,105)
177
                  ax2.set_ylim(-2.5,52.5)
178
                  ax2.set_autoscale_on(False)
179
                  im2=ax2.scatter(example.ReferenceCoordinates[:,0],example.R
180

    eferenceCoordinates[:,1],c=example.ExternalForce[:,0])

                  fig.colorbar(im2,ax=ax2)
181
                  ax2.set_title('Applied External Loads x Magnitude')
                  ax3=ax[1][0]
                  ax3.set_xlim(-5,105)
                  ax3.set_ylim(-2.5,52.5)
185
                  ax3.set_autoscale_on(False)
186
                  im3=ax3.scatter(example.ReferenceCoordinates[:,0],example.R
187

    eferenceCoordinates[:,1],c=example.InternalForce[:,0])

                  fig.colorbar(im3,ax=ax3)
188
                  ax3.set_title('Internal Force x Magnitude')
189
                  ax4=ax[1][1]
190
                  ax4.set_xlim(-5,105)
                  ax4.set_ylim(-2.5,52.5)
                  ax4.set_autoscale_on(False)
                  im4=ax4.scatter(example.ReferenceCoordinates[:,0],example.R_{|}
194
                  _{\hookrightarrow} eferenceCoordinates[:,1],c=[i.LocalDamageIndex() for i
                     in example.MaterialPointList])
                  fig.colorbar(im4,ax=ax4)
195
                  im4.colorbar.vmax=1.0
196
                  \verb"im4.colorbar.vmin=0.0"
197
                  ax4.set_title('Local Damage Index')
198
199
                  fig.savefig(f'Madenci_Oterkus_Plate_Example_v4_wFailure{int | 

→ egrator.step}')
                  pickle.dump([example,integrator],open(f'Madenci_Oterkus_Pla |
201

    te_Example_v4_wFailure{integrator.step}','wb'))
```