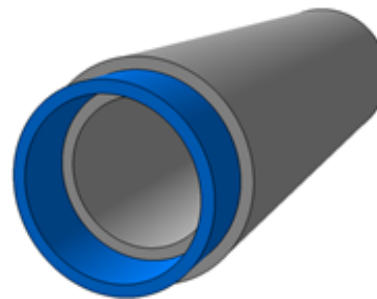
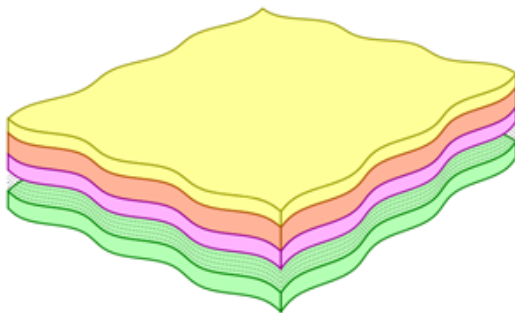


Transient Field Computation in multilayered structures



Time $t \rightarrow$ complex Laplace variable s

Space:

- ▷ material properties invariant with respect to $\mathbf{x} = (x, y)$
- ▷ Horizontal position $\mathbf{x} \rightarrow$ Horizontal wavevector \mathbf{k}
- ▷ Computation in the (\mathbf{k}, z, s) -domain
- ▷ ODEs with respect to the vertical position z

Space:

- ▷ material properties invariant with respect to θ and z
- ▷ Axial position $z \rightarrow$ ax. wavenumber k
- ▷ Azimuthal position $\theta \rightarrow$ az. wavenumber n
- ▷ Computation in the (r, n, k, s) -domain
- ▷ ODEs with respect to the radial position r

Transient Field Computation in multilayered structures

▷ The displacement vector $\tilde{\mathbf{U}}(z)$ satisfies in each plane layer (\mathbf{n} unit vertical vector, \mathbb{I} identity matrix):

$$(\mathbf{n} \diamond \mathbf{n}) \tilde{\mathbf{U}}''(z) - \mathfrak{i} [(\mathbf{n} \diamond \mathbf{k}) + (\mathbf{k} \diamond \mathbf{n})] \tilde{\mathbf{U}}'(z) - [(\mathbf{k} \diamond \mathbf{k}) + \rho s^2 \mathbb{I}] \tilde{\mathbf{U}}(z) = -\tilde{\mathbf{F}}(z) \quad (1)$$

$$\text{Stress vector in the } z\text{-direction: } \tilde{\Sigma}_z(z) = (\mathbf{n} \diamond \mathbf{n}) \tilde{\mathbf{U}}'(z) - \mathfrak{i} (\mathbf{n} \diamond \mathbf{k}) \tilde{\mathbf{U}}(z) \quad (2)$$

▷ The displacement vector $\tilde{\mathbf{U}}(r)$ satisfies in each tubular layer:

$$\begin{aligned} \left[\mathbb{T} = \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \right] & \quad (\mathbf{n}_r \diamond \mathbf{n}_r) \tilde{\mathbf{U}}''(r) + \\ & \quad \left\{ -\mathfrak{i} k (\mathbf{n}_r \diamond \mathbf{n}_z + \mathbf{n}_z \diamond \mathbf{n}_r) + \right. \\ & \quad \left. \frac{1}{r} [(\mathbf{n}_r \diamond \mathbf{n}_r) - \mathfrak{i} ((\mathbf{n}_r \diamond \mathbf{n}_\theta) (n \mathbb{I} + \mathfrak{i} \mathbb{T}) + (n \mathbb{I} + \mathfrak{i} \mathbb{T}) (\mathbf{n}_\theta \diamond \mathbf{n}_r))] \right\} \tilde{\mathbf{U}}'(r) - \\ & \quad \left\{ [\rho s^2 \mathbb{I} + k^2 (\mathbf{n}_z \diamond \mathbf{n}_z)] + \right. \\ & \quad \left. \frac{k}{r} [\mathfrak{i} (\mathbf{n}_r \diamond \mathbf{n}_z) + (n \mathbb{I} + \mathfrak{i} \mathbb{T}) (\mathbf{n}_\theta \diamond \mathbf{n}_z) + (\mathbf{n}_z \diamond \mathbf{n}_\theta) (n \mathbb{I} + \mathfrak{i} \mathbb{T})] + \right. \\ & \quad \left. \frac{1}{r^2} (n \mathbb{I} + \mathfrak{i} \mathbb{T}) (\mathbf{n}_\theta \diamond \mathbf{n}_\theta) (n \mathbb{I} + \mathfrak{i} \mathbb{T}) \right\} \tilde{\mathbf{U}}(r) = -\tilde{\mathbf{F}}(r) \end{aligned} \quad (3)$$

$$\text{Radial stress: } \tilde{\Sigma}_r(r) = (\mathbf{n}_r \diamond \mathbf{n}_r) \tilde{\mathbf{U}}'(r) - \mathfrak{i} \left[\frac{1}{r} (\mathbf{n}_r \diamond \mathbf{n}_\theta) (n \mathbb{I} + \mathfrak{i} \mathbb{T}) + k (\mathbf{n}_r \diamond \mathbf{n}_z) \right] \tilde{\mathbf{U}}(r) \quad (4)$$

Transient Field Computation in multilayered structures

Exact solutions of Eq. (1) without volumic source in each plane layer: $\forall z, z_{\beta-1} < z < z_{\beta}$, six partial waves:

$$\tilde{\mathbf{U}}(z) = \underbrace{\sum_{i=1}^3 a_{\beta,i} \exp[-\mathfrak{i} \kappa_{\beta,i} (z - z_{\beta})] \mathbf{p}_{\beta,i}}_{\text{upgoing waves}} + \underbrace{\sum_{i=4}^6 a_{\beta,i} \exp[-\mathfrak{i} \kappa_{\beta,i} (z - z_{\beta-1})] \mathbf{p}_{\beta,i}}_{\text{downgoing waves}} . \quad (5)$$

(General anisotropy)

Sources at interfaces:

$$\Delta \tilde{\mathbf{U}}(z_{\beta}) = \boldsymbol{\Phi}_{\beta} \quad \text{or/and} \quad \Delta \tilde{\boldsymbol{\Sigma}}_z(z_{\beta}) = \boldsymbol{\Psi}_{\beta} \quad (6)$$

Exact solutions of Eq. (3) without volumic source in each tubular layer: $\forall r, r_{\beta-1} < r < r_{\beta}$, six partial waves:

$$\tilde{\mathbf{U}}(r) = \underbrace{\sum_{i=1}^3 a_{\beta,i} \mathbf{I}_{n,\beta,i}(\eta_{\beta,i} r)}_{\text{ingoing waves}} + \underbrace{\sum_{i=4}^6 a_{\beta,i} \mathbf{K}_{n,\beta,i}(\eta_{\beta,i} r)}_{\text{outgoing waves}} . \quad (7)$$

(functions including modified Bessel functions and normalization by exponentials)

(Limitation: transversely isotropy with axial symmetry)

Sources at interfaces:

$$\Delta \tilde{\mathbf{U}}(r_{\beta}) = \boldsymbol{\Phi}_{\beta} \quad \text{or/and} \quad \Delta \tilde{\boldsymbol{\Sigma}}_r(r_{\beta}) = \boldsymbol{\Psi}_{\beta} \quad (8)$$

Transient Field Computation in multilayered structures

Some considerations on computation

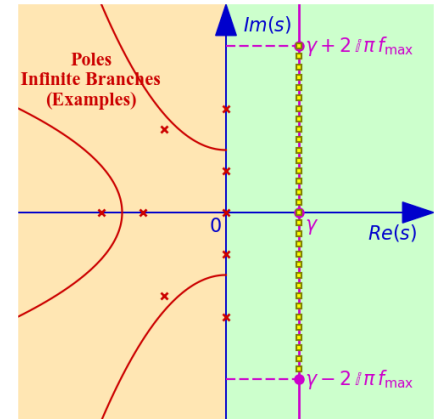
LAPLACE transform: $H(s) = \int_0^\infty h(t) e^{-st} dt$.

Bromwich-Mellin Formula:

$$\forall \gamma > 0, h(t) = e^{\gamma t} \int_{-\infty}^{+\infty} H(\gamma + 2i\pi f) e^{2i\pi f t} df. \quad (9)$$

$f \mapsto H(\gamma + 2i\pi f)$ is the Fourier Transform of the signal $t \mapsto h(t) e^{-\gamma t}$.

1d time grid: $t_m = m \delta t$, $0 \leq m < 2 N_t$, duration $d = 2 N_t \delta t$



The *FFT* can be used while both the Nyquist-Shannon criterion and its dual are satisfied: [Cooley & Tukey, 1965], [Phinney, 1965]

- Band-limited spectrum: $\forall f > f_{\max} = \frac{1}{2\delta t}$, $H(\gamma + 2i\pi f) \approx 0$
- Finite duration: $\forall t, t \notin [0, d[$, $h(t) e^{-\gamma t} \approx 0$

Transient Field Computation in multilayered structures

Some considerations on computation

2d space grid:

$$\left\{ \begin{array}{l} x_i = i \delta x, \quad -N_x < i \leq N_x, \quad \text{Period: } 2 N_x \delta x ; \\ y_j = j \delta y, \quad -N_y < j \leq N_y, \quad \text{Period: } 2 N_y \delta y . \end{array} \right. \Longleftrightarrow \left\{ \begin{array}{l} k_{xi} = i \delta k_x, \quad -N_x < i \leq N_x, \quad k_{x \max} = \pi / \delta x ; \\ k_{yj} = j \delta k_y, \quad -N_y < j \leq N_y, \quad k_{y \max} = \pi / \delta y . \end{array} \right.$$

or

$$\left\{ \begin{array}{l} \theta_i = i / (\pi N_\theta), \quad -N_\theta < i \leq N_\theta, \quad \text{Period: } 2 \pi ; \\ z_j = j \delta z, \quad -N_z < j \leq N_z, \quad \text{Period: } 2 N_z \delta z . \end{array} \right. \Longleftrightarrow \left\{ \begin{array}{l} n, \quad -N_\theta < n \leq N_\theta ; \\ k_{zj} = j \delta k_z, \quad -N_z < j \leq N_z, \quad k_{z \max} = \pi / \delta z . \end{array} \right.$$

Massively Parallel Computation

Diffraction by a Delamination

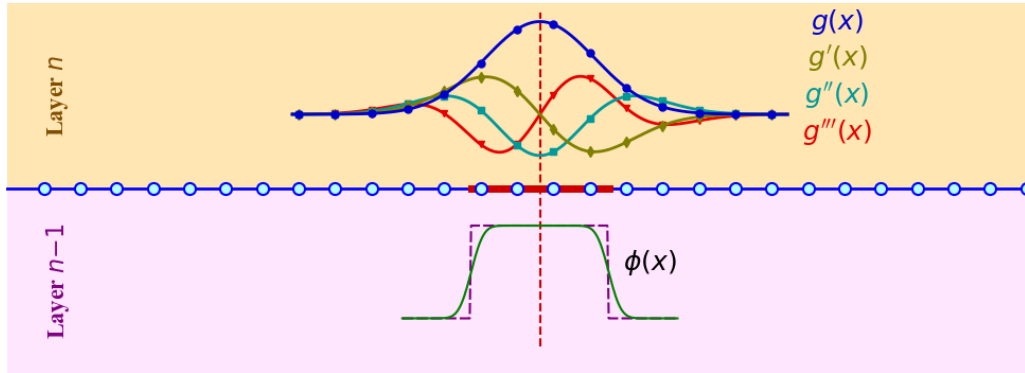


Figure 1: A 2D defect between two layers The ϕ function describing the defect is here the indicator function $\mathbb{1}_{\mathcal{D}}$, **smoothed** or **not**.

Incident field (vertical stress) on the interface (at $z = z_I$): $\sigma_z^{[\text{inc}]}(\mathbf{x}, s)$

Diffracted field (vertical stress) on the interface: $\sigma_z^{[\text{dif}]}(\mathbf{x}, s) = \int \mathcal{G}(\mathbf{x} - \boldsymbol{\xi}, s) \Delta \mathbf{u}(\boldsymbol{\xi}, s) d\boldsymbol{\xi}$

Equation to be solved: $\forall \mathbf{x} \in \mathcal{D}$, $\sigma_z(\mathbf{x}, s) = \sigma_z^{[\text{inc}]}(\mathbf{x}, s) + \sigma_z^{[\text{dif}]}(\mathbf{x}, s) = \mathbf{0}$

Numerically, we want to minimize: $\int \sigma_z(\mathbf{x}, s) \cdot \sigma_z(\mathbf{x}, s)^* \phi(\mathbf{x}) d\mathbf{x}$

Diffraction by a Delamination

An inner product associated to the defect shape

The Shannon's interpolation formula: $\mathbf{u}(\mathbf{x}) = \sum_n \text{sc}(\mathbf{x} - \mathbf{x}_n) \mathbf{u}_n$, where $\mathbf{u}_n = \mathbf{u}(\mathbf{x}_n)$, $\text{sc}(x) = \sin(\pi x / \delta x) \delta x / (\pi x)$ (2D), and $\text{sc}[(x, y)] = \sin(\pi x / \delta x) \sin(\pi y / \delta y) \delta x \delta y / (\pi^2 x y)$ (3D).

We can define a *positive semi-definite inner product*^a of 2 discretized fields:

$$\begin{aligned} \langle \mathbf{u}, \mathbf{v} \rangle &= \int \mathbf{u}(\mathbf{x}) \cdot \mathbf{v}(\mathbf{x})^* \phi(\mathbf{x}) \, d\mathbf{x} = \sum_{n,m} \left[\int \text{sc}(\mathbf{x} - \mathbf{x}_n) \text{sc}(\mathbf{x} - \mathbf{x}_m) \phi(\mathbf{x}) \, d\mathbf{x} \right] (\mathbf{u}_n \cdot \mathbf{v}_m^*) = \mathbf{u} \cdot (\mathcal{A} \mathbf{v}^*) \\ &= (\mathcal{R} \mathbf{u}) \cdot (\mathcal{R} \mathbf{v}^*) . \end{aligned} \quad (10)$$

The inner product $\langle \bullet, \bullet \rangle$ is completely characterized by the \mathcal{R} matrix which is substantially less expensive to store than the \mathcal{A} matrix ($r \times N$ against N^2 without using sparse matrix storage).

^a (i) $\langle \mathbf{u}, \mathbf{v} \rangle = \langle \mathbf{v}, \mathbf{u} \rangle$; (ii) $\langle \alpha \mathbf{u}_1 + \beta \mathbf{u}_2, \mathbf{v} \rangle = \alpha \langle \mathbf{u}_1, \mathbf{v} \rangle + \beta \langle \mathbf{u}_2, \mathbf{v} \rangle$; (iii) $\langle \mathbf{u}, \mathbf{u} \rangle \geq 0$; but $\langle \mathbf{u}, \mathbf{u} \rangle = 0 \not\Rightarrow \mathbf{u} = \mathbf{0}$.

Diffraction by a Delamination

An inner product associated to the defect shape

$$\langle \mathbf{u}, \mathbf{v} \rangle = (\mathcal{R} \mathbf{u}) \cdot (\mathcal{R} \mathbf{v}^*) .$$

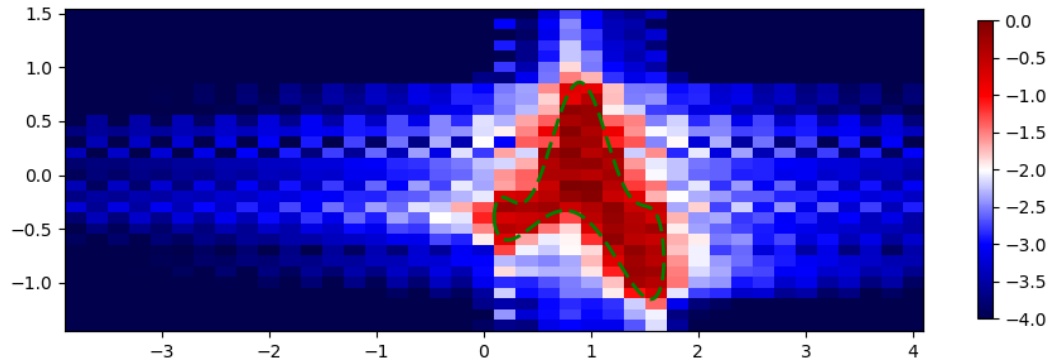


Figure 2: Map of $2 \log_{10} [(\max_{\ell} |r_{\ell ij}|)_{i,j} / \max_{\ell ij} |\mathcal{R}|]$. The dashed line is the boundary of the defect.

Diffraction by a Delamination

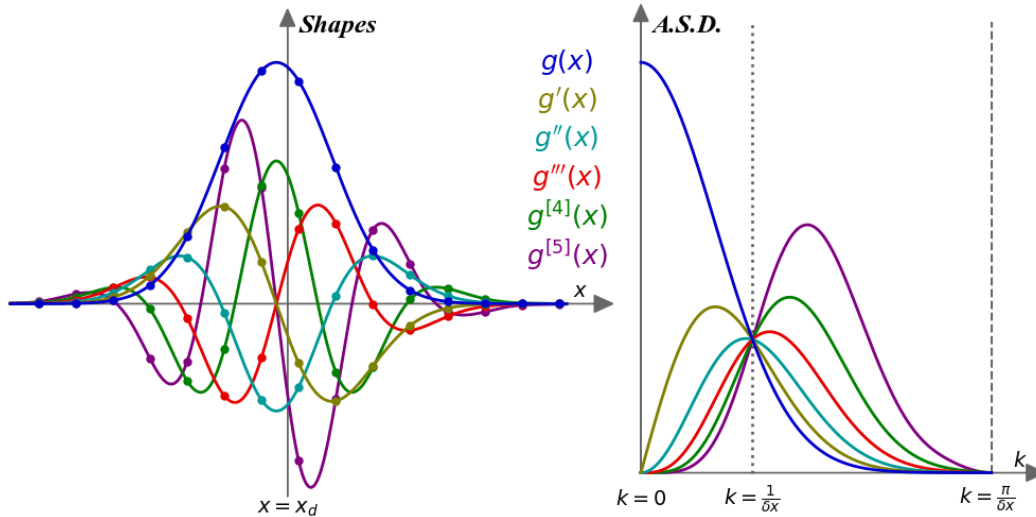
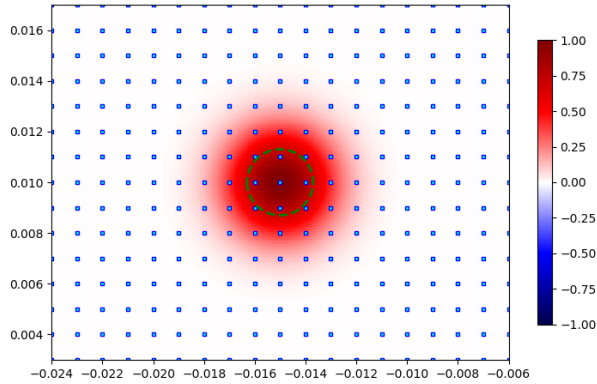


Figure 3: The Gaussian shape $x \mapsto \exp\left\{-2 \left[(x - x_d)/\delta x\right]^2 / 9\right\}$ and its derivatives, which corresponds to approximations of the Dirac delta function and its derivatives, satisfying the Nyquist-Shannon Criterion (wavenumbers less than $\pi/\delta x$, where δx denotes the discretization step). x and k denote the position and the wavenumber, respectively.



(a) Gaussian shape, defect and grid.

Radius: $1.3\delta x$

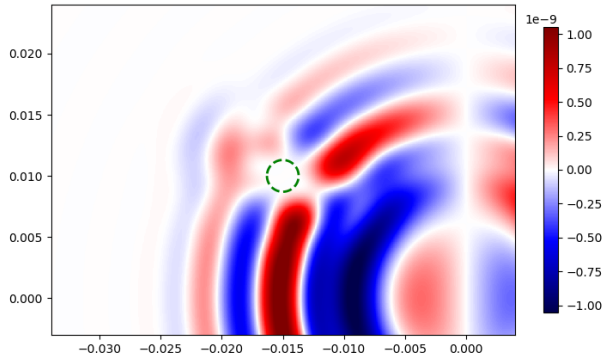
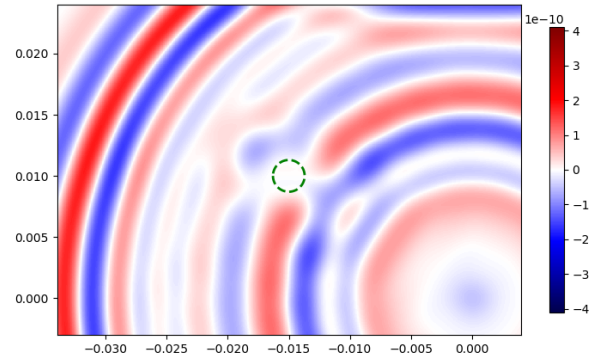
Number of nodes in the defect: 5

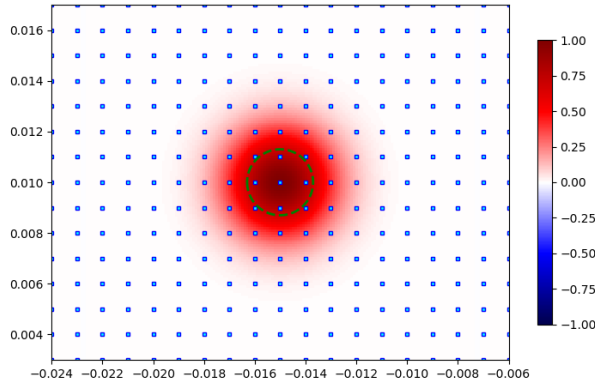
Number of lines in the \mathcal{R} matrix: 19

Degrees of freedom: $57 = 19 \times 3$

Size of the basis: $30 = 3 \times (1 + 2 + 3 + 4)$

Derivatives of orders 1 to 3

(b) Total field $\sigma_{xz}(x, y, z, t)$.(c) Total field $\sigma_{zz}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Radius: $1.3\delta x$

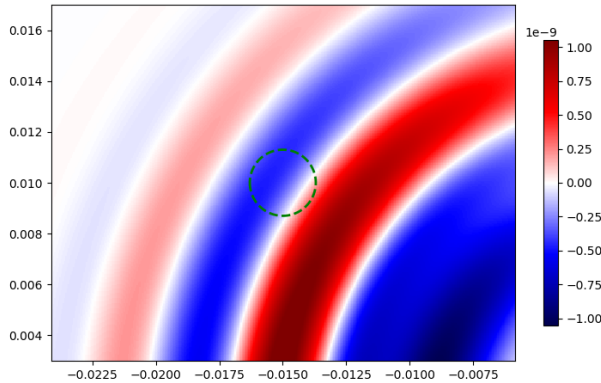
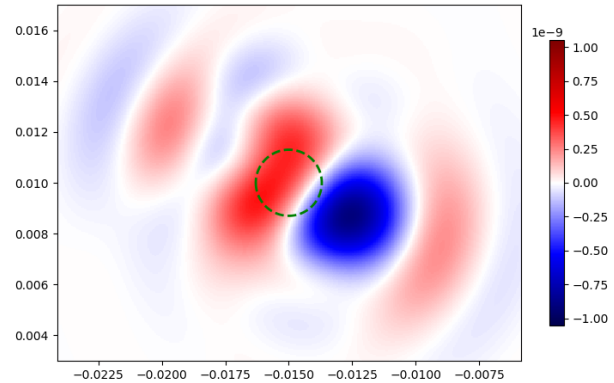
Number of nodes in the defect: 5

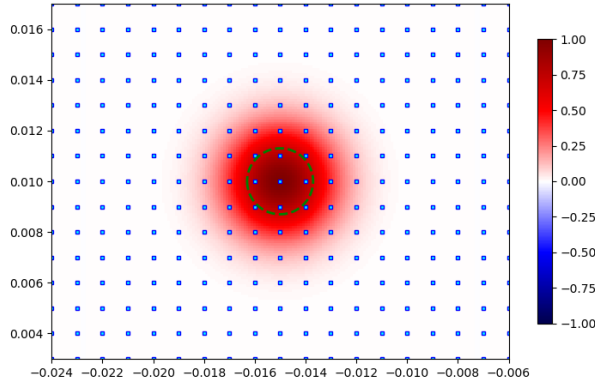
Number of lines in the \mathcal{R} matrix: 19

Degrees of freedom: $57 = 19 \times 3$

Size of the basis: $30 = 3 \times (1 + 2 + 3 + 4)$

Derivatives of orders 1 to 3

(d) Incident field $\sigma_{xz}^{[\text{inc}]}(x, y, z, t)$.(e) Diffracted field $\sigma_{xz}^{[\text{dif}]}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Radius: $1.3 \delta x$

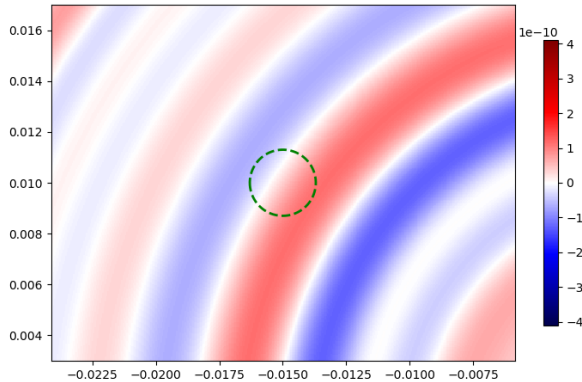
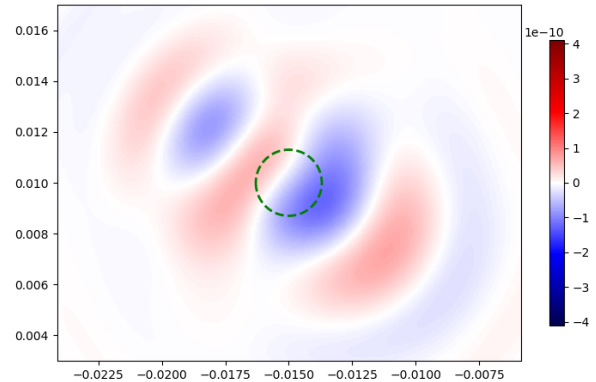
Number of nodes in the defect: 5

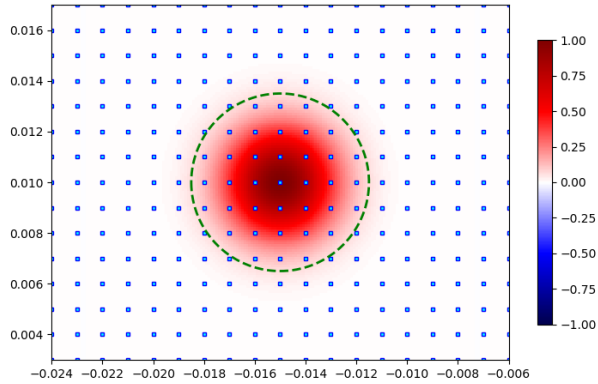
Number of lines in the \mathcal{R} matrix: 19

Degrees of freedom: $57 = 19 \times 3$

Size of the basis: $30 = 3 \times (1 + 2 + 3 + 4)$

Derivatives of orders 1 to 3

(f) Incident field $\sigma_{zz}^{[\text{inc}]}(x, y, z, t)$.(g) Diffracted field $\sigma_{zz}^{[\text{dif}]}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Radius: $3.5 \delta x$

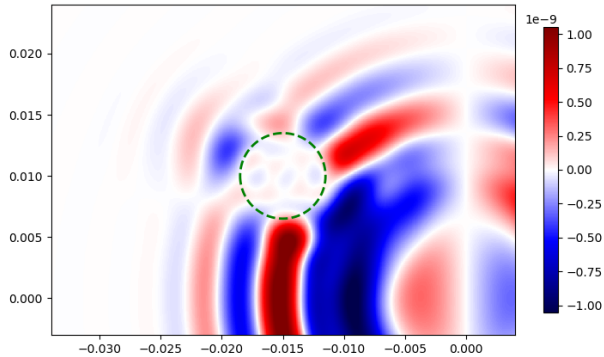
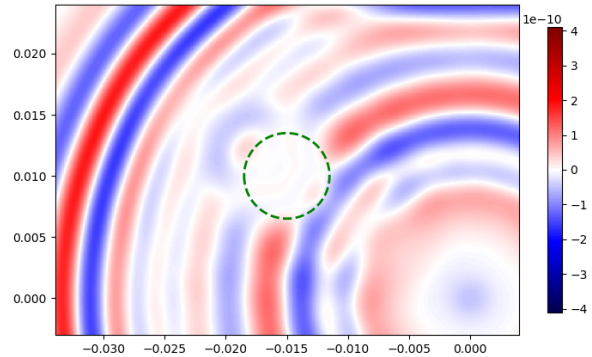
Number of nodes in the defect: 37

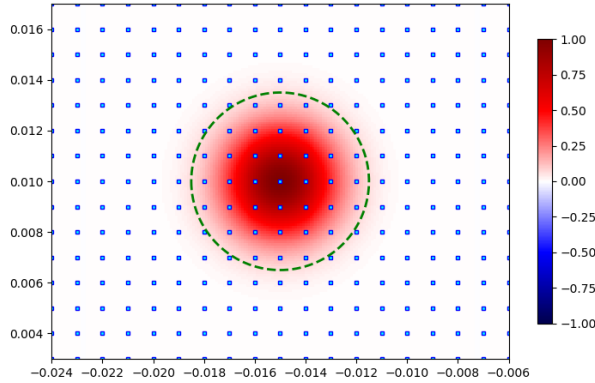
Number of lines in the \mathcal{R} matrix: 80

Degrees of freedom: $240 = 80 \times 3$

Size of the basis: $63 = 3 \times (1 + 2 + 3 + 4 + 5 + 6)$

Derivatives of orders 1 to 5

(b) Total field $\sigma_{xz}(x, y, z, t)$.(c) Total field $\sigma_{zz}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Radius: $3.5 \delta x$

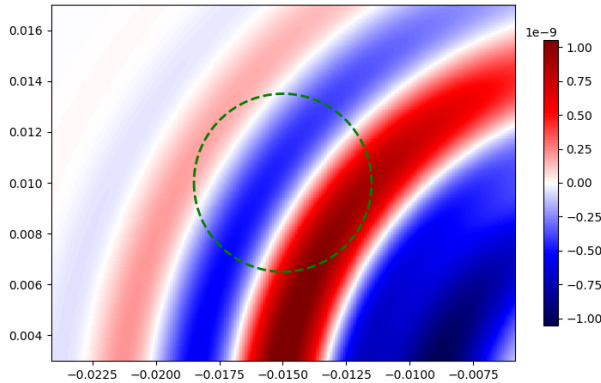
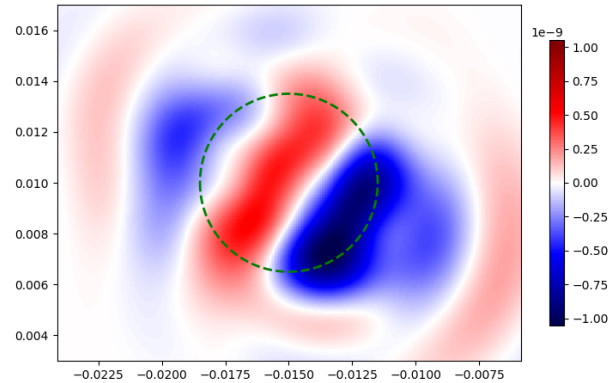
Number of nodes in the defect: 37

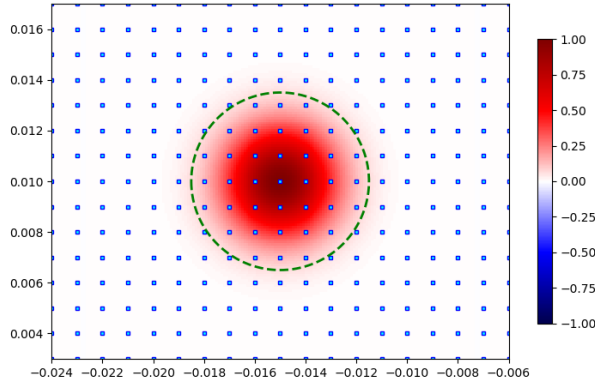
Number of lines in the \mathcal{R} matrix: 80

Degrees of freedom: $240 = 80 \times 3$

Size of the basis: $63 = 3 \times (1 + 2 + 3 + 4 + 5 + 6)$

Derivatives of orders 1 to 5

(d) Incident field $\sigma_{xz}^{[\text{inc}]}(x, y, z, t)$.(e) Diffracted field $\sigma_{xz}^{[\text{dif}]}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Radius: $3.5 \delta x$

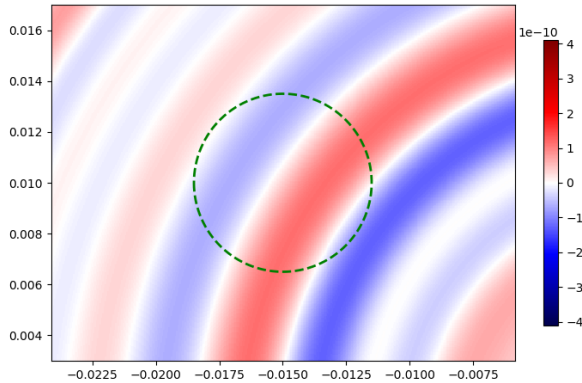
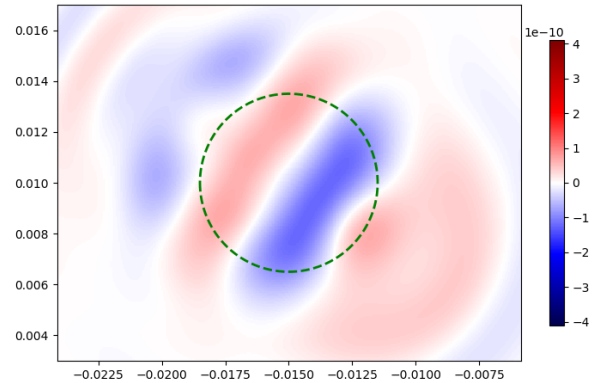
Number of nodes in the defect: 37

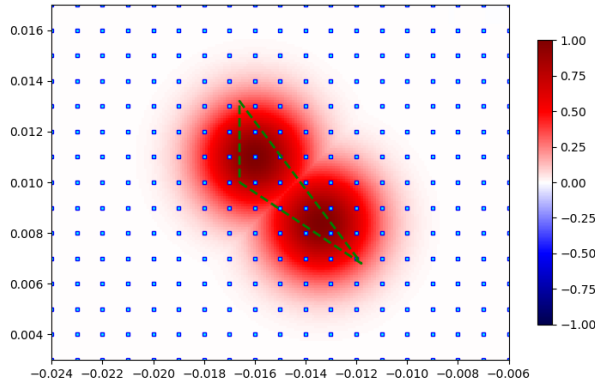
Number of lines in the \mathcal{R} matrix: 80

Degrees of freedom: $240 = 80 \times 3$

Size of the basis: $63 = 3 \times (1 + 2 + 3 + 4 + 5 + 6)$

Derivatives of orders 1 to 5

(f) Incident field $\sigma_{zz}^{[\text{inc}]}(x, y, z, t)$.(g) Diffracted field $\sigma_{zz}^{[\text{dif}]}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Triangular Defect, 2 Gaussians Number of nodes

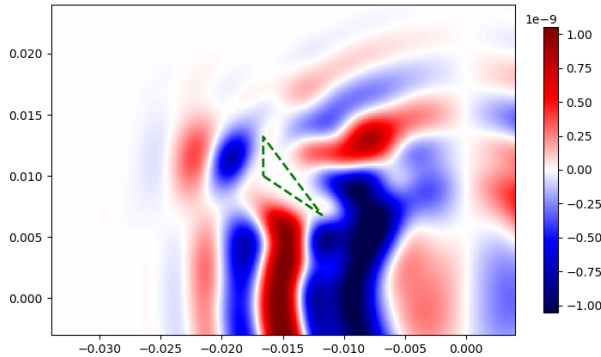
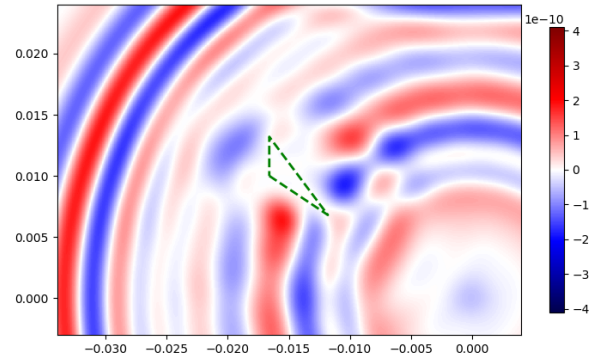
in the defect: 9

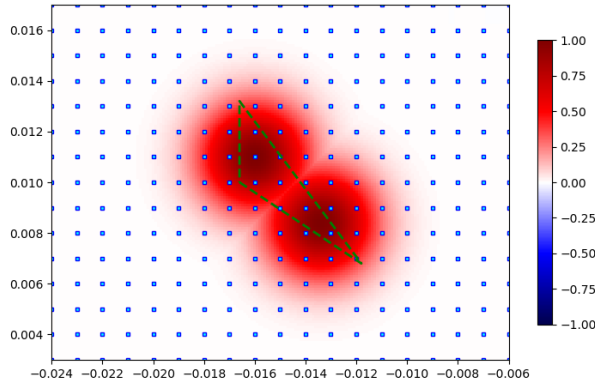
Number of lines in the \mathcal{R} matrix: 30

Degrees of freedom: $90 = 30 \times 3$

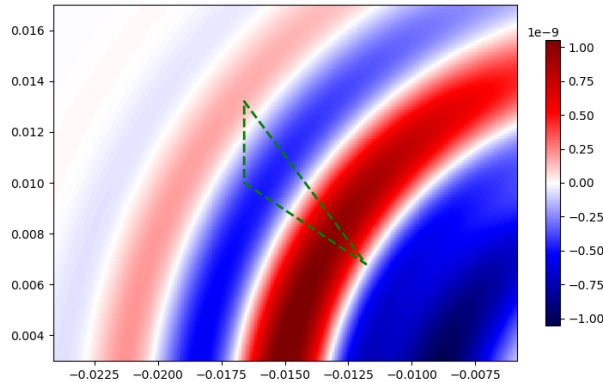
Size of the basis: $60 = 2 \times [3 \times (1 + 2 + 3 + 4)]$

Derivatives of orders 1 to 3

(b) Total field $\sigma_{xz}(x, y, z, t)$.(c) Total field $\sigma_{zz}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

(d) Incident field $\sigma_{xz}^{[\text{inc}]}(x, y, z, t)$.

Triangular Defect, 2 Gaussians Number of nodes

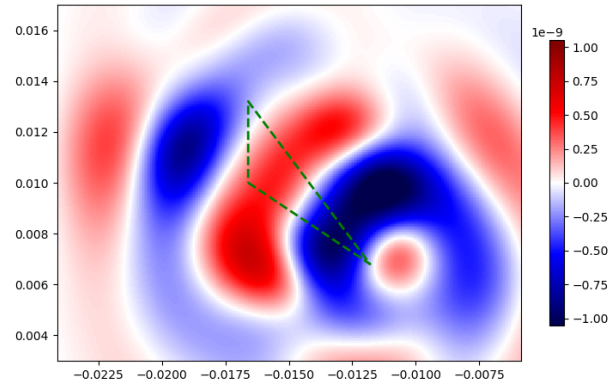
in the defect: 9

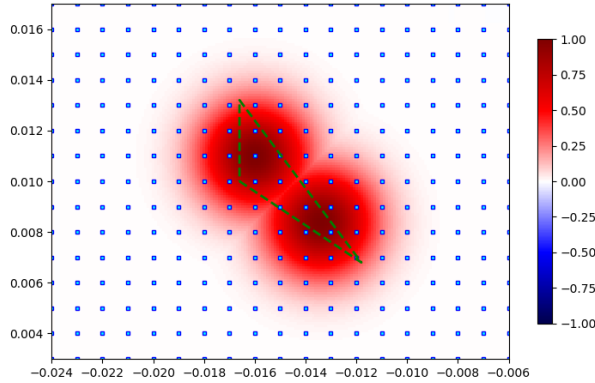
Number of lines in the \mathcal{R} matrix: 30

Degrees of freedom: $90 = 30 \times 3$

Size of the basis: $60 = 2 \times [3 \times (1 + 2 + 3 + 4)]$

Derivatives of orders 1 to 3

(e) Diffracted field $\sigma_{xz}^{[\text{dif}]}(x, y, z, t)$.



(a) Gaussian shape, defect and grid.

Triangular Defect, 2 Gaussians Number of nodes

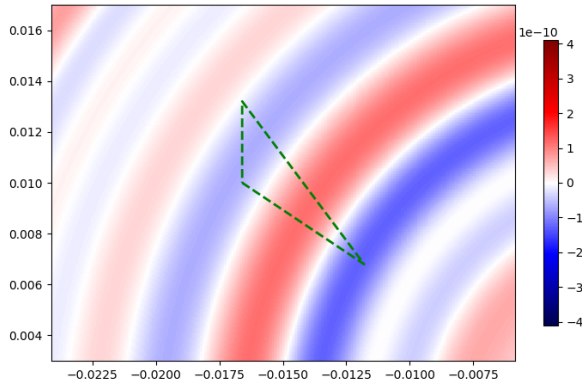
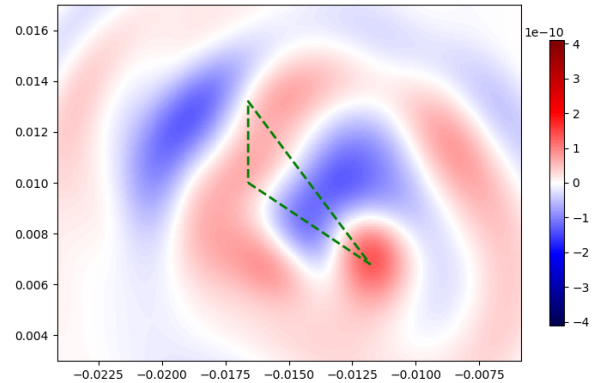
in the defect: 9

Number of lines in the \mathcal{R} matrix: 30

Degrees of freedom: $90 = 30 \times 3$

Size of the basis: $60 = 2 \times [3 \times (1 + 2 + 3 + 4)]$

Derivatives of orders 1 to 3

(f) Incident field $\sigma_{zz}^{[\text{inc}]}(x, y, z, t)$.(g) Diffracted field $\sigma_{zz}^{[\text{dif}]}(x, y, z, t)$.

Hybrid computation: example of a stiffener

