

1. A turbine stage with a mass flow rate 25 kg/s, has equal inlet and outlet velocities at the mean radius and the following design data

Inlet temperature $T_{o1}$	850 K	Axial velocity (const through stage) $c_z$	300 m/s
Inlet pressure $p_{o1}$	400 kPa	Blade speed $U_m$	420 m/s
Nozzle efflux angle $\alpha_2$	60°	Stage exit swirl $\alpha_3$	-15°

- (a) Determine the rotor blade gas angles ( $\beta_{2,3}$ ) degree of reaction, blade loading coefficient  $\psi$ , and power output.
- (b) Assuming a nozzle loss coefficient  $\lambda_n$  of 0.05, calculate the nozzle throat area required ignoring the effect of boundary layers.

Methodology Steps for part (b):

1. First determine if the Mach number at station 2 (at the exit to the stator/nozzle) is supersonic. If it is, the nozzle is shaped like a CD nozzle and you have to find the nozzle throat area. The throat area is determined from  $A_t = \dot{m} / (\rho_t c_t)$ , where  $c_t$  is the throat velocity. In this step, T2 is calculated using total enthalpy conservation from station 1 to 2.
2. From the nozzle loss coefficient, calculate T2s (the temperature that would be reached isentropically). Given, P01, T01 and T2s, calculate, P2.
3. State 1 properties can be calculated from using enthalpy equation and pressure temperature isentropic relation.
4. Since State 1 properties and State 2 properties are known, determine the polytropic efficiency from the pressure temperature relationship involving polytropic efficiency.
5. Once polytropic efficiency is known the same calculation in step 4 can be done from State 1 to the throat of the nozzle.
6. Nozzle loss coefficient is given by

$$T_2 - T_{2s} = \frac{\lambda_n c_2^2}{2c_{ph}}$$

7. Also, assume  $\gamma = 1.33$ ,  $C_{ph} = 1148 \frac{J}{(K.kg)}$  (However, if you have already solved the problem using standard  $\gamma = 1.4$ ,  $C_{ph} = 1005 \frac{J}{(K.kg)}$ , the solution will be graded without any loss in credit.

2. An axial flow turbine stage has a free-vortex design and the following data:

Inlet stagnation temperature, $T_{o1}$	1500 K	Inlet stagnation pressure, $p_{o1}$	850 kPa
No swirl at exit, exit velocity, $c_3$	180 m/s	Degree of reaction at mean radius, $R'_m$	0.5
Nozzle loss coefficient, $\lambda_n$	0.04	Turbine adiabatic efficiency	0.93
Hub-to-tip ratio, $\zeta = r_h/r_t$	0.6	Flow coefficient, $c_z/U_m$	0.6

Calculate:

- (a) the stagnation pressure ratio across the stage;
- (b) the static pressures  $p_1$ ,  $p_2$  at the mean radius;

- (c) the angles  $\beta_{2t}$ ,  $\beta_{3t}$  and degree of reaction  $R'_t$  at the tip. Sketch the velocity triangles at the blade tip.
- (d) the angles  $\beta_{2h}$ ,  $\beta_{3h}$  and degree of reaction  $R'_h$  at the root (hub). Sketch the velocity triangles at the root of the blades.