Sparse polynomial surrogates for non-intrusive, high-dimensional uncertainty quantification of aerodynamic and aeroelastic computations

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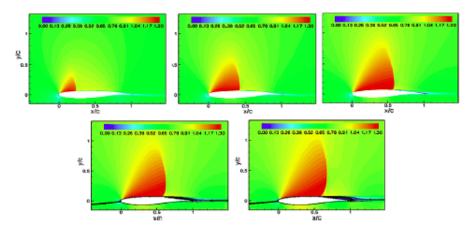
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Some motivations...



Mach number isocontour fields with 5 different inflow Mach number conditions ($\underline{M}_{\infty}=0.73$) for an OAT15A profile: $0.92 \times \underline{M}_{\infty}$, $0.96 \times \underline{M}_{\infty}$, \underline{M}_{∞} , $1.04 \times \underline{M}_{\infty}$, $1.08 \times \underline{M}_{\infty}$.

Simon-Guillen-Sagaut-Lucor, Comput. Methods Appl. Mech. Engng. 199, 1091 (2010)

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Overview

Background on UQ in CFD

Sparse reconstruction

3 Application to BC-02: RAE2822 transonic airfoil (2D)

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Uncertainty Quantification in CFD – Model problem

• A generic computational model g involving d parameters $\boldsymbol{\xi} = (\xi_1, \xi_2, \dots, \xi_d) \in \mathbb{R}^d$:

$$\mathcal{Y} \ni y = g(\xi_1, \xi_2, \dots \xi_d)$$
.

• A polynomial surrogate model g_N of order N:

$$g pprox g_{\textit{N}}(\emph{\textbf{x}}) = \arg\min_{\pi \in \mathbb{P}^{\textit{P}}[\emph{\textbf{x}}]} rac{1}{2} \int_{\mathbb{R}^d} |g(\emph{\textbf{x}}) - \pi(\emph{\textbf{x}})|^2 \mathcal{P}_{\Xi}(\mathrm{d}\emph{\textbf{x}}) \,,$$

of which desired "convergence" $\mathbb{E}\{|g_N(\xi)-g(\xi)|^2\}\to 0$ as $N\to\infty$ depends on \mathcal{P}_Ξ (and does not necessarily hold).

• Embedded projection (spectral stochastic finite elements), non-intrusive projection, "collocation", kriging, regression...

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Non-intrusive UQ - Polynomial chaos (projection)

• Assume a (truncated) orthonormal basis $\mathcal{B}^N \equiv \{\psi_\alpha\}_{\alpha=0}^N$ of $L^2(\Omega, \mathcal{P}_\Xi)$ is available, s.t.:

$$\int_{\mathbb{R}^d} \psi_{\alpha}(\mathbf{x}) \psi_{\beta}(\mathbf{x}) \mathcal{P}_{\Xi}(\mathrm{d}\mathbf{x}) = (\psi_{\alpha}, \psi_{\beta})_{L^2} = \delta_{\alpha\beta} \,.$$

- Then $g_N = \sum_{\alpha=0}^N g_\alpha \psi_\alpha$ where $g_\alpha = (g, \psi_\alpha)_{12}, 0 \le \alpha \le N$.
- But using the quadrature Θ^M , $g_N \simeq \sum_{\alpha=0}^N g_\alpha^M \psi_\alpha$ with:

$$g_{\alpha}^{M} = \sum_{\ell=1}^{M} \omega_{\ell} y_{\ell} \psi_{\alpha}(\xi_{\ell}), \quad 0 \leq \alpha \leq N.$$

• Remark: $\mathcal{P}_{\Xi} = \otimes_{i=1}^{d} \mathcal{N}(0,1)$ is called polynomial chaos (PC), and generalized polynomial chaos (gPC) otherwise.

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Non-intrusive UQ - Outcome

- Therefore we need:
 - **4** a quadrature rule in \mathbb{R}^d : $\mathbf{\Theta}^M \equiv \{\boldsymbol{\xi}_\ell, \omega_\ell\}_{\ell=1}^M$;

 - a to perform repeated evaluations $\{y_\ell = g(\xi_\ell)\}_{\ell=1}^{M}$:
 to assess the accuracy of g_N (UQ-surrogate) independently of the accuracy of g (CFD solver).
- **Problem**: $M \gg 1$, and even $M \gg 100$, which is often unaffordable (and actually useless).

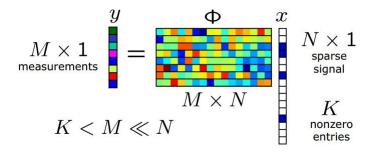
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Compressed sensing



Candès-Romberg-Tao Commun. Pure Appl. Math. **59**(8), 1207 (2006) Donoho IEEE Trans. Inform. Theory **52**(4), 1289 (2006)

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Sparse reconstruction techniques - Principle

• Sparse polynomial decompositions via convex ℓ_1 -minimization (Basis Pursuit Denoising, Chen-Donoho-Saunders 1998) whenever $M \ll N$ and only few coefficients g_{α} are non zero:

$$\mathbf{g}^{\star} = \arg\min_{\mathbf{g} \in \mathbb{R}^{N}} \{ \| \mathbf{W} \mathbf{g} \|_{1}; \ \| \mathbf{y} - \Phi \mathbf{g} \|_{2} \le \varepsilon \}. \tag{$P_{1,\varepsilon}$}$$

• Here **W** is some weighting, $\mathbf{g} = (g_0, g_1, \dots g_N)^\mathsf{T}$,

$$[\mathbf{\Phi}]_{\ell\alpha} = \psi_{\alpha}(\boldsymbol{\xi}_{\ell}),$$

and the sampling points $\{\xi_\ell\}_{\ell=1}^M$ should be selected s.t. the Vandermonde-type measurement matrix Φ has maximum incoherence.

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Definition (Coherence)

$$\mu(\boldsymbol{\Theta}^{M}, \mathcal{B}^{N}) = \max_{\substack{\mathbf{0} \leq \alpha \leq N \\ \mathbf{1} \leq \ell \leq M}} |\psi_{\alpha}(\boldsymbol{\xi}_{\ell})|^{2}.$$

Theorem (1)

Assume g_N is K-sparse on the gPC basis \mathcal{B}^N . Then if M measurements $\{\xi_\ell\}_{\ell=1}^M$ are selected at random, and:

$$M \geq C \cdot \mu(\boldsymbol{\Theta}^{M}, \mathcal{B}^{N}) \cdot K \cdot \log N$$

for some C > 0, the solution to $(P_{1,0})$ is exact with overwhelming (sic) probability.

Remark: as a rule of thumb, $M \ge 4K$ is enough for a successful recovery.

Definition (Restricted isometry constant)

The smallest number $\delta_{\mathcal{K}} < 1$ s.t.:

$$(1 - \delta_K) \|\mathbf{g}_K\|_2^2 \le \|\mathbf{\Phi}\mathbf{g}_K\|_2^2 \le (1 + \delta_K) \|\mathbf{g}_K\|_2^2$$

for all K-sparse vectors $\mathbf{g}_K \in \mathcal{X}_K := \{\mathbf{g} \in \mathbb{R}^N; \ \|\mathbf{g}\|_0 \le K\}.$

Theorem (2)

Assume $\delta_{2K} < \sqrt{2} - 1$. Then the solution \mathbf{g}^{\star} to $(P_{1,\varepsilon})$ satisfies:

$$\|\mathbf{g}^{\star} - \mathbf{g}\|_{2} \leq C_{0} \frac{\|\mathbf{g}_{\kappa} - \mathbf{g}\|_{1}}{\sqrt{\kappa}} + C_{1}\varepsilon$$

for some $C_0,\,C_1>0$ depending only on $\delta_{2K}.$

Remark: the theorem allows to deal with imprecise measurements $\varepsilon > 0$ and approximately sparse vectors.

Overview

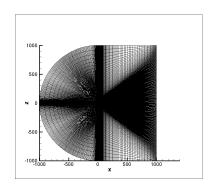
Background on UQ in CFD

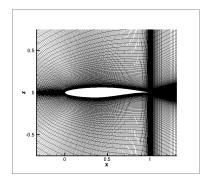
Sparse reconstruction

3 Application to BC-02: RAE2822 transonic airfoil (2D)

Numerical model

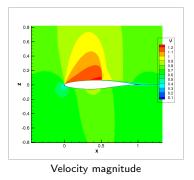
• RANS + Spalart-Allmaras model, $769c \times 193c$ mesh:

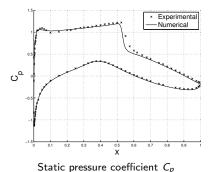




- Multigrid approach for the NS system over 3 grid levels with 2 iterations on the coarse grid and 1 fine level iteration for the turbulent equation.
- 2000 iterations with Roe flux and 2nd order MUSCL scheme for the convective term of the NS system.

Cambier-Heib-Plot Mechanics & Industry 14(3), 159 (2013)





- Shock wave well captured, good agreement with experiments (AGARD Report #AR-138 1979, NPARC Alliance Validation Archive 1998).
- Typical computational time: 2 hours.

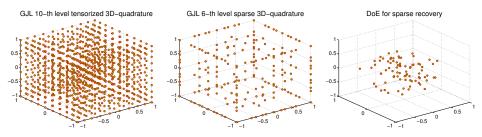
Definition of the uncertainties (d = 3)

• The thickness-to-chord ratio $r \equiv \xi_1$, free stream Mach number $M_{\infty} \equiv \xi_2$, and angle of attack $\alpha \equiv \xi_3$ are d=3 variable parameters following $\beta_{\rm I}(a,b)$ marginal probability laws.

	a = b	X_m	X_M
ξ1	4	0.97 × <u>r</u>	1.03 × <u>r</u>
ξ_2	4	$0.95 \times \underline{M}_{\infty}$	$1.05 \times \underline{M}_{\infty}$
ξ3	4	$0.98 imes \underline{\alpha}$	$1.02 imes \underline{\alpha}$

- Remark: $\xi \sim \beta_{\rm I}(a,b)$ arises from Jaynes' MaxEnt once (i) the compact support $[X_m, X_M]$ (ii) the means $\mathbb{E}\{\log(\xi-X_m)\}$ and $\mathbb{E}\{\log(X_M-\xi)\}$ are known.
- Our aim is to construct polynomial surrogates for the drag, lift and pitching moment coefficients C_D , C_I and C_m using gPC adapted to the foregoing PDFs (Jacobi polynomials).

Sampling sets (design of experiments DoE)



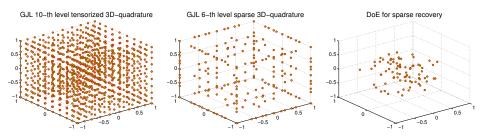
• The 1-dimensional Gauss-Jacobi quadrature Θ_1^M :

$$\int_{-1}^1 f(x) (1-x)^a (1+x)^b \mathrm{d}x \simeq \sum_{\ell=1}^{M-M_b} \omega_\ell f(\xi_\ell) + \sum_{\ell'=1}^{M_b} \omega_{M-M_b+\ell'} f(\xi_{M-M_b+\ell'})$$

is exact for polynomials up to order $2M-1-M_b$, where M_b is the number of fixed nodes (e.g. ± 1).

- $ightharpoonup M_b = 0$ is the classical Gauss-Jacobi (GJ) rule;
- $M_b = 1$ is the Gauss-Jacobi-Radau (GJR) rule;
- $M_b = 2 \ (-\xi_{N-1} = \xi_N = 1)$ is the Gauss-Jacobi-Lobatto (GJL) rule.
- Multi-dimensional quadratures may be obtained by tensorization and/or sparsification.

Sampling sets (design of experiments DoE)



• k-th level d-dimensional sparse grid (Smolyak 1963):

$$\Theta_{d,k} = \sum_{k+1 < j_1 + \dots + j_d < k+d} \Theta_1^{j_1} \otimes \dots \otimes \Theta_1^{j_d}.$$

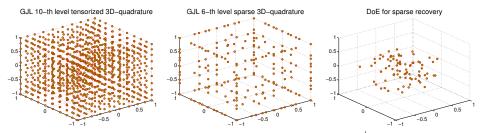
• Example: k = 5, d = 3, then M = 99 using a 1D GJL rule,

$$\Theta_{3,5} = \Theta_1^2 \otimes \Theta_1^2 \otimes \Theta_1^2 + \Theta_1^2 \otimes \Theta_1^2 \otimes \Theta_1^3 + \Theta_1^2 \otimes \Theta_1^3 \otimes \Theta_1^3 + \mathsf{perm}.$$

• The k-th level d-dimensional sparse rule based on GJL nodes is exact for d-dimensional polynomials of total order 2k-3 (Novak-Ritter 1999, Heiss-Winschel 2008).

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Sampling sets (design of experiments DoE)



• Curse of dimensionality: $M = k^d$ for the product rule, while $M \sim \frac{(2d)^k}{k!}$ for the sparse rule with k fixed and $d \gg 1$.

k d	2	3	4	5	6
2	4	8	16	32	64
3	8	20	48	112	256
4	17	50	136	352	880
5	29	99	304	872	2384
6	53	201	673	2082	6092
7	85	363	1337	4483	14072
8	133	647	2585	9293	31025
9	193	1079	4697	18143	64469
10	273	1769	8321	34323	129197

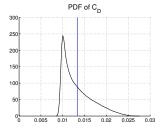
• Sparse quadratures typically outperform product quadratures for $d \ge 4$.

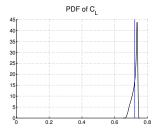
Output statistics by 10-th level GJL product rule (N = 165, M = 1000)

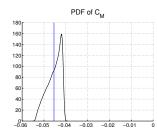
• Mean/variance:

	μ	σ
C_D	133.37e-04	34.13e-04
C_L	72.274e-02	1.670e-02
C _m	-453.99e-04	32.24e-04

PDFs:







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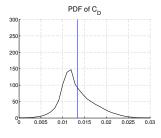
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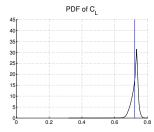
Output statistics by 6-th level GJL sparse rule (N = 35, M = 201)

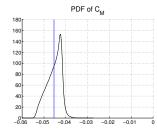
• Mean/variance:

	μ	σ
C_D	133.38e-04	34.10e-04
C_L	72.269e-02	1.673e-02
C _m	-453.96e-04	32.18e-04

PDFs:





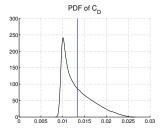


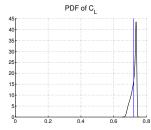
Output statistics by ℓ_1 -minimization (N=165, M=80)

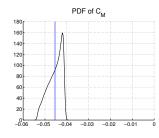
• Mean/variance:

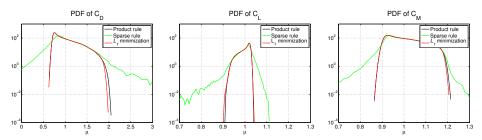
	μ	σ
C_D	133.33e-04	34.05e-04
C_L	72.271e-02	1.670e-02
C _m	-453.95e-04	32.18e-04

PDFs:







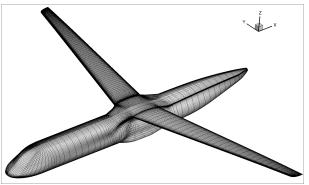


- ullet Sparse recovery by ℓ_1 -minimization assumes low-order interactions between the variable parameters;
- Sparsity can be proved for some parametric, possibly non-linear elliptic/parabolic PDEs (Chkifa-Cohen-Schwab 2014)-but for the present model it is rather observed a posteriori;
- Higher dimensions may be addressed alike-but invoking e.g. a McDiarmid inequality is that relevant?
- Optimal Uncertainty Quantification (Lucas-Owhadi-Ortiz 2008, Owhadi et al. 2013) to compute bounds of the probability of occurrence of a given critical scenario.

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Numerical model

• RANS + Spalart-Allmaras model, 9,008,512 cells:



- Implicit LU-SSOR phase;
- Multigrid approach for the NS system over 3 grid levels;
- Jameson centered scheme with additional artificial viscosity outside of the boundary layers;
- Backward Euler time integration scheme;
- Typical computational time: 6 hours on 60 cores.

Cambier-Heib-Plot Mechanics & Industry 14(3), 159 (2013)

Definition of the uncertainties (d = 10)

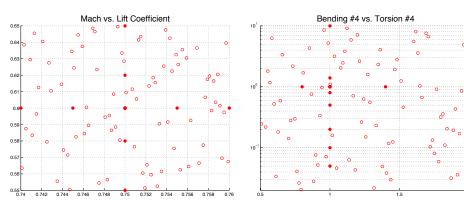
• The Mach number $M \equiv \xi_1$, lift coefficient $C_L \equiv \xi_2$, 4 wing bending parameters ξ_3, \ldots, ξ_6 , and 4 wing torsion parameters ξ_7, \ldots, ξ_{10} are d=10 variable parameters following uniform marginal probability laws.

	X _m	X_M
ξ_1	0.74	0.76
ξ2	0.55	0.65
$\xi_3 \dots \xi_6$	0.5 × <u>/</u>	2.0 × <u>I</u>
$\xi_7 \dots \xi_{10}$	0.02 × <u>J</u>	10.0 × <u>J</u>

• Our aim is to construct polynomial surrogates for the angle of attack α , drag coefficients C_{Ds} and C_{Dv} computed at the wing skin and in the far-field, respectively, pitching moment coefficient C_m , wing tip bend U, and wing tip twist ϕ using PC adapted to the foregoing PDFs (Legendre polynomials).

Sampling set (design of experiments DoE)

• The DoE is constituted by a combination of 18 manually generated sampling points (•) and 83 randomly generated sampling points (o) using Latin Hypercube Sampling (LHS).

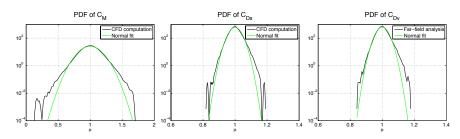


Output statistics by ℓ_1 -minimization (N = 285, M = 101)

ullet Mean, variance, root-mean square error, and Kullback-Leibler divergence from a Normal distribution \mathcal{N} :

	C _m	c_{Ds}	c_{Dv}	α	U	φ
μ	-11.63e-02	219.83e-04	218.69e-04	2.53	2.16	-6.10
σ	1.55e-02	6.53e-04	6.28e-04	0.20	0.26	0.80
e ₂	4.70e-03	0.45e-03	0.35e-03	1.88e-03	1.65e-03	3.97e-03
$D_{KL}(\bar{P} N)$	1.10e-02	1.11e-02	1.39e-02	1.40e-02	0.50e-02	0.62e-02

• PDFs:



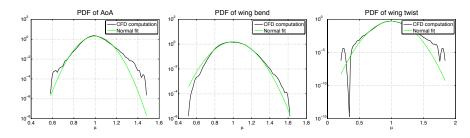
• Sensitivity to at most 2 or 3 parameters out of 10.

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PDFs:



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