

$$1) \dot{x}(+) = A \times c(+) + B u(+)$$

$$y(-) = C \times c(-) + D u(-)$$

MU - 418

Bring Adam Ceylon
22/10/844
M.E - PHYS

$$A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, C = [1 \ 1], D = 0$$

$$\tau = 0.1s, 20H$$

$$a) F = e^{AT} G = \int_0^t e^{At} d\sigma B \quad G = A^{-1} (e^{AT} - I) B$$

(if F has inverse)

$$F = e^{AT} = \frac{1}{2} \begin{bmatrix} s+1 & 0 \\ 0 & s+2 \end{bmatrix}^{-1} (sI - A)^{-1}$$

$$sI - A = \begin{bmatrix} s+1 & 0 \\ 0 & s+2 \end{bmatrix} \Rightarrow (sI - A)^{-1} = \begin{bmatrix} \frac{1}{s+1} & 0 \\ 0 & \frac{1}{s+2} \end{bmatrix}$$

$$- \lambda^{-1} \left\{ \frac{1}{s+1} \right\} = e^{-t}, \quad \lambda^{-1} \left\{ \frac{1}{s+2} \right\} = e^{-2t}$$

$$F = e^{AT} = \begin{bmatrix} e^{-t} & 0 \\ 0 & e^{-2t} \end{bmatrix} \xrightarrow{\tau=0.1s} F \approx \begin{bmatrix} 0.905 & 0 \\ 0 & 0.819 \end{bmatrix}$$

$$A^{-1} = \begin{bmatrix} -1 & 0 \\ 0 & -1/2 \end{bmatrix}, \quad e^{AT} - I = \begin{bmatrix} e^{-t} - 1 & 0 \\ 0 & e^{-2t} - 1 \end{bmatrix}$$

$$G = \begin{bmatrix} -1 & 0 \\ 0 & -1/2 \end{bmatrix} \begin{bmatrix} e^{-t} - 1 & 0 \\ 0 & e^{-2t} - 1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 - e^{-t} \\ \frac{1}{2} (1 - e^{-2t}) \end{bmatrix}$$

$$G \approx \begin{bmatrix} 0.0952 \\ 0.0906 \end{bmatrix}$$

$$x[k+1] = F \times [k] + G u[k]$$

$$y[k] = C x[k] + D u[k]$$

$$F = \begin{bmatrix} 0.905 & 0 \\ 0 & 0.819 \end{bmatrix}$$

$$G = \begin{bmatrix} 0.0952 \\ 0.0906 \end{bmatrix}$$

$$C = [1 \ 1], D = 0$$

b) λ_d , discrete poles are eigenvalues of F .

$$\lambda_d = e^{\lambda_c T} \text{ (relationship with cont. poles)}$$

$$\lambda_c \Rightarrow \det(sI - A) = \det \begin{bmatrix} s+1 & 0 \\ 0 & s+2 \end{bmatrix} = 0$$

$$\Rightarrow \lambda_{c,1} = -1, \lambda_{c,2} = -2$$

$$\lambda_d = e^{\lambda_c T} \cdot \begin{array}{l} \boxed{\lambda_{d,1}} = e^{-1(0.1)} = \boxed{0.904837} \\ \boxed{\lambda_{d,2}} = e^{-2(0.1)} = \boxed{0.818731} \end{array} \xrightarrow{\text{from cont. poles rel.}}$$

$$\det(zI - F) = \det \begin{bmatrix} z - e^{-0.1} & 0 \\ 0 & z - e^{-0.2} \end{bmatrix} = 0$$

$$\det(zI - F) = (z - e^{-0.1})(z - e^{-0.2}) = 0$$

$$\begin{array}{l} \boxed{\lambda_{d,1} = e^{-0.1}} \\ \boxed{= 0.904837} \end{array} \quad \begin{array}{l} \boxed{\lambda_{d,2} = e^{-0.2}} \\ \boxed{= 0.818731} \end{array} \xrightarrow{\text{from eigenvals of } F} \xrightarrow{\text{equivalent}}$$

2) If the closed-loop bandwidth is 3 Hz, the sampling freq. should be 10-20 times faster than that bandwidth. (Theoretical min. is (Nyquist) 2-times)

$$f_s = 50 - 100 \text{ Hz} \Rightarrow T = 0.01 - 0.02 \text{ s}$$

If sampling is too slow:

- Causes aliasing and phase delay, which destabilizes the closed loop
- The discrete model no longer represents the true dynamics

If sampling is too fast:

- Increases noise sensitivity and computational load without much performance gain.

A good practice of T would be 0.01 s (100 Hz)
if meas. sys. is available of capacity.

4) d) For the plant $G_p(s) = \frac{4}{s^2 + 2s + 4}$

Standard second-order form $\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$

$$\omega_n = 2 \text{ rad/s} \quad 2\zeta\omega_n = 2$$

$$\zeta = 0.5$$

The 90% settling time of a second order sys.

$$t_{90\%} \approx \frac{4}{\zeta\omega_n} = \frac{4}{0.5 \times 2} = 4s$$

Sensor has $[G_{cs}) = \frac{1}{0.1s + 1}]$ small time const.

$T = 0.1s$. Overall settling time is dominated by the plant.

with a sampling interval $T = 0.02s$

$$N_s \approx \frac{t_{90\%}}{T} \approx \frac{4}{0.02} = 200 \text{ samples}$$

Therefore, for an input to die out around

$\boxed{200 \approx N_b}$, or FIR horizon is ideal.

One can scan between 150 - 250 interval to find a further finer N_b value (due to noise, bias etc. N_b may fluctuate.)

at (e) we find this value.