

A Multifrequency Multistage Fingerprinting-based Radiolocation System Based

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Abstract—This paper presents a multifrequency and multistage indoor robot localization system based on fingerprinting. The proposed system relies on a 900 MHz Long Range Radio (LoRa) along with 2.4 GHz Wireless Fidelity (WiFi) and Bluetooth (BT) networks. By exploiting different propagation characteristics of different Radio Frequency (RF) signal wave within a Gated Recurrent Unit (GRU) framework, Received Signal Strength (RSS) measurements are used for indoor localization purposes. Similar to conventional fingerprinting systems, the system is consisted of two phases: data acquisition and learning (offline), and localization (online). In offline phase, the signal maps for various AP's are constructed via RSS information and path loss exponent is learned by a network consisted of GRU, whereas the online phase contains an information fusion based localization method. *Add some result once get it*

I. INTRODUCTION

Inverse pyramid:

- P1: Background
 - 1) Inverse pyramid
 - 2) Last sentence: introduce the area of the title of your paper as a significant topic
 - 3) 5 refs (books, review papers, journals, no conf)
- P2-3: Background
 - 1) Original classification: Support the objectives with each sentence
 - 2) Appreciate their work, their focus however different
 - 3) no technical words
 - 4) 10 refs (journal, conference papers)
- P4: Objectives
 - 1) 1-3 objectives
 - 2) the first sentence: this paper presents

The organization of the paper as follows. Section II lays out the fundamentals of the radio wave propagation, while Section III covers the details of the proposed system. Section IV demonstrates the validity of the proposed system in different environments. In Section V, the experimentation results will be concluded and future work will be addressed.

II. FUNDAMENTALS OF RADIO WAVE PROPAGATION IN RADIOLOCATIONING

This section will cover the fundamentals of radio wave propagation in regards to Fingerprinting-based Indoor Radiolocation Systems (FIRL). FIRLs are consisted of two

main phases. The first phase, i.e. offline phase, involves with collecting some form of measurements about the anchor nodes placed in the environment, with corresponding positions. Let $m_j^i \in \mathbb{Z}^1$ and $d_j^i \in \mathbb{R}^1$ to be the measurement obtained from anchor node i at a location j , and the radial distance of between location j and the anchor node i , respectively. The measurement space $\mathbf{m}^i = \{m_j^i | j = 1 \dots n_{loc}\} \in \mathbb{R}^{n_{node}}$ are often constructed in either frequency domain [refer CSI], or time domain. The measurements are then used to approximate the propagation function f_d^i of each anchor node, with which $\mathbb{Z}^1 \mapsto \mathbb{R}^1$.

$$f_d^i(m_j^i) = d_j^i \quad (1)$$

One of the most popular fingerprint is Received Signal Strength (RSS) in FIRLs due to its simplicity in acquiring the fingerprints. The fundamental relationship between transmitted and received signal strengths P_t and $P_r(d)$ occurred between ideal antennas in an empty space with a distance d separation is characterized by Friis' Free Space Equation (FFSE) given below [1].

$$P_r(d) = \frac{P_t G_t G_r \lambda^2}{(4\pi d)^2} \quad (2)$$

In Equation (2), G_t , and G_r denote unitless gains of transmitter and receiver antennas, respectively, whereas λ is the wavelength of the radio wave. However well-known, FFSE is not able to model propagation mechanisms, i.e. reflection, diffraction or scattering occurring along the the propagation path, due to the fact that it can only model Line-of-sight (LOS) propagation. Thus, it is often impractical to utilize it in indoor localization problems where reflection and diffraction occurs along the propagation path. Moreover, since the received signal strength is often minuscule level, FFSE is denoted in decibel scale relative to a milliwatt.

$$\tilde{P}_r(d) = \tilde{P}_t + 10 \log G_t + 10 \log G_r + 20 \log \lambda - 20 \log d - 20 \log 4\pi \quad (3)$$

$\tilde{P}_r(d)$ and \tilde{P}_t represent received and transmitted signal strengths decibel scale. However, neither Equation (2), nor Equation (3) holds true for the distance $0 < d < \lambda$. Thus, received signal strength generally is denoted relative to a

reference point d_0 with a prior corresponding received signal strength.

$$\tilde{P}_r(d) = \tilde{P}_r(d_0) + 20 \log \frac{d_0}{d} \quad (4)$$

Based on FFSE, path loss occurring along the propagation path can be derived as the difference between transmitted and received signal strength. Equation (5) represents a special Path Loss (PL) model, i.e. Log-distance Path Loss (LDPL) which describes the attenuation relative to a reference point. One of the major advantages of LDPL model over FFSE is that LDPL model can account for obstructions and corresponding wave propagation in the space with varying values of PL exponent n .

$$\overline{PL}(d) = \overline{PL}(d_0) + 10n \log \frac{d}{d_0} \quad (5)$$

$$n = \begin{cases} < 2, & \text{if the space structure guides the radio waves} \\ & \text{along the propagation path} \\ = 2, & \text{if the space is empty,} \\ > 2, & \text{if there are obstructions along the propagation} \\ & \text{path} \end{cases} \quad (6)$$

One of the most visited solution in FIRLs is to estimate n by fitting a curve to collected fingerprints. Given a mean PL at an unknown location $\overline{PL}(d)$, PL exponent n and a mean PL at the reference point d_0 $\overline{PL}(d_0)$, the propagation function of anchor node i f_d^i can be obtained by solving LDPL for the radial distance d^i .

$$f_d^i = d_0^i 10^{\left(\frac{\overline{PL}(d) - \overline{PL}(d_0)}{10n} \right)} = d_j^i \quad (7)$$

However, in order to obtain radial distance from anchor node i d^i , PL exponent n should be estimated from the data collected during the offline phase. Let $\mathbf{m}^i = \{\tilde{P}_r^{i,j}(d) | j = 1 \dots n_{loc}\}$ and $\mathbf{d}^i = \{d_j^i | j = 1 \dots n_{loc}\}$ be the RSS fingerprints acquired from anchor node i during surveying and corresponding distances from anchor node i , respectively. The estimated radial distance from anchor node i \hat{d}^i can be obtained with the approximated propagation function $\hat{f}_d^i(m_j^i, n_i^*)$.

$$\hat{f}_d^i(m_j^i, n_i^*) = d_0^i 10^{\left(\frac{\tilde{P}_t - \tilde{P}_r^{i,j}(d) - \overline{PL}(d_0)}{10n_i^*} \right)} = \hat{d}_j^i \quad (8)$$

where n^* is the overall PL exponent which minimizes the absolute localization error $|d_j^i - \hat{f}_d^i(m_j^i, n^*)|$ where $j = 1 \dots n_{loc}$.

$$n_i^* = \arg \min_n e^i = \arg \min_n \{d_j^i - \hat{f}_d^i(m_j^i, n)\} \quad (9)$$

After obtaining the approximated propagation function, the measurements acquired from the anchor nodes are mapped to relative radial distances in order to distinguish the absolute position of the agent in the environment, which forms the offline phase of the FIRLs.

III. MULTIFREQUENCY MULTISTAGE RADIOLOCATION SYSTEM

This section will explain Multifrequency Multistage Radiolocation System (MFMS) in greater detail. Akin to other FIRLs, MFMS consists of two main phases. During the offline phase, RSS information from anchor nodes are collected at many locations in the environment and used to approximate the radio wave propagation function. The online phase, on the other hand, makes use of the approximated propagation function obtained in the former phase. However, one major difference between MFMS and conventional FIRL approaches is that MFMS employs three types of radio setups to infer the location of the agent.

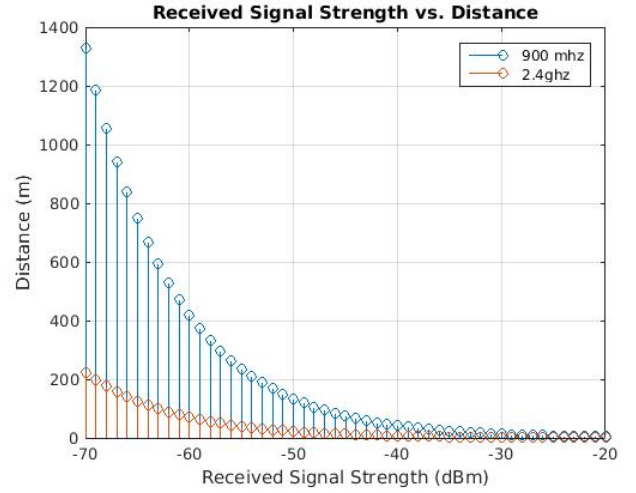


Fig. 1: RSSI readings of NLoS and LoS APs acquired with a stationary agent

The main motivation behind employing multisource information is to exploit the diversity of the propagation characteristics of the different frequencies. As it can be seen in the Equation (5) and Figure 1, the received power and separation distance has a log-linear relationship. This figure implies two fundamental problems in radiolocation systems: The first problem is that as the carrier frequency increases path loss increases significantly, which limits the radio coverage and localization ability of the system in large environments. On the other hand, as the carrier frequency increases, the separation between two antennas, i.e. the anchor node and the target to be localized, can be identified with finer spatial resolution. Therefore, the trade-off between radio coverage and spatial localization resolution can be resolved by employing different frequencies in indoor localization systems by fusing the information acquired from the anchor nodes using different carrier frequency. Thus, MFMS employs a Long Range Radio (LoRa) radio (900 MHz), a WiFi Access Point (AP) and a Bluetooth (2.4 GHz) beacon in each anchor nodes. Table I tabulates the specifications of the radios consisting each anchor node, while Figure 2 demonstrates the details of the anchor nodes. In detail, wider spatial coverage is achieved by using LoRa modules

TABLE I: The specifications of radios used in anchor nodes

Property	WiFi	Bluetooth	LoRa
Frequency [MHz]:	2400	2400	900
Communication Bandwidth:	1-11 Mbps	Upto 4 Mbps	10 Kbps
Transmission Power P_t [dBm]:	17	10	24
Reciever Sensivity [dBm]:	?	-98	-101
Communication Range [m]:	<20	10	>100

working at 900 MHz while finer spatial resolution provided by WiFi and Bluetooth both working at 2.4 GHz frequency.



Fig. 2: MFMS Anchor Nodes

A. Temporally- and Spatially-coherent Path Loss Exponent Estimation

This section covers the details of the joint path loss exponent estimation which forms the first stage of MFMS. We approach the FIRL problem in the scope of curve fitting. However, unlike many approaches proposed mentioned earlier, MFMS does not try to blindly fit a function which best explains the training data given the location labels. Moreover, MFMS does not consider the path loss exponent as a variable describing the whole localization environment. Instead, we approach the problem as curve fitting for path loss exponent differing in value in the environment and time. In detail, the path loss exponent for MFMS is a function of both location and time. Therefore, the proposed system is able account for non-uniform distribution of obstructions in space.

Let $\Omega = \{g_i | i = 1 \dots n_{grid}\}$, is the localization environment which is divided into n_{grid} number of grids g . An arbitrary position $x \in \Omega$ can be in a shadowed region for any anchor node; thus, MFMS selectively chooses which anchor nodes to use to localize the agent in Ω . This selection is performed by mapping the measurement vector $\mathbf{m}_j^k \in \mathbb{Z}^{n_{node}}$ with a set of weights $\mathbf{w}_g \in \mathbb{R}^{n_{node}}$ such that $\sum_g \mathbf{w}_g = 1$. The weights of each grid is learned with a softmax classifier, which is depicted in Figure 3, based on LoRa measurements due to the fact that the higher probability of observing multiple LoRa



Fig. 3: The softmax classifier assigns weights for each anchor node based on the evidence representing the probability of residing in a grid cell g .

modules in arbitrary positions in the environment, thanks to the smaller path loss they introduce. Equation (10) shows the result of the selection process.

$$\widetilde{\mathbf{m}}_j^k = \mathbf{w}_g \mathbf{m}_j^k \quad (10)$$

For each anchor node, the path loss exponent is estimated with LDPL model in a least square sense. Hence, MFMS incorporates the physical parameters into location estimation process.

$$n_g^{*,i} = \arg \min_n \{\|\mathbf{x}_g\|_2 - f_d(\cdot)\} \quad (11)$$

where \mathbf{x}_g denotes the center position of grid g , and $f_d(\cdot)$ denotes LDPL model.

B. Pinpoint Localization

This section gives details of the second stage of the MFMS which is the pinpoint localization. After localizing the agent in grid-level and selecting which anchor nodes to be employed, the propagation function $\hat{g}_d(\cdot)$ can be formulated as below:

$$\hat{g}_d(\widetilde{\mathbf{m}}_j^{k-n_m:k}, \mathbf{n}_g^*) = \hat{\mathbf{x}} \quad (12)$$

where $\widetilde{\mathbf{m}}_j^{k-n_m:k}$, \mathbf{n}_g^* , and $\hat{\mathbf{x}}$ are the weighted measurement vector between time steps $k - n_m$ and k , the estimated path loss exponent vector of each anchor node for grid g and the estimated absolute position of the agent, respectively. As it can be seen in Equation (12), the propagation function incorporates the weighted measurements with the spatially- and temporally-coherent path loss exponent so that the physical characteristics of the radio waves, represented with the path loss, are enforced into the model as a parameter.

The propagation function of WiFi $\hat{g}_d^w(\cdot)$ and Bluetooth $\hat{g}_d^b(\cdot)$ anchors are approximated with two separate recurrent neural networks, consisting of three layers of Gated Recurrent Unit (GRU) [2]. These functions are attained with a Stochastic Gradient Descent (SGD) based back-propagation algorithm. After



600x400

Fig. 4: GRU

approximating the propagation functions, these are employed to estimate the location of the agent. Specifically, the pin-pointing algorithm incorporates the spatially- and temporally-coherent path loss exponent along with the weighted measurements to estimate \hat{x}^w and \hat{x}^b , estimated positions by using WiFi measurements and Bluetooth measurements, respectively.

Figure 4 depicts the Stage-II of MFMS in an unfolded representation.

C. Information Fusion

This section of the paper further explains the Stage-III of the MFMS. The Stage-III is essentially an information fusion layer of the model where location estimates of WiFi and Bluetooth measurements are fused into one final entity. The incorporation of two estimates are achieved in the framework of a Neural Network (NN) consisting of 3 layers. The network is in a gradually narrowing structure such that the first, second and last layer contain 8, 4, 2 neurons, respectively. Figure 5 demonstrates the Phase-III.



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Fig. 5: Two location estimates of WiFi and Bluetooth approximations are fused with a 3 layered-NN.

IV. EXPERIMENTATION

A. Experimental Setup

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B. Results

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V. CONCLUSIONS AND FUTURE WORK

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ACKNOWLEDGMENTS

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1200×400

Fig. 6: MFMS Model